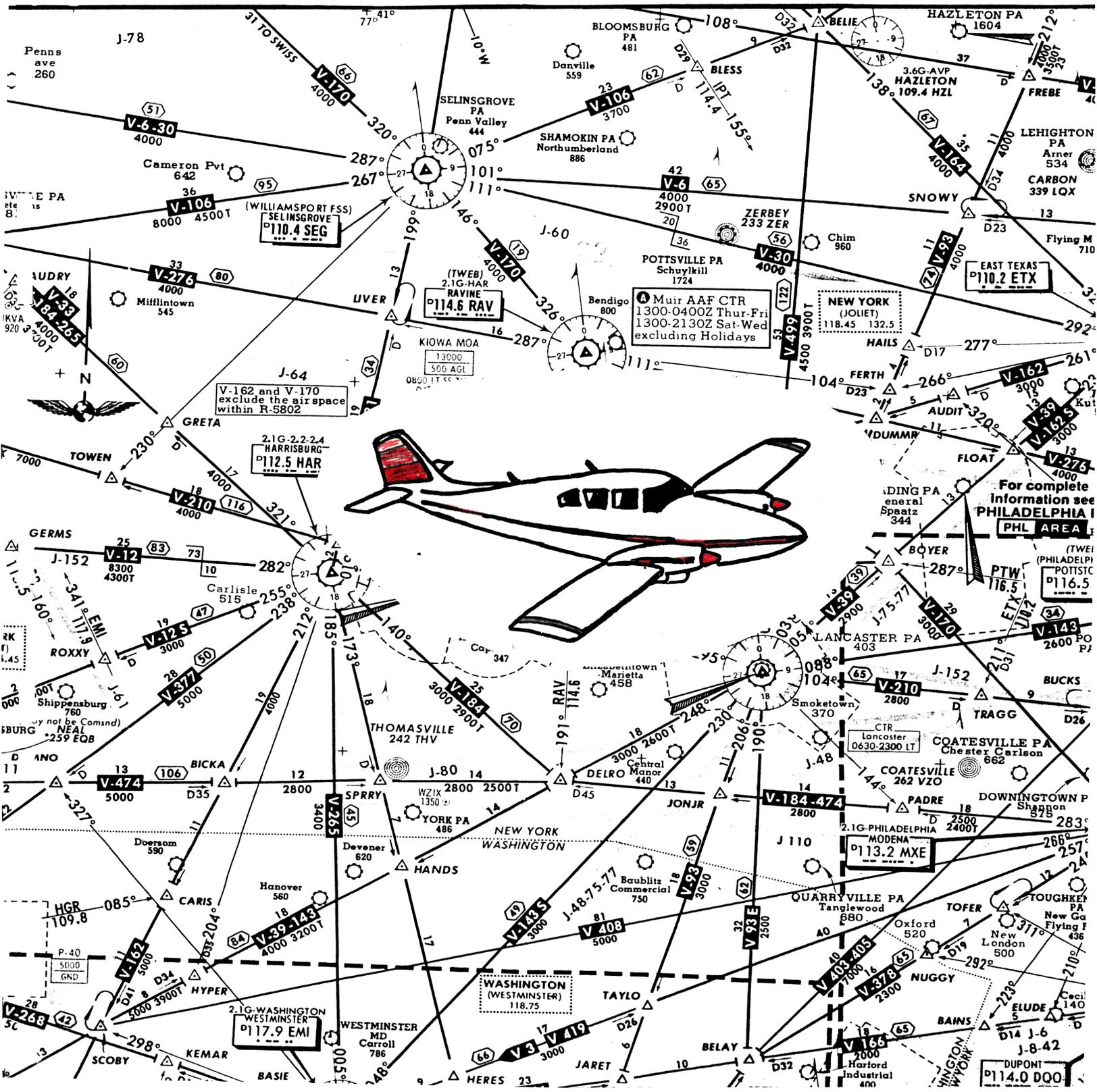


# AREA NAVIGATION RNAV Program for the HP 41C/CV

by  
Robert A. Tims

and Other Programs





AIR NAVIGATION/\*RNAV\*  
NAVIGATION FORMULAS

DISTANCE: The Great Circle distance between fixes is calculated by the following formulas:

$$d = \text{COS}^{-1}[\text{SIN}(\text{LAT})\text{SIN}(\text{LAT}') + \text{COS}(\text{LAT})\text{COS}(\text{LAT}')\text{COS}(\text{LNG} - \text{LNG}')] ]$$

$$\text{(Distance in NM)} = 60d$$

Where: LAT' and LNG' are the coordinates of the "from" fix.  
LAT and LNG are the coordinates of the "to" fix.

Using Atari functions the formula for d is:

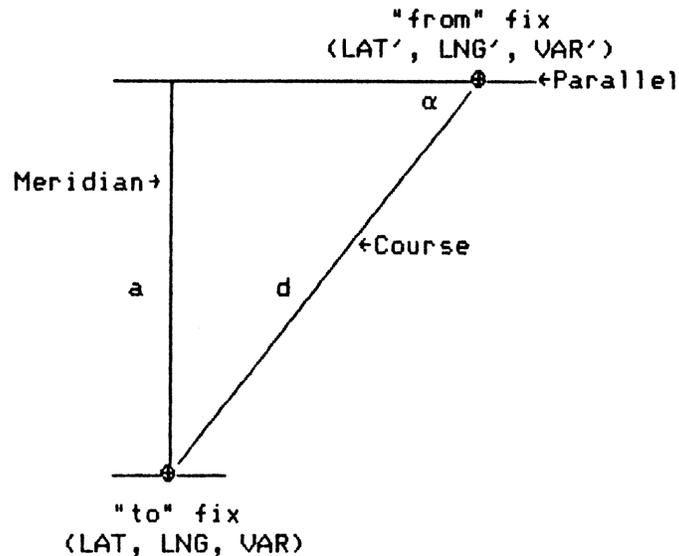
$$d = 90 - \text{TAN}^{-1}[X / (1 - X^2)^2]$$

$$X = [\text{SIN}(\text{LAT})\text{SIN}(\text{LAT}') + \text{COS}(\text{LAT})\text{COS}(\text{LAT}')\text{COS}(\text{LNG} - \text{LNG}')] ]$$

AIR NAVIGATION/\*RNAV\*  
NAVIGATION FORMULAS

COURSE: The course is derived by finding the angle " $\alpha$ " between the parallel passing through the "from" fix and the Course. The angle " $\alpha$ " is then corrected for East/West direction of travel.

A diagram illustrating the relationships is given below with the formulas:



$$a = \cos^{-1}(Y) \quad \text{Atari functions: } a = 90 - \tan^{-1}[Y / (1 - Y^2)^2]$$

$$\text{Where } Y = [\sin(LAT) \sin(LAT') + \cos(LAT) \cos(LAT')]$$

$$d = \cos^{-1}(X) \quad \text{Atari functions: } d = 90 - \tan^{-1}[X / (1 - X^2)^2]$$

$$\text{Where } X = [\sin(LAT) \sin(LAT') + \cos(LAT) \cos(LAT') \cos(LNG - LNG')]$$

$$\alpha = \sin^{-1}(A) \quad \text{Atari functions: } \alpha = \tan^{-1}[A / (1 - A^2)^2] [\text{SGN}(LAT - LAT')]$$

$$\text{Where } A = \sin(a) / \sin(d)$$

If  $(LNG' - LNG) < 0$  then  $TC = 270 + \alpha$  (Westerly direction of travel.)

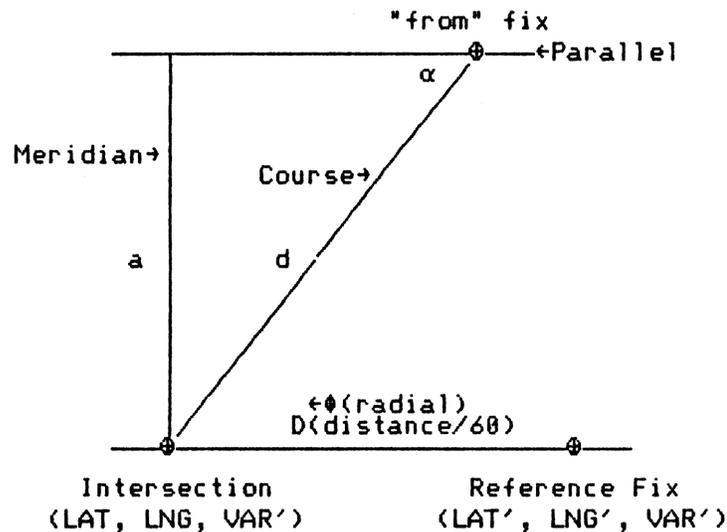
If  $(LNG' - LNG) \geq 0$  then  $TC = 90 - \alpha$  (Easterly direction of travel.)

$MC = TC + VAR'$ , and if  $VAR \neq VAR'$  then  $MC = TC + VAR' / TC + VAR$

AIR NAVIGATION/\*RNAV\*  
NAVIGATION FORMULAS

INTERSECTIONS: Intersections are always defined by the radial (magnetic bearing) and distance from a known fix (reference navaid). The program uses this information along with the coordinates of the reference fix to derive the coordinates of the intersection. These coordinates are then used the same as the coordinates of any other fix.

A diagram illustrating the relationships and the formulas is given below:



$$\text{LAT} = \text{LAT}' + \text{SIN}^{-1}[(\text{SIN } D)(\text{COS } \phi)]$$

$$\text{LNG} = \text{LNG}' - \text{SIN}^{-1}[\frac{(\text{SIN } D)(\text{SIN } \phi)}{\text{COS}[(\text{LAT} + \text{LAT}')/2]}]$$

The formulas using Atari functions:

$$\text{LAT} = \text{LAT}' + \text{TAN}^{-1}[X/(1-X^2)^2]$$

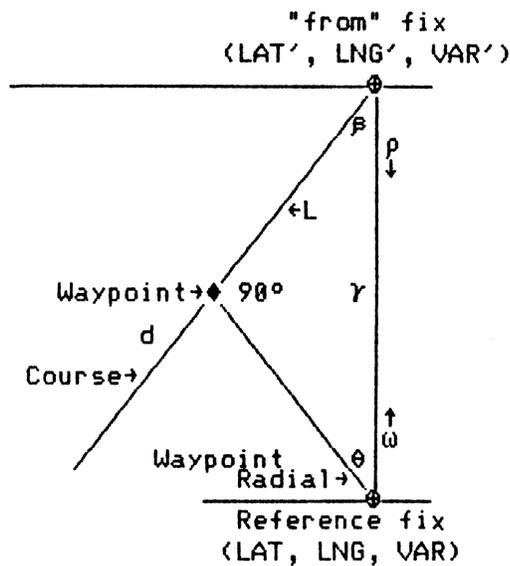
Where  $X = (\text{SIN } D)(\text{COS } \phi)$

$$\text{LNG} = \text{LNG}' - \text{TAN}^{-1}[Y/(1-Y^2)^2]$$

Where  $Y = [(\text{SIN } D)(\text{SIN } \phi)]/\text{COS}[(\text{LAT} + \text{LAT}')/2]$

AIR NAVIGATION/\*RNAV\*  
NAVIGATION FORMULAS

WAYPOINTS: Waypoints are calculated by deriving the bearing and distance of the waypoint from the reference navaid along the radial that is perpendicular to the course. This will form a spherical right triangle between the waypoint, reference navaid, and the "from" fix:



The bearing ( $\rho$ ) and distance angle ( $\gamma$ ) from the "from" fix to the reference fix is calculated first. The angle,  $\gamma$ , is calculated with the same formula as used to find the course distance angle ( $d$ ), and  $\rho$  is calculated the same way as the true course. The bearing ( $\omega$ ) from the reference fix to the "from" fix and is the reciprocal of  $\rho$ ,  $\omega = \rho \pm 180$ . The angle,  $\beta$ , is the difference between the bearing ( $\rho$ ) and the true course. This angle is expressed as:

$$-180^\circ \leq \beta \leq 180^\circ$$

If  $\beta > |90^\circ|$  then the way point will not be usable because it will occur the other side of the "from" fix.

## AIR NAVIGATION/\*RNAV\* NAVIGATION FORMULAS

The distance (L) between the "from" fix and the waypoint is calculated with the following formula:

$$L=60[\text{SIN}^{-1}[\text{SIN}(|\theta|)\text{SIN}(\gamma)]] \quad \theta=90-\beta$$

Using the Atari functions the formula becomes:

$$L=60[\text{TAN}^{-1}[X/(1-X^2)^2]]$$

Where  $X=\text{SIN}(|\theta|)\text{SIN}(\gamma)$

The waypoint radial and distance are calculated with the following formulas:

$$\text{Waypoint radial} = \omega + \text{SGN}(\beta)(\theta) + \text{VAR}$$

$$\text{Waypoint distance} = 60[\text{SIN}^{-1}[\text{SIN}(|\beta|)\text{SIN}(\gamma)]]$$

Using Atari functions:

$$\text{Waypoint distance} = 60[\text{TAN}^{-1}[Y/(1-Y^2)^2]]$$

Where  $Y=\text{SIN}(|\beta|)\text{SIN}(\gamma)$

### TERMINAL WAYPOINTS

The terminal waypoints are calculated by letting the reference navaid be the "from" fix and the terminal airport be the "to" fix. The same formulas used to find the true course and distance are used. The reference navaid's magnetic variation is added to the bearing from the reference fix to the terminal airport to obtain the proper radial. The reference navaid's magnetic variation is also used to obtain the magnetic course from the departure airport or to the destination airport as the case may be.



CURRENT AIRWAY PROGRAM



# HP41C AIRNAV Program

by Robert A. Tims

Copyright 1986

01*LBL "AIRNAV"	47*LBL 21	95 X<>Y
02 19	48 CLA	96 RCL 16
03 PSIZE	49 ARCL 01	97 X>Y?
04*LBL 01	50 "F TO WP?"	98 GTO 21
05 32	51 CF 23	99 RDN
06 X<>F	52 XEQ 04	100 ENTER↑
07 SF 21	53 FC? 23	101 X<> 16
08 SF 23	54 GTO 02	102 XEQ 03
09 CF 29	55 "WP:"	103 ADV
10 0	56 ARCL 05	104 FIX 1
11 STO 17	57 ASTO 05	105 CLA
12 "FROM?"	58 XEQ 08	106 ARCL 05
13 XEQ 04	59 STO 10	107 XEQ 15
14 CF 05	60 180	108 CLA
15 RCL 05	61 +	109 RCL 07
16 STO 18	62 90	110 XEQ 10
17 FC?C 08	63 RCL 00	111 "+, "
18 XEQ 09	64 RCL 10	112 RCL 10
19*LBL 20	65 -	113 SIN
20 CLA	66 1	114 RCL 09
21 ARCL 05	67 P-R	115 *
22 ASTO 01	68 R-P	116 ASIN
23 "F TO?"	69 RDN	117 60
24 CF 23	70 X<0?	118 *
25 XEQ 04	71 SF 05	119 ARCL X
26 FC? 23	72 ABS	120 "+ NM"
27 GTO 22	73 STO 10	121 XEQ 15
28 ADV	74 -	122 RCL 00
29 XEQ 08	75 X<=0?	123 STO 04
30 STO 00	76 GTO 21	124 ADV
31 RCL 10	77 STO 07	125 RCL 05
32 FIX 0	78 FC?C 05	126 STO 01
33 RND	79 CHS	127 GTO 21
34 ST+ 17	80 +	128*LBL 02
35 STO 15	81 RCL 08	129 CF 06
36 RCL 05	82 +	130 RCL 11
37 STO 11	83 X<> 07	131 STO 05
38 RCL 06	84 SIN	132 RCL 14
39 STO 12	85 RCL 09	133 STO 09
40 RCL 07	86 *	134 RCL 15
41 STO 13	87 ASIN	135 RCL 16
42 RCL 08	88 60	136 XEQ 03
43 STO 14	89 *	137 RCL 12
44 0	90 FIX 0	138 STO 02
45 STO 16	91 RND	139 RCL 13
46 SF 06	92 RCL 15	140 STO 03
	93 X<=Y?	141 RCL 09
	94 GTO 21	142 STO 04
		143 GTO 20



# HP41C AIRNAV Program

by Robert A. Tims

Copyright 1986

144*LBL 03	190*LBL 06	240*LBL 00
145 FIX 0	191 AON	241 FC? 06
146 -	192 TONE 8	242 FS? 07
147 CLA	193 PROMPT	243 GTO 06
148 ARCL 01	194 AOFF	244 RCL 02
149 FC? 55	195 FC? 23	245 STO 06
150 GTO 00	196 RTN	246 RCL 03
151 ACA	197 FC? 06	247 STO 07
152 CLA	198 CF 08	248 RCL 04
153 SF 13	199 ASTO 05	249 STO 08
154 * TO *	200 4	250 RCL 05
155 ACA	201 ALENG	251 STO 11
156 CF 13	202 X<Y?	252 SF 07
157 CLA	203 GTO 00	253 CF 23
158*LBL 00	204 SF 25	254 8
159 FC? 55	205 XEQ IND 05	255 *NEED FIX?*
160 "+"	206 FC?C 25	256 XEQ 05
161 ARCL 05	207 GTO 01	257 CF 07
162 XEQ 15	208*LBL 07	258 RCL 01
163 *MC="	209 STO IND 09	259 FS? 23
164 RCL 00	210 DSE 09	260 RCL 05
165 RCL 04	211 RDN	261 STO 10
166 +	212 HR	262 RCL 11
167 STO 06	213 STO IND 09	263 STO 05
168 XEQ 10	214 DSE 09	264 CF 22
169 RDN	215 RDN	265 *RADIAL?*
170 CLX	216 HR	266 TONE 8
171 RCL 06	217 STO IND 09	267 PROMPT
172 RCL 00	218 RTN	268 CLA
173 RCL 08	219*LBL 01	269 ARCL 05
174 +	220 CF 22	270 SF 23
175 X*Y?	221 "+ LAT?"	271 FC?C 22
176 "+/"	222 TONE 8	272 GTO 04
177 X*Y?	223 PROMPT	273 *DME?*
178 XEQ 10	224 CLA	274 TONE 8
179 XEQ 15	225 ARCL 05	275 PROMPT
180 *DIST="	226 FC?C 22	276 CLA
181 ARCL T	227 GTO 00	277 ARCL 05
182 "+ NM"	228 "+ LNG?"	278 FC? 22
183 GTO 15	229 TONE 8	279 GTO 04
184*LBL 04	230 PROMPT	280 X<Y
185 8	231 CLA	281 FC? 55
186 FS? 05	232 ARCL 05	282 GTO 00
187 4	233 FC?C 22	283 ADV
188*LBL 05	234 GTO 00	284 "+ * WP:"
189 STO 09	235 "+ VAR?"	285 ARCL 10
	236 TONE 8	286 PRA
	237 PROMPT	287 CLA
	238 FS? 22	288 FIX 1
	239 GTO 07	289 XEQ 10
		290 RDN



# HP41C AIRNAV Program

by Robert A. Tims

Copyright 1986

291*LBL 00	333*LBL 08		426*LBL 00
292 ", "	334 RCL 06		427 100
293 ARCL Y	335 SIN	383*LBL 09	428 X>Y?
294 "+ NM"	336 RCL 02	384 RCL 05	429 "+0"
295 FS? 55	337 SIN	385 STO 01	430 SQRT
296 XEQ 15	338 *	386 CLA	431 X>Y?
297 RCL 08	339 STO 09	387 ARCL 05	432 "+0"
298 FS? 05	340 RCL 06	388 "+ WP?"	433 ARCL Y
299 STO 04	341 COS	389 SF 06	434 FC? 55
300 -	342 RCL 02	390 CF 23	435 RTN
301 STO 09	343 COS	391 XEQ 04	436 ACA
302 RDN	344 *	392 CF 06	437 "a"D"
303 60	345 STO 10	393 FC? 23	438 ASTO X
304 /	346 +	394 RTN	439 ACSPEC
305 SIN	347 ACOS	395 ADV	440 CLA
306 STO 10	348 SIN	396 "WP:"	441 RTN
307 RCL 09	349 RCL 06	397 ARCL 05	442*LBL 22
308 SIN	350 RCL 02	398 ASTO 05	443 FC?C 08
309 *	351 -	399 CLA	444 XEQ 09
310 ASIN	352 SIGN	400 ARCL 01	445 ADV
311 RCL 09	353 *	401 "+ * "	446 CLA
312 COS	354 RCL 10	402 ARCL 05	447 ARCL 18
313 RCL 10	355 RCL 07	403 XEQ 15	448 "+ TO "
314 *	356 RCL 03	404 CLA	449 ARCL 11
315 ASIN	357 -	405 RCL 01	450 AVIEW
316 RCL 06	358 X<0?	406 STO 05	451 FIX 0
317 +	359 SF 05	407 XEQ 09	452 "T/DIST "
318 STO 06	360 COS	408 100	453 ARCL 17
319 FS? 05	361 *	409 +	454 FS? 55
320 STO 02	362 RCL 09	410 RCL 08	455 "+ NM"
321 LASTX	363 +	411 +	456*LBL 15
322 +	364 ACOS	412 FIX 1	457 FC? 55
323 2	365 SIN	413 XEQ 10	458 GTO 00
324 /	366 STO 09	414 "+, "	459 ACA
325 COS	367 LASTX	415 ARCL 10	460 PRBUF
326 /	368 60	416 "+ NM"	461 RTN
327 ST- 07	369 *	417 GTO 15	462 GTO 01
328 RCL 07	370 STO 16	418*LBL 10	463*LBL 00
329 FS? 05	371 RDN	419 RND	464 TONE 8
330 STO 03	372 /	420 360	465 AVIEW
331 SF 08	373 ASIN	421 MOD	466 END
332 RTN	374 FS? 05	422 X#0?	
	375 CHS	423 GTO 00	
	376 90	424 LASTX	
	377 +	425 +	
	378 100		
	379 FS?C 05		
	380 CLX		
	381 +		
	382 RTN		



RNAV

(USES Extended Memory)



LBL'DAL  
LBL'ADS  
LBL'BUJ  
LBL'PRX  
LBL'SLR  
LBL'UIM  
END 155 BYTES

01\*LBL "DAL"  
02 32.5051  
03 96.5142  
04 -8  
05 RTN  
06\*LBL "ADS"  
07 32.5806  
08 96.501  
09 -8  
10 RTN  
11\*LBL "BUJ"  
12 33.1659  
13 96.2153  
14 -8  
15 RTN  
16\*LBL "PRX"  
17 33.3232  
18 95.2653  
19 -8  
20 RTN

21\*LBL "SLR"  
22 33.1155  
23 95.3233  
24 -8  
25 RTN  
26\*LBL "UIM"  
27 32.5249  
28 95.22  
29 -8  
30 END

LBL'OKC  
LBL'ADM  
LBL'TUL  
LBL'KOKC  
END 107 BYTES

01\*LBL "OKC"  
02 35.2633  
03 97.4621  
04 -9  
05 RTN  
06\*LBL "ADM"  
07 34.1241  
08 97.1005  
09 -9  
10 RTN  
11\*LBL "TUL"  
12 36.1146  
13 95.4716  
14 -8  
15 RTN  
16\*LBL "KOKC"  
17 35.2335  
18 97.3602  
19 -9  
20 END

LBL'CP5  
LBL'FAM  
LBL'STL  
LBL'TOY  
END 112 BYTES

01\*LBL "CP5"  
02 38.3418  
03 90.0934  
04 -3  
05 RTN  
06\*LBL "FAM"  
07 37.4024  
08 90.1402  
09 -5  
10 RTN  
11\*LBL "STL"  
12 38.5138  
13 90.2856  
14 -5  
15 RTN  
16\*LBL "TOY"  
17 38.4421  
18 89.5507  
19 -4  
20 END

LBL'BHM  
LBL'VUZ  
LBL'HAB  
END 79 BYTES

01\*LBL "BHM"  
02 33.335  
03 86.4516  
04 -2  
05 RTN  
06\*LBL "VUZ"  
07 33.4012  
08 86.5359  
09 -2  
10 RTN  
11\*LBL "HAB"  
12 34.1142  
13 88.0045  
14 -2  
15 END

LBL'BNA  
LBL'GHM  
END 52 BYTES

01\*LBL "BNA"  
02 36.071  
03 86.4057  
04 -2  
05 RTN  
06\*LBL "GHM"  
07 35.5002  
08 87.2706  
09 3  
10 END

LBL'AEX  
LBL'ESF  
LBL'MLU  
LBL'SHV  
END 103 BYTES

01\*LBL "AEX"  
02 31.1523  
03 92.3002  
04 -7  
05 RTN  
06\*LBL "ESF"  
07 31.234  
08 92.1744  
09 -7  
10 RTN  
11\*LBL "MLU"  
12 32.31  
13 92.0209  
14 -6  
15 RTN  
16\*LBL "SHV"  
17 32.4616  
18 93.4835  
19 -7  
20 END

LBL'GLH  
LBL'GRW  
LBL'JAN  
LBL'KJAN  
END 106 BYTES

01\*LBL "GLH"  
02 33.3124  
03 90.5858  
04 -4  
05 RTN  
06\*LBL "GRW"  
07 33.2749  
08 90.1638  
09 -3  
10 RTN  
11\*LBL "JAN"  
12 32.3026  
13 90.1003  
14 -5  
15 RTN  
16\*LBL "KJAN"  
17 32.184  
18 90.0433  
19 -5  
20 END

1. JBR  
LAT: 35.4952  
LNG: 90.3847  
VAR: -4  
2. AGO  
LAT: 33.1400  
LNG: 93.1300  
VAR: -6  
3. ARG  
LAT: 36.0636  
LNG: 90.5713  
VAR: -4  
4. BVX  
LAT: 35.4328  
LNG: 91.3904  
VAR: -4  
5. CNG  
LAT: 37.0031  
LNG: 88.5013  
VAR: -3  
6. CGI  
LAT: 37.1339  
LNG: 89.3420  
VAR: -3  
7. DGD  
LAT: 37.0124  
LNG: 92.5236  
VAR: -6  
8. ELD  
LAT: 33.1522  
LNG: 92.4438  
VAR: -7  
9. FSM  
LAT: 35.2318  
LNG: 94.1617  
VAR: -6  
10. FSM:  
LAT: 35.2010  
LNG: 94.2203  
VAR: -6  
11. FYV  
LAT: 36.0018  
LNG: 94.1012  
VAR: -7  
12. F43  
LAT: 33.1100  
LNG: 92.4000  
VAR: -5  
13. GQE  
LAT: 35.2049  
LNG: 90.2841  
VAR: -4  
14. HOT  
LAT: 34.2843  
LNG: 93.0526  
VAR: -6

15. HRO  
LAT: 36.1906  
LNG: 93.1247  
VAR: -6  
16. HRO:  
LAT: 36.1541  
LNG: 93.0916  
VAR: -6  
17. H37  
LAT: 36.1025  
LNG: 94.0715  
VAR: -7  
18. JBR:  
LAT: 35.5229  
LNG: 90.3518  
VAR: -4  
19. JKS  
LAT: 35.3556  
LNG: 88.2132  
VAR: -2  
20. LIT  
LAT: 34.4039  
LNG: 92.1049  
VAR: -5  
21. LIT:  
LAT: 34.4349  
LNG: 92.1359  
VAR: -5  
22. MAW  
LAT: 36.3318  
LNG: 89.5441  
VAR: -3  
23. MEM  
LAT: 35.0345  
LNG: 89.5853  
VAR: -3  
24. MKL  
LAT: 35.3613  
LNG: 88.5437  
VAR: -2  
25. MKO  
LAT: 35.3930  
LNG: 95.2145  
VAR: -7  
26. MON  
LAT: 33.3343  
LNG: 91.4256  
VAR: -4  
27. M03  
LAT: 35.0442  
LNG: 92.2535  
VAR: -6  
28. M07  
LAT: 35.1245  
LNG: 91.4412  
VAR: -5

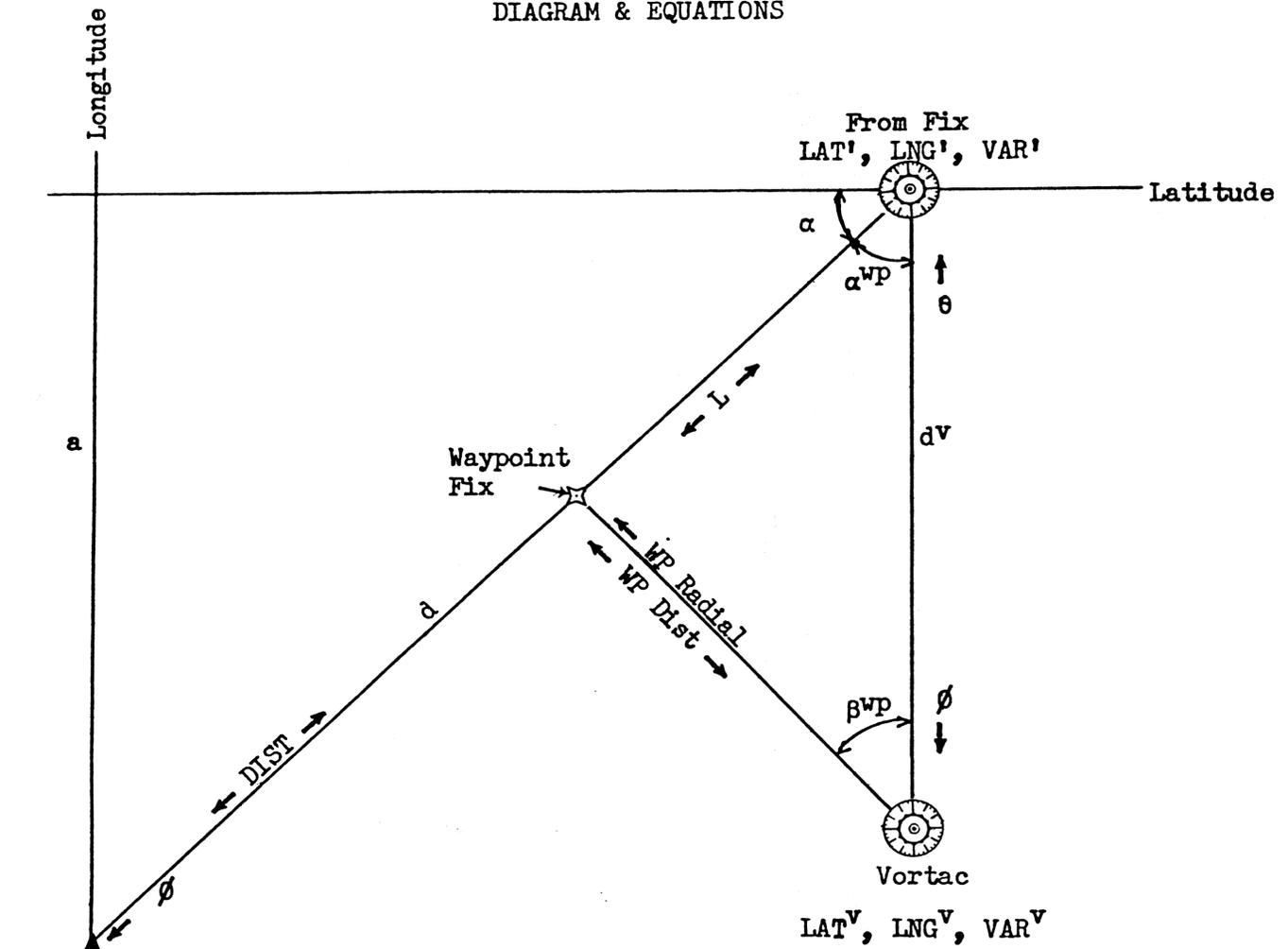
29. PAH  
LAT: 37.0339  
LNG: 88.4625  
VAR: -3  
30. PBF  
LAT: 34.1448  
LNG: 91.5534  
VAR: -4  
31. PBF:  
LAT: 34.1028  
LNG: 91.5608  
VAR: -4  
32. PGO  
LAT: 34.4049  
LNG: 94.3632  
VAR: -7  
33. ROG  
LAT: 36.2210  
LNG: 94.0630  
VAR: -7  
34. RSN  
LAT: 32.3045  
LNG: 92.3745  
VAR: -6  
35. RZC  
LAT: 36.1447  
LNG: 94.0716  
VAR: -7  
36. SGF  
LAT: 37.2121  
LNG: 93.2002  
VAR: -7  
37. TXK  
LAT: 33.3050  
LNG: 94.0423  
VAR: -7  
38. TXK:  
LAT: 33.2713  
LNG: 93.5927  
VAR: -7  
39. 2M9  
LAT: 36.2200  
LNG: 92.2800  
VAR: -6  
40. 3R8  
LAT: 31.4415  
LNG: 93.0545  
VAR: -7

DATA REG=160  
CHAR=908  
EM REG=130

RNAV P124  
F R130

EMDIR

DIAGRAM & EQUATIONS



To Fix  
LAT, LNG, VAR

$$\text{WP Radial} = \theta^V \pm \beta^{\text{WP}} + \text{VAR}^V$$

$$\text{WP Dist} = 60 \sin^{-1} (\sin |\alpha^{\text{WP}}| \sin d^V)$$

$$\text{LAT} = \text{LAT}' + \sin^{-1} [(\sin d)(\cos \phi)]$$

$$\text{LNG} = \text{LNG}' - \sin^{-1} \frac{(\sin d)(\sin \phi)}{\cos [(\text{LAT} + \text{LAT}')/2]}$$

$$\text{DIST} = 60d$$

$$d = \cos^{-1} [\sin \text{LAT} \sin \text{LAT}' + \cos \text{LAT} \cos \text{LAT}' \cos (\text{LNG} - \text{LNG}')] ]$$

$$\alpha = \sin^{-1} \left( \frac{\sin a}{\sin d} \right)$$

$$\phi = \text{TC} = 270^\circ + \alpha \text{ or } 90^\circ - \alpha$$

$$a = \cos^{-1} (\sin \text{LAT} \sin \text{LAT}' + \cos \text{LAT} \cos \text{LAT}')$$

01*LBL "RNAV"		62 100	
02 19		63 +	$\theta^v$
03 PSIZE		64 90	
04*LBL 01		65 RCL 00	$\phi$
05 32		66 RCL 10	
06 X<>F		67 -	$\alpha^{WP}$
07 SF 21		68 1	
08 SF 23		69 P-R	
09 CF 29		70 R-P	$-180 \leq \alpha^{WP} \leq 180$
10 0		71 RDN	
11 STO 17		72 X<0?	
12 "F"		73 SF 05	
13 SEEKPTA		74 ABS	$ \alpha^{WP} $
14 "FROM?"	Departure point	75 STO 10	
15 XEQ 04	Coordinates	76 -	$\beta^{WP}$
16 CF 05		77 X<=0?	WP behind starting fix?
17 RCL 05		78 GTO 21	
18 STO 18	Departure ident.	79 STO 07	
19 FC?C 08	If fix isn't a WP	80 FC?C 05	
20 XEQ 09	Prompt for a terminal WP	81 CHS	
21*LBL 20	PRIMARY LEGS	82 +	
22 CLA		83 RCL 00	$Var^v$
23 ARCL 05		84 +	Waypoint radial
24 ASTO 01		85 X<> 07	$\beta^{WP}$
25 "+ TO?"		86 SIN	
26 CF 23		87 RCL 09	$Sin d^v$
27 XEQ 04	Coordinates	88 *	
28 FC? 23	Input declined?	89 ASIN	
29 GTO 22		90 60	
30 ADV		91 *	
31 XEQ 08	True course & distance	92 FIX 0	
32 STO 00	$\phi$	93 RND	L
33 RCL 10	Distance	94 RCL 15	<i>(Handwritten: PLS-FIN)</i>
34 FIX 0		95 X<=Y?	WP behind starting fix?
35 RND		96 GTO 21	
36 ST+ 17	Total distance sum	97 X<>Y	
37 STO 15	Leg distance	98 RCL 16	
38 RCL 05		99 X>Y?	WP behind last WP?
39 STO 11		100 GTO 21	
40 RCL 06	Save ending coordinates	101 RDN	
41 STO 12		102 ENTER↑	L
42 RCL 07		103 X<> 16	Last L
43 STO 13		104 XEQ 03	Output leg data
44 RCL 08		105 ADV	
45 STO 14		106 FIX 1	
46 0		107 CLA	
47 STO 16		108 ARCL 05	
48 SF 06	Computing waypoints	109 XEQ 15	Output WP ident.
49*LBL 21	SECONDARY LEGS	110 CLA	
50 CLA		111 RCL 07	
51 ARCL 01		112 XEQ 10	Azimuth format
52 "+ TO WP?"		113 "+, "	
53 CF 23		114 RCL 10	$ \alpha^{WP} $
54 XEQ 04	Coordinates	115 SIN	
55 FC? 23	Waypoint declined?	116 RCL 09	$Sin d^v$
56 GTO 02		117 *	
57 "WP:"		118 ASIN	
58 ARCL 05		119 60	
59 ASTO 05		120 *	WP radial
60 XEQ 08	$\phi^v$	121 ARCL X	
61 STO 10		122 "+ NM"	

123 XEQ 15	Output WP data	184 "F NM"	
124 RCL 08		185 GTO 15	Output leg distance
125 STO 04	Var update	186*LBL 04	COORDINATE INPUT
126 ADV		187 8	
127 RCL 05		188 FS? 05	Departure point?
128 STO 01		189 4	
129 GTO 21		190*LBL 05	
130*LBL 02		191 STO 09	
131 CF 06		192*LBL 06	
132 RCL 11		193 AON	
133 STO 05		194 TONE 8	
134 RCL 14		195 PROMPT	
135 STO 08	Var update	196 AOFF	
136 RCL 15		197 FC? 23	Input declined?
137 RCL 16		198 RTN	
138 XEQ 03	Output leg data	199 FC? 06	
139 RCL 12		200 CF 08	
140 STO 02		201 ASTO 05	
141 RCL 13		202 3	If identifier is
142 STO 03	Update starting	203 ALENG	three or four letters
143 RCL 08	coordinates.	204 X=Y?	than search "F" file,
144 STO 04		205 GTO 01	and prgm memory.
145 GTO 20		206 4	
146*LBL 03	LEG OUTPUT	207 X*Y?	
147 FIX 0		208 GTO 00	
148 -		209*LBL 01	
149 CLA		210 SF 25	
150 ARCL 01		211 XEQ IND 05	Search prgm memory for
151 FC? 55		212 FS?C 25	fix program
152 GTO 00		213 GTO 07	
153 ACA		214 0	
154 CLA		215 SEEKPT	
155 SF 13		216 POSFL	Search "F" file
156 " TO "	Identifiers	217 X<0?	Ident. found?
157 ACA		218 GTO 01	
158 CF 13		219 GETREC	
159 CLA		220 GETREC	
160*LBL 00		221 ANUM	
161 FC? 55		222 GETREC	
162 "F"		223 ANUM	
163 ARCL 05		224 GETREC	
164 XEQ 15	Output	225 ANUM	
165 "MC="		226*LBL 07	Store fix coordinates
166 RCL 00	∅	227 STO IND 09	
167 RCL 04	Var'	228 DSE 09	
168 +	MC'	229 RDN	
169 STO 06		230 HR	
170 XEQ 10	Azimuth format	231 STO IND 09	
171 RDN		232 DSE 09	
172 CLX		233 RDN	
173 RCL 06	MC'	234 HR	
174 RCL 00	∅	235 STO IND 09	
175 RCL 08	Var	236 RTN	
176 +	MC	237*LBL 01	Prompt for coordinates
177 X*Y?		238 CF 22	
178 "F"		239 "F LAT?"	
179 X*Y?	Var changed?	240 TONE 8	
180 XEQ 10	Azimuth format	241 PROMPT	
181 XEQ 15	Output MC	242 CLA	
182 "DIST="		243 ARCL 05	
183 ARCL T	Leg distance	244 FC?C 22	

245 GTO 00		306 FIX 1	
246 "+ LNG?"		307 XEQ 10	Output intersection data
247 TONE 8		308 RDN	
248 PROMPT		309*LBL 00	
249 CLA		310 ", "	
250 ARCL 05		311 ARCL Y	
251 FC?C 22		312 "+ NM"	
252 GTO 00		313 FS? 55	
253 "+ VAR?"		314 XEQ 15	
254 TONE 8		315 RCL 08	
255 PROMPT		316 FS? 05	
256 FS? 22		317 STO 04	
257 GTO 07		318 -	
258*LBL 00	INTERSECTION	319 STO 09	
259 FC? 06	WP or Reference fix?	320 RDN	
260 FS? 07		321 60	
261 GTO 06		322 /	d
262 RCL 02		323 SIN	Sin d
263 STO 06	Prior fix coordinates	324 STO 10	
264 RCL 03	to be used for the	325 RCL 09	∅
265 STO 07	reference fix.	326 SIN	
266 RCL 04		327 *	
267 STO 08		328 ASIN	
268 RCL 05		329 RCL 09	
269 STO 11		330 COS	
270 SF 07	Reference fix flag	331 RCL 10	
271 CF 23		332 *	
272 8		333 ASIN	
273 "NEED FIX?"		334 RCL 06	Lat'
274 XEQ 05		335 +	
275 CF 07		336 STO 06	Lat
276 RCL 01		337 FS? 05	Departure fix?
277 FS? 23	Reference fix used?	338 STO 02	
278 RCL 05		339 LASTX	
279 STO 10		340 +	
280 RCL 11		341 2	
281 STO 05		342 /	
282 CF 22		343 COS	
283 "RADIAL?"	Prompt for $\phi_{mc}$	344 /	
284 TONE 8		345 ST- 07	
285 PROMPT		346 RCL 07	Lng
286 CLA		347 FS? 05	
287 ARCL 05		348 STO 03	
288 SF 23		349 SF 08	
289 FC?C 22		350 RTN	
290 GTO 04		351*LBL 08	TC & DISTANCE
291 "DME?"	Prompt for distance	352 RCL 06	
292 TONE 8		353 SIN	
293 PROMPT		354 RCL 02	
294 CLA		355 SIN	
295 ARCL 05		356 *	Sin Lat Sin Lat'
296 FC? 22		357 STO 09	
297 GTO 04		358 RCL 06	
298 X<>Y		359 COS	
299 FC? 55		360 RCL 02	
300 GTO 00		361 COS	
301 ADV		362 *	
302 "+ * WP: "		363 STO 10	Cos Lat Cos Lat'
303 ARCL 10		364 +	
304 PRA	Output Idents.	365 ACOS	
305 CLA		366 SIN	Sin a

LBL'RNAV  
END

867 BYTES

367 RCL 06		428 RCL 08	Var <sup>v</sup>
368 RCL 02		429 +	
369 -	+ Northerly	430 FIX 1	
370 SIGN	- Southerly	431 XEQ 10	Format azimuth
371 *		432 "I, "	
372 RCL 10		433 ARCL 10	d <sup>v</sup>
373 RCL 07		434 "I NM"	
374 RCL 03		435 GTO 15	
375 -		436+LBL 10	DEGREE FORMAT
376 X<0?		437 RND	
377 SF 05	Easterly	438 360	
378 COS		439 MOD	
379 *		440 X#0?	
380 RCL 09		441 GTO 00	
381 +		442 LASTX	
382 ACOS	d	443 +	
383 SIN		444+LBL 00	
384 STO 09	Sin d	445 100	
385 LASTX		446 X>Y?	
386 60		447 "I0"	
387 *		448 SQRT	
388 STO 10	Distance	449 X>Y?	
389 RDN		450 "I0"	
390 /		451 ARCL Y	
391 ASIN	$\alpha$	452 FC? 55	
392 FS? 05		453 RTN	
393 CHS		454 ACA	
394 90		455 "a"D"	Degree Character =
395 +		456 ASTO X	\$ F4 61 22 44 86
396 180		457 ACSPEC	
397 FS?C 05		458 CLA	
398 CLX		459 RTN	
399 +	$\emptyset$	460+LBL 22	DESTINATION
400 RTN		461 FC?C 00	Fix a WP?
401+LBL 09	TERMINAL WAYPOINT	462 XEQ 09	Prompt for terminal WP
402 RCL 05		463 ADV	
403 STO 01		464 CLA	
404 CLA		465 ARCL 18	
405 ARCL 05		466 "I TO "	Terminal identifiers
406 "I WP?"	Prompt for WP	467 ARCL 11	
407 SF 06		468 AVIEW	
408 CF 23		469 FIX 0	
409 XEQ 04		470 "I/DIST	
410 CF 06		471 ARCL 17	Total trip distance
411 FC? 23	WP declined?	472 FS? 55	
412 RTN		473 "I NM"	
413 ADV		474+LBL 15	Output
414 "WP:"		475 FC? 55	
415 ARCL 05		476 GTO 00	
416 ASTO 05		477 ACA	
417 CLA		478 PRBUF	
418 ARCL 01		479 RTN	
419 "I * "		480 GTO 01	
420 ARCL 05		481+LBL 00	
421 XEQ 15	Output ident	482 TONE 8	
422 CLA		483 AVIEW	
423 RCL 01		484 END	
424 STO 05			
425 XEQ 08	$\emptyset^v$		
426 180			
427 +	$\emptyset^v$		

**DATA REGISTERS**

00	True course		
01	Ident'		
02	Lat'		
03	Lng'		
04	Var'		
05	Ident		
06	Lat		
07	Lng		
08	Var		
09	scratch		
10	scratch		
11	Ident <sup>s</sup>		
12	Lat <sup>s</sup>		
13	Lng <sup>s</sup>		
14	Var <sup>s</sup>		
15	Leg distance		
16	WP distance		
17	Total distance		
18	Departure ident		

**STATUS**

SIZE 19 TOT. REG. 133 USER MODE  
 ENG \_\_\_\_\_ FIX \_\_\_\_\_ SCI \_\_\_\_\_ ON X OFF \_\_\_\_\_  
 DEG X RAD \_\_\_\_\_ GRAD \_\_\_\_\_

**FLAGS**

#	INIT S/C	SET INDICATES	CLEAR INDICATES
05	S	Departure fix	
		Easterly course	Westerly course
		$\alpha^{WP} < 0$	$\alpha^{WP} < 0$
06	C	Computing a WP	
07	C	Reference fix	
08	C	Terminal fix is a WP	

**ASSIGNMENTS**

FUNCTION	KEY	FUNCTION	KEY
XEQ "NAV"	25 (TAN)		

LBL'RNAV  
 END 867 BYTES

by Robert A. TIMS

Sample Problem

PBF: \* WP:PBF  
 182.2°, 4.4 NM

HILLE \* WP:PBF  
 034.0°, 66.0 NM

PBF: to WP:LIT  
 MC=032°/031°  
 DIST=17 NM

WP:LIT  
 121.1°, 27.6 NM

WP:LIT to HILLE  
 MC=031°/032°  
 DIST=53 NM

HILLE to JBR  
 MC=023°  
 DIST=48 NM

JBR \* WP:ARG  
 134.3°, 22.4 NM

PBF: TO JBR  
 T/DIST 118 NM







LBL \*TAS  
 END 177 BYTES

This program converts calibrated airspeed (CAS) to mach number (M) and true airspeed (TAS). Inputs required are pressure altitude (PALT), aircraft recovery coefficient (C<sub>T</sub>) and indicated air temperature (IAT). Values for recovery coefficient vary from 0.6 to 1.0, but 0.8 is a good value for most aircraft

The formulas used are less accurate for mach numbers above 1.0 (i.e., supersonic flight).

$$\text{Pressure ratio} \left( \frac{P}{P_0} \right) = \left[ \frac{518.67 - 3.566 \times 10^{-3} \text{ PALT}}{518.67} \right]^{5.2563}$$

$$M^2 = 5 \left[ \left( \frac{P_0}{P} \left\{ \left[ 1 + 0.2 \left( \frac{\text{CAS}}{661.5} \right)^2 \right]^{3.5} - 1 \right\} + 1 \right)^{0.2857} - 1 \right]$$

$$\text{TAS} = 38.96M \sqrt{(IAT + 273) \left[ C_T \left( \frac{1}{(1 + 0.2 M^2)} - 1 \right) + 1 \right]}$$

				SIZE: 008
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	To compute mach number and true airspeed		<input type="checkbox"/> XEQ TAS	PALT= (ALT)?
2	Input pressure altitude.	PALT, ft.	<input type="checkbox"/> R/S	CAS= (CAS)?
3	Input calibrated airspeed.	CAS, kt.	<input type="checkbox"/> R/S	CT= (CT)?
4	Input aircraft recovery coefficient.	C <sub>T</sub>	<input type="checkbox"/> R/S	IAT= (IAT)?
5	Input indicated air temperature.	IAT, °C	<input type="checkbox"/> R/S	MACH M TAS= (TAS)

01 LBL "TAS"	49 1
02 SF 21	50 -
03 FIX 0	51 RCL 05
04 RCL 01	52 /
05 "PALT="	53 1
06 ARCL X	54 +
07 "t?"	55 3.5
08 PROMPT	56 1/X
09 STO 01	57 Y↑X
10 RCL 02	58 1
11 "CAS="	59 -
12 ARCL X	60 5
13 "t?"	61 *
14 PROMPT	62 SQRT
15 STO 02	63 STO 06
16 RCL 03	64 FIX 2
17 "IAT="	65 "MACH "
18 ARCL X	66 ARCL X
19 "t?"	67 AVIEW
20 PROMPT	68 RCL 06
21 STO 03	69 X↑2
22 FIX 1	70 5
23 RCL 04	71 /
24 "CT="	72 1
25 ARCL X	73 +
26 "t?"	74 1/X
27 PROMPT	75 1
28 STO 04	76 -
29 RCL 01	77 RCL 04
30 -3566 E-6	78 *
31 *	79 1
32 518.67	80 +
33 +	81 273
34 LASTX	82 RCL 03
35 /	83 +
36 5.2563	84 *
37 Y↑X	85 SQRT
38 STO 05	86 RCL 06
39 RCL 02	87 *
40 661.5	88 38.96
41 /	89 *
42 X↑2	90 FIX 0
43 5	91 "TAS="
44 /	92 ARCL X
45 1	93 AVIEW
46 +	94 END
47 3.5	
48 Y↑X	



WEIGHT + BALANCE

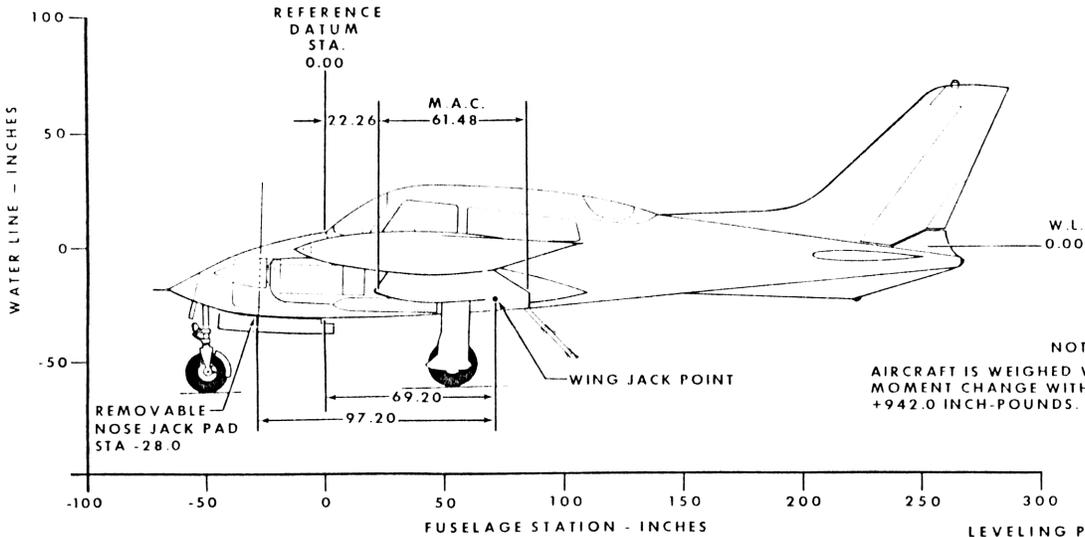


# WEIGHT & BALANCE DATA

# 310Q

SERIAL NO. 31000601 AND ON

SERIAL NUMBER 310Q0726 REGISTRATION NUMBER N4155Q DATE 4-4-73



NOTE  
AIRCRAFT IS WEIGHED WITH GEAR EXTENDED.  
MOMENT CHANGE WITH GEAR RETRACTED IS  
+942.0 INCH-POUNDS.

LEVELING PROVISIONS  
LONGITUDINAL - LEFT SIDE OF  
FUSELAGE @ STA 59.10 & 88.90  
LATERAL - BOTTOM OF FUSELAGE  
@ STA 37.5

computed

### AIRCRAFT AS WEIGHED

POSITION	SCALE READING	SCALE DRIFT	TARE	NET WEIGHT
LEFT WING				
RIGHT WING				
NOSE				
AIRCRAFT TOTAL AS WEIGHED				
NOSE NET WEIGHT →				
$\text{CG ARM OF AIRCRAFT AS WEIGHED} = (69.2) - \frac{(97.2) \times (\text{Net Weight})}{\text{Total As Weighed}} = (\text{CG}) \text{ INCHES AFT OF DATUM}$				

NOTE

It is the responsibility of the pilot to insure that the aircraft is loaded properly. The licensed empty weight, CG and useful load for this aircraft as delivered from the factory is shown below. If the aircraft has been altered, refer to the latest weight and balance data for this information.

### USEFUL LOAD

LICENSED GROSS WEIGHT	5300 LBS
LICENSED EMPTY WEIGHT	3552
USEFUL LOAD	1748

### LICENSED EMPTY WEIGHT AND C G

ITEM	WEIGHT (LBS)	CG ARM (IN)	MOMENT (IN-LBS)	
AIRCRAFT (CALCULATED)	3485	38.4	133,855.	
UNDRAINABLE FLUIDS	18.0	13.9	250	
DRAINABLE UNUSABLE FUEL @ 6 LBS PER GALLON	TIP MAIN	12.0	528	
	WING AUXILIARY	6.0	282	
	WING LOCKER LEFT	<del>12.0</del>	<del>44.0</del>	<del>528</del>
	WING LOCKER RIGHT	<del>12.0</del>	<del>44.0</del>	<del>528</del>
PAINT	31.0	43.2	1323	
OPTIONAL EQUIPMENT				
LICENSED EMPTY WEIGHT	3552	38.4	136,238.	

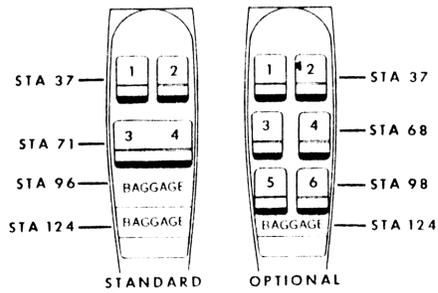
*Amended - 5-25-73*

*3610*

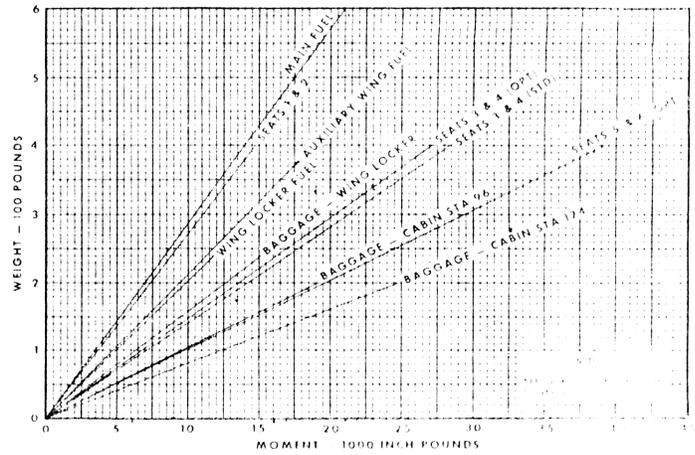
*38.08*



**PASSENGER SEAT AND BAGGAGE BAY  
MOMENT ARMS**



**LOADING MOMENTS CHART**



The following information is provided to enable a check of the aircraft load to determine if it falls within the approved center of gravity limits.

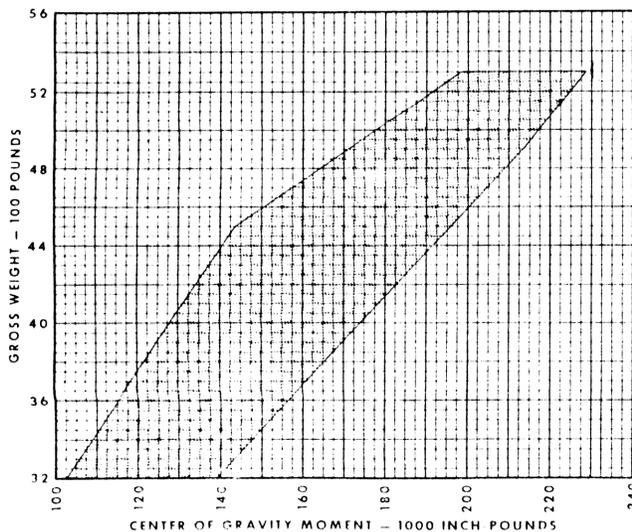
- 1) Determine weights, then obtain moments of useful load items from Loading Moments Chart, or multiply weight times CG arm.
- 2) Enter these weights and moments in the Loading Manifest Chart and total.
- 3) Enter the Center of Gravity Moment - Inch Pounds chart with the takeoff weight and center of gravity moment in inch pounds. If the intersection of these points falls within the envelope, the load is approved.

- 4) If desired, the Center of Gravity Moment Envelope - Inches chart may be used to determine whether the load is approved. CG arm is equal to the total moment divided by the total weight. Enter the chart with the takeoff weight and CG arm. If the intersection of these points fall within the envelope, the load is approved.

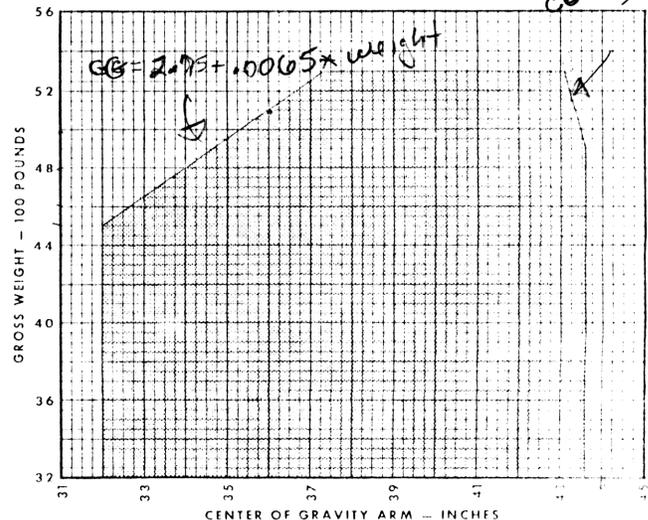
**LOADING MANIFEST CHART**

ITEM		WEIGHT (LBS)	CG ARM (IN)	MOMENT (1000 IN LBS)
LICENSED EMPTY WEIGHT		3552	38.4	136.2
ALLOWABLE USEFUL LOAD 1748 LBS.	PILOT & PASSENGER SEATS 1 & 2	340	37	12.6
	PASSENGER SEATS 3 & 4	340	68	23.1
	PASSENGER SEATS 5 & 6	280	98	27.4
	BAGGAGE - CABIN STA 96		96	
	- CABIN STA 124		124	
	- WING LOCKER	23	63	1.4
	OIL (24 QT INCLUDING UNUSABLE)	45	-3.5	-0.2
	FUEL - TIP MAIN	600	35	21.0
- WING AUXILIARY	120	47	5.6	
- WING LOCKER		49		
TAKEOFF GROSS WEIGHT		5300	42.8	227.1
SUBTRACT ALL FUEL INCLUDED ABOVE	FUEL - TIP MAIN	600	35	21.0
	- WING AUXILIARY	120	47	5.6
	- WING LOCKER		49	
ADD MINIMUM FUEL - TIP MAIN		133	35	4.7
ESTIMATED LANDING WEIGHT		4713	43.5	205.2

**CG MOMENT ENVELOPE—INCH POUNDS**



**CG MOMENT ENVELOPE—INCHES**





LBL'WB  
END

401 BYTES

C310 N41550

PILOTS= 200  
ROW 2= 300  
ROW 3= 0  
AFT BAG= 50  
WING BAG= 100  
MAIN FUEL= 100  
AUX FUEL= 0  
T/FUEL= 100  
CG LIMITS: 34.63 43.48  
CG= 40.49  
GW= 4905 LBS

01\*LBL "WB"  
02 12  
03 PSIZE  
04 CLRG  
05 ADV  
06 FIX 0  
07 "C310 N41550"  
08 SF 12  
09 AVIEW  
10 CF 12  
11 SF 21  
12 SF 22  
13 CF 29  
14 ADV  
15 37  
16 STO 00  
17 68  
18 STO 01  
19 98  
20 STO 02  
21 124  
22 STO 03  
23 63  
24 STO 04  
25 35  
26 STO 05  
27 47  
28 STO 06  
29 CLX  
30 "PILOTS"  
31 XEQ 06  
32 "ROW 2"  
33 XEQ 06  
34 "ROW 3"  
35 CF 22  
36 XEQ 06  
37 "AFT BAG"  
38 XEQ 06  
39 "WING BAG"  
40 XEQ 06

ARM moments

PILOTS

ROW 2

ROW 3

BAGGAGE

WING LOCKERS

TIP TANKS

AUX TANKS

41 163  
42 1645  
43 RCL 08  
44 -  
45 6  
46 /  
47 "FUEL<= "  
48 ARCL X  
49 X<Y?  
50 AVIEW  
51 CLX  
52 "MAIN FUEL"  
53 XEQ 05  
54 "AUX FUEL"  
55 XEQ 05  
56 "T/FUEL= "  
57 ARCL 10  
58 AVIEW  
59 3655  
60 ST+ 08  
61 37.56  
62 \*  
63 RCL 09  
64 +  
65 RCL 08  
66 /  
67 STO 09  
68 4500  
69 RCL 08  
70 X<Y?  
71 GTO 01  
72 32  
73 GTO 02  
74\*LBL 01  
75 .0065  
76 \*  
77 2.75  
78 +  
79\*LBL 02  
80 STO 07  
81 4900  
82 RCL 08  
83 X<Y?  
84 GTO 03  
85 43.48  
86 GTO 04  
87\*LBL 03  
88 -.000775  
89 \*  
90 47.2775  
91 +  
92\*LBL 04  
93 FIX 2  
94 "CG LIMITS: "  
95 ARCL 07  
96 "+ "  
97 ARCL X  
98 FC? 55  
99 AVIEW  
100 FS? 55  
101 PRA  
102 RCL 09  
103 CLA  
104 X<Y?  
105 "AFT "  
106 RCL 07  
107 X<Y?  
108 "FWD "  
109 "FCG= "  
110 ARCL Y  
111 AVIEW  
112 GTO 10  
113\*LBL 05  
114 "+= "  
115 PROMPT  
116 ST+ 10  
117 ARCL X  
118 FS? 55  
119 PRA  
120 6  
121 \*  
122 GTO 07  
123\*LBL 06  
124 "+= "  
125 PROMPT  
126 ARCL X  
127 FS? 55  
128 PRA  
129\*LBL 07  
130 ST+ 08  
131\*LBL 08  
132 RCL IND 11  
133 X<Y?  
134 \*  
135 ST+ 09  
136 1  
137 ST+ 11  
138 CLX  
139 RTH  
140\*LBL 09  
141 -  
142 "OVER WT "  
143 ARCL X  
144 AVIEW  
145 RTH  
146\*LBL 10  
147 FIX 0  
148 "GW= "  
149 ARCL 08  
150 "+ LBS"  
151 AVIEW  
152 RCL 08  
153 5300  
154 X<Y?  
155 XEQ 09  
156 ADV  
157 ADV  
158 ADV  
159 ADV  
160 ADV  
161 END

Gross wt.

Empty. C.G.

TOTAL moments

C.G.

FWD C.G.

FWD C.G

AFT C.G.

FUEL Weight

ADD weight

TOTAL WT

MOMENTS



WIND CORRECTION



# W I N D   C O R R E C T I O N   H P - 4 1 C   P R O G R A M

Note: All velocities are absolute values.

## True Heading:

$$TH=TC+SIN^{-1}[Wv*SIN(Wd-TC)/TAS]$$

Wv=Wind Velocity  
Wd=Wind Direction

## Ground Speed:

$$GS=[(TAS*SIN(TH)-Wv*SIN(Wd))^2+(TAS*COS(TH)-Wv*COS(Wd))^2]^{1/2}$$

If  $COS(Wd-TH)$  is negative and  $TAS < Wv$  then the GS is negative.

## Wind Direction:

$$Wd=TAN^{-1}[(TAS*SIN(TH)-GS*SIN(TC))/(TAS*COS(TH)-GS*COS(TC))]$$

If  $TAS*COS(TH)-GS*COS(TC)$  is negative then add 180 to the Wd.

## Wind Velocity:

$$Wv=[(TAS*SIN(TH)-GS*SIN(TC))^2+(TAS*COS(TH)-GS*COS(TC))^2]^{1/2}$$

## Data Registers:

R00 - Time in HR format  
R01 - Wd  
R02 - Wv  
R03 - TC  
R04 - TAS  
R05 - TH  
R06 - GS  
R07 - Distance

LBL \*WCA  
END

591 BYTES

01\*LBL \*WCA\*  
02 8  
03 PSIZE  
04 FIX 0  
05 CF 29  
06 CLRG  
07\*LBL 16  
08 0  
09 X<>F  
10 CF 22  
11 \*GS/TH WIND"  
12 PROMPT  
13\*LBL A GS + TH  
14 ADV  
15 1  
16 \*WIND DIR=" Get  
17 XEQ 20 Wind  
18 2  
19 \*WIND VEL=" Get  
20 XEQ 23 TC + TAS  
21 XEQ 17  
22 RCL 01  
23 RCL 03  
24 -  
25 SIN  
26 RCL 02 WCA  
27 \*  
28 RCL 04  
29 /  
30 ASIN TC  
31 RCL 03  
32 +  
33 XEQ 21 DEGREE MOD  
34 STO 05 TH  
35 SIN  
36 RCL 04  
37 \*  
38 RCL 01  
39 SIN  
40 RCL 02  
41 \*  
42 -  
43 X↑2  
44 RCL 05 GS  
45 COS  
46 RCL 04  
47 \*  
48 RCL 01  
49 COS  
50 RCL 02  
51 \*  
52 -  
53 X↑2

54 +  
55 SQRT  
56 STO 06  
57 RCL 01  
58 RCL 05  
59 -  
60 COS  
61 X<0?  
62 GTO 01  
63 RCL 04  
64 RCL 02  
65 -  
66 SIGN  
67 ST\* 06  
68\*LBL 01  
69 ADV  
70 5  
71 \*TH=" OUTPUT  
72 SF 01 TH + GS  
73 FS? 55  
74 SF 02  
75 XEQ 20  
76 6  
77 \*GS=" Get DISTANCE  
78 SF 01  
79 FS? 55  
80 SF 02  
81 XEQ 23  
82 ADV  
83 XEQ 18  
84 RCL 07  
85 RCL 06  
86 /  
87 HMS  
88 \*TIME=" OUTPUT  
89 FS? 55 TIME enRoute  
90 GTO 02  
91 FIX 4  
92 ARCL X  
93 FIX 0  
94 PROMPT  
95 GTO C  
96\*LBL 02  
97 XEQ 19  
98\*LBL C  
99 ADV  
100 ADV  
101 ADV  
102 ADV  
103 ADV  
104 GTO 16  
105\*LBL E PAPER OUT  
106 ADV WIND

GS  
DIRECTION

OUTPUT  
TH + GS

Get DISTANCE

OUTPUT  
TIME enRoute

PAPER OUT

WIND

107 \*TIME=" Input Time  
108 PROMPT enRoute  
109 FC?C 22 - IF input  
110 GTO 03 declared  
111 HR goto  
112 STO 00 GS INPUT  
113 LASTX  
114 FS? 55 Print Time  
115 XEQ 19 Get Distance  
116 XEQ 18  
117 RCL 07  
118 RCL 00  
119 / G.S.  
120 STO 06  
121 ADV  
122 FS? 55  
123 SF 02  
124\*LBL 03 Get or Output  
125 6 GS  
126 \*GS=" GS  
127 XEQ 23  
128 5 Get  
129 \*TH=" TH  
130 XEQ 20  
131 XEQ 17 Get TC + TAS  
132 180 - used if direction  
133 RCL 05 is southern  
134 SIN  
135 RCL 04  
136 \*  
137 RCL 03  
138 SIN  
139 RCL 06  
140 \*  
141 -  
142 RCL 05  
143 COS  
144 RCL 04  
145 \*  
146 RCL 03  
147 COS  
148 RCL 06  
149 \*  
150 -  
151 X<0? Test for  
152 SF 01 Direction  
153 /  
154 ATAN  
155 FS?C 01  
156 +  
157 XEQ 21 DEGREE MOD  
158 STO 01  
159 RCL 05 7

Get or Output  
GS

Get  
TH

Get TC + TAS  
used if direction  
is southern

Wind  
Direction

Test for  
Direction

DEGREE MOD

160 SIN  
161 RCL 04  
162 \*  
163 RCL 03  
164 SIN  
165 RCL 06  
166 \*  
167 -  
168 X↑2  
169 RCL 05  
170 COS  
171 RCL 04  
172 \*  
173 RCL 03  
174 COS  
175 RCL 06  
176 \*  
177 -  
178 X↑2  
179 +  
180 SORT  
181 STO 02  
182 ADV  
183 1  
184 "WIND DIR="  
185 SF 01  
186 FS? 55  
187 SF 02  
188 XEQ 20  
189 2  
190 "WIND VEL="  
191 SF 01  
192 FS? 55  
193 SF 02  
194 XEQ 23  
195 GTO C  
196+LBL 17  
197 3  
198 "TC="  
199 XEQ 20  
200 4  
201 "TAS="  
202 GTO 23  
203+LBL 18  
204 FIX 1  
205 RCL 07  
206 RND  
207 "DIST="  
208 FS? 55  
209 ACA  
210 ARCL X  
211 PROMPT  
212 FS?C 22

wind velocity

output wind

INPUT TC  
↓  
TAS  
INPUT DISTANCE

213 STO 07  
214 FIX 0  
215 FC? 55  
216 RTN  
217 FIX 1  
218 RND  
219 ACX  
220 FIX 0  
221 " NM"  
222 ACA  
223 PRBUF  
224 RTN  
225+LBL 19  
226 ACA  
227 INT  
228 ACX  
229 " H"  
230 114  
231 XTOA  
232 ACA  
233 LASTX  
234 FRC  
235 100  
236 \*  
237 INT  
238 ACX  
239 " M"  
240 105  
241 XTOA  
242 110  
243 XTOA  
244 ACA  
245 LASTX  
246 FRC  
247 100  
248 \*  
249 RND  
250 ACX  
251 " S"  
252 101  
253 XTOA  
254 99  
255 XTOA  
256 ACA  
257 PRBUF  
258 RTN  
259+LBL 20  
260 RCL IND X  
261 RND  
262 XEQ 22  
263 FS? 55  
264 ACA  
265 ARCL X

PRINT TIME

INPUT Degree or Direction

266 FC?C 02  
267 PROMPT  
268 XEQ 21  
269 FS?C 01  
270 GTO 04  
271 FS?C 22  
272 STO IND Z  
273+LBL 04  
274 FC? 55  
275 RTN  
276 RND  
277 XEQ 22  
278 ACX  
279 "a"0"  
280 ASTO X  
281 ACSPEC  
282 PRBUF  
283 RTN  
284+LBL 21  
285 360  
286 MOD  
287+LBL 22  
288 X>0?  
289 RTN  
290 360  
291 +  
292 RTN  
293+LBL 23  
294 RCL IND X  
295 RND  
296 FS? 55  
297 ACA  
298 ARCL X  
299 FC?C 02  
300 PROMPT  
301 FS?C 01  
302 GTO 05  
303 ABS  
304 FS?C 22  
305 STO IND Z  
306+LBL 05  
307 FC? 55  
308 RTN  
309 RND  
310 ACX  
311 CLA  
312 " K"  
313 116  
314 XTOA  
315 115  
316 XTOA  
317 ACA  
318 PRBUF  
319 END

Degree Mod

0° = 360°

INPUT speed



CAP GRID SEARCH



# CAP GRID SEARCH HP-41C PROGRAM

*SAMPLE PRINTOUT  
2 legs instead of 8*

## Data Registers:

R00 - True Course  
 R01 - Ident'  
 R02 - Lat'  
 R03 - Lng'  
 R04 - Var'  
 R05 - Ident  
 R06 - Lat  
 R07 - Lng  
 R08 - Var  
 R09 - Scratch  
 R10 - Scratch  
 R11 - Total Distance  
 R12 - Grid Leg 1b Lat/Lng  
 R13 - # of Legs  
 R14 - Exit Lat/Lng  
 R14 - Lat/Lng Increment  
 R15 - 1st Waypoint Ident  
 R16 - 2nd Waypoint Ident

## Flags:

F00 - Computing the Grid  
 F01 - East/West Search  
 F02 - Compute End of Leg, Point b  
 F03 - Compute Exit Waypoints  
 F04 - Initialize Grid Parameters  
 F05 - Base Fix  
 F05 - Easterly Course

Note: Lat & Lng are in degrees & tenths.  
 Fix coordinates are given in program form.  
 Grid parameters are given in program form.  
 (See example given on last page)

JBR  
 ARG: 134.3°, 22.4 NM

TC=244°  
 MC=248°  
 DIST=28.7 NM

FIX  
 ARG: 196.6°, 31.1 NM  
 GQE: 292.6°, 38.1 NM

TC=090°  
 MC=096°  
 DIST=8.7 NM

ENTRY  
 ARG: 180.5°, 29.2 NM  
 GQE: 299.2°, 30.5 NM

TC=090°  
 MC=096°  
 DIST=12.2 NM

LEG 1b  
 ARG: 157.2°, 30.7 NM  
 GQE: 317.5°, 21.3 NM

TC=180°  
 MC=176°  
 DIST=7.0 NM

LEG 2a  
 ARG: 160.7°, 37.4 NM  
 GQE: 302.1°, 16.4 NM

TC=270°  
 MC=266°  
 DIST=12.2 NM

EXIT  
 ARG: 179.6°, 36.2 NM  
 GQE: 286.8°, 27.3 NM

TC=042°  
 MC=038°  
 DIST=25.9 NM

JBR  
 GQE: 340.2°, 30.2 NM

T/DIST=94.7 NM

01\*LBL "GRID"  
02 17  
03 PSIZE  
04\*LBL 30  
05 32  
06 X<>F  
07 SF 21  
08 CF 22  
09 CF 23  
10 CF 29  
11 0  
12 STO 11  
13 "BASE?"  
14 XEQ 03  
15 FC?C 23  
16 GTO 30  
17\*LBL 01  
18 RCL 05  
19 STO 01  
20 ADV  
21 CLA  
22 ARCL 01  
23 FC? 55  
24 GTO 02  
25 SF 12  
26 PRA  
27 CF 12  
28\*LBL 02  
29 FS? 00  
30 GTO 15  
31 FS? 02  
32 GTO 16  
33 XEQ 09  
34 FS?C 23  
35 XEQ 09  
36\*LBL 20  
37 CLA  
38 ARCL 01  
39 "T/DIST?"  
40 XEQ 03  
41 FS?C 23  
42 GTO 21  
43 ADV  
44 "T/DIST="

SET FLOS  
CLEAR OTHERS

GET BASE

COMPUTE GRID  
LEG

EXIT  
WAYPOINTS

FIND  
WAYPOINTS

GET FIX

ENDING

PAPER OUT

61 RND  
62 ST+ 11  
63 STO 10  
64 FIX 0  
65 "TC=" *Print TC mc Dist leg*  
66 RCL 00  
67 XEQ 13  
68 XEQ 11  
69 "MC=" *Print TC mc Dist leg*  
70 RCL 00  
71 RCL 04  
72 +  
73 STO 09  
74 XEQ 13  
75 CLX  
76 RCL 09  
77 RCL 00  
78 RCL 08  
79 +  
80 X\*Y?  
81 "T/" *Print TC mc Dist leg*  
82 X\*Y?  
83 XEQ 13  
84 XEQ 11  
85 FIX 1  
86 "DIST=" *Print TC mc Dist leg*  
87 ARCL 10  
88 "T NM" *Print TC mc Dist leg*  
89 XEQ 11  
90 RCL 06  
91 STO 02  
92 RCL 07  
93 STO 03  
94 RCL 08  
95 STO 04  
96 GTO 01  
97\*LBL 03  
98 8  
99 FS?C 05  
100 4  
101 STO 09  
102\*LBL 04  
103 ADV  
104 TONE 8  
105 PROMPT  
106 AOFF  
107 FC? 23  
108 RTN  
109 ASTO 05  
110 SF 25  
111 XEQ IND 05  
112 FC?C 25  
113 GTO 07  
114\*LBL 05  
115 STO IND 09  
116 DSE 09  
117 RDN  
118 XEQ 06  
119 STO IND 09  
120 DSE 09

GET FIX  
COORDINATES

121 RDN  
122 XEQ 06  
123 STO IND 09  
124 RTN  
125\*LBL 06  
126 100  
127 \*  
128 HMS  
129 100  
130 /  
131 HR  
132 RTN  
133\*LBL 07  
134 "T LAT?"  
135 TONE 8  
136 PROMPT  
137 CLA  
138 ARCL 05  
139 FC?C 22  
140 GTO 04  
141 "T LNG?"  
142 TONE 8  
143 PROMPT  
144 CLA  
145 ARCL 05  
146 FC?C 22  
147 GTO 04  
148 "T VAR?"  
149 TONE 8  
150 PROMPT  
151 CLA  
152 ARCL 05  
153 FC?C 22  
154 GTO 04  
155 GTO 05  
156\*LBL 08  
157 RCL 06  
158 SIN  
159 RCL 02  
160 SIN  
161 \*  
162 STO 09  
163 RCL 06  
164 COS  
165 RCL 02  
166 COS  
167 \*  
168 STO 10  
169 +  
170 ACOS  
171 SIN  
172 RCL 06  
173 RCL 02  
174 -  
175 SIGN  
176 \*  
177 RCL 10  
178 RCL 07  
179 RCL 03  
180 -

CALCULATE

TC

+

LEG DISTANCE

181 X<0?  
182 SF 05  
183 COS  
184 \*  
185 RCL 09  
186 +  
187 ACOS  
188 SIN  
189 STO 09  
190 LASTX  
191 60  
192 \*  
193 STO 10  
194 RDN  
195 /  
196 ASIN  
197 FS? 05  
198 CHS  
199 90  
200 +  
201 180  
202 FS?C 05  
203 CLX  
204 +  
205 RTN  
206\*LBL 09  
207 CLA  
208 ARCL 01  
209 "+ WP?"  
210 XEQ 03  
211 FC? 23  
212 RTN  
213\*LBL 10  
214 CLA  
215 FS? 55  
216 " " "  
217 ARCL 05  
218 "+: "  
219 XEQ 08  
220 180  
221 +  
222 RCL 08  
223 +  
224 FIX 1  
225 XEQ 13  
226 "+, "  
227 ARCL 08  
228 FS? 55  
229 "+ NM"  
230\*LBL 11  
231 FC? 55  
232 GTO 12  
233 ACA  
234 PRBUF  
235 RTN  
236\*LBL 12  
237 TONE 8  
238 RVIEW  
239 RTN  
240\*LBL 13

GET WAYPOINT

OUT PUT  
WAYPOINT  
DATA

OUTPUT  
DATA

OUTPUT  
degrees

241 RND  
242 360  
243 MOD  
244 X\*0?  
245 GTO 14  
246 LASTX  
247 +  
248\*LBL 14  
249 100  
250 X>Y?  
251 "+0"  
252 SQRT  
253 X>Y?  
254 "+0"  
255 ARCL Y  
256 FC? 55  
257 RTN  
258 ACA  
259 "a\*D"  
260 ASTO X  
261 ACSPEC  
262 CLA  
263 RTN  
264\*LBL 15  
265 FC?C 04  
266 GTO 16  
267 RCL 12  
268 XEQ 06  
269 STO 12  
270 3  
271 FS? 01  
272 2  
273 RCL 14  
274 XEQ 06  
275 RCL IND Y  
276 -  
277 RCL 13  
278 /  
279 STO 14  
280 1 E3  
281 ST/ 13  
282 SF 02  
283\*LBL 16  
284 FC? 55  
285 XEQ 12  
286 RCL 15  
287 STO 05  
288 8  
289 STO 09  
290 SF 25  
291 XEQ IND 15  
292 FC? 25  
293 GTO 00  
294 XEQ 05  
295 XEQ 10  
296 RCL 16  
297 STO 05  
298 8  
299 STO 09  
300 XEQ IND 16

INITIALIZE  
GRID  
PARAMETERS

LEG INCREMENT  
LEG COUNTER

CALCULATE  
WAYPOINTS

301 FC?C 25  
302 GTO 00  
303 XEQ 05  
304 XEQ 10  
305\*LBL 00  
306 FS?C 03  
307 GTO 20  
308 FIX 0  
309 FC?C 02  
310 GTO 00  
311 CF 00  
312 ISG 13  
313 SF 00  
314 "LEG "  
315 ARCL 13  
316 "+b"  
317 FC? 00  
318 "EXIT"  
319 ASTO 05  
320 RCL 04  
321 STO 09  
322 RCL 03  
323 FS? 01  
324 X<> 12  
325 STO 07  
326 RCL 02  
327 FC? 01  
328 X<> 12  
329 STO 06  
330 FC? 00  
331 SF 03  
332 GTO 21  
333\*LBL 00  
334 SF 02  
335 RCL 13  
336 1  
337 +  
338 "LEG "  
339 ARCL X  
340 "+a"  
341 ASTO 05  
342 RCL 04  
343 STO 09  
344 RCL 14  
345 RCL 03  
346 FC? 01  
347 +  
348 STO 07  
349 RCL 14  
350 RCL 02  
351 FS? 01  
352 +  
353 STO 06  
354 GTO 21  
355 END

END GRID

LEG END

LEG  
START

01\*LBL "45CD"  
02 "LEG1 TC"  
03 90  
04 COS  
05 X=0?  
06 SF 01  
07 "LEG1 END"  
08 90.45  
09 STO 12  
10 "NO. LEGS"  
11 8  
12 1  
13 -  
14 STO 13  
15 "EXIT"  
16 35.305  
17 91  
18 FS? 01  
19 X<Y  
20 STO 14  
21 "WAYPOINTS"  
22 "ARG"  
23 ASTO 15  
24 "GOE"  
25 ASTO 16  
26 "ENTRY"  
27 ASTO 05  
28 35.375  
29 91  
30 -4  
31 SF 00  
32 SF 04  
33 RTN  
34\*LBL "ARG"  
35 36.066  
36 90.572  
37 -4  
38 RTN  
39\*LBL "GOE"  
40 35.209  
41 90.287  
42 -4  
43 RTN  
44\*LBL "JBR"  
45 35.499  
46 90.388  
47 -4  
48 RTN  
49\*LBL "FIX"  
50 35.375  
51 91.107  
52 -4  
53 END

A GRID 45 SECTORS C+D

— 1<sup>st</sup> leg  
COURSE = 90° SEARCH SAMPLE

— ENDING LNG  
(IF S/U SEARCH WOULD BE LAT)

— must be greater than 1

EXIT COORDINATES

— E/W SEARCH - STORES LNG

N/S SEARCH - STORES LAT

— 1<sup>st</sup> & 2<sup>nd</sup> WAYPOINTS

ENTRY COORDINATES - includes VAR

— compute the grid flag

— PARAMETER FLAG

— misc. fixes needed

— A fix west of 1<sup>st</sup> leg  
JUST SOUTH OF NEWPORT AIRPORT





**CURVE FITTING**

For a set of data points  $(x_i, y_i)$ ,  $i = 1, 2, \dots, n$ , this program can be used to fit the data to any of the following curves:

1. Straight line (linear regression):  $y = a + bx$ .
2. Exponential curve:  $y = ae^{bx}$  ( $a > 0$ ),
3. Logarithmic curve:  $y = a + b \ln x$ ,
4. Power curve:  $y = ax^b$  ( $a > 0$ ).

The regression coefficients  $a$  and  $b$  are found by solving the following equivalent system of linear equations.

$$An + B\sum X_i = \sum Y_i$$

$$A\sum X_i + B\sum X_i^2 = \sum Y_i X_i$$

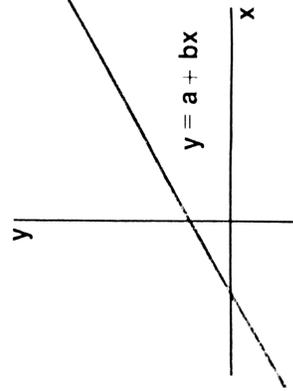
The relations of the variables are defined by the following:

Regression	A	B	$X_i$	$Y_i$
Linear	$a$	$b$	$x_i$	$y_i$
Exponential	$\ln a$	$b$	$x_i$	$\ln y_i$
Logarithmic	$a$	$b$	$\ln x_i$	$y_i$
Power	$\ln a$	$b$	$\ln x_i$	$\ln y_i$

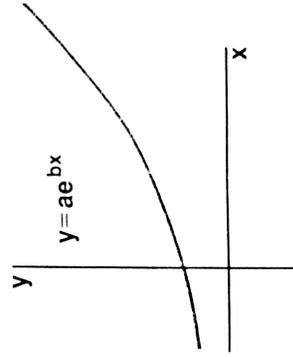
The coefficient of determination is:

$$R^2 = \frac{A\sum Y_i + b\sum X_i Y_i - \frac{1}{n}(\sum Y_i)^2}{\sum(Y_i^2) - \frac{1}{n}(\sum Y_i)^2}$$

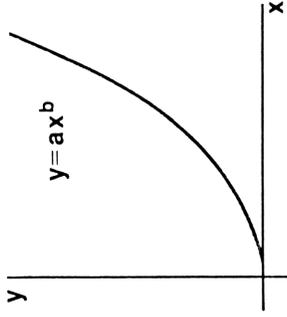
**Linear Regression**



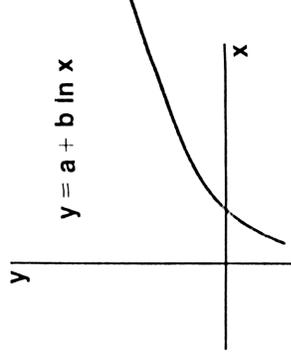
**Exponential Curve Fit**



**Power Curve Fit**



**Logarithmic Curve Fit**



**Remarks:**

1. The program applies the least square method, either to the original equations (straight line and logarithmic curve) or to the transformed equations (exponential curve and power curve).
2. Negative and zero values of  $x_i$  will cause a calculator error for logarithmic curve fits. Negative and zero values of  $y_i$  will cause a machine error for exponential curve fits. For power curve fits both  $x_i$  and  $y_i$  must be positive, non-zero values.
3. As the differences between  $x$  and/or  $y$  values become small, the accuracy of the regression coefficients will decrease.

STEP	INSTRUCTIONS	INPUT	FUNCTION	SIZE: 016	DISPLAY
1	Set status and key in the program				
2	Initialize the program for STRAIGHT LINE or for EXPONENTIAL CURVE or for LOGARITHMIC CURVE or for POWER CURVE		$\boxed{\text{XEQ}} \boxed{\text{LIN}}$ $\boxed{\text{XEQ}} \boxed{\text{EXP}}$ $\boxed{\text{XEQ}} \boxed{\text{LOG}}$ $\boxed{\text{XEQ}} \boxed{\text{POW}}$		LIN EXP LOG POW
3	Repeat step 3 and 4 for $i=1, 2, \dots, n$ input: $x_i, y_i$	$x_i$ $y_i$	$\boxed{\text{ENTER}}$ $\boxed{\text{A}}$		(i)
4	If you made a mistake in inputting $x_k$ and $y_k$ , then correct by	$x_k$ $y_k$	$\boxed{\text{ENTER}}$ $\boxed{\text{C}}$		(k-1)
5	Calculate $R^2$ and regression coefficients $a$ and $b$		$\boxed{\text{E}}$ $\boxed{\text{R/S}}$ $\boxed{\text{R/S}}$		$R^2 = (R^2)$ $a = (a)$ $b = (b)$

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
6	Calculate estimated y from regression, input x	x	$\boxed{R/S}$	$Y_c = (\hat{y})$
7	Repeat step 6 for different x's			
8	Repeat step 5 if you want the results again			
9	To use the same program for another set of data, initialize the program by $\rightarrow$		$\boxed{\text{LIN}}$	LIN or EXP or LOG or POW
10	then go to step 3 To use another program, go to step 2			

**Example 1:**

Fit a straight line to the following set of data and compute  $\hat{y}$  for  $x = 37$  and  $x = 35$ .

$x_i$	40.5	38.6	37.9	36.2	35.1	34.6
$y_i$	104.5	102	100	97.5	95.5	94

**Keystrokes:**

$\boxed{XEQ}$   $\boxed{ALPHA}$   $\boxed{LIN}$   $\boxed{ALPHA}$   
 40.5  $\boxed{ENTER}$   $\boxed{ENTER}$  104.5  $\boxed{A}$   
 38.6  $\boxed{ENTER}$   $\boxed{ENTER}$  102  $\boxed{A}$   
 37.9  $\boxed{ENTER}$   $\boxed{ENTER}$  100  $\boxed{A}$   
 36.2  $\boxed{ENTER}$   $\boxed{ENTER}$  97.5  $\boxed{A}$   
 35.2  $\boxed{ENTER}$   $\boxed{ENTER}$  95.5  $\boxed{A}$   
 35.2  $\boxed{ENTER}$   $\boxed{ENTER}$  95.5  $\boxed{C}$   
 35.1  $\boxed{ENTER}$   $\boxed{ENTER}$  95.5  $\boxed{A}$   
 34.6  $\boxed{ENTER}$   $\boxed{ENTER}$  94  $\boxed{A}$   
 $\boxed{E}$   
 $R2 = 0.99$   
 $a = 33.53$   
 $b = 1.76$   
 $Y_c = 98.65$   
 $Y_c = 95.13$

**Display:**

LIN  
 1.00  
 2.00  
 3.00  
 4.00  
 5.00  
 4.00  
 5.00  
 6.00  
 $R2 = 0.99$   
 $a = 33.53$   
 $b = 1.76$   
 $Y_c = 98.65$   
 $Y_c = 95.13$

Oops!  
 Correct error.  
 Use proper values.

**Example 2:**

Fit an exponential curve to the following set of data and compute  $\hat{y}$  for  $x = 1.5$  and  $x = 2$ .

$x_i$	.72	1.31	1.95	2.58	3.14
$y_i$	2.16	1.61	1.16	.85	0.5

**Keystrokes:**

$\boxed{XEQ}$   $\boxed{ALPHA}$   $\boxed{EXP}$   $\boxed{ALPHA}$   
 .72  $\boxed{ENTER}$   $\boxed{ENTER}$  2.16  $\boxed{A}$   
 1.31  $\boxed{ENTER}$   $\boxed{ENTER}$  1.61  $\boxed{A}$   
 1.95  $\boxed{ENTER}$   $\boxed{ENTER}$  1.16  $\boxed{A}$   
 2.58  $\boxed{ENTER}$   $\boxed{ENTER}$  .85  $\boxed{A}$   
 3.15  $\boxed{ENTER}$   $\boxed{ENTER}$  .05  $\boxed{A}$   
 3.15  $\boxed{ENTER}$   $\boxed{ENTER}$  .05  $\boxed{C}$   
 3.14  $\boxed{ENTER}$   $\boxed{ENTER}$  0.5  $\boxed{A}$   
 $\boxed{E}$   
 $R2 = 0.98$   
 $a = 3.45$   
 $b = -0.58$   
 $Y_c = 1.44$   
 $Y_c = 1.08$

If you don't make a mistake you can skip two steps.

**Display:**

EXP  
 1.00  
 2.00  
 3.00  
 4.00  
 5.00  
 4.00  
 5.00  
 $R2 = 0.98$   
 $a = 3.45$   
 $b = -0.58$   
 $Y_c = 1.44$   
 $Y_c = 1.08$

**Example 3:**

Fit a logarithmic curve to the following set of data and compute  $\hat{y}$  for  $x = 8$  and  $x = 14.5$ .

$x_i$	3	4	6	10	12
$y_i$	1.5	9.3	23.4	45.8	60.1

**Keystrokes:**

$\boxed{XEQ}$   $\boxed{ALPHA}$   $\boxed{LOG}$   $\boxed{ALPHA}$   
 3  $\boxed{ENTER}$   $\boxed{ENTER}$  1.5  $\boxed{A}$   
 4  $\boxed{ENTER}$   $\boxed{ENTER}$  9.3  $\boxed{A}$   
 6  $\boxed{ENTER}$   $\boxed{ENTER}$  23.4  $\boxed{A}$   
 10  $\boxed{ENTER}$   $\boxed{ENTER}$  45.8  $\boxed{A}$   
 12  $\boxed{ENTER}$   $\boxed{ENTER}$  60.1  $\boxed{A}$   
 12  $\boxed{ENTER}$   $\boxed{ENTER}$  60.1  $\boxed{C}$   
 12  $\boxed{ENTER}$   $\boxed{ENTER}$  60.1  $\boxed{A}$   
 $\boxed{E}$   
 $R2 = 0.98$   
 $a = -47.02$   
 $b = 41.39$   
 $Y_c = 39.06$   
 $Y_c = 63.67$

**Display:**

LOG  
 1.00  
 2.00  
 3.00  
 4.00  
 5.00  
 4.00  
 5.00  
 $R2 = 0.98$   
 $a = -47.02$   
 $b = 41.39$   
 $Y_c = 39.06$   
 $Y_c = 63.67$

Another mistake!

Example 4:

Fit a power curve to the following set of data and compute  $\hat{y}$  for  $x = 18$  and  $x = 23$ .

$x_i$	10	12	15	17	20	22	25	27	30	32	35
$y_i$	0.95	1.05	1.25	1.41	1.73	2.00	2.53	2.98	3.85	4.59	6.02

Keystrokes:

Display:

<b>XEQ</b> <b>ALPHA</b>	<b>POW</b>	<b>ALPHA</b>	<b>POW</b>
10 <b>ENTER</b>	0.95 <b>A</b>		1.00
12 <b>ENTER</b>	1.05 <b>A</b>		2.00
15 <b>ENTER</b>	1.25 <b>A</b>		3.00
17 <b>ENTER</b>	1.41 <b>A</b>		4.00
20 <b>ENTER</b>	1.73 <b>A</b>		5.00
22 <b>ENTER</b>	2.00 <b>A</b>		6.00
25 <b>ENTER</b>	2.53 <b>A</b>		7.00
27 <b>ENTER</b>	2.98 <b>A</b>		8.00
30 <b>ENTER</b>	3.85 <b>A</b>		9.00
32 <b>ENTER</b>	4.59 <b>A</b>		10.00
35 <b>ENTER</b>	60.2 <b>A</b>		11.00
35 <b>ENTER</b>	60.2 <b>C</b>		10.00
35 <b>ENTER</b>	6.02 <b>A</b>		11.00

Error correction again.

**R2 = 0.94**  
**a = 0.03**  
**b = 1.46**  
**Y. = 1.76**  
**Y. = 2.52**

Programming Highlight

This program uses a single section of code for most of the calculations it needs to do. Since each of the four types of curve fitting requires the input data to be in a different form, it would seem that a different program should be used for each curve type. Instead, each of the set-up programs, LIN, LOG, EXP, and POW, stores a code in register 00. Then the single function on line 32, XEQ IND 00, takes care of the four different ways of processing the input data by executing the function whose label is stored in register 00.

01*LBL "LIN"	45*LBL E		
02 S	46 PCL 15		
03 "LIN"	47 PCL 11		
04 GTO 13	48 PCL 10		
05*LBL "EXP"	49 PCL 10		
06 S	50 XEQ 04		
07 "EXP"	51 STO 03		
08 GTO 13	52 PCL 12		
09*LBL "LOG"	53 PCL 11		
10 S	54 PCL 10		
11 "LOG"	55 PCL 14		
12 GTO 13	56 XEQ 04		
13*LBL "POW"	57 PCL 03		
14 S	58 S		
15 "POW"	59 STO 04		
16*LBL 13	60 XEQ IND		
17 XEQ "INH"	05		
T...	61 STO 06		
18 STO 08	62 PCL 15		
19 RSTO 08	63 PCL 14		
20 CREG 10	64 PCL 10		
21 CLC	65 PCL 12		
22 BEEP	66 XEQ 04		
23 RVIEW	67 PCL 03		
24 STOP	68 S		
25*LBL C	69 STO 05		
26 XEQ C	70*LBL 03		
27 XEQ IND	71 PCL 04		
00	72 PCL 12		
28 C-	73 S		
29 STOP	74 PCL 05		
30*LBL A	75 PCL 14		
31 XEQ A	76 +		
32 XEQ IND	77 PCL 12		
00	78 PCL 15		
33 S+	79 PCL 15		
34 STOP	80 PCL 15		
35*LBL 07	81 S		
36 LH	82 STO*09		
37 RTH	83 PCL 13		
38*LBL 08	84 PCL 09		
39 LH	85 PCL 13		
40*LBL 06	86 -		
41 XEQ Y	87 S		
42 LH	88 "P2"		
43 XEQ Y	89 XEQ 88		
44 PTH	90 PCL 06		
	91 S		
	92 XEQ 88		
	93 PCL 05		
	94 "b"		

Calculate A, b and a, b.

Power P<sup>-1</sup>  
 Power P

R00 = Index  
 R01 = x  
 R02 = y  
 R03 = det  
 R04 = A

R05 = b  
 R06 = a  
 R07 = used  
 R08 = LIN or EXP or LOG or POW  
 R09 = (2y) 2 n

<pre> 95 GT0 01 96 LBL 06 97 LBL 08 98 ETX 99 LBL 05 100 LBL 07 101 RTN 102 LBL 09 103 * 104 STO 07 105 RDN 106 * 107 RCL 07 108 - 109 RTN 110 LBL 00 111 "Y." 112 LBL 01 113 "H=" 114 RCCL X 115 RVIEW <del>116 FS= 55</del> 117 STOP 118 LBL 04 119 GT0 IND 00 120 LBL 08 121 RCL 05 122 YX 123 GT0 09 124 LBL 06 125 RCL 05 126 * 127 ETX 128 LBL 09 129 RCL 06 130 * 131 GT0 00 132 LBL 07 133 LN 134 LBL 05 135 RCL 05 136 * 137 RCL 06 138 + 139 GT0 00 140 LBL 88 141 "H=" 142 RCCL X 143 RVIEW 144 RTN                 </pre>	<p>Inverse transform</p> <p>Coefficient of Determination</p> <p>Calculate r<sup>2</sup>.</p> <p>Input x to calculate y.</p>	<pre> 145 LBL 3 146 GT0 IND 02 147 LBL "INI T" 148 CLPG 149 CF 00 150 CF 01 151 CF 02 152 SF 21 153 SF 27 154 CF 29 155 RTN                 </pre> <p>Important: status Size = 016 Σ = 10 Fix 2</p> <p>Flags used FD0 FD1 FD2 FD3 FD4 FD5 FD6 FD7 FD8 FD9 FD0 FD1 FD2 FD3 FD4 FD5 FD6 FD7 FD8 FD9</p>	<p>Re-initialize.</p> <p>For initializing.</p>
<pre> R10 = ΣX R11 = ΣX² R12 = ΣY R13 = ΣY² R14 = ΣXY R15 = n                 </pre>			

# CURVE FITTING

01*LBL "LIN"	45*LBL E	96*LBL 06
02 5	46 RCL 16	97*LBL 08
03 "LIN"	47 RCL 12	98 E+X
04 GTO 13	48 RCL 11	99*LBL 05
05*LBL "EXP"	49 RCL 11	100*LBL 07
06 6	50 XEQ 09	101 RTN
07 "EXP"	51 STO 03	102*LBL 09
08 GTO 13	52 RCL 13	103 *
09*LBL "LOG"	53 RCL 12	104 STO 07
10 7	54 RCL 11	105 RDH
11 "LOG"	55 RCL 15	106 *
12 GTO 13	56 XEQ 09	107 RCL 07
13*LBL "POW"	57 RCL 03	108 -
14 8	58 /	109 RTN
15 "POW"	59 STO 04	110 FC? 55
16*LBL 13	60 XEQ IND 00	111 CF 21
17 FC? 55	61 STO 06	112*LBL 00
18 SF 21	62 RCL 16	113 "Y."
19 STO 00	63 RCL 15	114*LBL 01
20 ASTD 00	64 RCL 11	115 "F="
21 CLS	65 RCL 13	116 ARCL X
22 ADV	66 XEQ 09	117 AVIEW
23 AVIEW	67 RCL 03	118 RTN
24 STOP	68 /	119*LBL 04
25*LBL C	69 STO 05	120 GTO IND 00
26 X<>Y	70*LBL 03	121*LBL 08
27 XEQ IND 00	71 RCL 04	122 RCL 05
28 S-	72 RCL 13	123 Y+X
29 STOP	73 *	124 GTO 09
30*LBL A	74 RCL 05	125*LBL 06
31 X<>Y	75 RCL 15	126 RCL 05
32 XEQ IND 00	76 *	127 *
33 S+	77 +	128 E+X
34 STOP	78 RCL 13	129*LBL 09
35*LBL 07	79 X+2	130 RCL 06
36 LN	80 RCL 16	131 *
37 RTN	81 /	132 GTO 00
38*LBL 00	82 STO 09	133*LBL 07
39 LN	83 -	134 LN
40*LBL 06	84 RCL 14	135*LBL 05
41 X<>Y	85 RCL 09	136 RCL 05
42 LN	86 -	137 *
43 X<>Y	87 /	138 RCL 06
44 RTN	88 "R2"	139 +
	89 XEQ 01	140 GTO 00
	90 RCL 06	141*LBL a
	91 "a"	142 GTO IND 00
	92 XEQ 01	143 END
	93 RCL 05	
	94 "b"	
	95 GTO 01	

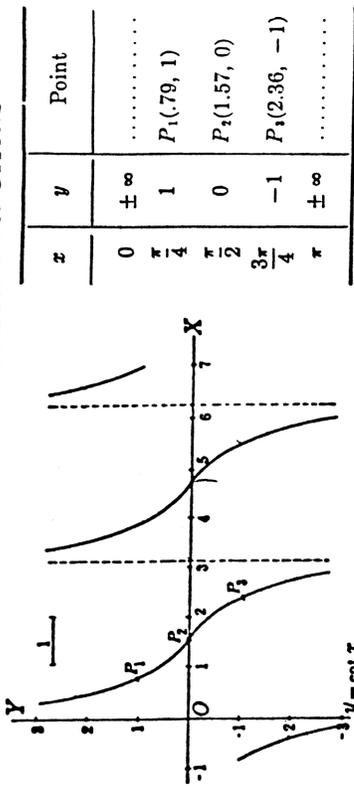




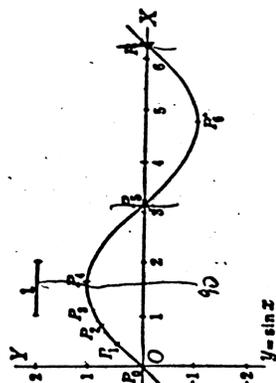


TRIGONOMETRY

GRAPHS OF THE TRIGONOMETRIC FUNCTIONS

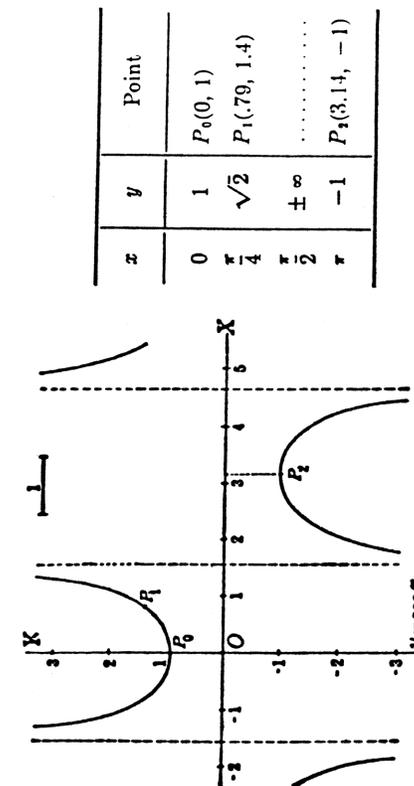


$x$	$y$	Point
0	0	$P_3(0, 0)$
$\frac{\pi}{6} = .52$	.50	$P_1(.52, .50)$
$\frac{\pi}{4} = .79$	.71	$P_2(.79, .71)$
$\frac{\pi}{3} = 1.05$	.87	$P_3(1.05, .87)$
$\frac{\pi}{2} = 1.57$	1	$P_4(1.57, 1)$
$\frac{2\pi}{3} = 3.14$	0	$P_5(3.14, 0)$
$\frac{3\pi}{4} = 4.71$	-1	$P_6(4.71, -1)$
$2\pi = 6.28$	0	$P_7(6.28, 0)$

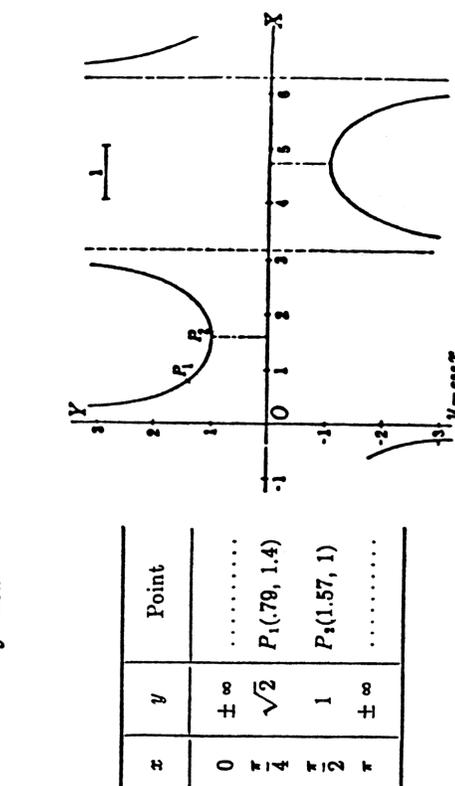
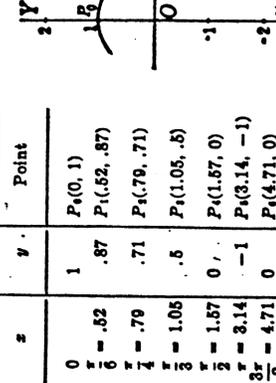


TRIGONOMETRY

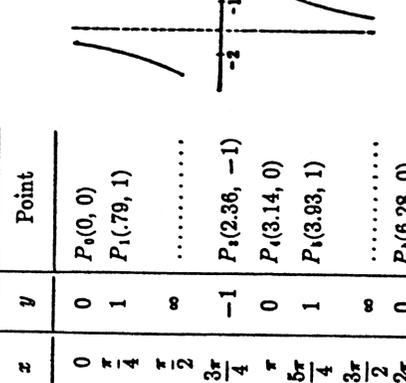
\*GRAPHS OF THE TRIGONOMETRIC FUNCTIONS



$x$	$y$	Point
0	1	$P_3(0, 1)$
$\frac{\pi}{6} = .52$	.87	$P_1(.52, .87)$
$\frac{\pi}{4} = .79$	.71	$P_2(.79, .71)$
$\frac{\pi}{3} = 1.05$	.5	$P_3(1.05, .5)$
$\frac{\pi}{2} = 1.57$	0	$P_4(1.57, 0)$
$\frac{2\pi}{3} = 3.14$	-1	$P_5(3.14, -1)$
$\frac{3\pi}{4} = 4.71$	0	$P_6(4.71, 0)$
$2\pi = 6.28$	1	$P_7(6.28, 1)$



$x$	$y$	Point
0	0	$P_3(0, 0)$
$\frac{\pi}{4} = .79$	1	$P_1(.79, 1)$
$\frac{\pi}{2} = 1.57$	$\infty$	.....
$\frac{3\pi}{4} = 4.71$	-1	$P_2(4.71, -1)$
$\pi = 3.14$	0	$P_4(3.14, 0)$
$\frac{5\pi}{4} = 7.85$	1	$P_5(7.85, 1)$
$\frac{3\pi}{2} = 4.71$	$\infty$	.....
$2\pi = 6.28$	0	$P_7(6.28, 0)$



## TRIGONOMETRY

### TRIGONOMETRIC FUNCTIONS IN A RIGHT-ANGLED TRIANGLE

If  $A$ ,  $B$ , and  $C$  are the vertices ( $C$  the right angle), and  $a$ ,  $b$ , and  $h$  the sides opposite respectively,

$$\text{sine } A = \sin A = \frac{a}{h},$$

$$\text{cosine } A = \cos A = \frac{b}{h},$$

$$\text{tangent } A = \tan A = \frac{a}{b},$$

$$\text{cotangent } A = \cot A = \text{ctn } A = \frac{b}{a},$$

$$\text{secant } A = \sec A = \frac{h}{b},$$

$$\text{cosecant } A = \text{csc } A = \frac{h}{a}.$$

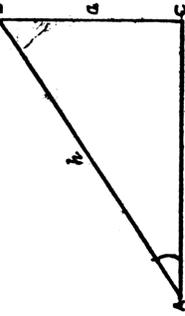


Fig. 4

$$\text{exsecant } A = \text{exsec } A = \sec A - 1$$

$$\text{versine } A = \text{vers } A = 1 - \cos A$$

$$\text{coversine } A = \text{covers } A = 1 - \sin A$$

$$\text{haversine } A = \text{hav } A = \frac{1}{2} \text{ vers } A$$

### RELATIONS BETWEEN DEGREE OF ACCURACY OF COMPUTED LENGTHS AND ANGLES

When solving a triangle for any of its parts the following should be observed:

- | Length to:           | (requires) | Angle to:               |
|----------------------|------------|-------------------------|
| 2 significant digits |            | nearest 30' = 0.5°      |
| 3 significant digits |            | nearest 05' = 0.083°    |
| 4 significant digits |            | nearest 01' = 0.0167°   |
| 5 significant digits |            | nearest 0.1' = 0.00167° |

### SIGNS AND LIMITS OF VALUE ASSUMED BY THE FUNCTIONS

Function	Quadrant I		Quadrant II		Quadrant III		Quadrant IV	
	Sign	Value	Sign	Value	Sign	Value	Sign	Value
sin.....	+	0 to 1	+	1 to 0	-	0 to 1	-	1 to 0
cos.....	+	1 to 0	-	0 to 1	-	1 to 0	+	0 to 1
tan.....	+	0 to ∞	-	∞ to 0	+	0 to ∞	-	∞ to 0
cot.....	+	∞ to 0	-	0 to ∞	+	∞ to 0	-	0 to ∞
sec.....	+	1 to ∞	-	∞ to 1	-	1 to ∞	+	∞ to 1
cosec.....	+	∞ to 1	+	1 to ∞	-	∞ to 1	-	1 to ∞

\* The sign in front of radical depends on quadrant in which  $x$  falls.

## TRIGONOMETRY

### VALUE OF THE FUNCTIONS OF VARIOUS ANGLES

	0°	30°	45°	60°	90°	180°	270°
sin.....	0	$\frac{1}{2}$	$\frac{1}{\sqrt{2}}$	$\frac{1}{2}\sqrt{3}$	1	0	-1
cos.....	1	$\frac{1}{2}\sqrt{3}$	$\frac{1}{\sqrt{2}}$	$\frac{1}{2}$	0	-1	0
tan.....	0	$\frac{1}{\sqrt{3}}$	1	$\sqrt{3}$	∞	0	∞
cot.....	∞	$\sqrt{3}$	1	$\frac{1}{\sqrt{3}}$	0	∞	0
sec.....	1	$\frac{2}{\sqrt{3}}$	$\sqrt{2}$	2	∞	-1	∞
cosec.....	∞	2	$\sqrt{2}$	$\frac{2}{\sqrt{3}}$	1	∞	-1

### EXPONENTIAL DEFINITIONS OF CIRCULAR FUNCTIONS

$$\sin x = \frac{1}{2i}(e^{ix} - e^{-ix}) \quad \text{cosec } x = \frac{2i}{e^{ix} - e^{-ix}}$$

$$\left(\frac{e^x - 1}{e^x + 1}\right) = \tan \frac{x}{2}$$

$$\sec x = \frac{2}{e^{ix} + e^{-ix}}$$

$$\tan x = \frac{e^{ix} - e^{-ix}}{i(e^{ix} + e^{-ix})} \quad \cot x = \frac{i(e^{ix} + e^{-ix})}{e^{ix} - e^{-ix}}$$

### RELATIONS OF THE FUNCTIONS

$$\sin x = \frac{1}{\text{cosec } x}$$

$$\text{cosec } x = \frac{1}{\sin x}$$

$$\cos x = \frac{1}{\sec x}$$

$$\sec x = \frac{1}{\cos x}$$

$$\tan x = \frac{1}{\cot x} = \frac{\sin x}{\cos x}$$

$$\sin^2 x + \cos^2 x = 1.$$

$$\cot x = \frac{1}{\tan x} = \frac{\cos x}{\sin x}$$

$$1 + \tan^2 x = \sec^2 x.$$

$$* \sin x = \pm \sqrt{1 - \cos^2 x}.$$

$$* \cos x = \pm \sqrt{1 - \sin^2 x}.$$

$$* \tan x = \pm \sqrt{\sec^2 x - 1}.$$

$$* \sec x = \pm \sqrt{\tan^2 x + 1}.$$

$$* \cot x = \pm \sqrt{\text{cosec}^2 x - 1}.$$

$$* \text{cosec } x = \pm \sqrt{\cot^2 x + 1}.$$

$$\sin x = \cos(90^\circ - x) = \sin(180^\circ - x).$$

$$\cos x = \sin(90^\circ - x) = -\cos(180^\circ - x).$$

$$\tan x = \cot(90^\circ - x) = -\tan(180^\circ - x).$$

$$\cot x = \tan(90^\circ - x) = -\cot(180^\circ - x).$$

$$\text{cosec } x = \cot \frac{x}{2} - \cot x.$$

TRIGONOMETRY

FUNCTIONS OF SUMS OF ANGLES

$$\begin{aligned} \sin(x \pm y) &= \sin x \cos y \pm \cos x \sin y. \\ \cos(x \pm y) &= \cos x \cos y \mp \sin x \sin y. \\ \tan(x \pm y) &= \frac{\tan x \pm \tan y}{1 \mp \tan x \tan y}. \end{aligned}$$

FUNCTIONS OF MULTIPLE ANGLES

$$\begin{aligned} \sin 2x &= 2 \sin x \cos x. \\ \cos 2x &= \cos^2 x - \sin^2 x = 2 \cos^2 x - 1 = 1 - 2 \sin^2 x. \\ \sin 3x &= 3 \sin x - 4 \sin^3 x. \\ \cos 3x &= 4 \cos^3 x - 3 \cos x. \\ \sin 4x &= 8 \cos^3 x \sin x - 4 \cos x \sin x. \\ \cos 4x &= 8 \cos^4 x - 8 \cos^2 x + 1. \\ \sin 5x &= 5 \sin x - 20 \sin^3 x + 16 \sin^5 x. \\ \cos 5x &= 16 \cos^5 x - 20 \cos^3 x + 5 \cos x. \\ \sin 6x &= 32 \cos^5 x \sin x - 32 \cos^3 x \sin x + 6 \cos x \sin x. \\ \cos 6x &= 32 \cos^6 x - 48 \cos^4 x + 18 \cos^2 x - 1. \end{aligned}$$

$$\tan 2x = \frac{2 \tan x}{1 - \tan^2 x}$$

$$\cot 2x = \frac{\cot^2 x - 1}{2 \cot x}$$

$$\tan 3x = \frac{3 \tan x - \tan^3 x}{1 - 3 \tan^2 x}$$

$$\sin \frac{1}{2}x = \pm \sqrt{\frac{1 - \cos x}{2}}$$

$$\cos \frac{1}{2}x = \pm \sqrt{\frac{1 + \cos x}{2}}$$

$$\tan \frac{1}{2}x = \pm \sqrt{\frac{1 - \cos x}{1 + \cos x}} = \frac{1 - \cos x}{\sin x} = \frac{\sin x}{1 + \cos x}$$

\* The sign in front of radical depends on quadrant in which  $x$  falls.

TRIGONOMETRY

MISCELLANEOUS RELATIONS

$$\begin{aligned} \sin x \pm \sin y &= 2 \sin \frac{1}{2}(x \pm y) \cdot \cos \frac{1}{2}(x \mp y). \\ \cos x + \cos y &= 2 \cos \frac{1}{2}(x + y) \cdot \cos \frac{1}{2}(x - y). \\ \cos x - \cos y &= -2 \sin \frac{1}{2}(x + y) \cdot \sin \frac{1}{2}(x - y). \\ \sin x \cos y &= \frac{1}{2} [\sin(x + y) + \sin(x - y)] \\ \cos x \sin y &= \frac{1}{2} [\sin(x + y) - \sin(x - y)] \\ \cos x \cos y &= \frac{1}{2} [\cos(x + y) + \cos(x - y)] \\ \sin x \sin y &= \frac{1}{2} [\cos(x - y) - \cos(x + y)] \\ \tan x \pm \tan y &= \frac{\sin(x \pm y)}{\cos x \cdot \cos y}, \quad \cot x \pm \cot y = \frac{\pm \sin(x \pm y)}{\sin x \cdot \sin y}. \\ 1 + \tan x &= \tan(45^\circ + x), \quad \frac{\cot x + 1}{\cot x - 1} = \cot(45^\circ - x). \\ \frac{\sin x \pm \sin y}{\cos x \pm \cos y} &= \tan \frac{1}{2}(x \pm y). \\ \frac{\sin x + \sin y}{\sin x - \sin y} &= -\cot \frac{1}{2}(x \mp y). \\ \frac{\sin x + \sin y}{\sin x - \sin y} &= \frac{\tan \frac{1}{2}(x + y)}{\tan \frac{1}{2}(x - y)}. \\ \sin^2 x - \sin^2 y &= \sin(x + y) \cdot \sin(x - y). \\ \cos^2 x - \cos^2 y &= -\sin(x + y) \sin(x - y). \\ \cos^2 x - \sin^2 y &= \cos(x + y) \cos(x - y). \end{aligned}$$

INVERSE TRIGONOMETRIC FUNCTIONS

The following table lists each of the six inverse trigonometric functions together with the interval of its principal value:

Function	Interval containing principal value	
	$x$ positive or zero	$x$ negative
$y = \sin^{-1} x$ and $\tan^{-1} x$ .....	$0 \leq y \leq \pi/2$	$-\pi/2 \leq y < 0$
$y = \cos^{-1} x$ and $\cot^{-1} x$ .....	$0 \leq y \leq \pi/2$	$\pi/2 < y \leq \pi$
$y = \sec^{-1} x$ and $\csc^{-1} x$ .....	$0 \leq y \leq \pi/2$	$-\pi \leq y \leq -\pi/2$

Usually the first letter in "arc" or the name of the inverse trigonometric functions is capitalized if the principal value is desired. Thus

$$\text{Arc sin } \frac{1}{2} = \text{Sin}^{-1} \frac{1}{2} = \frac{\pi}{6}$$

while  $\text{arc sin } \frac{1}{2} = \frac{\pi}{6} + 2\pi n$  or  $\frac{5\pi}{6} + 2\pi n$

In the calculus both for differentiation or integral formulas, capitalization is not adhered to strictly, but principal values are always understood for inverse trigonometric functions when used unless specifically stated otherwise.

RELATIONS BETWEEN SIDES AND ANGLES OF ANY PLANE TRIANGLE

In a triangle with angles  $A, B,$  and  $C$  and sides opposite  $a, b,$  and  $c$  respectively,

$$\frac{a}{\sin A} = \frac{b}{\sin B} = \frac{c}{\sin C} = \text{diameter of the circumscribed circle.}$$

$$a^2 = b^2 + c^2 - 2bc \cos A.$$

$$a = b \cos C + c \cos B.$$

$$\cos A = \frac{b^2 + c^2 - a^2}{2bc}$$

$$\tan \frac{A-B}{2} = \frac{a-b}{a+b} \cot \frac{C}{2}$$

$$\sin A = \frac{2}{bc} \sqrt{s(s-a)(s-b)(s-c)},$$

where  $s = \frac{1}{2}(a+b+c)$  and  $r = \sqrt{\frac{(s-a)(s-b)(s-c)}{s}}$ .

$$\sin \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{bc}}$$

$$\cos \frac{A}{2} = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{A}{2} = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}} = \frac{r}{s-a}$$

$$\frac{a+b}{a-b} = \frac{\sin A + \sin B}{\sin A - \sin B} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} = \frac{\cot \frac{1}{2}C}{\tan \frac{1}{2}(A-B)}$$

$$h = d \frac{\sin \alpha \sin \beta}{\sin(\alpha + \beta)} = \frac{d}{\cot \alpha + \cot \beta}$$

Similarly

$$h = d \frac{\sin \alpha \sin \beta'}{\sin(\beta' - \alpha)} = \frac{d}{\cot \alpha - \cot \beta'}$$

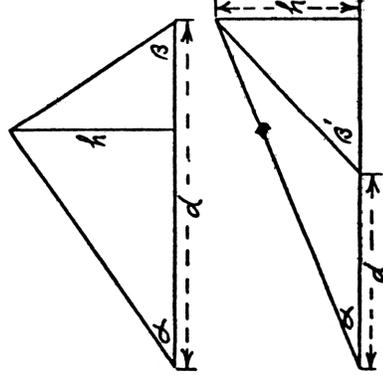


Fig. 5

RELATIONS IN ANY SPHERICAL TRIANGLE

If  $A, B$  and  $C$  be the three angles and  $a, b,$  and  $c$  the opposite sides,

$$\frac{\sin A}{\sin a} = \frac{\sin B}{\sin b} = \frac{\sin C}{\sin c}$$

$$\cos a = \cos b \cos c + \sin b \sin c \cos A = \frac{\cos b \cos(c \pm \theta)}{\cos \theta}$$

where  $\tan \theta = \tan b \cos A.$

$$\cos A = -\cos B \cos C + \sin B \sin C \cos a.$$

$$\sin \frac{1}{2}A = \sqrt{\frac{\sin(s-b)\sin(s-c)}{\sin b \sin c}}$$

where  $s = \frac{1}{2}(a+b+c).$

$$\cos \frac{1}{2}A = \sqrt{\frac{\sin s \sin(s-a)}{\sin b \sin c}}$$

$$\tan \frac{1}{2}A = \frac{\sin(s-a)}{\sin(s-b)\sin(s-c)}$$

where  $r = \frac{\sin s}{\sin(s-b)\sin(s-c)}$

$$\cos \frac{1}{2}a = \frac{\cos(S-B)\cos(S-C)}{\sin B \sin C}$$

where  $S = \frac{1}{2}(A+B+C).$

$$\sin \frac{1}{2}a = \sqrt{\frac{\cos S \cos(S-A)}{\sin B \sin C}}$$

$$\tan \frac{1}{2}a = R \cos(S-A)$$

$$\text{where } R = \frac{-\cos S}{\cos(S-A)\cos(S-B)\cos(S-C)}$$

$$\tan \frac{a+b}{2} = \frac{\cos \frac{A-B}{2}}{\cos \frac{A+B}{2}} \tan \frac{a-b}{2} = \frac{C}{\cos \frac{a+b}{2}}$$

$$\tan \frac{c}{2} = \frac{\cos \frac{A+B}{2}}{\cos \frac{A-B}{2}} \cot \frac{a+b}{2}$$

$$\tan \frac{a-b}{2} = \frac{\sin \frac{A-B}{2}}{\sin \frac{A+B}{2}} \tan \frac{a-b}{2} = \frac{C}{\sin \frac{a+b}{2}}$$

$$\tan \frac{c}{2} = \frac{\sin \frac{A+B}{2}}{\sin \frac{A-B}{2}} \cot \frac{a+b}{2}$$

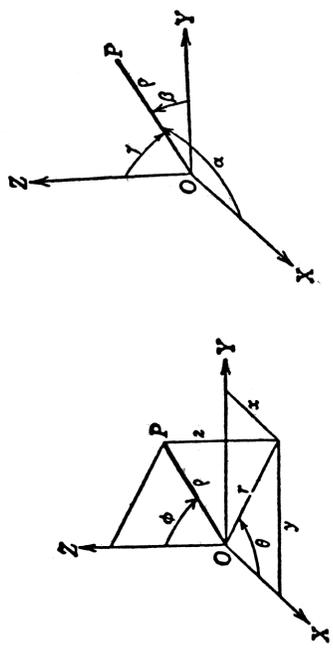
$$\text{hav } a = \text{hav}(b-c) + \sin b \sin c \text{ hav } A$$

$$\text{hav } A = \frac{\sqrt{\text{hav}[a+(b-c)] \text{hav}[a-(b-c)]}}{\sin b \sin c}$$

ANALYTICAL GEOMETRY  
TRANSFORMATION OF COORDINATES (Continued)  
SOLID ANALYTICAL GEOMETRY

Space Coordinates

1. Rectangular System  $x, y, z$ .
2. Cylindrical System  $r, \theta, z$ .
3. Spherical System  $\rho, \theta, \phi$ . In certain situations it is desirable to interchange the symbols  $\phi$  for  $\theta$  and vice versa.
4. Polar Space System  $\rho, \alpha, \beta, \gamma$ .



Relations of Coordinates of Systems in Terms of  $x, y, z$

Cylindrical	Spherical	Polar Space
$r = \sqrt{x^2 + y^2}$ $\theta = \tan^{-1} \frac{y}{x}$ $z = z$	$\rho = \sqrt{x^2 + y^2 + z^2}$ $\theta = \tan^{-1} \frac{y}{x}$ $\phi = \cos^{-1} \left( \frac{z}{\sqrt{x^2 + y^2 + z^2}} \right)$	$\rho = \sqrt{x^2 + y^2 + z^2}$ $\alpha = \cos^{-1} \left( \frac{x}{\sqrt{x^2 + y^2 + z^2}} \right)$ $\beta = \cos^{-1} \left( \frac{y}{\sqrt{x^2 + y^2 + z^2}} \right)$ $\gamma = \cos^{-1} \left( \frac{z}{\sqrt{x^2 + y^2 + z^2}} \right)$

Relations of Rectangular Coordinates  $(x, y, z)$  in Terms of Cylindrical, Spherical and Polar Space Coordinates

Cylindrical	Spherical	Polar Space
$x = r \cos \theta$ $y = r \sin \theta$ $z = z$	$x = \rho \sin \phi \cos \theta$ $y = \rho \sin \phi \sin \theta$ $z = \rho \cos \phi$	$x = \rho \cos \alpha$ $y = \rho \cos \beta$ $z = \rho \cos \gamma$

ANALYTICAL GEOMETRY  
TRANSFORMATION OF COORDINATES  
Rectangular System

- (1) Translation only of axes parallel to themselves. The coordinates of new origin with respect to old axes:  $x = h, y = k$ . Primed letters designate new coordinates.

$$x' = x - h \quad x = x' + h$$

$$y' = y - k \quad y = y' + k$$

- (2) Rotation of axes with fixed origin.

Angle of rotation =  $\theta$

$$x' = x \cos \theta + y \sin \theta \quad x = x' \cos \theta - y' \sin \theta$$

$$y' = y \cos \theta - x \sin \theta \quad y = y' \cos \theta + x' \sin \theta$$

- (3) Origin translated and axes rotated. Symbols same as above

$$x' = (x - h) \cos \theta + (y - k) \sin \theta$$

$$y' = (y - k) \cos \theta - (x - h) \sin \theta$$

$$x = x' \cos \theta - y' \sin \theta + h$$

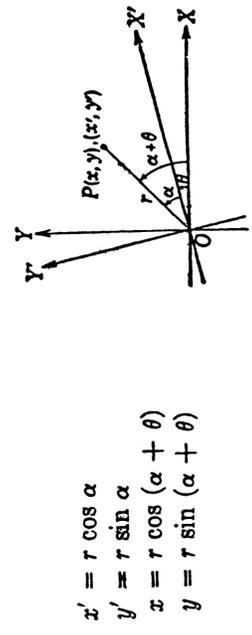
$$y = y' \cos \theta + x' \sin \theta + k$$

Relation between Rectangular and Polar Coordinates

$$x = r \cos \theta \quad r = \sqrt{x^2 + y^2} \quad \sin \theta = \frac{y}{\sqrt{x^2 + y^2}}$$

$$y = r \sin \theta \quad \theta = \tan^{-1} \frac{y}{x} \quad \cos \theta = \frac{x}{\sqrt{x^2 + y^2}}$$

Rotation of Polar Axes through Angle  $\theta$



$$x' = r \cos \alpha$$

$$y' = r \sin \alpha$$

$$x = r \cos (\alpha + \theta)$$

$$y = r \sin (\alpha + \theta)$$

