

## INTRODUCTION

This HP-19C/HP-29C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.
They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.
You will find general information on how to key in and run programs under "A Word about Program Usage" in the Applications book you received with your calculator.
We hope that this Solutions book will be a valuable tool in your work and would appreciate your comments about it.

The program material contained herein is supplied without representation or warranty of any kind. Hewlett-Packard Company therefore assumes no responsibility and shall have no liability, consequential or otherwise, of any kind arising from the use of this program material or any part thereof.

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* This program also appears in the HP-19C/29C Applications book, but is included here for the sake of completeness.


## AZIMUTH-BEARING CONVERSIONS



Angle conventions for azimuth and quadrant bearings as used in this solution book are shown above.

Thus azimuths are measured from the north meridian following North American surveying conventions. Bearings are measured from the meridian in the quadrant in which the line falls. Quadrant codes are shown in the above sketch.

Often it is desirable to have a quick, easy method to convert to or from azimuths and bearings. In this solutions book, for example, some inputs and outputs may be in azimuths rather than bearings, or vice versa, when you desire the alternate form. The simple keystroke routines on the following page are helpful in making these conversions: If you have a number of conversions to perform the calculator program will be more convenient and faster. Subroutine 1 converts bearings to azimuths. Subroutine 2 converts azimuths to bearings. You may want to separate the two parts and only key in one section if all your conversions are in one direction.

Examp1e:

1. Convert bearing $S 34^{\circ} 56^{\prime} 37^{\prime \prime} \mathrm{W}$ to an azimuth.
2. Convert bearing $\mathrm{N} 85^{\circ} 24^{\prime} 47^{\prime \prime} \mathrm{W}$ to an azimuth.
3. Convert azimuth of $162^{\circ} 15^{\prime} 32^{\prime \prime}$ to bearing/quadrant.
4. Convert azimuth of $39^{\circ} 42^{\prime} 26^{\prime \prime}$ to bearing/quadrant.

## Solution:

1. 34.5ET ENT*

ㄱ. GR:
214.567 wn AZ.
2. 85.2447 ENT 4.0000 ESE1
274.3513 ** AZ.
3. 162.1572 G5E2
17.442? w* BRG.

Fe
2. ** QD.
4. 39.4226 ESE2


## KEYSTROKE ROUTINES

| STEP | instructions | INPUT DATA/UNITS | KEYS |  |  |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AZIMUTHS TO BEARINGS: |  |  |  |  |  |  |
| 1 | Azimuth $=0^{\circ}$ to $90^{\circ}$ | AZ (D.MS) | No CAL | LATION |  |  | BRG (D.MS) |
|  |  |  |  |  |  |  | $Q \mathrm{D}=1$ |
| 2 | Azimuth $=90^{\circ}$ to $180^{\circ}$ | 180 | ENTER $\uparrow$ |  |  |  |  |
|  |  | AZ (D.MS) | g | $\rightarrow$ H | - | f |  |
|  |  |  | $\rightarrow$ H.MS |  |  |  | BRG (D.MS) |
|  |  |  |  |  |  |  | $Q \mathrm{D}=2$ |
| 3 | Azimuth $=180^{\circ}$ to $270^{\circ}$ | AZ (D.MS) | ENTER $\uparrow$ | 180 | - |  | BRG (D.MS) |
|  |  |  |  |  |  |  | $Q D=3$ |
| 4 | Azimuth $=270^{\circ}$ to $360^{\circ}$ | 360 | ENTER $\uparrow$ |  |  |  |  |
|  |  | AZ (D.MS) | g | $\rightarrow \mathrm{H}$ | - | f |  |
|  |  |  | $\rightarrow$ H.MS |  |  |  | BRG (D.MS) |
|  |  |  |  |  |  |  | $Q \mathrm{D}=4$ |
|  | BEARINGS TO AZIMUTHS: |  |  |  |  |  |  |
| 5 | Quadrant $=1$ | BRG (D.MS) | NO CAL | LATION |  |  | AZ (D.MS) |
|  |  |  |  |  |  |  |  |
| 6 | Quadrant $=2$ | 180 | ENTER $\uparrow$ |  |  |  |  |
|  |  | BRG (D.MS) | g | $\rightarrow$ H | - | f |  |
|  |  |  | $\rightarrow$ H.MS |  |  |  | AZ (D.MS) |
| 7. | Quadrant $=3$ | BRG (D.MS) | ENTER $\uparrow$ | 180 | + |  | AZ (D.MS) |
|  |  |  |  |  |  |  |  |
| 8 | Quadrant $=4$ | 360 | ENTER 1 , |  |  |  |  |
|  |  | BRG (D.MS) | g | $\rightarrow \mathrm{H}$ | - | f |  |
|  |  |  | $\rightarrow$ H.MS |  |  |  | AZ (D.MS) |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |




## FIELD ANGLE OR BEARING TRAVERSE

This program uses angles and/or deflections turned from a reference azimuth and horizontal distances, to compute the coordinates of successive points in a traverse. For a closed traverse, the area enclosed and closure distance and azimuth are computed.

Equations:
$\mathrm{N}_{\mathrm{i}+1}=\mathrm{N}_{1}+$ HDist $\cos \mathrm{AZ}$
$E_{i+1}=E_{1}+H D i s t \sin A Z$
Area $=\sum_{k=1}^{n} \operatorname{LAT}_{k}\left(\frac{1}{2} \operatorname{DEP}_{k}+\sum_{j=1}^{k-1} \operatorname{DEP}{ }_{j}\right)$
where:
$\operatorname{DEP}_{k}=E_{k+1}-E_{k}$ and $\operatorname{LAT}_{k}=N_{k+1}-N_{k}$

Remarks:

If the user does not desire to do Field Angle Traverse, steps 012 through 026 may be eliminated; if he does not desire to do Bearing Traverse, steps 064 through 080 may be eliminated.

Angles left and deflections left must be entered as negative numbers.

This program assumes the calculator is set in DEG mode.

Example 1:
Field Angle Traverse
Traverse the figure below starting at

$$
\frac{N \quad 150}{E 400}
$$



Solution:

| 232.3772 | $\begin{aligned} & +\# \# \\ & R / s \end{aligned}$ | （ N ） |
| :---: | :---: | :---: |
| 367.1498 | ＋${ }_{\text {\＃}}$ | （E） |
| －100．4559 | SEE |  |
| 131.3955 | 暒戠 |  |
| 124．8080 | F／S |  |
| 149．9448 | ＋ ＋$_{\text {ct }}$ | （ N ） |
|  | Fes |  |
| 399.7829 | － ch $^{\text {c }}$ | （E） |
|  | 6985 |  |
| 26558．8264 | 䡏 | （Area） |
|  | P6 |  |
| $0.277 \%$ |  | （Error Dist．） |
|  | P／S | （Error AZ） |
| 246.1844 | －${ }_{\text {韦 }}$ |  |

## Example 2：

Bearing Traverse
Traverse the figure below starting at

$$
\frac{\mathrm{N} \quad 100}{\mathrm{E} 500}
$$



Solution：

| 180.8008 ENT＊ |  |  |
| :---: | :---: | :---: |
| 586.8690 ESE |  |  |
| 184.0090 | 俥 |  |
| 86.0223 ENT4 |  |  |
| 1．80日 65E4 |  |  |
| 86.8223 | ＋ 䉼 $^{\text {c }}$ |  |
| 183.5880 | R／S |  |
| 107.1482 | ＋ Ha $^{\text {c }}$ | （N） |
|  | Prs |  |
| 683.2529 | ＋${ }_{\text {＋}}$ | （E） |
| 18.5843 ENTT |  |  |
| 4．日000 ESE4 |  |  |
| 341.8117 | ＋ H $_{\text {\％}}$ |  |
| 181.9600 | Res |  |
| 293.5657 | 䡃戠 | （ N ） |
|  | Peg |  |
| 579.8939 | ＋${ }_{\text {a }}$ | （E） |
| 64.1319 | ENT ${ }^{+}$ |  |
| 3.8000 | ESB4 |  |
| 244.1719 | ＊＊＊ |  |
| 120.4480 | Rs |  |
| 151.1880 | ＋${ }_{\text {H }}^{\text {H }}$ | （N） |
|  | F／s |  |
| 461.6395 | ＋+ ¢ | （E） |
| 37.2651 | ENT4 |  |
| 2.8806 | 6SP4 |  |
| 142.3769 | ＋${ }_{\text {\％}}$ |  |
| 63.1700 | F／S |  |
| 101.8366 | ＊${ }_{\text {\％}}$ | （N） |
|  | P／${ }^{\text {c }}$ |  |
| 580.8498 | ＋${ }_{\text {H }}$ | （E） |
|  | 6SE5 |  |
| 8955.4922 |  | （Area） |
|  | F／S |  |
| 1.8378 | ＋${ }_{\text {H }}^{\text {\％}}$ | （Error Dist．） |
|  | R／G |  |
| 2.4219 | ＊＊＊ | （Error AZ） |


| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program. |  |  |  |
| 2 | Key in beginning coordinates | BEG N | ENT $\uparrow$ |  |
|  |  | BEG E | GSB 1 | 180.00 |
|  | For Field Angle Traverse: |  |  |  |
| 3 | Key in reference azimuth away | REF AZ | R/S | AZ (D.MS) |
|  | from beginning point. |  |  |  |
| 4 | Key in field angle: |  |  |  |
|  | Angle right | ang. righ | GSB 2 | AZ (D.MS) |
|  | or Angle left (-) | -ang. left | GSB 2 | AZ (D.MS) |
|  | or Deflection right | deflect.rt | GSB 3 | AZ (D.MS) |
|  | or Deflection left ( - ) | -deflectulf | GSB 3 | AZ (D.MS) |
| 5 | Key in horizontal distance and compute |  |  |  |
|  | coordinates | HDist | $\mathrm{R} / \mathrm{S}$ | N |
|  |  |  | R/S | E |
|  | or |  |  |  |
|  | For Bearing Traverse: |  |  |  |
| $3{ }^{\prime}$ | Key in bearing*and quadrant code. | BRG (D.MS) | ENT $\uparrow$ |  |
|  |  | QD | GSB 4 | AZ (D.MS) |
| $4^{\prime}$ | Key in horizontal distance and compute |  |  |  |
|  | coordinates. | HDist | R/S | N |
|  |  |  | R/S | E |
|  | Repeat steps $3,4,5$, or $3^{\prime}, 4^{\prime}$ for successive |  |  |  |
|  | courses. |  |  |  |
| 6 | For closed figure: Compute area, error |  |  |  |
|  | distance, and error azimuth. |  | [GSB 5 | Area |
|  |  |  | R/S | Error Dist |
|  | * If azimuth is known rather than bearing, |  | R/S | Error AZ |
|  | enter azimuth with $\mathrm{QD}=1$. |  |  |  |
|  |  |  | $\square \square$ |  |
|  |  |  | $1[\square]$ |  |
|  |  |  |  |  |
|  |  |  | $\square$ |  |
|  |  |  | $\square$ |  |
|  |  |  | ] |  |
|  |  |  | $\square$ |  |
|  |  |  | $][\square$ |  |
|  |  |  | $\square$ |  |
|  |  |  | ] $\square$ |  |
|  |  |  | $\square \square$ |  |


| 01 | WEL! | Store starting | 50 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 92 | FIM4 | point coordinates | 5 | $\vdots$ |  |
| 02 | CLPE | and $180^{\circ}$ | 52 | PCl? |  |
| 64 | STOI |  | 57 |  |  |
| $0 \cdot$ | $\mathrm{X}+\mathrm{H}$ |  | 54 | $\times$ |  |
| 66 | sto |  | 5 | ST+ |  |
| 87 | i |  | 56 | FCLE |  |
| 69 | $\theta$ |  | 5 | FCL |  |
| 09 | $\square$ |  | 56 | $+$ |  |
| 10 | STCS |  | 59 | Fe | *** |
| 11 | Fes |  | 64 | FCL |  |
| 12 | +4 |  | 61 | FCL 1 |  |
| 13 | FCl? | Reference azimuth | 62 | + |  |
| 14 | + ${ }^{+}$ |  | $6 ?$ | Fe | *** |
| 15 | + |  | 64 | *LEL 4 |  |
| 15 | GTOE |  | 65 | \%+' |  |
| 17 | WLEL2 |  | 5 | ctoc |  |
| 18 | + + | Angle input | 67 | X +1 | Convert bearing and |
| 12 | PCL 3 |  | 68 | ENT* | quadrant code to |
| 28 | + H |  | 69 | EUTA | azimuth. |
| 21 | + |  | 76 | 2 |  |
| 22 | +hre |  | 71 | $\div$ |  |
| 23 | *LEL 3 | Deflection angle | 72 | IUT |  |
| 24 | + + | input | 73 | FCl 3 |  |
| 25 | PCL 4 |  | 74 | X |  |
| 26 | - |  | P | $\underline{+Y}$ |  |
| 27 | *LEL |  | 76 | RCL |  |
| 28 | + |  | 7 | X |  |
| 29 | + |  | 78 | cos |  |
| 76 | ${ }^{+}$ | Compute azimuth | 79 | RCIS |  |
| 3 | ULEL9 |  | 80 | + + |  |
| 72 | 8+ |  | 81 | x |  |
| 3 | V19 |  | 82 | - |  |
| 34 | Cre |  | 83 | groe |  |
| 35 | 亏 |  | 84 | WLEL5 | Area |
| 76 | 6 |  | ge | PCLE |  |
| 77 | 0 |  | 86 | AES |  |
| 38 | + |  | 87 | Prg | *** |
| 79 | *LELE |  | 89 | $\mathrm{FCL} \mathrm{T}^{\text {P }}$ |  |
| 40 | STC4 |  | 89 | FCle |  |
| 41 | -HME |  |  | + + | Setup for closure |
| 42 | FS | *** |  | Pe | *** |
| 47 | CT+ |  |  |  |  |
| 44 | PCL 4 | Input horizontal |  | PG |  |
| 45 | 品 | distance |  |  |  |
| 46 | + |  |  |  |  |
| 47 | ST+E |  |  |  |  |
| 48 | $\mathrm{K}+\mathrm{Y}$ $8 \mathrm{~T}+7$ | Compute next coord. and accumulate area |  |  |  |
| 49 | $6 T+7$ |  |  |  |  |

REGISTERS

| 0 | 1 Beg. | 2 Beg. N | $3 \quad 180$ | 4 | AZ | 5 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 6 Lat. | 7 Dep. | 8 Area | 9 Bearing | .0 | .1 |  |
| .2 | 3 | 4 | .5 | 16 | 17 |  |
| 18 | 19 | 20 | 21 | 22 | 23 |  |
| 24 | 25 | 26 | 27 | 29 |  |  |

*** indicates that "Print $X$ " may be inserted or used to replace " $\mathrm{R} / \mathrm{S}$ ".

## inverse with CLosure

This program calculates the distance and azimuth of the line joining two points. For a closed inverse, the area enclosed and closure distance and azimuth are computed.

## Equations:

$H D=\sqrt{\left(N_{i}-N_{i-1}\right)^{2}+\left(E_{i}-E_{i-1}\right)^{2}}$

$$
A Z=\tan ^{-1} \frac{E_{i}-E_{i-1}}{N_{i}-N_{i-1}}
$$

$$
\text { Area }=\sum_{k=1}^{n} \operatorname{LAT}_{k}\left({\frac{1}{2} D E P_{k}}^{n} \sum_{j=1}^{k-1} \operatorname{DEP}_{j}\right)
$$

where

$$
\mathrm{DEP}_{\mathrm{k}}=\mathrm{E}_{\mathrm{k}+1}-\mathrm{E}_{\mathrm{k}} \text { and }
$$

$$
\mathrm{LAT}_{\mathrm{k}}=\mathrm{N}_{\mathrm{k}+1}-\mathrm{N}_{\mathrm{k}}
$$

Example: Inverse the figure below starting at


Begin $\frac{\text { N } 100.000}{E 200.000}$

Solution:
$\left.\begin{array}{|c|c|c|c|c|c|}\hline \text { STEP } & \text { INSTRUCTIONS } & \text { INPUT } \\ \text { OATA/UNITS }\end{array}\right]$

*** "Print $X$ " may replace or be used with "R/S"

## SIDESHOTS

This program is used to make sideshots or radials from a point. Two methods may be used for a sideshot, 1) input a bearing and distance and calculate the point coordinates, or 2 ) input the point coordinates and calculate the azimuth and distance to the point.

Equations:

$$
\begin{aligned}
& N=N_{0}+H \text { Dist } \cos A Z \\
& E=N_{0}+H \text { Dist sin } A Z
\end{aligned}
$$

Example:

Solutions:

| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program |  |  |  |
| 2 | Enter hub coordinates | N | ENT $\uparrow$ |  |
|  |  | E | GSB |  |
| 3 a | For bearing sideshot: Enter bearing and quad- | BRG (D.MS) | ENT $\uparrow$ |  |
|  | rant; | QD | GSB] [ 2 | AZ (D.MS) |
|  | enter horizontal distance and compute point | H Dist | R/S | N |
|  | coordinates. |  | R/S | E |
|  | *If azimuth is known rather than bearing, |  | 1 |  |
|  | enter azimuth with $\mathrm{QD}=1$. |  | 1 |  |
|  |  |  | [ \| | |  |
| 3b | For inverse sideshot: enter coordinates of | N | ENT $\uparrow$ |  |
|  | sideshot point and compute horizontal distance | E | [GSB \|| 3 | H Dist |
|  | azimuth |  | R/S | AZ (D.MS) |
|  |  |  | 1 |  |
| 4 | Repeat step 3 for all desired sideshots. |  | 11 |  |
|  |  |  | \| 1 |  |
|  |  |  | ] 1 |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | 11 |  |
|  |  |  | 111 |  |
|  |  |  | 11 |  |
|  |  |  | \| 1 |  |
|  |  |  | 1 |  |
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|  |  |  | 1 |  |
|  |  |  | 1 |  |
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|  |  |  | \| 1 |  |
|  |  |  | \| |  |
|  |  |  | \| 1 |  |
|  |  |  | \| |  |
|  |  |  | \| |  |
|  |  |  | $1 \mid$ |  |
|  |  |  | \| |  |


*** "Print $X$ " may replace or be used with "R/S"

## COMPASS RULE ADJUSTMENT

This program adjusts a traverse by the compass rule. It is intended to follow the program "Field Angle or Bearing Traverse" (with closure). However, if the correct coordinates of the last point and the total distance traversed are known, these parameters can be used in lieu of executing the closure program.

If this program is not used immediately after "Field Angle or Bearing Traverse" (with closure) or the storage registers have been altered since the closure program was run, enter the following data into the specified storage registers:

Register Parameter:

1. Correct closing easting.
2. Correct closing northing.
3. Total distance traversed.
4. Calculated ending northing.
5. Calculated ending easting.

The Inverse program may be used to obtain adjusted bearings, distances and area.

## Equations:

$$
\begin{aligned}
& C_{L}=\frac{(\Delta N) \text { (Dist) }}{\sum \text { Dist }} \\
& C_{D}=\frac{(\Delta E) \text { (Dist) }}{\sum D i s t} \\
& \text { Where: } \quad C_{L}=\text { Correction to latitude of } \\
& \text { a course. } \\
& C_{D}=\text { Correction to departure of } \\
& \text { a course. }
\end{aligned}
$$

Examp1e:
667.147 Total distance traversed
400.000 Correct closing easting
150.000 Correct closing northing
399.783 Calculated ending easting
149.905 Calculated ending northing

POINT UNADJUSTED
NO. COORDINATES
$2 \quad \mathrm{~N}=224.515$
$E=561.615$
$3 \quad \frac{\mathrm{~N}}{\mathrm{E}}=356.529$
$4 \quad \mathrm{~N}=232.337$

Ending \& ( $\mathrm{N}=149.905$
Beginning $\}_{\mathrm{E}}=\overline{399.783}$
Solution:


| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program |  |  |  |  |
| 2 | Store data | Beg N | STO | 2 |  |
|  | Note: If this program is run immediately | Beg E | STO | 1 |  |
|  | following "Field Angle or Bearing Traverse", | EHDist | STO |  |  |
|  | these values are already stored in the | C1 LAT | STO | 6 |  |
|  | correct registers. | C1 DEP | STO | 7 |  |
| 3 | Initialize |  | GSB | 1 |  |
| 4 | Compute adjusted coordinates | Unadj N | ENT $\uparrow$ |  |  |
|  |  | Unadj E | GSB | 2 | Adj N |
|  |  |  | R/S |  | Adj E |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  | *N.E. Coordinates must be reentered in the |  |  |  |  |
|  | same sequence as originally traversed, |  |  |  |  |
|  | starting at the second point. |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  | 11 |  |  |
|  |  |  | $1]$ |  |  |
|  |  |  | 1 |  |  |
|  |  |  | 1 |  |  |
|  |  |  | $\|1\|$ |  |  |
|  |  |  | 1 \| |  |  |
|  |  |  | 1 |  |  |
|  |  |  |  |  |  |
|  |  |  | 1 |  |  |
|  |  |  | \|| |  |  |
|  |  |  | \| 1 |  |  |
|  |  |  | \| 1 |  |  |
|  |  |  | 11 |  |  |
|  |  |  | \| 1 |  |  |
|  |  |  | \| 1 |  |  |
|  |  |  | 11 |  |  |
|  |  |  | $1 \mid$ |  |  |
|  |  |  | \| 1 | I |  |
|  |  |  | \| | \| |  |
|  |  |  |  |  |  |



## CURVE SOLUTIONS

Given values for any of the following pairs, this program computes the remaining parameters plus the sector, segment, and fillet areas: $\Delta$ and $C ; \Delta$ and $R$; $\triangle$ and $T$; $R$ and $T$; $R$ and $L$; $R$ and $C$.

Equations

```
\frac{1}{2}\Delta= \mp@subsup{\operatorname{tan}}{}{-1}(T/R)=\mp@subsup{\operatorname{sin}}{}{-1}(\frac{1}{2}C/R)=90L/\piR
    T = R tan ( (1/2 A)
    C=2T cos (\frac{1}{2}\Delta)
    R = T/tan (\frac{1}{2}\Delta)=C/(2 sin (\frac{1}{2}\Delta))
    L}=\Delta\pi\textrm{R}/18
Sector area = LR/2
Segment area = Sector area-\frac{1}{2}CR cos(\frac{1}{2}\Delta)
Fillet area = T R-Sector area
Where: T = Tangent distance
    C = Chord length
    L = Arc length
    R = Radius
    | Central angle
```


$\mathrm{R}=223.181$
$\Delta=45^{\circ} 30^{\prime} 23^{\prime \prime}$
$\frac{1}{2} \Delta=22^{\circ} \quad 45^{\prime} 11^{\prime \prime}$
$C=172.636$
$\mathrm{T}=93.602$
$\mathrm{L}=177.258$
Sector area $=19780.36$
Segment area $=2015.00$
Fillet area $=1109.87$

Solution:

| 227.1810 | cta | R |
| :---: | :---: | :---: |
| 172,666 | CTas | C |
|  | CSE: |  |
| 223.1810 | $P 6$ | R |
| 22.752 | +4 | $\Delta / 2$ |
|  | Fs |  |
| 03.6022 | +6 | T |
|  | Re |  |
| 172.6360 | +4.4 | C |
|  | Fe |  |
| 17.2584 | W4 | L |
|  | PS |  |
| 9760.356 | ** | Sector Area |
|  | PS |  |
| 2014.0959 | ** | Segment Area |
|  | RE |  |
| 1109.6705 | 4.4 | Fillet Area |



***"PrintX" may be inserted or used to replace "R/S"

## HORIZONTAL CURVE LAYOUT

This program calculates various field data for layout of an horizontal circular curve. The required information on the curve is the PC station and the radius or degree of curve. With this data one computes successively the arc length, deflection angle from tangent to chord, the long chord from PC to current station, and the short chord from previous station to current station. In addition, the tangent offset and tangent distance are available if desired.

If the central angle is known the program also will compute the total arc length from PC to PT, the station PT and the length of the tangent from $P C$ to $P I$.

In the program, stations are entered in the form XXXX. XX for station
$X X+X X . X X$. For example: $20+10.00$ is entered as 2010.00. The degree of curve D, (or central angle subtending an arc of 100 ft .) is entered in degrees with a negative sign, always.

## PC Deflections



Field data output for PC deflections consist of:
STA-current station
ANG-deflection angle from tangent to long chord.
LC-long chord from PC to current station

```
SC-Short chord from previous station
        to current station
\(\Delta \Delta\)-central angle
    PI-point of intersection of tangents
PC, PT-ends of curve
    L-Arc length
    R-radius
```

Tangent Offsets and Distances


Field data output for tangent offsets consist of:

$$
\begin{aligned}
& \text { STA-current station } \\
& \text { TD-tangent distance } \\
& \text { TO-tangent offset } \\
& \text { T-distance from PC to PI }
\end{aligned}
$$

## HORIZONTAL CURVE LAYOUT

Example：

```
Compute field data for a curve with a
central angle of 35'30' and degree of
curve of 12 }\mp@subsup{}{}{\circ}3\mp@subsup{0}{}{\prime}\mathrm{ . The PC station is
7+85.40.
Solution：
```

| 795.4000 EHT＊ |  |  |
| :---: | :---: | :---: |
| －12． 3000 | CSE1 |  |
| 785.4000 | ＊＊＊ | （PC） |
|  | RCL 1 |  |
| 458.3662 | 㒳 | （R） |
| 800.6000 | GSE2 | （For STA．8） |
| 14.6009 | ＊＊＊ | （L） |
|  | Res |  |
| 0.5445 | ＊＊ | （ANG） |
|  | Res |  |
| 14.5994 | ＊＊＊ | （LC） |
|  | Res |  |
| 14.5994 | W＊ | （SC） |
|  | RCLE |  |
| 0.2325 | ＊${ }^{\text {a }}$ | （TO） |
|  | RCIS |  |
| 14.5975 | ＊＊ | （TD） |
| 900． 0000 | GSE2 | （For STA．9） |
| 114.6000 | ＊${ }^{*}$ | （L） |
|  | R\％ |  |
| 7．0945 | ＊＊＊ | （ANG） |
|  | R／S |  |
| 114.3018 | bl | （LC） |
|  | R／S |  |
| 99.8018 | ＊＊＊ | （SC） |
|  | RCLE |  |
| 14.2516 | 䋛 | （T0） |
|  | RCL9 |  |
| 113.4098 | 䊂伟 | （TD） |


| 1090． 9000 | GSE2 | （For STA．10） |
| :---: | :---: | :---: |
| 214.6000 | ＊＊ | （L） |
|  | R／S |  |
| 13.2445 | ＊＊＊ | （ANG） |
|  | R／S |  |
| 212.6454 | ＊＊＊ | （LC） |
|  | R／S |  |
| 99.8018 | ＊＊＊ | （SC） |
|  | RCL8 |  |
| 49.3252 | 粎 | （TO） |
|  | FCL 9 |  |
| 206.8455 | ＊＊＊ | （TD） |
| 35．3000 | GSE？ |  |
| 284.0080 | ＊＊＊ | （L） |
|  | R\％ |  |
| 1069．4000 | ＊＊＊ | （PT） |
|  | R／S |  |
| 146.7242 | ＊＊＊ | （T） |
| 1969．4000 | GSE2 | （Field data：PT） |
| 284.0000 | ＊＊＊ | （L） |
|  | FG |  |
| 17．4500 | ＊＊＊ | （ANG） |
|  | Re |  |
| 279.4796 | ＊＊＊ | （LC） |
|  | $F \mathrm{E}$ |  |
| 69.3337 | W4 | （SC） |

User Instructions

| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program. |  |  |  |  |
| 2 | Input beginning station of curve | PC | ENT $\uparrow$ |  | PC |
| 3 | Input radius | R | GSB | 1 |  |
|  | or degree of curve (as a negative number) | -D (D.MS) | GSB |  |  |
|  |  |  |  |  |  |
| $3{ }^{\prime}$ | Radius or degree of curve are available if |  | RCL |  | R |
|  | desired. |  | RCL | 2 | D |
| 4 | Input station | STA | GSB | 2 | L(Arc.leng) |
|  |  |  | R/S |  | def. angle |
|  |  |  | [R/S |  | long chord |
|  |  |  | R/S |  | short chor |
| $4^{\prime}$ | Tangent offset, TO, and tangent distance, |  |  |  |  |
|  | TD, are available if desired. |  | RCL | 8 | T0 |
|  |  |  | RCL | 9 | TD |
| 5 | Input central angle | $\triangle$ (D.MS) | GSB | 3 | Arc. lengt |
|  |  |  | R/S |  | station PT |
|  |  |  | R/S |  | T , length |
|  |  |  |  |  |  |
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*** indicates that "Print $X$ " may be inserted or used to replace "R/S".

## BEARING-DISTANCE AND BEARING-BEARING INTERSECTION

This program computes the coordinates of the point of intersection of two lines: 1) one of known bearing through known coordinates and the other of known length from a point of known coordinates; or 2) when the bearing of each line is known and the coordinates of a point on each line are known. For the first case, both solutions may be computed.

Equations:

## Bearing-Distance

$$
\begin{aligned}
& A z_{12}=\tan ^{-1} \frac{E_{2}-E_{1}}{N_{2}-N_{1}} \\
& \text { h = Dist } 12 \text { sin } \phi \\
& \mathrm{b}=\sqrt{\text { Dist }_{2}^{2}-\mathrm{h}^{2}} \\
& \mathrm{~N}=\mathrm{N}_{1}+\left(\left(\text { Dist }_{12} \cos \phi\right)+\mathrm{b}\right) \cos \left(\mathrm{Az}_{1}\right) \\
& E=E_{1}+\left(\left(\text { Dist }_{12} \cos \phi\right)+b\right) \sin \left(\mathrm{Az}_{1}\right) \\
& \text { where: } A Z_{12}=\text { Azimuth of line from } \\
& \text { point } 1 \text { to point } 2 \\
& A Z_{1}=\text { Azimuth of line } 1 \\
& \phi=\text { Angle between line } 1 \text { and } \\
& \text { line from point } 1 \text { to } \\
& \text { point } 2 \\
& \text { h = Perpendicular distance } \\
& \text { from point } 2 \text { to line } 1 \\
& \mathrm{~b}=\text { Distance from point of } \\
& \text { intersection to the } \\
& \text { point where the perpendi- } \\
& \text { cular (h) intersects line } \\
& 1 \\
& \text { Dist } 2=\text { Length of line } 2 \text { (the } \\
& \text { known distance) } \\
& \mathrm{N}_{2} \mathrm{E}_{2}=\text { Northing, easting of point } \\
& 1 \\
& \mathrm{~N}_{2} \mathrm{E}_{2}=\text { Northing, easting of point } \\
& 2 \\
& \text { Dist }_{12}=\text { Distance from point } 1 \text { to } \\
& \text { point } 2
\end{aligned}
$$

```
            Bearing-Bearing
    N = N N + Dist (cos AZ I )
    E = E1 + Dist (sin AZ )
Dist = Dist 12 sin (AZ 2-AZ 12 )
```

where:

$$
\begin{aligned}
\mathrm{AZ}_{12}= & \text { Azimuth of } 1 \text { ine from point } \\
& 1 \text { to point } 2
\end{aligned}
$$

```
AZ l = Azimuth of line 1
AZ2}=\mathrm{ Azimuth of line 2
N}\mp@subsup{|}{1}{}\mp@subsup{E}{1}{}=\mathrm{ Northing, easting of point l
N}\mp@subsup{N}{2}{}\mp@subsup{E}{2}{}=\mathrm{ Northing, easting of point 2
N,E = Northing, easting of intersect
        point
Dist = Distance from point 1 to inter-
        section
Dist 12 = Distance from point 1 to point
        2
```

Example 1:

$\overline{E_{1}}=250.000$

Solution:

> 75.0600 ENT*
> 250.0000 GE1 460.0600 ENT 604.0000 Re 45.4550 Ent
> 1. D00e GeE 25.3070 EUT* 4. 0000 ESE GEP4
> 596.5457 WH
> 505,2631 Wh E

Examp1e 2:
(FAR SOLUTION-
AZIMUTH ENTERED AS $\quad \mathbf{N}=\mathbf{6 9 3 . 2 0 9 6}$ AWAY FROM POINT 1) $\quad \bar{E}=\mathbf{6 6 8 . 6 0 8 9}$

NEAR SOLUTIONAZIMUTH ENTERED TOWARD POINT 1) /

$\mathrm{N}_{1}=\mathbf{3 0 0 . 0 0 0}$
$\overline{E_{1}}=200.000$

Solution:



***"Print X" may replace or be used with "R/S"

## DISTANCE-DISTANCE INTERSECTION

Given two lines, each of known length and originating from two known points, this program computes the intersection coordinates. There are two possible solutions; this program calculates the one found by proceeding in a clockwise direction from the first known point to the second known point. The other solution is found by reversing the entry of the known point coordinates.

Equations:

$$
\begin{aligned}
& \phi=\cos ^{-1} \frac{\text { Dist }_{12}{ }^{2}+\text { Dist }_{1}^{2}-\text { Dist }_{2}^{2}}{2\left(\text { Dist }_{1}\right)\left(\text { Dist }_{12}\right)} \\
& A Z=\tan ^{-1} \frac{E_{2}-E_{1}}{N_{2}-N_{l}}
\end{aligned}
$$

$\mathrm{N}=\mathrm{N}_{\mathrm{l}}+$ Dist $_{l} \cos (\mathrm{AZ}-\phi)$

$$
E=E_{l}+\text { Dist }_{l} \sin (A Z-\phi)
$$

```
where: \phi = Angle between line 1 and
                line 1+2
    Dist }\mp@subsup{1}{2}{}=\mathrm{ Distance from point 1 to
                point 2
    Dist 
    Dist2 = Known distance along line 2
    N N\mp@code{E E = Northing, easting of point 1}
        N,E = Northing, easting of inter-
        section point
        AZ = Azimuth of line from point
                1 to point 2
```


## Example:



Solution:

|  | Clf |
| :---: | :---: |
| 179.1690 | ENT* |
| 132,3790 | GSE1 |
| 95.6010 | ENT* |
| 26.8730 | GSE2 |
| 17.3820 | ENTA |
| 147.7476 | ESES |
| 139.8558 | *** |
|  | F 8 |
| 190.6925 | *** |


| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program |  |  |  |  |
| 2 | Enter distances | Dist 1 | ENT $\uparrow$ |  |  |
|  |  | Dist 2 | GSB | 1 |  |
| 3 | Enter points 1 and 2* and calculate | N 1 | ENT $\uparrow$ |  |  |
|  | intersection | E 1 | GSB | 2 |  |
|  |  | N 2 | ENT $\uparrow$ |  |  |
|  |  | E 2 | GSB | 3 | N |
|  |  |  | R/S |  | E |
|  |  |  |  |  |  |
|  |  |  |  | $\square$ |  |
|  |  |  |  |  |  |
|  |  |  |  | $\square$ |  |
|  |  |  |  | $0$ |  |
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|  |  |  |  | 1 |  |
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|  |  |  |  | $1$ |  |
|  | * Two solutions are possible. For the |  |  |  |  |
|  | alternate solutions reverse the order |  |  |  |  |
|  | of entering points 1 and 2 |  |  |  |  |
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*** 'Print X' may be used to replace "R/S"

## OFFSET FROM A POINT TO A LINE

Given the point of known coordinates with a line of known bearing passing through it and a second point of known coordinates, this program calculates the offset distance from the second point to the line, the distance from the intersection to the first known point, the coordinates of the intersection, and the azimuth from the point of intersection to the second point.

Equations:
Dist ${ }_{B O}=\sqrt{\left(N_{O}-N_{B}\right)^{2}+\left(E_{O}-E_{B}\right)^{2}}$

$$
\begin{aligned}
& \text { Dist }_{B I}=\sqrt{\left(N_{O}-N_{I}\right)^{2}+\left(E_{O}-E_{I}\right)^{2}} \\
& N_{1}=\frac{E_{O}-E_{B}+N_{O} \operatorname{ctn}\left(A z_{B I}\right)+N_{B} \tan \left(A z_{B I}\right)}{\operatorname{ctn}\left(A z_{B I}\right)+\tan \left(A z_{B I}\right)} \\
& E_{1}=E_{B}+\left(N_{I}-N_{B}\right) \tan \left(A z_{B I}\right)
\end{aligned}
$$

Where: Dist $_{\text {BO }}=$ Distance from point to offset point
Dist $_{\text {BI }}=$ Distance from base point to intersection point
Dist $_{\text {IO }}=$ Distance from intersection point to offset point
$\mathrm{N}_{\mathrm{O}}, \mathrm{E}_{\mathrm{O}}=$ Northing, easting of offset point
$N_{B}, E_{B}=$ Northing, easting of base point
$N_{I}, E_{I}=$ Northing, easting of intersection point
$A Z_{B I}=$ Known $A Z$ from base point to intersection point

Example:


Solution:

| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program |  |  |  |  |
| 2 | Store data | $\mathrm{N}_{\mathrm{B}}$ | STO | 1 |  |
|  |  | $\mathrm{E}_{\mathrm{B}}$ | STO | 21 |  |
|  |  | $\mathrm{N}_{\mathrm{O}}$ | STO | 3 |  |
|  |  | $\mathrm{E}_{0}$ | STO | 4 |  |
|  |  | BRG** | STO | 5 |  |
|  |  | QD** | STO | 6 |  |
|  |  | 180 | STO | 7 |  |
| 3 | Run |  | GSB | 17 | $\mathrm{N}_{\mathrm{I}}$ |
|  |  |  | R/S |  | $\mathrm{E}_{\mathrm{I}}$ |
|  |  |  | R/S |  | O.D. |
|  |  |  | $\mathrm{R} / \mathrm{S}$ |  | I.D. |
|  |  |  | R/S |  | 0.AZ* |
|  | *Offset azimuth may be incorrect for |  |  |  |  |
|  | bearings of 0 , but for these cases, the |  |  |  |  |
|  | offset azimuth may be obtained by |  |  |  |  |
|  | inspection |  |  |  |  |
|  |  |  |  |  |  |
|  | **If azimuth is known rather than bearing | Az(H.MS) | STO | 5 |  |
|  |  |  |  |  |  |
|  |  | 1 | STO | 61 |  |
|  |  |  |  |  |  |
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*** "Printx" may be inserted or used to replace "R/S".

## EARTHWORK

## VOLUME BY AVERAGE END AREA

Routines labeled 1 and 2 calculate the end area for any station, volume from previous station, and accumulated volume to the present station. Inputs are the elevations and distances from the centerline for all points of $a$ cross section and the interval from the previous station.

## Equations:

$$
\begin{aligned}
& V \text { avg }=\left(\mid \text { Area }_{i}|+| \text { Area }_{i-1} \mid\right) \frac{I}{2} \\
& \text { Area }=\frac{1}{2}\left[\text { Elev }_{1}\left(\text { H Dist }_{2}-\text { HDist }_{\mathrm{n}}\right)+\right. \\
& \text { Elev }_{2}\left(\text { H Dist }_{3}-\text { HDist }_{1}\right)+ \\
&\left.\cdots+\text { Elev }_{n}\left(\text { H Dist }_{1}-\text { HDist }\right)\right]
\end{aligned}
$$

Where: $V$ avg = Average volume between two stations
Area $=$ Cross sectional area at a station
H Dist $=$ Horizontal distance from centerline at cross section
Elev = Elevation at a point on the cross section
I = Interval between stations
Subscript i refers to current point
Subscript $n$ refers to last point
Numeric subscript refers to point number

VOLUME OF BORROW PIT
Routines labeled 3-6 calculate the volume of fill which can be taken from a borrow pit given grid dimensions and elevations at the grid intersections. Volume is available for each grid section and also as an accumulative volume for all previous sections.

If several grid blocks have the same horizontal dimensions, the sum of the volumes of all these blocks can be calculated at once. For example, if three rectangular blocks have the same dimensions, the 12 elevations are entered before pressing GSB 6.

Equations:

```
Vo1
Vol = (Width)(Length)(Elev)
Where: Vol
                grid section
    Base = Base of triangle
        Ht = Height of triangle
    Elev = Elevation of grid section
                (depth of cut)
            Vol = Volume of rectangular
                grid section
    Width = Width of rectangle
    Length = Length of rectangle
```


## Example 1:



Example 2：
CLRG
0.0000 GSB2 1st Sta．
0.0000 ENT个 Starting at $0 / 0$ \＆
0. 月月 18 GSB1 Going CCW．

B．0日BD ENTT
1月：月AD日 6SB1 -2 ： QAAB ENT $\uparrow$ 12． 1 ABAD GSB1
7．00R4 ENT个
20．ABAR GSB1
6． 8 R19 ENTA
－3：в
7 日月a月 ENT个
－18．DEAB GSB1
-2.8 R日B ENT个
-12.80 E® GSB1
O．RBOB ENTA
$-18.8908 \mathrm{ESB1}$
0.8909 ENT个 Reinput lst Elev \＆

O． 0 日0日 GSB1 Dist．
25．


D． 1000 ENTA
D．gana GSB1
0． 1200 ENT $\uparrow$
12．0000 GSB1
－1：घúด̆ ENT个
14： 0080 GSB1
－1．日anã ENTA
15．иै
18． 1000 ENT个
30．80at GSB1
8． 1000 ENTA
6． 18100 65B1
7．日0日G ENT个
－21．日㫙 6SB1
4． 8804 ENTT
－17．000G 6SB1
－1．gana ENT个
－18． 1000 ESB1
O．00BE ENTT
－8．1046 GSB1
（1） 000 ENT

50．9ana 6SB2
597． 6852 ＊＊K
RCL5
497：6852＊＊Vo1．（interna1）
321．5490＊＊＊Area


|  | CLE |
| :---: | :---: |
| 12．0000 | ENT $\uparrow$ |
| 35.0800 | GSB3 |
| 2． 38019 | GSB5 |
| 3．1600 | GSBS |
| 3．4йй | 6SB5 |
|  | GSB6 |
| 616．0800 | ＊＊＊ |


| 25． $\operatorname{angay}$ | ENTA |  |  |
| :---: | :---: | :---: | :---: |
| 35．дapay | GSB4 | 12：Яुलिดิ ENT个 |  |
| 2.3 зй | GS85 | 25．ดुทด GSB4 |  |
| 3． 4 促 | GSB5 | 3．8йด̆ด GSB5 |  |
| 3.10 an | GSB5 | 3．19［19 GSB5 |  |
| 2.9000 | 6SB5 | 3.6045 CSB5 |  |
| 2.9080 | GSB5 | 3． 62 日4 ESB5 |  |
| 3．1星品 | 6585 | 3．Зий GSB5 |  |
| 3.3 990 | GSB5 | 3．30109 GSB5 |  |
| 3.3999 | GSB5 | 2．gnan GSB5 |  |
| 2.7081 | 6SB5 | 2． 2 90］ | OSB5GSB6 |
| 2.7098 | 6SB5 |  |  |
| 2.4099 | 6SB5 | 1867． 5480 | $\begin{aligned} & \text { *** G.Vol. } \\ & \text { R/S } \end{aligned}$ |
| 2． 6 为 | GSB5 |  |  |
|  | GSEG | 16457．8754 | ＊＊＊A．Vol． |
| 459．3756 | ＊＊＊ | Vol． |  |

25．ดดต่ ENT个

## 12：9990 GSB3

3．19月明 GSBS
3：4GQ9 GSB5
3．8008 GSE5
6SB6
515． 908 粈系 G．Vol．

| STEP | INSTRUCTIONS | INPUT DATA/UNITS | KEYS |  | OUTPUT DATA/UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Key in the program |  |  |  |  |
|  | VOLUME BY AVERAGE END AREA: |  |  |  |  |
| 2 | Initialize |  | f | REG |  |
| 3 | If station has zero end area go to step 6 |  |  |  |  |
| 4 | Input elevation and distance from the | Elev | ENT $\uparrow$ |  |  |
|  | centerline | Dist | GSB | 1 |  |
| 5 | Repeat step 4 working around the section until |  |  |  |  |
|  | first Elev. and Dist. have been reinput |  |  |  |  |
| 6 | Input interval from previous station and |  |  |  |  |
|  | calculate total volume | Int. (ft) | GSB | 2 | $\begin{aligned} & \text { Total } \left.{ }^{\text {Tot }} \begin{array}{l} \text { (yds } \end{array}\right) \text { vol } \\ & \hline \end{aligned}$ |
|  | (Note: input 0 interval if first station) |  |  |  |  |
| 7 | For volume of interval |  | RCL | 5 | $\begin{aligned} & \text { Int } \cdot{ }^{3}{ }^{3} \mathrm{val}^{2} . \end{aligned}$ |
| 8 | For area of cross section |  | RCL | 4 | Area (ft ${ }^{2}$ ) |
| 9 | Go to step 3 for a new section, Step 2 for a |  |  |  |  |
|  | new case |  |  |  |  |
|  |  |  |  |  |  |
|  | VOLUME OF BORROW PIT |  |  |  |  |
| 10 | Initialize |  | f | $\Sigma$ |  |
| 11a | For triangular area | Base | ENT $\uparrow$ |  |  |
|  |  | Height | GSB | 3 |  |
| 11b | For rectangular area | Width | ENT $\uparrow$ |  |  |
|  |  | Length | GSB | 4 |  |
| 12 | Input as many elevations as needed to describe |  |  |  |  |
|  | each corner, pressing GSB 5 after each entry | Elev | GSB | 5 |  |
| 13 | Calculate grid section volume |  | GSB | 6 | G. Vol (ft ${ }^{3}$ |
| 14 | Calculate accumulated volume |  | k/s |  | A.Vol ( $\mathrm{ft}^{3}$ ) |
|  |  |  |  |  |  |
|  | (To convert cubic feet to cubic yards divide |  |  |  |  |
|  | by 27.) |  |  |  |  |
|  |  |  |  |  |  |
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## COORDINATE TRANSFORMATION

This program translates, rotates, and rescales coordinates. Traverse rotation angle is entered as a negative value for counterclockwise rotation and positive for clockwise rotation. The translation factors are calculated by entering old and new grid system coordinates for the same point; rotation is also about this point.

Equations:
$A z_{R}=\phi+\tan ^{-1} \frac{E_{i}-E_{p}}{N_{i}-N_{p}}$
$H^{\text {Dist }}=S \sqrt{\left(N_{i}-N_{p}\right)^{2}+\left(E_{i}-E_{p}\right)^{2}}$
$N=H$ Dist $_{S} \cos \left(\mathrm{AZ}_{\mathrm{R}}\right)+\mathrm{N}_{\mathrm{T}}$
$E=H$ Dist ${ }_{s} \sin \left(A Z_{R}\right)+E_{T_{1}}$

Where: $A Z_{R}=$ Rotated azimuth

$$
\left.\begin{array}{rl}
\phi= & \text { Rotation angle } \\
\mathrm{N}_{\mathrm{i}} \mathrm{E}_{\mathrm{i}}= & \text { Northing, easting of } \\
& \text { current point before } \\
& \text { transformation }
\end{array}\right\} \begin{aligned}
& \mathrm{N}_{\mathrm{p}} \mathrm{E}_{\mathrm{p}}= \begin{array}{l}
\text { Original northing, easting } \\
\text { of pivot point }
\end{array} \\
& \mathrm{HD} \mathrm{Dist}_{\mathrm{S}}= \begin{array}{l}
\text { Scaled horizontal } \\
\\
\text { distance }
\end{array} \\
& \mathrm{S}= \text { Scale factor } \\
& \mathrm{N}, \mathrm{E}= \text { Northing, easting after } \\
& \text { transformation } \\
& \mathrm{N}_{\mathrm{T}_{1}, \mathrm{E}_{\mathrm{T}}=}=\begin{array}{l}
\text { Northing, easting of } \\
\\
\begin{array}{l}
\text { pivot point after } \\
\text { transformation }
\end{array}
\end{array}
\end{aligned}
$$

Note: The scale factor is taken as one, unless the new grid system is to a different scale.

Example:
Coordinates before transformation are those computed by Compass Rule

Adjustment.

| COORDINATES IN <br> OLD SYSTEM | COORDINATES IN <br> NEW SYSTEM |
| :--- | :--- |
| N $150.000 *$ <br> E 400.000 | $\frac{\mathrm{~N}}{\mathrm{E}} \frac{100.00 *}{350.00}$ |
| N | 224.540 |
| E | 561.673 |


| $\mathrm{N} \quad 356.577$ |
| :--- |
| $\mathrm{E} \quad 468.710$ |


| N | 232.414 |
| :--- | :--- |
| E | 307.327 |

* Rotated about this point

Rotation Angle $=-3^{\circ} 00^{\prime} 00^{\prime \prime}$
Scale Factor $=1.00$

## Solution:

| -3.aper gra |  |  |
| :---: | :---: | :---: |
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| 515.358 | *** | E |
| 756.500 | ENTA |  |
| 468.7100 | SSE3 |  |
| 302.ETP | 4. | N |
|  | Fs |  |
| 499.4262 | -** | E |
| 232.446 | ENT* |  |
| 20.3279 | ESE: |  |
| 107.1512 | ver | N |
|  | FE |  |
| 26.75 | ... | E |




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