

## INTRODUCTION

This HP-19C/HP-29C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.
They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.
You will find general information on how to key in and run programs under "A Word about Program Usage" in the Applications book you received with your calculator.
We hope that this Solutions book will be a valuable tool in your work and would appreciate your comments about it.

The program material contained herein is supplied without representation or warranty of any kind. Hewlett-Packard Company therefore assumes no responsibility and shall have no liability, consequential or otherwise, of any kind arising from the use of this program material or any part thereof.

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## PROPERTIES OF CIRCULAR SECTIONS

This program performs an interchangeable solution for four properties of circular sections. Given either the moment of inertia I, diameter d, polar moment of inertia J, or area A, the remaining properties can be calculated.


EQUATIONS:

$$
\begin{aligned}
& I=\frac{\pi d^{4}}{64} \\
& J=\frac{\pi d^{4}}{32} \\
& A=\frac{\pi d^{2}}{4}
\end{aligned}
$$

## EXAMPLE 1:

If the moment of inertia of a section must be 60 in ., what is the necessary diameter? What is the polar moment of inertia? What is the area?

## EXAMPLE 2:

The diameter of a section is 10 centimeters. What is the moment of inertia? What is the polar moment of inertia? What is the area?

SOLUTIONS:


## User Instructions

| STEP | INSTRUCTIONS | INPUT |
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| DATA/UNITS |  |  | (



## PROPERTIES OF RECTANGULAR SECTIONS

This program performs an interchangeable solution for the moment of inertia I, the width $b$ and the height $h$ of a rectangular section. When $b$ and $h$ are known, the polar moment of inertia J and the section area can also be found.


EQUATIONS:

$$
\begin{aligned}
& I=\frac{b h^{3}}{12} \\
& J=\frac{b h\left(b^{2}+h^{2}\right)}{12} \\
& A=b h
\end{aligned}
$$

REMARKS:
Values of polar moment of inertia J calculated by this program must not be used to calculate torsional stress and strain in rectangular members.

## EXAMPLE:

What is the moment of inertia of a section with $b=3$ and $h=5$ ? What is the polar moment of inertia? What is the area? What would b have to be if $\mathrm{I}=40$ ?

SOLUTION:

| 5.00 ENT* |  |  |
| :---: | :---: | :---: |
| 3.00 | ENT $\uparrow$ |  |
| 0.00 | 6S81 |  |
| 31.25 | *** | (in. ${ }^{4}$ ) |
|  | R/S |  |
| 15.80 | *** | (in. ${ }^{2}$ ) |
|  | R/S |  |
| 42.50 | *** | ${ }^{4}$ ) |
| 5.00 | Enta |  |
| 0.80 | ENTt |  |
| 40.06 | GSE1 |  |
| 3.84 | *** | (in.) |

3.00 ENT 1
0.00 6SE1
31.25 ** (in. ${ }^{4}$ ) (in. ${ }^{2}$ )
(in. ${ }^{4}$ )
5.00 ENT
-.
3.84 ** (in.)

User Instructions



## PROPERTIES OF ANNULAR SECTIONS

This program provides an interchangeable
SOLUTION: solution for the moment of inertia $I$, the outside diameter $\mathrm{d}_{\mathrm{O}}$, and the inside diameter $d_{j}$ of an annular section. Once $d_{0}$ and $d_{i}$ are known, the polar moment of inertia $J$ and the area of the section can be calculated.


## EXAMPLE:

If $d_{i}$ equals 3 inches and I equals $10 \mathrm{in}^{4}$, what is $d_{0}$ ? What is $A$ ?

What would I be if $d_{o}$ equals 4.5 inches?

## User Instructions



Program Listings


## THIN-WALLED PRESSURE VESSELS

This program can be used to correlate diameter, stress, pressure and thickness for cylindrical and spherical pressure vessels. Either the hoop stress $\mathrm{s}_{\mathrm{c}}$ or the longitudinal stress $S_{L}$ may be input for cylinders. For spheres, only the hoop stress $s_{\text {sphere }}$ is applicable.


REMARKS:
The thickness of the walls must be negligible with respect to the value of the radius. The equations are not valid in the neighborhood of end closures for cylindrical vessels.

## EXAMPLE 1:

A basketball has a diameter of 9.3 inches. The thickness of the cord layer which resists virtually all of the internal pressure is $1 / 32$ inch. The recommended pressure is 9 pounds per square inch. What is the stress in the cord layer?

## EXAMPLE 2:

A four inch diameter pipe contains steam at 1000 pounds per square inch. What thickness is required if hoop stress is not to exceed 15000 pounds per square inch?

SOLUTIONS:

## EQUATIONS:

for hoop stress in cylinders: $s_{C}=\frac{\mathrm{Pr}}{\mathrm{t}}$
for longitudinal stress in cylinders:
$s_{L}=\frac{P r}{2 t}$
for hoop stress in spheres: $s_{\text {sphere }}=\frac{\mathrm{Pr}}{2 \mathrm{t}}$
where:
P is internal pressure;
$D$ is diameter of vessel ( $r=D / 2$ );
$t$ is thickness of vessel

1. 9.30 ENTT

$$
0.00 \text { ENTT }
$$

$$
9.00 \text { ENT }
$$

$$
32.00 \quad 1 \%
$$

GSE1
669.60 ** (psi)
2. 4.00 ENTA
15000.80 ENTA
$2.60 \div \mathrm{s}_{\mathrm{C}} / 2$
1000.00 ENTT
0.00 ESE1
Q. 13 ** (in)

User Instructions


Program Listings


## STRESS IN THICK-WALLED CYLINDERS

This program calculates the radial and tangential components of normal stress for thick-walled, cylindrical, pressure vessels.


EQUATIONS:

$$
\begin{aligned}
& s_{r}=\frac{r_{i}{ }^{2} P_{i}-r_{0}{ }^{2} P_{0}}{r_{o}{ }^{2}-r_{i}{ }^{2}}-\frac{r_{i}{ }^{2} r_{0}{ }^{2}\left(P_{i}-P_{0}\right)}{r^{2}\left(r_{0}{ }^{2}-r_{i}{ }^{2}\right)} \\
& s_{t}=\frac{r_{i}{ }^{2} P_{i}-r_{0}{ }^{2} P_{0}}{r_{o}{ }^{2}-r_{i}{ }^{2}}+\frac{r_{i}{ }^{2} r_{0}{ }^{2}\left(P_{i}-P_{0}\right)}{r^{2}\left(r_{0}{ }^{2}-r_{i}{ }^{2}\right)}
\end{aligned}
$$

where:
$s_{r}$ is the radial component of stress;
$s_{t}$ is the tangential component of stress;
$r_{i}$ is the internal radius;
$r_{0}$ is the outer radius;
$r$ is the radius where calculated stresses occur;
$P_{i}$ is the internal pressure;
$P_{\circ}$ is the outside pressure.

## EXAMPLE:

A cylinder has an inner radius of 1.00 inch and an outer radius of 2.00 inches. The inner pressure is 10,000 pounds per square inch and the outer pressure is 150 pounds per square inch. What are the values of radial and tangential stresses for radii of $1.00,1.25,1.75$ and 2.00 inches?

SOLUTION:

| 1.80 6SE1 |  |  |
| :---: | :---: | :---: |
| 2. 98 ENT* |  |  |
| 150. 60 ENTA |  |  |
| 1.60 ENT 4 |  |  |
| 18080.80 | R/S |  |
| -10800. 90 |  | $s_{r} \mathrm{psi}$ |
| 16266.67 | + ${ }_{\text {¢ }}$ | $\mathrm{s}_{\mathrm{t}} \mathrm{psi}$ |
| 1.25 | 6SE1 | st ${ }^{\text {Psi}}$ |
|  | Prs |  |
| -5272.80 | * ${ }_{\text {* }}$ |  |
|  | $X+Y$ | ${ }^{\text {S }}$ r |
| 11538.67 | ** |  |
| 1.75 | 6SB | $\mathrm{S}_{\mathrm{t}}$ |
|  | R/S |  |
| -1155.10 | 束* | $S_{r}$ |
|  | $\underline{x+i}$ | ${ }^{r}$ |
| 7421.77 | *** | St |
| 2.80 | GSE: | St |
|  | R. ${ }^{\text {c }}$ |  |
| -150.00 | + ${ }^{\text {\% }}$ | Sr |
|  | $\underline{x+y}$ | sr |
| 6416.67 | * ${ }_{\text {\% }}$ | $s t$ |

REMARKS:
A negative stress indicates compression.
REFERENCE:
J.E. Shigley, Mechanical Engineering Design, McGraw Hill, 1963.

## User Instructions

| STEP | INSTRUCTIONS | INPUT <br> OATA/UNITS | KEYS |
| :---: | :--- | :--- | :--- | :--- | :--- |
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## MOHR CIRCLE FOR STRESS

Given the state of stress on an element, the principal stresses and their orientation can be found. The maximum shear stress and its orientation can also be found.


Stress State


EQUATIONS:

$$
\begin{aligned}
s_{s \max } & =\sqrt{\left(\frac{s_{x}-s_{y}}{2}\right)^{2}+s_{x y}^{2}} \\
s_{1} & =\frac{s_{x}+s_{y}}{2}+s_{s \max } \\
s_{2} & =\frac{s_{x}+s_{y}}{2}-s_{s_{\max }} \\
\theta & =1 / 2 \tan ^{-1}\left(\frac{2 s_{x y}}{s_{x}-s_{y}}\right) \\
\theta_{s} & =1 / 2 \tan ^{-1}-\left(\frac{s_{x}-s_{y}}{2 s_{x y}}\right)
\end{aligned}
$$

where:
$\mathrm{s}_{\text {smax }}$ is the maximum shear stress;
$s_{1}$ and $s_{2}$ are the principal norma stresses;
$\theta$ is the angle of rotation from the principal axis to the original axis;
$\theta_{S}$ is the angle of rotation from the axis of maximum shear stress to the original axis;
$s_{x}$ is the stress in the $x$ direction;
$s_{y}$ is the stress in the $y$ direction;
$s_{x y}$ is the shear stress on the

## REFERENCE:

Spotts, M.F., Design of Machine Elements, Prentic-Ha11, 1971.

## EXAMPLE:

If $s_{x}=25000 \mathrm{psi}, \mathrm{s}_{\mathrm{y}}=-5000 \mathrm{psi}$, and
$s_{x y}=4000$ psi, compute the principal stresses and the maximum shear stress.


SOLUTION:

```
25000.00 ENT:
-5000.00 ENTA
4000.00 GSE1
25524.17 *** sos (psi)
-5524.17 *** s_ (psi)
    7.47 *** 0 (degrees)
    ****
    R/S
15524.17 ** s s smax (psi)
```

| STEP | instructions | INPUT DATA/UNITS | KEY | $\begin{gathered} \text { OUTPUT } \\ \text { DATA/UNITS } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1. | Key in the program |  |  |  |
| 2. | Enter the following: |  |  |  |
|  | Stress in the x direction (negative for | $S_{x}$ | ENT $\uparrow$ |  |
|  | compression) |  |  |  |
|  | Stress in the y direction (negative for | $S_{y}$ | ENT $\uparrow$ |  |
|  | compression) |  |  |  |
|  | Shear stress | $S_{x y}$ |  |  |
| 3. | Compute the following: |  |  |  |
|  | First principal stress |  | GSB | $\mathrm{S}_{1}$ |
|  | Second principal stress |  | R/S | $\mathrm{S}_{2}$ |
|  | Angle of rotation (principal) |  | R/S | $\theta$ |
|  | Angle of rotation (shear) |  | R/S | $\theta_{S}$ |
|  | Maximum shear stress |  | R/S | $\mathrm{s}_{\text {smax }}$ |
|  | NOTE: Do not disturb the stack during |  |  |  |
|  | step 3 |  |  |  |
| 4. | For a new case, go to step 2. |  |  |  |
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# CIRCULAR PLATES WITH SIMPLY SUPPORTED EDGES 

This program can be used to calculate the deflection and stress at the center of a simply supported circular plate with uniformly distributed or concentrated central loads.

EQUATIONS:
for a concentrated central load:

$$
\begin{aligned}
& y_{\max }=\frac{(3+\mu) \mathrm{Pr}^{2}}{16 \pi(1+\mu) D} \\
& s_{\max }=\frac{P}{h^{2}}\left[(1+\mu)\left(0.485 \ln \frac{r}{h}+0.52\right)+0.48\right]
\end{aligned}
$$

for a uniformly distributed load:

$$
\begin{aligned}
& y_{\max }=\frac{(5+\mu) W r^{4}}{64 D(1+\mu)} \\
& s_{\max }=\frac{3(3+\mu) W r^{2}}{8 h^{2}}
\end{aligned}
$$

where:

$$
D=\frac{E h^{3}}{12\left(1-\mu^{2}\right)}
$$

$y_{\text {max }}$ is the maximum deflection;
$\mathrm{S}_{\text {max }}$ is the maximum stress;
$\mu$ is Poisson's ratio;
$E$ is the modulus of elasticity;
$h$ is the thickness of the plate;
$r$ is the radius of the plate;
$W$ is the uniformly distributed load;
$P$ is the concentrated central load.

## REFERENCES:

Spotts, M.F., Design of Machine Elements, Prentice-Hall, Inc., 1971.

## REMARKS:

Deflections must be small compared to thickness of plate.

## EXAMPLE 1:

Assuming that a manhole cover with an automobile tire at its center may be modeled as a simply supported flat plate with concentrated central load, what is the deflection at the center of the plate? What is the stress?

$$
\begin{aligned}
& \mathrm{E}=30 \times 10^{6} \mathrm{psi} \\
& \mathrm{~h}=0.75 \mathrm{in} \\
& \mu=0.3 \\
& \mathrm{r}=15 \mathrm{in} \\
& \mathrm{P}=1500 \mathrm{lb}
\end{aligned}
$$

## EXAMPLE 2:

A simply supported $1 / 4$ inch thick plate ( $E=30 \times 10^{6}, \mu=0.3$ ) withstands 50 pounds per square inch. If the radius is 5 inches, what is the deflection and what is the stress at the center of the plate?

SOLUTIONS:
(1)

| $30 .+65$ | ENT* | (2) $30 .+86$ | ENT ${ }^{\text {P }}$ |
| :---: | :---: | :---: | :---: |
| 0.75 | ENT $\dagger$ | 0.25 | ENT $\uparrow$ |
| 0.30 | ENT* | 0.30 | ENT $\uparrow$ |
| 15.00 | 6581 | 5.60 | CSE1 |
| 1500.00 | CSB2 | 50.00 | 6SE3 |
| 0.01 | *** (in) | 0.05 | *** (in) |
|  | PF |  | R/9 |
| 8119.49 | ** ${ }^{\text {(psi) }}$ | 24750.00 | *** (psi) |

User Instructions

| STEP | instructions | $\begin{gathered} \text { INPUT } \\ \text { DATA/UNITS } \end{gathered}$ | KEYS |  | OUTPUT datalunits |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | Key in the program |  |  |  |  |
| 2. | Input modulus of elasticity | E | ENT $\uparrow$ |  | E |
| 3. | Input thickness of plate | h | ENT $\uparrow$ |  | h |
| 4. | Input Poisson's ratio | $\mu$ | ENT $\uparrow$ |  |  |
| 5. | Input radius of plate | $r$ | GSB | 1 |  |
| 6. | If the load is distributed go to step 10 |  |  |  |  |
| 7. | Input concentrated load and calculate |  |  |  |  |
|  | deflection | P | GSB | 2 | $y_{\text {max }}$ |
| 8. | Calculate maximum stress |  | R/S |  | $\mathrm{s}_{\text {max }}$ |
| 9. | For new load go to step 7. For new case |  |  |  |  |
|  | go to step 2. |  |  |  |  |
| 10. | Input distributed load and calculate |  |  |  |  |
|  | deflection | W | GSB | 3 | $y_{\text {max }}$ |
| 11. | Calculate maximum stress |  | R/S |  | $\mathrm{s}_{\text {max }}$ |
| 12. | For new load go to step 10. For new case |  |  |  |  |
|  | go to step 2. |  |  |  |  |
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## CIRCULAR PLATES WITH FIXED EDGES

This program can be used to calculate the maximum deflection and stress for a circular plate with fixed edges. Either central concentrated loads or distributed loads may be input.

EQUATIONS:

$$
\begin{aligned}
& y_{\max }=\frac{P r^{2}}{16 \pi D} \\
& s_{\max }=\frac{P}{h^{2}}(1+\mu)\left(0.485 \ln \frac{r}{h}+0.52\right)
\end{aligned}
$$

for distributed loads:

$$
\begin{aligned}
& y_{\max }=\frac{W r^{4}}{64 D} \\
& s_{\max }=\frac{3 W r^{2}}{4 h^{2}} \quad \text { (at edge of plate) }
\end{aligned}
$$

where:

$$
D=\frac{E h^{3}}{12\left(7-\mu^{2}\right)}
$$

$y_{\text {max }}$ is the maximum deflection
$\mathrm{s}_{\text {max }}$ is the maximum stress;
P is the concentrated load;
$W$ is the distributed load;
$r$ is the radius of the plate;
$h$ is the thickness of the plate;
$\mu$ is Poisson's ratio;
$E$ is the modulus of elasticity.

## REFERENCE:

Spotts, M.F., Design of Machine Elements, Prentice-Hall, Inc., 1971.

REMARKS:
Deflections must be small compared to the thickness of plate.

## EXAMPLE 1:

The cap on a pressure vessel is a $1 / 4$ inch thick steel plate ( $\mathrm{E}=30 \times 10^{6} \mathrm{psi}$, $\mu=0.3$ ) with a 6 inch radius. It is clamped to the opening of the pressure vessel by a ring of bolts. What are the maximum and minimum deflections and stresses in the plate if pressure cycles from 50 to 60 psi ?

EXAMPLE 2:
An adjustable focal length mirror is to derive its concaved shape due to a variable force applied at its center. The mirror is chrome plated steel ( $\mathrm{E}=30 \times 10^{6} \mathrm{psi}, \mu=0.3$ ), 0.1 inches thick and has a radius of 12 inches. What is the deflection of the center for a force of 6.0 pounds. The edges are held securely.

SOLUTIONS:
(1)
$36 .+86$ ENT
0.25 ENTA
(2)
30. +aE ENTT
0. 38 ENT个
0.10 ENTA
0.30 ENTA
6.80 GSE:
12.80 6581
50.006583
6.00 GSE2
0.82 ** (in)min
FIX5
R/S (psi)
21600.00
60.00 GSB3
Q. 03 *** (in) max
Fs
$25920.00 * *(\mathrm{psi})$

## User Instructions

| STEP | Instructions | $\begin{gathered} \text { INPUT } \\ \text { DATA/UNITS } \end{gathered}$ | KEYS |  | $\begin{gathered} \text { OUTPUT } \\ \text { DATA/UNITS } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | Key in the program |  |  |  |  |
| 2. | Input modulus of elasticity | E | ENT $\uparrow$ |  | E |
| 3. | Input thickness of plate | h | ENT $\uparrow$ |  | h |
| 4. | Input Poisson's ratio | $\mu$ | ENT $\uparrow$ |  | $\mu$ |
| 5. | Input radius of plate | $r$ | GSB | 1 | D |
| 6. | If the load is distributed go to step 10 |  |  |  |  |
| 7. | Input concentrated load and calcu? ate |  |  |  |  |
|  | deflection | P | GSB | 2 | $y_{\text {max }}$ |
| 8. | Calculate maximum stress |  | R/S |  | $\mathrm{s}_{\text {max }}$ |
| 9. | For new load go to step 7. For new case |  |  |  |  |
|  | go to step 2 |  |  |  |  |
| 10. | Input distributed load and calculate |  |  |  |  |
|  | deflection | W | GSB | 3 | $y_{\text {max }}$ |
| 11. | Calculate maximum stress |  | R/S |  | ${ }^{S_{\text {max }}}$ |
| 12. | For new load go to step 10. For new case |  |  |  |  |
|  | go to step 2. |  |  |  |  |
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## COMPRESSIVE BUCKLING

This program performs an interchangeable solution for the four properties of slender compression members or columns: $P_{c r}$, the critical buckling load; $E$, the modulus of elasticity; $I$, the minimum moment of inertia; and $\ell$, the length of the member.

## EQUATIONS:

Three configurations are possible, identified by the number of fixed ends on the member: 0, both ends hinged; 1 , one end free and one fixed; 2, both ends fixed.


## REMARKS:

Uncertainties such as the amount of restraint at the ends, eccentricity of the load, initial warp, nonhomogeneity of the material and deflection caused by lateral loads, can cause very significant changes in the behavior of a compressive member.

EXAMPLE 1:
If an 8 inch steel ( $\mathrm{E}=30 \times 10^{6} \mathrm{psi}$ ) piston rod (a piston rod has zero fixed ends) must withstand a load of 15000 pounds without buckling, what moment of inertia must it have?

EXAMPLE 2:
Steel columns 40 feet long are used to support a bridge. What is the maximum load that the column can withstand without buckling? Assume 1 fixed end. $\mathrm{E}=30 \times 10^{6} \mathrm{psi}, \mathrm{I}=700 \mathrm{in}^{4}$.

SOLUTIONS:
(1)

```
    0.00 6581
        15000.00 ENTT
            30.+86 ENTT
        0.00 ENTT
            8.00 GSE2
    3.24-03 *** I
        0.00 ENTA
    30.+86 ENTT
    700.00 ENT个
    480.00 ESE2
224893.33 *** P
```

(2) $1.00 \operatorname{GSB1}$

User Instructions



## ECCENTRICALLY LOADED COLUMNS

This program calculates the maximum deflection, the maximum moment, and the maximum stress in an eccentrically loaded column under compressive stress.


EQUATIONS:

$$
\begin{aligned}
& y_{\max }=e\left[\sec \frac{\ell}{2} \sqrt{\frac{P}{E I}}-1\right] \\
& M_{\max }=P\left[e+y_{\max }\right] \\
& S_{\max }=\frac{P}{A}\left[1+\frac{e c A}{I} \sec \frac{\ell}{2} \sqrt{\frac{P}{E I}}\right]
\end{aligned}
$$

where:

$$
\begin{aligned}
& y_{\max } \text { is the maximum deflection; } \\
& \mathrm{e} \text { is the eccentricity; } \\
& \text { l is the column length; } \\
& P \text { is the compressive load; } \\
& E \text { is the modulus of elasticity; } \\
& I \text { is the moment of inertia; } \\
& M_{\max } \text { is the maximum internal moment; } \\
& \mathrm{S}_{\max } \text { is the maximum normal stress } \\
& \text { in the column; } \\
& \mathrm{C} \text { is the distance from the } \\
& \text { neutral axis of the column to } \\
& \text { the outer surface; } \\
& \text { A is the area of the cross } \\
& \text { section }
\end{aligned}
$$

REMARKS:
Columns must be of constant cross section. Stresses may not exceed the elastic limit of the material.

REFERENCE:
Spotts, M.F., Design of Machine Elements, Prentice-Hall, 1971.

## EXAMPLE:

A column 50 feet long is to support 8000 pounds. The load is to be offset 6 inches. What are the maximum values of deflection, moment, and stress in the member?

$$
\begin{aligned}
& E=30 \times 10^{6} \\
& I=107 \mathrm{in}^{4} \\
& A=7 \mathrm{in}^{2} \\
& C=2 \mathrm{in}
\end{aligned}
$$

## SOLUTION:

User Instructions

| STEP | instructions | $\begin{array}{\|c\|} \hline \text { INPUT } \\ \text { DATA/UNITS } \\ \hline \end{array}$ | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | Key in the program |  |  |  |  |
| 2. | Initialize |  | g | RAD |  |
| 3. | Store data: |  |  |  |  |
|  | Moment of inertia | I | STO | 1 |  |
|  | Modulus of elasticity | E | STO | 2 |  |
|  | Length of column | $\ell$ | STO | 3 |  |
|  | Eccentricity | e | STO | 4 |  |
|  | Load | P | STO | 5 |  |
| 4. | To calculate maximum deflection |  | GSB | 1 | $y_{\text {max }}$ |
| 5. | To calculate maximum moment |  | GSB | 2 | $M_{\text {max }}$ |
| 6. | To calculate maximum stress: |  |  |  |  |
| 6 a. | Enter distance from neutral axis | c | ENT $\uparrow$ |  |  |
| 6b. | Enter section area and run | A |  | 3 | ${ }^{\text {max }}$ |
| 7. | For a new case, go to step 3 and store |  |  |  |  |
|  | different value(s). |  |  |  |  |
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NOTES

In the Hewlett-Packard tradition of supporting HP programmable calculators with quality software, the following titles have been carefully selected to offer useful solutions to many of the most often encountered problems in your field of interest. These ready-made programs are provided with convenient instructions that will allow flexibility of use and efficient operation. We hope that these Solutions books will save your valuable time. They provide you with a tool that will multiply the power of your HP-19C or HP-29C many times over in the months or years ahead.

Mathematics Solutions<br>Statistics Solutions<br>Financial Solutions<br>Electrical Engineering Solutions<br>Surveying Solutions<br>Games<br>Navigational Solutions<br>Civil Engineering Solutions Mechanical Engineering Solutions<br>Student Engineering Solutions

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