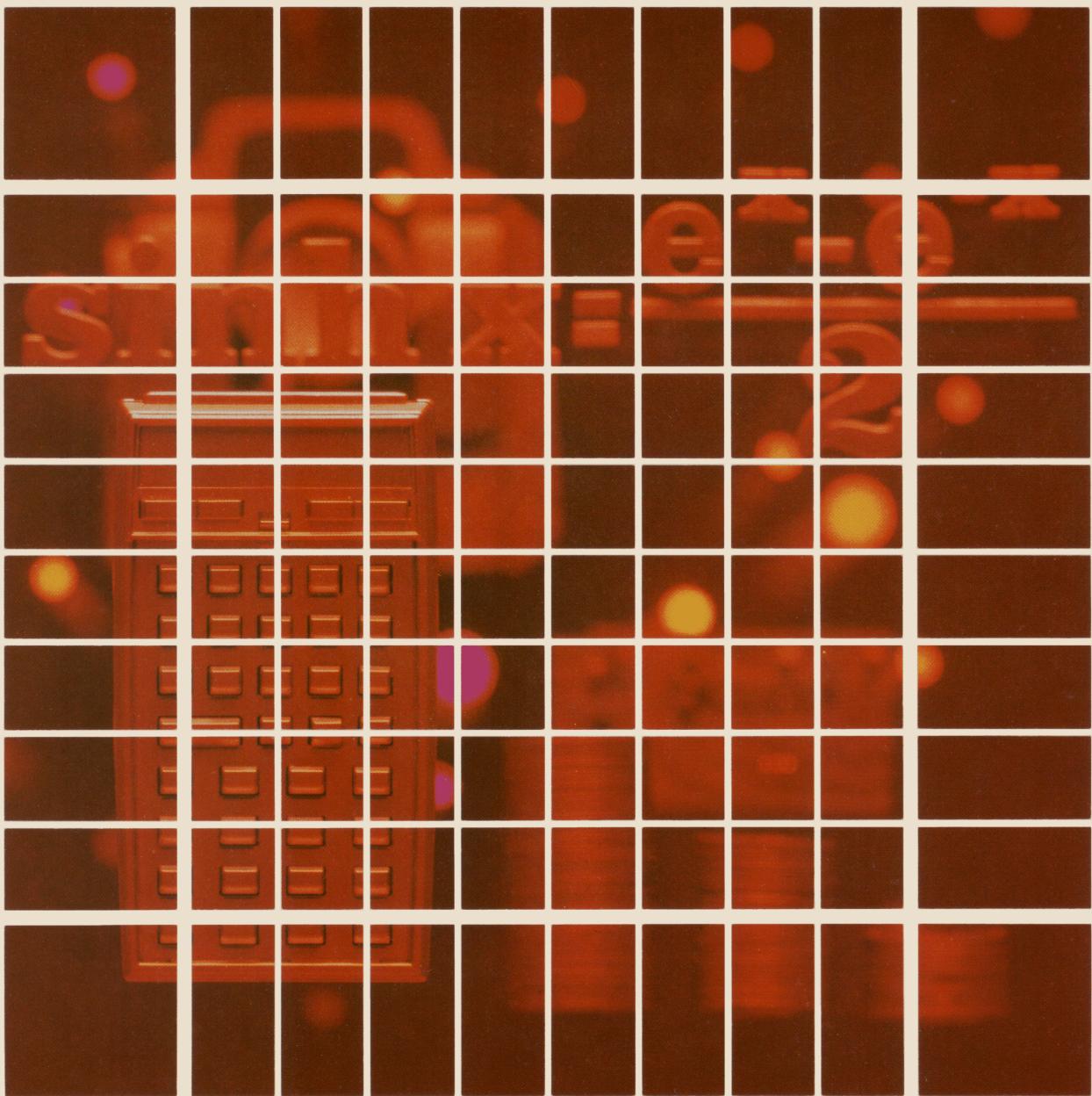


HEWLETT-PACKARD

HP-41

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Electrical Engineering**

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The program material contained herein is supplied without representation or warranty of any kind. Hewlett-Packard Company therefore assumes no responsibility and shall have no liability, consequential or otherwise, of any kind arising from the use of this program material or any part thereof.

INTRODUCTION

This HP-41C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.

KEYING A PROGRAM INTO THE HP-41C

There are several things that you should keep in mind while you are keying in programs from the program listings provided in this book. The output from the HP 82143A printer provides a convenient way of listing and an easily understood method of keying in programs without showing every keystroke. This type of output is what appears in this handbook. Once you understand the procedure for keying programs from the printed listings, you will find this method simple and fast. Here is the procedure:

1. At the end of each program listing is a listing of status information required to properly execute that program. Included is the SIZE allocation required. Before you begin keying in the program, press **XEQ ALPHA SIZE ALPHA** and specify the allocation (three digits; e.g., 10 should be specified as 010).

Also included in the status information is the display format and status of flags important to the program. To ensure proper execution, check to see that the display status of the HP-41C is set as specified and check to see that all applicable flags are set or clear as specified.

2. Set the HP-41C to PRGM mode (press the **PRGM** key) and press **■ GTO** **• •** to prepare the calculator for the new program.
3. Begin keying in the program. Following is a list of hints that will help you when you key in your programs from the program listings in this handbook.

- a. When you see " (quote marks) around a character or group of characters in the program listing, those characters are ALPHA. To key them in, simply press **ALPHA**, key in the characters, then press **ALPHA** again. So "SAMPLE" would be keyed in as **ALPHA "SAMPLE" ALPHA**.
- b. The diamond in front of each LBL instruction is only a visual aid to help you locate labels in the program listings. When you key in a program, ignore the diamond.
- c. The printer indication of divide sign is /. When you see / in the program listing, press **+**.
- d. The printer indication of the multiply sign is × . When you see × in the program listing, press **×**.
- e. The h character in the program listing is an indication of the **APPEND** function. When you see h, press **■ APPEND** in ALPHA mode (press **■** and the K key).
- f. All operations requiring register addresses accept those addresses in these forms:

nn (a two-digit number)

IND nn (INDIRECT: **■**, followed by a two-digit number)

X, Y, Z, T, or L (a STACK address: **•** followed by X, Y, Z, T, or L)

IND X, Y, Z, T or L (INDIRECT stack: **■ •** followed by X, Y, Z, T, or L)

Indirect addresses are specified by pressing **■** and then the indirect address. Stack addresses are specified by pressing **•** followed by X, Y, Z, T, or L. Indirect stack addresses are specified by pressing **■ •** and X, Y, Z, T, or L.

Printer Listing

```
01♦LBL "SAM
PLE"
02 "THIS IS
A"
03 "H-SAMPLE
"
04 AVIEW
05 6
06 ENTER↑
07 -2
08 /
09 ABS
10 STO IND
L
11 "R3="
12 ARCL 03
13 AVIEW
14 RTN
```

Keystrokes

■ LBL	ALPHA	SAMPLE	ALPHA
ALPHA	THIS IS A	ALPHA	
ALPHA	■ APPEND	SAMPLE	
■	AVIEW	ALPHA	
6			
ENTER↑			
2	CHS		
+			
XEQ	ALPHA	ABS	ALPHA
STO	■	•	L
ALPHA	R3=	■	ARCL
■	AVIEW		
ALPHA			
■	RTN		

Display

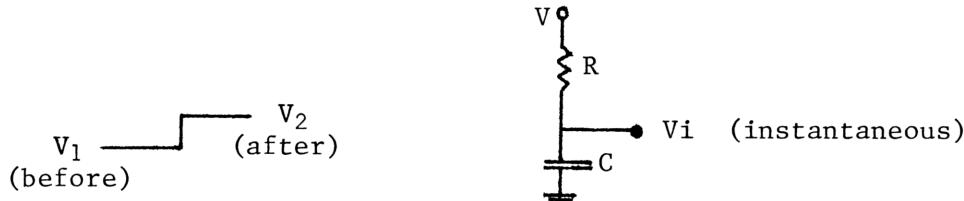
01 LBL^T SAMPLE
02^T THIS IS A
03^T H-SAMPLE
04 AVIEW
05 6
06 ENTER ↑
07 -2
08 /
09 ABS
10 STO IND L
11^T R3=
12 ARCL 03
13 AVIEW
14 RTN

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Compute the input impedance of a lossy transmission line terminated in Z_L .	
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RC TIMING

This program computes any one of the six variables shown, provided the other five are known.



V_1 = Voltage before step

C = Capacitance

V_2 = Voltage after step

Vi = Instantaneous voltage

R = Resistance

t = Time

All solutions are algebraically derived from this basic formula:

$$Vi = V_1 e^{-\frac{t}{RC}} + V_2 (1 - e^{-\frac{t}{RC}})$$

NOTE: For voltages across the resistor, remember that $V_R + V_C = V$ applies at all times.

Example:

A 555 type of integrated circuit timer uses an external RC configuration for time determination. When used as a one-shot its output pulse terminates when the capacitor charges to $2/3$ of the supply voltage. Until the pulse starts, the capacitor is shorted so $V_1 = 0$. Given a supply voltage of 12V, a $47\mu F$ capacitor, and you need a 1 second pulse, what size resistor should you use?

Keystrokes:

Display:

[XEQ] [ALPHA] SIZE [ALPHA] 007

$V1?$

[XEQ] [ALPHA] RC [ALPHA]

$V2?$

0 [R/S]

$VI?$

12 [R/S]

$C?$

8 [R/S]

$R?$

47 [EEX] 6 [CHS] [R/S]

$T?$

[R/S]

1.000 00

1 [R/S]

$R=19.37E3$

[XEQ] [ALPHA] R [ALPHA]

User Instructions

					SIZE: 007
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY	
1	Load program				
2	Begin execution and enter data, skip unknown by pressing [R/S].		[XEQ] RC	V1?	
		V ₁	[R/S]	V2?	
		V ₂	[R/S]	VI?	
		V _i	[R/S]	C?	
		C	[R/S]	R?	
		R	[R/S]	T?	
		t	[R/S]		
3	Execute for desired output:				
	V ₁		[XEQ] V1	V1=	
	V ₂		[XEQ] V2	V2=	
	V _i		[XEQ] VI	VI=	
	C		[XEQ] C	C=	
	R		[XEQ] R	R=	
	t		[XEQ] T	T=	
4	To vary one or more parameters simply place the new value in the appropriate register				
		V ₁	[STO] 01		
		V ₂	[STO] 02		
		V _i	[STO] 03		
		C	[STO] 04		
		R	[STO] 05		
		t	[STO] 06		
	Go to step 3				

Program Listings

01♦LBL "RC"		52 XEQ 00	
02 ENG 3		53 RCL 02	
03 CF 00		54 *	V ₁
04 "V1?"		55 RCL 03	
05 PROMPT	Initialize registers	56 X<>Y	
06 STO 01		57 -	
07 "V2?"		58 STO 00	
08 PROMPT		59 XEQ 03	
09 STO 02		60 RCL 00	
10 "VI?"		61 X<>Y	
11 PROMPT		62 /	
12 STO 03		63 STO 01	
13 "C?"		64 "V1="	
14 PROMPT		65 GTO 05	
15 STO 04		66♦LBL C	
16 "R?"		67 XEQ 01	
17 PROMPT		68 RCL 05	C
18 STO 05		69 *	
19 "T?"		70 RCL 06	
20 PROMPT		71 X<>Y	
21 STO 06		72 /	
22 STOP		73 STO 04	
23♦LBL "V2"		74 "C="	
24 XEQ 03	V ₂	75 GTO 05	
25 RCL 01		76♦LBL "R"	
26 *		77 XEQ 01	
27 RCL 03		78 RCL 04	R
28 X<>Y		79 *	
29 -		80 RCL 06	
30 STO 00		81 X<>Y	
31 XEQ 00		82 /	
32 RCL 00		83 STO 05	
33 X<>Y		84 "R="	
34 /		85 GTO 05	
35 STO 02		86♦LBL "T"	
36 "V2="		87 XEQ 01	
37 GTO 05		88 RCL 04	t
38♦LBL "VI"	V _i	89 RCL 05	
39 XEQ 03		90 *	
40 RCL 01		91 *	
41 *		92 STO 06	
42 STO 00		93 "T="	
43 XEQ 00		94♦LBL 05	
44 RCL 02		95 ARCL X	
45 *		96 AVIEW	
46 RCL 00		97 STOP	
47 +		98♦LBL 01	
48 STO 03		99 1	
49 "VI="		100 RCL 03	
50 GTO 05		101 RCL 01	
51♦LBL "V1"		102 -	

Program Listings

103 RCL 02		51	
104 RCL 01			
105 -			
106 /	$-\ln \left[1 - \frac{V_2 - V_1}{V_1 - V_2} \right]$		
107 -			
108 LN			
109 CHS			
110 RTN			
111♦LBL 00			
112 SF 05			
113 1	$e^{-t/RC}$ or $1 - e^{-t/RC}$	60	
114♦LBL 03			
115 RCL 06			
116 RCL 05			
117 RCL 04			
118 *			
119 /			
120 CHS			
121 E↑X			
122 FS?C 05		70	
123 -			
124 RTN			
125 .END.			
30		80	
40		90	
50		00	

RC TIMING

PROGRAM REGISTERS NEEDED: 31

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ROW 1 (1 - 4)



ROW 2 (4 - 10)



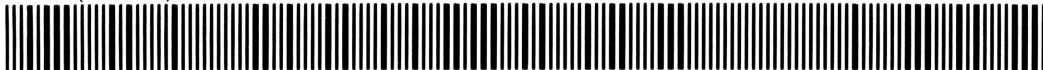
ROW 3 (11 - 19)



ROW 4 (19 - 24)



ROW 5 (24 - 34)



ROW 6 (35 - 38)



ROW 7 (39 - 47)



ROW 8 (48 - 51)



ROW 9 (52 - 60)



ROW 10 (61 - 67)



ROW 11 (67 - 76)



ROW 12 (76 - 83)



ROW 13 (84 - 87)



ROW 14 (88 - 97)



ROW 15 (98 - 110)



ROW 16 (111 - 122)



ROW 17 (122 - 125)



FREQUENCY RESPONSE OF A TRANSFER FUNCTION

For transfer function of the form:

$$G(s) = \frac{K_1(Z_2s + 1)}{s^{N_3}(Z_4s + 1)(Z_5s + 1)\left(\frac{s^2}{\omega_7^2} + \frac{2Z_6s}{\omega_7} + 1\right)}$$

the program computes $\angle G(j\omega)$, $|G(j\omega)|$ and $\log |G(j\omega)|$ for any input frequency ω .

Parameters K_1 , Z_2 , N_3 , Z_4 , Z_5 , Z_6 and ω_7 are stored in registers 01, 02, 03, 04, 05, 06, and 07 respectively.

NOTE: For type 0 systems, enter $N_3 = 0$. Z_2 , Z_4 and/or Z_5 can be entered as 0. If there is no quadratic term, enter Z_6 as 0 and ω_7 very large compared to $\frac{1}{Z_5}$, where Z_5 is the smallest first order term used (other than zero).

Example:

Find $|G(j\omega)|$, $\angle G(j\omega)$ and $\log |G(j\omega)|$ for $G(s) = \frac{12(s + 0.6)}{s(s + 1)(s^2 + 6s + 36)}$ frequency 0.01 rad/sec.

First put $G(s)$ into proper form: $G(s) = \frac{.2(1.67s + 1)}{s(s + 1)[(\frac{s}{6})^2 + (\frac{s}{6}) + 1]}$

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 010

[XEQ] [ALPHA] FREQ [ALPHA]

.2 [R/S]

Display:

K1=?

1.67 [R/S]

Z2=?

1 [R/S]

N3=?

1 [R/S]

Z4=?

0 [R/S]

Z5=?

.5 [R/S]

Z6=?

6 [R/S]

W=?

.01 [R/S]

$\angle G(j\omega) = 20.00$

[R/S]

$\angle G(j\omega) = -89.71$

[R/S]

$\log G = 1.30$

User Instructions

Program Listings

01♦LBL "FRE		51 1
02 FIX 2		52 R-P
03 "K1=?"	Store data	53 XEQ 01
04 PROMPT		54 RCL 08
05 STO 01		55 RCL 03
06 "Z2=?"		56 Y↑X
07 PROMPT		57 *
08 STO 02		58 X<>Y
09 "N3=?"		59 RCL 03
10 PROMPT		60 90
11 STO 03		61 *
12 "Z4=?"		62 +
13 PROMPT		63 CHS
14 STO 04		64 X<>Y
15 "Z5=?"		65 1/X
16 PROMPT		66 RCL 02
17 STO 05		67 RCL 08
18 "Z6=?"		68 *
19 PROMPT		69 RCL 01
20 STO 06		70 *
21 "W7=?"		71 RCL 01
22 PROMPT		72 R-P
23 STO 07		73 XEQ 01
24♦LBL "W2"		74 "G<JW>="
25 "W=?"		75 ARCL X
26 PROMPT		76 AVIEW
27 STO 08	-----	77 STOP
28 RCL 06		78 STO 09
29 RCL 07		79 X<>Y
30 /	$\left[\frac{S^2}{\omega_7^2} + \frac{2Z_6}{\omega_7} \right] + 1$	80 "zG<JW>="
31 2		-----
32 *		81 ARCL X
33 RCL 08		82 AVIEW
34 *		83 STOP
35 1		84 RCL 09
36 RCL 08		85 LOG
37 RCL 07		86 "LOG G="
38 /		87 ARCL X
39 X↑2		88 AVIEW
40 -		89 STOP
41 R-P	-----	90♦LBL 01
42 RCL 05		91 X<>Y
43 RCL 08	$Z_5 S + 1$	92 RDN
44 *		93 *
45 1		94 RDN
46 R-P		95 +
47 XEQ 01		96 RT
48 RCL 04		97 RTN
49 RCL 08	$Z_4 S + 1$	98 .END.
50 *		00

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS			
#	NAME	DECIMAL	SIZE		TOT. REG.	USER MODE
			ENG	DEG	34	ON OFF
00	K ₁	50		X	2	X
	Z ₂				SCI	
	N ₃				RAD	
	Z ₄				GRAD	
05	Z ₅	55				
	Z ₆					
	ω ₇					
	ω					
	G(jω)					
10		60				
15		65				
20		70				
25		75				
30		80				
35		85				
ASSIGNMENTS						
#	FUNCTION	KEY	FUNCTION	KEY	FUNCTION	KEY
40						
45						

FREQUENCY RESPONSE OF
A TRANSFER FUNCTION
PROGRAM REGISTERS NEEDED: 25

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ROW 1 (1 - 3)



ROW 2 (3 - 9)



ROW 3 (9 - 15)



ROW 4 (15 - 20)



ROW 5 (21 - 24)



ROW 6 (25 - 34)



ROW 7 (35 - 47)



ROW 8 (47 - 56)



ROW 9 (57 - 68)



ROW 10 (69 - 74)



ROW 11 (74 - 80)



ROW 12 (80 - 86)



ROW 13 (86 - 96)

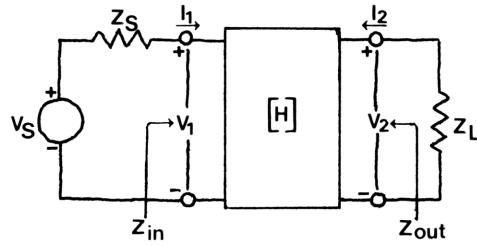


ROW 14 (97 - 98)



TRANSISTOR AMPLIFIER PERFORMANCE

This program computes certain small-signal properties of a transistor amplifier given the h-parameter matrix and the source and load impedances. Properties computed are: current and voltage gains, and input and output impedances.



Equations:

Definition of h-parameter matrix

$$\begin{bmatrix} v_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} h_i & h_r \\ h_f & h_0 \end{bmatrix} \begin{bmatrix} i_1 \\ v_2 \end{bmatrix}$$

Current gain

$$A_i = \frac{i_2}{i_1} = \frac{-h_f}{1 + h_0 Z_L}$$

Voltage gain

$$A_v = \frac{v_2}{v_1} = \frac{A_i Z_L}{Z_{in}}$$

Voltage gain with source resistor

$$A_{vs} = \frac{v_2}{v_s} = \frac{A_i Z_L}{Z_{in} + Z_s}$$

Input impedance

$$Z_{in} = h_i + h_r Z_L A_i$$

Output impedance

$$Z_{out} = \frac{h_i + Z_s}{h_0 h_i + h_0 Z_s - h_f h_r}$$

Example:

What are the small-signal properties of a transistor which has the following h-parameter matrix and has source and load impedances of 1000 and 10,000 ohms, respectively?

$$[h] = \begin{bmatrix} 1100 & 250E-6 \\ 50 & 25E-6 \end{bmatrix}$$

Keystrokes:

```
[USER]
[//][FIX] 2
[XEQ][ALPHA] SIZE [ALPHA] 023
0 [ENTER↑] 1100 [ENTER↑] 11
[XEQ][ALPHA] HP [ALPHA]
0 [ENTER↑] 250 [EEX] 6 [CHS]
[ENTER↑] 12 [XEQ][ALPHA] HP [ALPHA]
0 [ENTER↑] 50 [ENTER↑]
21 [XEQ][ALPHA] HP [ALPHA]
0 [ENTER↑] 25 [EEX] 6 [CHS]
[ENTER↑] 22 [XEQ][ALPHA] HP [ALPHA]
0 [ENTER↑] 1000 [ENTER ]
0 [ENTER↑] 10000 [XEQ][ALPHA] Z [ALPHA]
[A] MAG=-40.00 (Ai)
[R/S] Δ=0.00
[B] MAG=-400.00 (Av)
[R/S] Δ=0.00
[C] MAG=-200.00 (Avs)
[R/S] Δ=0.00
[D] MAG=1,000.00 (Zin)
[R/S] Δ=0.00
[E] MAG=52,500.00 (Zout)
[R/S]
```

Display:

(set USER mode)

User Instructions

Program Listings

01♦LBL "HP"		51 RCL 17	
02 STO 00		52 RCL 16	
03 3		53 XEQ 02	
04 -	Store matrix	54 RCL 03	
05 STO 01		55 RCL 02	
06 RDN		56 R-P	
07 STO IND		57 1/X	
08		58 X<>Y	
09 RDN		59 CHS	
10 STO IND		60 X<>Y	
11♦LBL "Z"		61 XEQ 01	
12 STO 14		62 GTO 20	
13 RDN		63♦LBL B	
14 STO 15		64 XEQ b	
15 RDN		65 1/X	
16 STO 16		66 X<>Y	Voltage gain
17 RDN		67 CHS	
18 STO 17		68 X<>Y	
19 CF 05		69 RCL 03	
20 STOP		70 RCL 02	
21♦LBL E		71 XEQ 01	
22 RCL 19		72 GTO 20	
23 RCL 22		73♦LBL C	
24 RCL 08		74 XEQ b	
25 RCL 11		75 RCL 17	
26 XEQ 01		76 RCL 16	
27 P-R		77 XEQ 02	Voltage gain
28 STO 02		78 1/X	
29 X<>Y		79 X<>Y	with source
30 STO 03		80 CHS	resistor
31 RCL 19		81 X<>Y	
32 RCL 22		82 RCL 03	
33 RCL 17		83 RCL 02	
34 RCL 16		84 XEQ 01	
35 XEQ 01		85 GTO 20	
36 P-R		86♦LBL D	
37 ST+ 02		87 CF 04	
38 X<>Y		88♦LBL 03	
39 ST+ 03		89 SF 05	
40 RCL 18		90 XEQ 00	
41 RCL 21		91 RCL 15	
42 RCL 09		92 RCL 14	
43 RCL 12		93 XEQ 01	
44 XEQ 01		94 RCL 09	
45 P-R		95 RCL 12	
46 ST- 02		96 XEQ 01	
47 X<>Y		97 RCL 08	
48 ST- 03		98 RCL 11	
49 RCL 08		99 XEQ 02	
50 RCL 11		100 FS? 04	
		101 RTN	
		102 GTO 20	

Program Listings

```

103♦LBL A
104 CF 05
105♦LBL 00
106 RCL 19
107 RCL 22
108 RCL 15
109 RCL 14
110 XEQ 01
111 P-R
112 1
113 +
114 R-P
115 RCL 18
116 CHS
117 RCL 21
118 1/X
119 XEQ 01
120 1/X
121 CHS
122 FS? 05
123 RTN
124 GTO 20
125♦LBL 01
126 X<>Y
127 RDN
128 *
129 RDN
130 +
131 R↑
132 RTN
133♦LBL 02
134 P-R
135 RDN
136 RDN
137 P-R
138 R↑
139 R↑
140 X<>Y
141 RDN
142 +
143 RDN
144 +
145 R↑
146 R-P
147 RTN
148♦LBL 20
149 "MAG="
150 XEQ 01
151 X<>Y
152 "z="
153♦LBL 01
154 ARCL X

```

Current gain

Multiply complex numbers

Add complex numbers

Display

```

155 AVIEW
156 STOP
157 RTN
158♦LBL b
159 SF 05
160 XEQ 00
161 RCL 15
162 RCL 14
163 XEQ 01
164 STO 02
165 X<>Y
166 STO 03
167 SF 04
168 XEQ 03
169 RTN
170 .END.

```

70

80

90

00

TRANSISTOR AMPLIFIER
PERFORMANCE
PROGRAM REGISTERS NEEDED: 40

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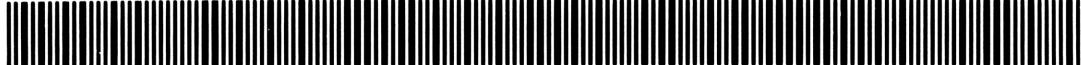
ROW 1 (1 - 7)



ROW 2 (8 - 15)



ROW 3 (16 - 23)



ROW 4 (23 - 32)



ROW 5 (32 - 39)



ROW 6 (39 - 46)



ROW 7 (47 - 54)



ROW 8 (55 - 63)



ROW 9 (63 - 71)



ROW 10 (72 - 77)



ROW 11 (77 - 85)



ROW 12 (85 - 92)



ROW 13 (93 - 99)



ROW 14 (100 - 106)



ROW 15 (107 - 115)



ROW 16 (116 - 124)



ROW 17 (124 - 135)



ROW 18 (136 - 148)



TRANSISTOR AMPLIFIER
PERFORMANCE

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ROW 19 (148 - 152)



ROW 20 (153 - 160)



ROW 21 (161 - 168)

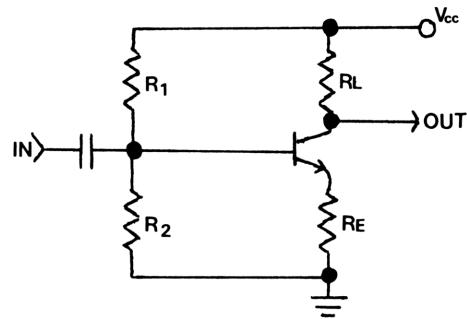


ROW 22 (169 - 170)



CLASS "A" TRANSISTOR AMPLIFIER BIAS OPTIMIZATION

This program is an automation of the method of bias optimization described in "Designing Class "A" Amplifiers to Meet Specified Tolerances," by Ward J. Helms (Electronics, August 8, 1974). The program requires the user to specify a set of parameters from which it determines, by an iterative technique, the optimum values for R_1 , R_2 , R_E , and R_L . The minimum power gain is also computed.



Equations:

First, values are specified for the following parameters:

- ΔI_{CQ} = maximum desired percentage variation of quiescent current
- T_{Amax} = maximum ambient temperature (use the maximum cast temperature for a transistor mounted on a heat sink)
- T_{Amin} = minimum ambient temperature
- T_{Jmax} = maximum junction temperature rating
- P_D = maximum rated power dissipation at 25°C
- I_1 = collector current, usually selected for convenience so that I_1 and 10 I_1 bracket the expected operating point
- ΔV_{BE} = typical base-emitter voltage change over the range of I_1 to 10 I_1 at 25°C
- V_{BE1min} = minimum base-emitter voltage at I_1 , 25°C
- V_{BE1max} = maximum base-emitter voltage at I_1 , 25°C

The transistor's thermal resistance is calculated:

$$\theta_{JA} = (T_{max} - 25^\circ\text{C})/P_D$$

and the minimum load resistance and emitter resistance are estimated:

$$R_{L1} = \frac{\theta_{JA} V_{CC}^2}{4.4(T_{Jmax} - T_{Amax})} = R_{Ln}$$

$$R_{E1} = 0.1 R_{L1} = R_{En}$$

Next, the quiescent, maximum, and minimum collector currents are calculated:

$$I_{CQ} = \frac{V_{CC}}{2(R_{Ln} + R_{En})}$$

$$I_{Cmax} = I_{CQ}(1 + \Delta I_{CQ})$$

$$I_{Cmin} = I_{CQ}(1 - \Delta I_{CQ})$$

From these, we can calculate the base-emitter voltage under hot, high-current conditions (V_{BE1X}) and under cold, low-current conditions (V_{BE1N}).

$$T_{max} = \theta_{JA} I_{CQ} \frac{V_{CC}}{2} + T_{Amax}$$

$$V_{BE1X} = V_{BE1min} + \Delta V_{BE} \log \frac{I_{Cmax}}{I_1} - 0.0022(T_{max} - 25^\circ C)$$

$$T_{min} = \theta_{JA} I_{CQ} \frac{V_{CC}}{2} (1 - (\Delta I_{CQ})^2) + T_{Amin}$$

$$V_{BE1N} = V_{BE1max} + \Delta V_{BE} \log \frac{I_{Cmin}}{I_1} - 0.0022(T_{min} - 25^\circ C)$$

Now, a better estimate for the emitter resistance can be made:

$$R_{E(n+1)} = \frac{-2(V_{BE1X} - V_{BE1N})}{I_{Cmax} - I_{Cmin}}$$

From this point, if $V_{BE1X} > V_{BE1N}$, then R_E is set to zero, R_L is increased by 10%, and the design procedure is repeated. Iterations continue until

$\frac{R_{E(n+1)} - R_{En}}{R_{En}} < .5\%$. If at any time the condition $T_{max} > T_{Jmax}$ occurs, R_L is increased by 10%.

When the iterative procedure is complete, T_{max} , I_{Cmax} , T_{min} , and I_{Cmin} are displayed.

Then values for

h_{FEmax} = maximum worst-case current gain at T_{max} or T_{min} and I_{Cmax} or I_{Cmin} and

h_{FEmin} = minimum worst-case current gain at T_{max} or T_{min} and I_{Cmax} or I_{Cmin}

are determined from the transistor's data sheet and the Thevenin-equivalent resistance (R_B) and voltage (V_{BB}) of the amplifier's bias network are calculated:

$$R_B = \frac{h_{FEmax} h_{FEmin} [R_E(n+1) (I_{Cmax} - I_{Cmin}) + V_{BEX} - V_{BEN}]}{h_{FEmax} I_{Cmin} - h_{FEmin} I_{Cmax}}$$

$$V_{BB} = V_{BEN} + I_{Cmin} \left(\frac{R_B}{h_{FEmin}} + R_{E(n+1)} \right)$$

Now the bias resistors R_1 and R_2 are calculated:

$$R_1 = \frac{R_B V_{CC}}{V_{BB}}$$

$$R_2 = \frac{R_B V_{CC}}{(V_{CC} - V_{BB})}$$

Finally, the minimum power gain and minimum signal power are calculated:

$$A_p = \frac{R_B R_L h_{FEmin}}{R_E (R_B + h_{FEmin} R_E)}$$

$$P_S = (1 - \Delta I_{CQ})^2 \left(\frac{V_{CC}^2 R_L}{8(R_L + R_E)^2} \right)$$

Example:

A single-stage class "A" amplifier is connected to a 30-V power supply. Calculate the maximum power output and maximum power gain obtained from a transistor over an ambient temperature range of 0°C to 70°C, with a maximum quiescent-current variation of ±20%.

From the transistor's data sheet:

$$T_{Jmax} \quad 150^\circ\text{C}$$

$$P_D \quad = 0.36 \text{ W}$$

$$\Delta V_{BE} \quad = 0.10 \text{ v from 3 to 30 mA}$$

$$V_{BE1min} \quad = 0.52 \text{ v at 3 mA at } 25^\circ\text{C}$$

$$V_{BE1max} \quad = 0.72 \text{ v at 3 mA at } 25^\circ\text{C}$$

$$I_1 \quad = 0.001 \text{ A}$$

Keystrokes:	Display:
[XEQ] [ALPHA] SIZE [ALPHA]	
017	
30 [STO] 00	
.2 [STO] 01	
70 [STO] 02	
0 [STO] 03	
150 [STO] 04	
.36 [STO] 05	
.001 [STO] 06	
.1 [STO] 07	
.52 [STO] 08	
.72 [STO] 09	
[XEQ] [ALPHA] BIAS [ALPHA]	T=148.E0
[R/S]	I=18.0E-3
[R/S]	T=74.8E0
[R/S]	I=12.0E-3
[R/S]	H MAX?
600 [R/S]	H MIN?
100 [R/S]	RE=115.E0
[R/S]	RL=888.E0
[R/S]	R2=4.18E3
[R/S]	R1=45.0E3
[R/S]	AP=22.9E0

User Instructions

SIZE: 017				
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Load program			
2	Store data			
		V _{CC}	[STO] 00	
		ΔI _{CQ}	[STO] 01	
		T _{Amax} °C	[STO] 02	
		T _{Amin} °C	[STO] 03	
		T _{Jmax}	[STO] 04	
		P _D	[STO] 05	
		I ₁	[STO] 06	
		ΔV _{BE}	[STO] 07	
		V _{BE1min}	[STO] 08	
		V _{BE1max}	[STO] 09	
3	Compute maximum and minimum temperatures and currents			
			[XEQ] BIAS	T= (max)
			[R/S]	I= (max)
			[R/S]	T= (min)
			[R/S]	I= (min)
			[R/S]	H MAX?
4	Input maximum and minimum h _{FE} to compute resistor values	h _{FEmax}	[R/S]	H MIN?
		h _{FEmin}	[R/S]	RE=
			[R/S]	RL=
			[R/S]	R2=
			[R/S]	R1=
	and minimum power gain		[R/S]	AP=

Program Listings

91+LBL "BIA		51 1	
92 ENG 2	⁰ JA	52 RCL 01	
93 RCL 04		53 X \neq 2	
94 25		54 -	
95 -		55 2	
96 RCL 05		56 *	
97 *		57 RCL 10	
98 STO 05		58 *	
99 RCL 00		59 RCL 05	
10 X \uparrow 2		60 *	
11 *		61 RCL 00	
12 RCL 04	R _{L1}	62 *	
13 RCL 02		63 RCL 03	
14 -		64 +	
15 4 .4		65 XEQ 03	
16 *		66 CHS	
17 *		67 1	
18 STO 13		68 RCL 01	
19 .1		69 -	
20 *	R _{E1}	70 XEQ 04	
21 STO 14		71 RCL 09	
22+LBL 00		72 +	
23 RCL 00		73 STO 16	
24 2	Loop	74 RCL 15	
25 *		75 X>Y?	
26 ENTER†		76 GTO 02	
27 ENTER†		77 -	
28 RCL 13		78 RCL 10	
29 RCL 14		79 *	
30 +		80 RCL 01	
31 *		81 *	
32 STO 10		82 RCL 14	
33 RCL 05		83 X<Y	
34 *		84 STO 14	
35 *		85 CHS	
36 RCL 02		86 .5	
37 +		87 X<=Y?	
38 RCL 04		88 GTO 00	
39 X<Y		89 FS? 01	
40 X>Y?		90 GTO 01	
41 GTO 05		91 SF 01	End Loop
42 XEQ 03		92 GTO 00	
43 CHS		93+LBL 01	
44 RCL 01		94 CF 01	
45 1		95 "H MAX?"	
46 +		96 PROMPT	
47 XEQ 04		97 "H MIN?"	
48 RCL 00		98 PROMPT	
49 +		99 STO 12	
50 STO 15		100 X<Y	
		101 STO 11	

R_B

Program Listings

102 RCL 01		153 LASTX	
103 2		154 RCL 03	
104 *		155 -	
105 RCL 10		156 /	
106 *		157 RCL 13	
107 RCL 14		158 RCL 14	
108 *		159 "RE="	
109 RCL 15		160 XEQ 02	
110 +		161 "RL="	Display
111 RCL 16		162 XEQ 02	
112 -		163 "R2="	
113 RCL 12		164 XEQ 02	
114 *		165 "R1="	
115 RCL 11		166 XEQ 02	
116 *		167 /	
117 1		168 RCL 12	
118 RCL 01		169 *	
119 -		170 RCL 02	Power gain
120 RCL 11		171 *	
121 *		172 LASTX	
122 1		173 RCL 14	
123 RCL 01		174 RCL 12	
124 +		175 *	
125 RCL 12		176 +	
126 *		177 /	
127 -		178 LOG	
128 /		179 10	
129 RCL 10		180 *	
130 /		181 "AP="	
131 STO 02		182 *LBL 02	
132 RCL 12		183 ARCL X	
133 /		184 AVIEW	
134 RCL 14	V _{BB}	185 STOP	
135 +		186 RDN	
136 RCL 19		187 RTN	
137 *		188 *LBL 03	
138 1		189 FS? 01	
139 RCL 01		190 XEQ A	
140 -		191 25	Temperature
141 *		192 -	calculations
142 RCL 16		193 2.2 E-3	
143 +		194 *	
144 STO 03		195 RTN	
145 RCL 00		196 *LBL A	
146 X<>Y		197 "T="	
147 /	R ₁	198 GTO D	
148 RCL 02		199 *LBL 04	
149 *		200 RCL 10	
150 RCL 02		201 *	
151 RCL 00	R ₂	202 FS? 01	
152 *		203 XEQ I	

Program Listings

204 RCL 06		51	
205 /			
206 LOG			
207 RCL 07			
208 *			
209 +			
210 RTN			
211 *LBL I			
212 "I="			
213 *LBL D	Display	60	
214 RRCL X			
215 AVIEW			
216 STOP			
217 RTN			
218 STO 02			
219 0			
220 STO 14			
221 *LBL 05			
222 1.1			
223 ST* 13			
224 GTO 00		70	
225 .END.			
30		80	
40		90	
50		00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS			
#	NAME	INITIAL VALUE	DESCRIPTION	STATUS		USER MODE	
				SIZE	TOT. REG.	ENG	FIX
				X	63		
						ON	OFF
							X
00	V _{CC}	50		SIZE	017	TOT. REG.	63
	ΔI _{CQ}			ENG	2	FIX	
	T _{Amin}			SCI		ON	
	T _{Amax}			RAD		OFF	
	T _{Jmax}			GRAD			
05	P ₀ θ _{JA}	55		FLAGS			
	I ₁			#	INIT S/C	SET INDICATES	CLEAR INDICATES
	ΔV _{BE}			01		Branch	No-Branch
	V _{BE1max}						
	V _{BE1min}						
10	I _{CQ}	60					
	h _{FEmax}						
	h _{FEmin}						
	R _{L1}						
	R _{E1}						
15	Used	65					
	Used						
20		70					
25		75					
30		80					
35		85					
ASSIGNMENTS				FUNCTION KEY FUNCTION KEY			
40		90					
45		95					

CLASS "A" TRANSISTOR AMPLIFIER
BIAS OPTIMIZATION
PROGRAM REGISTERS NEEDED: 46

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ROW 1 (1 - 4)



ROW 2 (5 - 15)



ROW 3 (16 - 27)



ROW 4 (28 - 40)



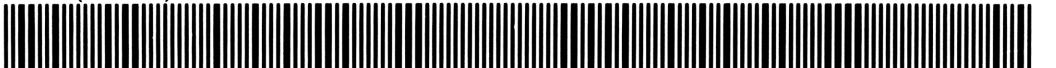
ROW 5 (41 - 48)



ROW 6 (49 - 61)



ROW 7 (62 - 70)



ROW 8 (71 - 81)



ROW 9 (82 - 90)



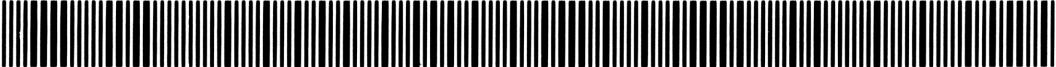
ROW 10 (91 - 95)



ROW 11 (95 - 101)



ROW 12 (102 - 113)



ROW 13 (114 - 126)



ROW 14 (127 - 139)



ROW 15 (140 - 151)



ROW 16 (152 - 160)



ROW 17 (160 - 164)



ROW 18 (164 - 170)



CLASS "A" TRANSISTOR AMPLIFIER
BIAS OPTIMIZATION

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ROW 19 (171 - 181)



ROW 20 (181 - 190)



ROW 21 (190 - 195)



ROW 22 (196 - 202)



ROW 23 (203 - 212)



ROW 24 (212 - 221)



ROW 25 (222 - 225)



ACTIVE FILTER DESIGN

This program computes element values for the standard active filter circuits shown. The user selects corner frequency f_0 or center frequency f_0 , midband gain A , peaking factor α , and a capacitor C . The program then prints out a list of elements which form the desired filter.

Equations:

$$\alpha = \frac{1}{Q} = 2\zeta, \text{ where } Q \text{ is quality factor and } \zeta \text{ is damping factor.}$$

Low pass filter

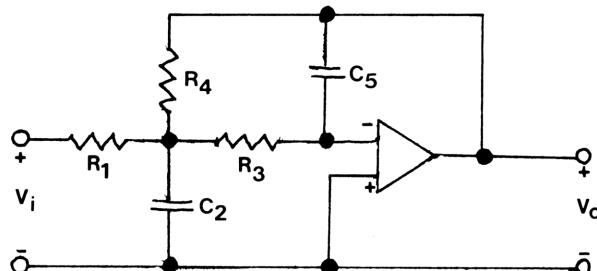
$$C_5 = C$$

$$C_2 = \frac{4C(A + 1)}{\alpha^2}$$

$$R_1 = \frac{\alpha}{4A\pi f_0 C}$$

$$R_3 = \frac{\alpha}{4\pi f_0 C(A + 1)} = \frac{A}{A + 1} R_1$$

$$R_4 = AR_1$$



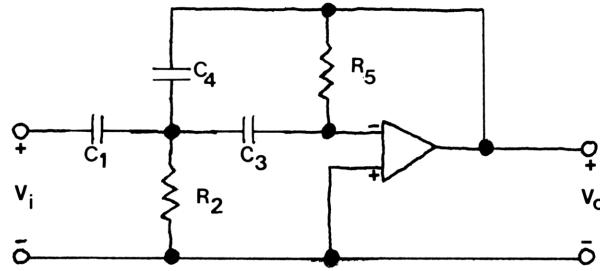
High pass filter

$$C_1 = C_3 = C$$

$$C_4 = \frac{C}{A}$$

$$R_2 = \frac{\alpha}{2\pi f_0 C (2 + \frac{1}{A})}$$

$$R_5 = \frac{2A + 1}{\alpha 2\pi f_0 C}$$



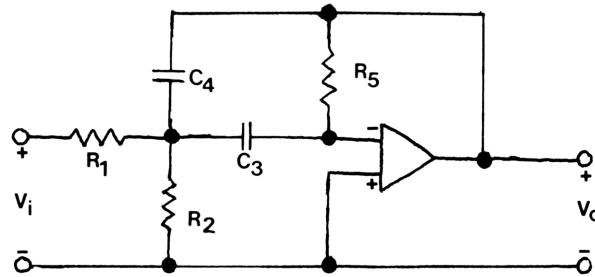
Bandpass filter

$$C_3 = C_4 = C$$

$$R_1 = \frac{1}{A 2\pi f_0 C \alpha}$$

$$R_2 = \frac{1}{(\frac{2}{\alpha} - A) 2\pi f_0 C \alpha}$$

$$R_5 = \frac{2}{\alpha 2\pi f_0 C}$$



Example:

Design a high-pass active filter with the following parameters:

$$f_0 = 10 \text{ Hz}$$

$$A = 10$$

$$\alpha = 1$$

$$C = 1 \mu\text{F}$$

Keystrokes: Display:

[XEQ] [ALPHA] SIZE [ALPHA]	
[XEQ] [ALPHA] AF [ALPHA]	F0?
10 [R/S]	A?
10 [R/S]	PF?
1 [R/S]	C?
1 [EEX] 6 [CHS] [R/S]	1.000 -06
[XEQ] [ALPHA] HP [ALPHA]	C1=C3=1.000E-6
[R/S]	C4=100.0E-9
[R/S]	R2=7.579E3
[R/S]	R5=334.2E3

User Instructions

Program Listings

01 *LBL "AF"		52 *	
02 ENG 3		53 "R4="	R ₄
03 "FO?"		54 XEQ 05	
04 PROMPT		55 RCL 03	C ₅
05 STO 00	Initialization	56 "C5="	
06 "R?"		57 GTO 05	
07 PROMPT		58 *LBL "HP"	-----
08 STO 01		59 RCL 03	High pass
09 "PF?"		60 "C1=C3="	C ₁ & C ₃
10 PROMPT		61 XEQ 05	
11 STO 02		62 RCL 01	
12 "C?"		63 /	C ₄
13 PROMPT		64 "C4="	
14 STO 03		65 XEQ 05	
15 STOP		66 XEQ A	
16 *LBL "LP"	Low pass	67 RCL 02	
17 RCL 02		68 X<>Y	
18 2		69 /	
19 /		70 2	
20 RCL 01	R ₁	71 RCL 01	R ₂
21 /		72 1/X	
22 XEQ A		73 +	
23 /		74 /	
24 STO 05		75 "R2="	
25 "R1="		76 XEQ 05	
26 XEQ 05	-----	77 RCL 03	
27 RCL 03		78 RCL 01	
28 4		79 2	
29 *		80 *	R ₅
30 RCL 01	C ₂	81 1	
31 1		82 +	
32 +		83 RCL 02	
33 *		84 /	
34 RCL 02		85 RCL 04	
35 X†2		86 /	
36 /		87 "R5="	
37 "C2="		88 GTO 05	
38 XEQ 05		89 *LBL "BP"	-----
39 RCL 02		90 XEQ A	Band pass
40 2		91 RCL 01	
41 /	R ₃	92 *	R ₁
42 RCL 01		93 RCL 02	
43 1		94 *	
44 +		95 1/X	
45 /		96 "R1="	
46 RCL 04		97 XEQ 05	
47 /		98 2	
48 "R3="		99 RCL 02	
49 XEQ 05		100 X†2	
50 RCL 01		101 /	
51 RCL 05		102 RCL 01	R ₂

Program Listings

103 --			51	
104 RCL 04				
105 *				
106 RCL 02				
107 *				
108 1/X				
109 "R2="				
110 XEQ 05				
111 RCL 03	C ₃ & C ₄			
112 "C3=C4="				
113 XEQ 05			60	
114 2				
115 RCL 02	R ₅			
116 /				
117 RCL 04				
118 /				
119 "R5="				
120 *LBL 05		-----		
121 ARCL X		Display		
122 AVIEW			70	
123 STOP				
124 RTN				
125 *LBL A		-----		
126 2		2πf ₀ C		
127 PI				
128 *				
129 RCL 00				
130 *				
131 RCL 03				
132 *				
133 STD 04			80	
134 RTN				
135 .END.				
40			90	
50			00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS				
00	f ₀	50		SIZE	006	TOT. REG.	40	USER MODE
	A			ENG	3	FIX		ON
	α			DEG	X	SCI		OFF
	C					RAD		GRAD
05	2πf ₀ C			FLAGS				
05	R1 (LP only)	55		#	INIT S/C	SET INDICATES	CLEAR INDICATES	
10		60						
15		65						
20		70						
25		75						
30		80						
35		85		ASSIGNMENTS				
40		90		FUNCTION	KEY	FUNCTION	KEY	
45		95						

ACTIVE FILTER DESIGN

PROGRAM REGISTERS NEEDED: 35

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ROW 1 (1 - 4)



ROW 2 (5 - 12)



ROW 3 (12 - 18)



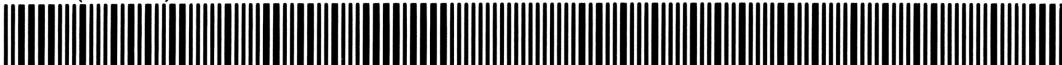
ROW 4 (19 - 26)



ROW 5 (26 - 37)



ROW 6 (37 - 45)



ROW 7 (46 - 53)



ROW 8 (53 - 57)



ROW 9 (58 - 60)



ROW 10 (60 - 65)



ROW 11 (66 - 75)



ROW 12 (75 - 84)



ROW 13 (85 - 89)



ROW 14 (89 - 96)



ROW 15 (97 - 107)



ROW 16 (108 - 112)



ROW 17 (112 - 119)



ROW 18 (119 - 128)



ACTIVE FILTER DESIGN

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ROW 19 (129 - 135)



BUTTERWORTH FILTER DESIGN

This program computes component values for Butterworth filters between equal terminations. Inputs are termination resistance, passband characteristics, and attenuation at some out-of-band frequency.

Before the filter elements can be calculated, a normalized frequency must be computed from the desired cutoff or center frequency and passband characteristics. The normalized frequency is computed by one of these formulas:

Low Pass

$$\omega_n = \frac{\omega}{\omega_0}$$

High Pass

$$\omega_n = \frac{\omega_0}{\omega}$$

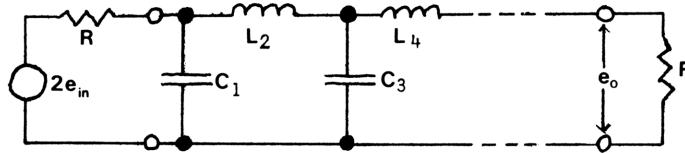
Band Pass

$$\omega_n = \frac{\omega^2 - \omega_0^2}{BW\omega}$$

Band Elimination

$$\omega_n = \frac{\omega_{BW}}{\omega_0^2 - \omega^2}$$

The basic form of the filter is this low-pass prototype:



whose elements are given by one of the following sets of formulas:

$$C_i = \frac{1}{\pi f_c R} \sin \frac{(2i-1)\pi}{2n}, \quad i = 1, 3, 5, \dots, n-1$$

$$L_i = \frac{R}{\pi f_c} \sin \frac{(2i-1)\pi}{2n}, \quad i = 2, 4, 6, \dots, n$$

where

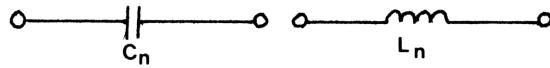
$$n = \text{INT} \left[\frac{1 + \ln(2 \times 10^{-\Delta dB/10} - 1)}{2 \ln(\omega/\omega_0)} \right]$$

Once the low-pass values have been calculated, if some other passband characteristic is desired, the components of the filter are changed by frequency transformation as shown.

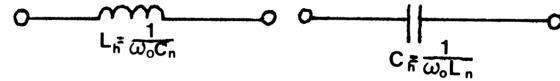
PASSBAND
CHARACTERISTIC

CIRCUIT ELEMENTS

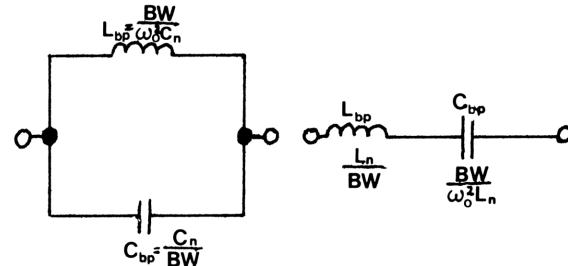
Low pass



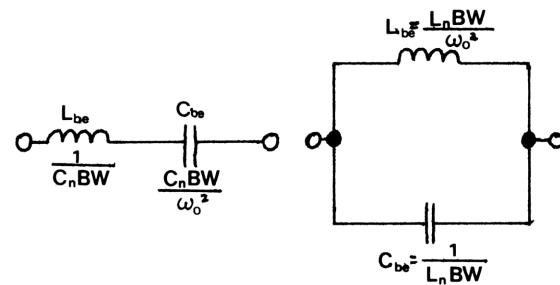
High pass



Band pass



Band elimination

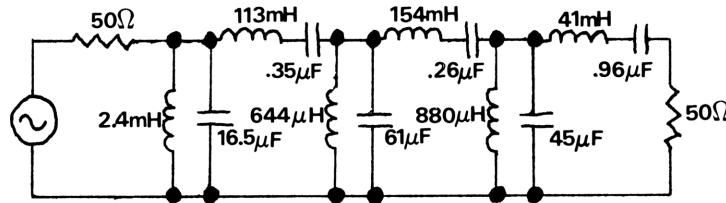


A bit of thought may be necessary to determine whether the L-C's are connected in series or parallel.

NOTE: The program will give erroneous results if asked to compute filter order when ΔdB is small (i.e., when $\Delta dB \sim \text{Loss } (\omega_0)$).

Example:

Design a 100 Hz wide Butterworth filter centered at 800 Hz with a 30 dB attenuation at 900 Hz. R_0 is 50Ω . The termination resistance R is 50Ω .



Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 016

[XEQ] [ALPHA] BUT [ALPHA]

50 [R/S]

800 [R/S]

[XEQ] [ALPHA] BP [ALPHA]

100 [R/S]

900 [R/S]

30 [R/S]

Display:

R=?

FO=?

BW=?

F1=?

A=?

N=6.000 E0

1.000 00

C=16.48 E-6

L=2.402 E-3

2.000 00

L=112.5 E-3

C=351.7 E-9

3.000 00

C=61.49 E-6

L=643.6 E-6

4.000 00

L=153.7 E-3

C=257.5 E-9

5.000 00

C=45.02 E-6

L=879.2 E-6

6.000 00

L=41.19 E-3

C=960.8 E-9

User Instructions

				SIZE: 016
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Load program			
2	Begin execution		[XEQ] BUT	R=?
		R, Ω	[R/S]	F0=?
		f ₀ , Hz	[R/S]	
3	Select filter type			
	Low pass		[XEQ] LP	F1=?
		f ₁ , Hz	[R/S]	A=?
		ΔdB	[R/S]	
	Go to step 4			
	High pass		[XEQ] HP	F1=?
		f ₁ , Hz	[R/S]	A=?
		ΔdB	[R/S]	
	Go to step 4			
	Band pass		[XEQ] BP	BW=?
		BW	[R/S]	F1=?
		f ₁ , Hz	[R/S]	A=?
		ΔdB	[R/S]	
	Go to step 4			
	Band elimination		[XEQ] BE	BW=?
		BW	[R/S]	F1=?
		f ₁ , Hz	[R/S]	A=?
		ΔdB	[R/S]	
4	Answer is displayed automatically			N=
			[R/S]	1.000 00
	(component number is displayed, then			C=
	component value.) Push [R/S] to continue		[R/S]	2.000 00
				L=

Program Listings

01♦LBL "BUT"		51 LN
"		52 ABS
02 ENG 3		53 ∕
03 RAD	Initialization	54 1
04 "R=?"		55 +
05 PROMPT		56 2
06 STO 05		57 ∕
07 "F0=?"		58 INT
08 PROMPT		59 STO 15
09 XEQ 10		60 STO 10
10 STO 07		61 "N=?"
11 STOP		62 ARCL X
12♦LBL "LP"		63 AVIEW
13 1		64 STOP
14 GTO 01		65♦LBL 08
15♦LBL "HP"		66 RCL 15
16 2		67 RCL 10
17 GTO 01		68 -
18♦LBL "BP"		69 1
19 3		70 +
20 GTO 01		71 STO 09
21♦LBL "BE"		72 2
22 4		73 *
23♦LBL 01		74 1
24 STO 14		75 -
25 3		76 PI
26 X>Y?		77 *
27 GTO 00		78 2
28 "BW=?"		79 ∕
29 PROMPT		80 RCL 15
30 XEQ 10		81 ∕
31 STO 08		82 SIN
32♦LBL 00	Compute filter order	83 2
33 "F1=?"		84 *
34 PROMPT		85♦LBL 09
35 "A=?"		86 STO 11
36 PROMPT		87 RCL 05
37 10		88 -1
38 ∕		89 RCL 09
39 10↑X		90 PSE
40 2		91 Y↑X
41 *		R ⁽⁻¹⁾ⁱ
42 1		92 Y↑X
43 -		93 *
44 LN		94 GTO IND
45 STO 12		14 Frequency
46 X<>Y		transformation
47 XEQ 10		95♦LBL 01
48 XEQ 07		96 RCL 07
49 RCL 12		97 ∕
50 X<>Y		98 XEQ 06
		99 GTO 00
		100♦LBL 02

Program Listings

101 RCL 07		152 GTO IND
102 *		14
103 1/X		153♦LBL 04
104 XEQ 06		154 XEQ 03
105 CHS		155 GTO 00
106 GTO 00		156♦LBL 02
107♦LBL 03		157 XEQ 01
108 SF 01		158♦LBL 00
109 RCL 08		159 1/X
110 /		160 CHS
111 XEQ 06		161 GTO 05
112 XEQ 00		162♦LBL 01
113 ABS		163 RCL 11
114 1/X		164 RCL 07
115 RCL 07		165 /
116 X↑2		166 GTO 05
117 /		167♦LBL 03
118 XEQ 06		168 RCL 11
119 CHS		169 X↑2
120 GTO 00		170 RCL 07
121♦LBL 04		171 X↑2
122 SF 01		172 -
123 RCL 08		173 RCL 11
124 *		174 /
125 RCL 07		175 RCL 08
126 X↑2		176 /
127 /		177♦LBL 05
128 XEQ 06		178 ABS
129 XEQ 00		179 STO 13
130 ABS		180 RTN
131 RCL 07		181♦LBL 06
132 X↑2		182 -1
133 *		183 RCL 09
134 1/X		184 Y↑X
135 XEQ 06		185 *
136 CHS		186 RTN
137♦LBL 00	-----	187♦LBL 10
138 "L="	Display	188 2
139 X<0?		189 *
140 "C="		190 PI
141 ABS		191 *
142 ARCL X		192 RTN
143 AVIEW		193 .END.
144 STOP		
145 FS?C 01		
146 RTN		
147 DSE 10	-----	
148 GTO 08		
149 RTN		
150♦LBL 07		
151 STO 11		
		00

BUTTERWORTH FILTER DESIGN

PROGRAM REGISTERS NEEDED: 43

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ROW 1 (1 - 4)



ROW 2 (4 - 10)



ROW 3 (11 - 15)



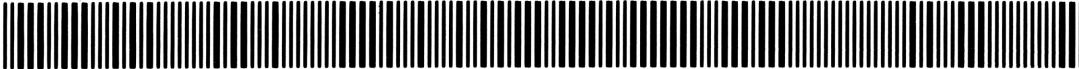
ROW 4 (15 - 19)



ROW 5 (20 - 26)



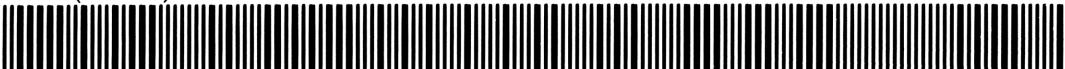
ROW 6 (27 - 32)



ROW 7 (33 - 37)



ROW 8 (38 - 48)



ROW 9 (48 - 59)



ROW 10 (60 - 69)



ROW 11 (70 - 82)



ROW 12 (83 - 94)



ROW 13 (94 - 103)



ROW 14 (104 - 111)



ROW 15 (111 - 119)



ROW 16 (120 - 128)



ROW 17 (129 - 137)



ROW 18 (138 - 145)



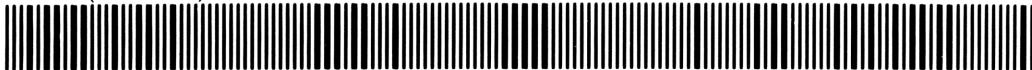
BUTTERWORTH FILTER DESIGN

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ROW 19 (145 - 154)



ROW 20 (154 - 161)



ROW 21 (162 - 173)



ROW 22 (174 - 185)



ROW 23 (186 - 193)



CHEBYSHEV FILTER DESIGN

This program computes component values for Chebyshev filters between equal terminations. Inputs are termination resistance, passband characteristics, attenuation at some out-of-band frequency, and allowable passband ripple.

Before the filter elements can be calculated, a normalized frequency must be computed from the desired cutoff or center frequency and passband characteristics. The normalized frequency is computed by one of these formulas:

Low Pass

$$\omega_n = \frac{\omega}{\omega_0}$$

High Pass

$$\omega_n = \frac{\omega_0}{\omega}$$

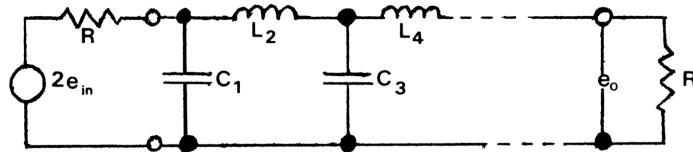
Band Pass

$$\omega_n = \frac{\omega^2 - \omega_0^2}{BW\omega}$$

Band Elimination

$$\omega_n = \frac{\omega BW}{\omega_0^2 - \omega^2}$$

The basic form of the filter is this low-pass prototype:



whose elements are given by one of the following sets of formulas:

$$C_i = \frac{G_i}{2\pi f_c R}, \quad i = 1, 3, 5, \dots, n$$

$$L_i = \frac{RG_i}{2\pi f_c}, \quad i = 2, 4, 6, \dots, n-1$$

where

$$G_1 = \frac{2a_1}{\gamma}$$

$$G_i = \frac{4a_{i-1}(a_i)}{(b_{i-1})(G_{i-1})}, \quad i = 2, 3, 4, \dots, n$$

$$\gamma = \sinh \left[\frac{\ln \left(\coth \frac{\varepsilon}{40 \log e} \right)}{2n} \right]$$

$$a_i = \sin \frac{(2i - 1)\pi}{2n}, \quad i = 1, 2, 3, \dots, n$$

$$b_i = \gamma^2 + \sin^2 \frac{i\pi}{n}, \quad i = 1, 2, 3, \dots, n - 1$$

$$\varepsilon = \left(10^{\Delta dB/10} - 1 \right)^{\frac{1}{2}}$$

The filter order is found by using Newton's method to solve for n in the following formula:

$$(\omega + \sqrt{\omega^2 - 1})^{2n} + (\omega + \sqrt{\omega^2 - 1})^{-2n} = \frac{4}{\varepsilon^2} (10^{\Delta dB/10} - 1) - 2$$

using

$$n = \frac{\ln \left[\frac{4}{\varepsilon^2} (10^{\alpha/10} - 1) - 2 \right]}{\ln(\omega + \sqrt{\omega^2 - 1})}$$

as an initial guess where α is attenuation in dB's.

The resulting value is then increased slightly:

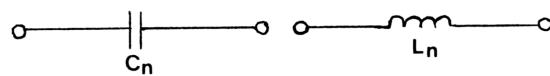
$$n \leftarrow \text{INT}(n + 1)$$

Once the low-pass values have been calculated, if some other passband characteristic is desired, the components of the filter are changed by frequency transformation as shown.

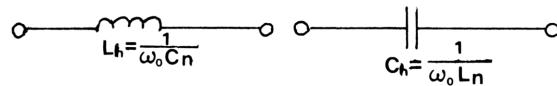
PASSBAND
CHARACTERISTIC

Low pass

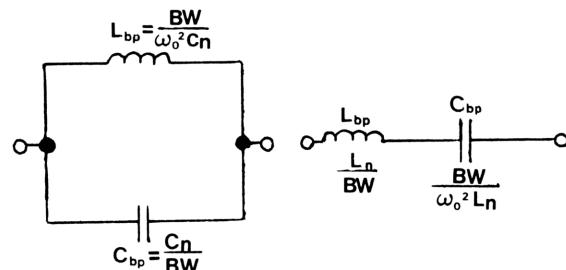
CIRCUIT ELEMENTS

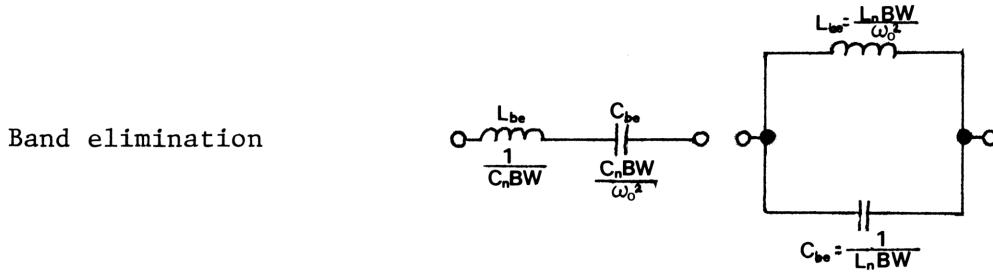


High pass



Band pass





A bit of thought may be necessary to determine whether the L-C's are connected in series or parallel.

NOTE: The program will give erroneous results if asked to compute filter order when ΔdB is small (i.e., when $\Delta\text{dB} \sim \text{Loss } (\omega_0)$).

Example:

Design a low pass Chebyshev filter with the following characteristics:

$R = 50\Omega$ $f_o = 500 \text{ Hz}$ pass band ripple = 3dB, and
30dB attenuation at 600 Hz.

Keystrokes:

```
[XEQ] [ALPHA] SIZE [ALPHA] 013
50 [STO] 00
500 [STO] 01
3 [STO] 03
30 [STO] 04
600 [STO] 05
```

```
[XEQ] [ALPHA] CHEB [ALPHA]
```

1 [R/S]

[R/S]

[R/S]

[R/S]

[R/S]

[R/S]

[R/S]

[R/S]

Display:

TYPE?

N=7.000E0

1.000 00

C=22.40E-6

2.000 00

L=12.29E-3

3.000 00

C=29.53E-6

4.000 00

L=12.79E-3

5.000 00

C=29.53E-6

6.000 00

L=12.29E-3

7.000 00

C=22.40E-6

User Instructions

Program Listings

01♦LBL "CHE B"		50 FS?C 02	
02 ENG 3	Convert	51 RTN	
03 RAD	Hz to r/s	52 GTO 05	
04 1		53♦LBL 03	
05 XEQ 09		54 RCL 05	
06 ST* 01		55 X↑2	
07 ST* 02		56 RCL 01	
08 ST* 05		57 X↑2	
09 RCL 03		58 -	
10 10	Convert	59 RCL 05	
11 /	dB to ε	60 ∕	
12 10↑X		61 RCL 02	
13 1		62 ∕	
14 -		63 FS?C 02	
15 SQRT		64 RTN	
16 STO 06		65♦LBL 05	
17 RCL 04		66 ABS	
18 10	Begin to	67 STO 08	
19 /	compute filter	68 ENTER↑	
20 10↑X	order	69 X↑2	
21 1		70 1	
22 -		71 -	
23 4		72 SQRT	
24 *		73 +	
25 RCL 06		74 STO 10	
26 X↑2		75 LN	
27 /		76 RCL 12	
28 2		77 LN	
29 -		78 X<>Y	
30 STO 12		79 ∕	
31 "TYPE?"		80 STO 09	
32 PROMPT	Filter type	81♦LBL 06	
33 STO 07		82 RCL 09	
34 GTO IND		83 RCL 10	
07		84 RCL 09	
35♦LBL 04		85 Y↑X	
36 SF 02		86 STO 05	
37 XEQ 03	Compute ω_n	87 ENTER↑	
38 GTO 00		88 1/X	
39♦LBL 02		89 +	
40 SF 02		90 RCL 12	
41 XEQ 01		91 -	
42♦LBL 00		92 RCL 05	
43 1/X		93 ENTER↑	
44 CHS		94 1/X	
45 GTO 05		95 -	
46♦LBL 01		96 ∕	
47 RCL 05		97 RCL 10	
48 RCL 01		98 LN	
49 /		99 ∕	
		100 2	
			Newton's method root finder

Program Listings

101 /		152 PI	
102 -		153 2	
103 STO 09		154 /	
104 LASTX		155 RCL 09	
105 ABS		156 /	
106 .01		157 SIN	
107 X<=Y?		158 STO 12	
108 GTO 06		159 2	
109 RCL 09		160 *	
110 2		161 RCL 08	
111 /		162 SQRT	
112 1		163 /	
113 +		164♦LBL 10	-----
114 INT		165 STO 05	
115 STO 09	Display n	166 RCL 00	
116 "N="		167 -1	Display i
117 ARCL X		168 RCL 11	
118 AVIEW		169 PSE	
119 STOP		170 Y↑X	
120 1		171 Y↑X	
121 STO 11		172 *	
122 RCL 03	Chebyshev	173 GTO IND	
123 40	setup	07	
124 /		174♦LBL 01	Frequency
125 1		175 RCL 01	transformation
126 E↑X		176 /	
127 LOG		177 XEQ 11	
128 /		178 GTO 00	
129 ENTER↑		179♦LBL 02	
130 +		180 RCL 01	
131 E↑X		181 *	
132 1		182 1/X	
133 X<>Y		183 XEQ 11	
134 +		184 CHS	
135 LASTX		185 GTO 00	
136 1		186♦LBL 03	
137 -		187 RCL 02	
138 /		188 /	
139 RCL 09		189 XEQ 11	
140 STO 10		190 SF 01	
141 2		191 XEQ 00	
142 *		192 1/X	
143 1/X		193 RCL 01	
144 Y↑X		194 X↑2	
145 ENTER↑		195 /	
146 1/X		196 XEQ 11	
147 -		197 CHS	
148 2		198 GTO 00	
149 /		199♦LBL 04	
150 X↑2		200 RCL 02	
151 STO 08		201 *	

Program Listings

202 RCL 01		253 /	
203 X↑2		254 RCL 08	
204 /		255 RCL 09	
205 XEQ 11		256 RCL 10	
206 SF 01		257 -	
207 XEQ 00		258 PI	
208 RCL 01		259 *	
209 X↑2		260 RCL 09	
210 *		261 /	
211 1/X		262 SIN	
212 XEQ 11		263 X↑2	
213 CHS	-----	264 +	
214♦LBL 00		265 /	
215 "L="		266 GTO 10	
216 X<0?	Display L & C	267♦LBL 11	
217 "C="		268 -1	
218 ABS		269 RCL 11	
219 ARCL X		270 Y↑X	
220 AVIEW		271 *	
221 STOP		272 RTN	
222 FS?C 01		273♦LBL 09	
223 RTN	-----	274 2	Multiply by
224 DSE 10		275 *	2π
225 GTO 07		276 PI	
226 RTN		277 *	
227♦LBL 07		278 RTN	
228 RCL 12	Loop	279 END	
229 RCL 09			
230 RCL 10			
231 -			
232 1	Chebyshev	80	
233 +	equations		
234 STO 11			
235 1			
236 -			
237 2			
238 *			
239 1			
240 +			
241 PI		90	
242 *			
243 2			
244 /			
245 RCL 09			
246 /			
247 SIN			
248 STO 12			
249 *			
250 4			
251 *			
252 RCL 05		00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS			
00	R	50	SIZE 013 ENG 3 DEG	TOT. REG.	62	USER MODE
	ω_0			FIX	SCI	ON OFF X
	BW			RAD X	GRAD	
	Ripple, dB					
	Attenuation					
	Attenuation freq.	55				
05	ϵ		FLAGS			
	Filter type		#	INIT S/C	SET INDICATES	CLEAR INDICATES
	ω_n			02	Return	Continue
	n			01	Return	Continue
10	Counter	60				
	i					
	Temporary Storage					
15		65				
20		70				
25		75				
30		80				
35		85				
ASSIGNMENTS						
			FUNCTION	KEY	FUNCTION	KEY
40		90				
45		95				

CHEBYSHEV FILTER DESIGN

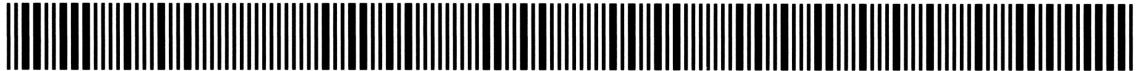
PROGRAM REGISTERS NEEDED: 51

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ROW 1 (1 : 5)



ROW 2 (5 : 12)



ROW 3 (13 : 24)



ROW 4 (25 : 32)



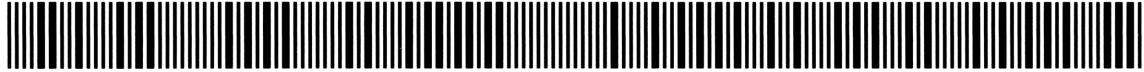
ROW 5 (33 : 40)



ROW 6 (40 : 49)



ROW 7 (50 : 60)



ROW 8 (61 : 72)



ROW 9 (73 : 85)



ROW 10 (86 : 98)



ROW 11 (99 : 108)



ROW 12 (109 : 118)



ROW 13 (119 : 130)



ROW 14 (131 : 143)



ROW 15 (144 : 156)



ROW 16 (157 : 168)



ROW 17 (169 : 178)



ROW 18 (178 : 187)



CHEBYSHEV FILTER DESIGN

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ROW 19 (188 : 195)



ROW 20 (196 : 205)



ROW 21 (205 : 212)



ROW 22 (212 : 219)



ROW 23 (220 : 229)



ROW 24 (230 : 242)



ROW 25 (243 : 255)



ROW 26 (256 : 267)



ROW 27 (268 : 279)



ROW 28 (279 : 279)



BODE PLOT OF BUTTERWORTH AND CHEBYSHEV FILTERS

This program provides gain, phase and group delay information for Bode plots of n-pole Butterworth or Chebyshev filters. A frequency transformation feature allows four types of filter characteristics: low pass, high pass, band pass, and band elimination. Frequency steps may be either linear (additive Δf) or logarithmic (multiplicative Δf).

The poles of an n-pole Butterworth filter are given by the following expression.

$$s = \sigma_k + j\omega_k = -\sin\left(\frac{2k-1}{n}\frac{\pi}{2}\right) - j \cos\left(\frac{2k-1}{n}\frac{\pi}{2}\right) \quad (k = 1, \dots, n)$$

The poles of a Chebyshev filter are derived from Butterworth poles by the following procedure.

Let $\beta_k = \frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}$

Then the new poles are given by

$$s_k = \sigma_k \sinh \beta_k + j \omega_k \cosh \beta_k$$

The gain, phase and delay functions of a filter are given by the following expressions.

The network transfer function is

$$\begin{aligned} H(j\omega) &= \frac{K}{(j\omega - s_1)(j\omega - s_2)\dots(j\omega - s_n)} \\ &= \frac{K}{(M_1 \angle \theta_1)(M_2 \angle \theta_2)\dots(M_n \angle \theta_n)} \\ &= \frac{K}{M(\omega) \angle \theta(\omega)} \end{aligned}$$

in which K is a constant chosen such that

$$|H(j0)| = 1$$

The magnitude of the transfer function is

$$|H(j\omega)| = \frac{K}{\prod_{i=1}^n \sqrt{\sigma_i^2 + (\omega - \omega_i)^2}}$$

and its phase is

$$\arg [H(j\omega)] = -\theta(\omega) = -\sum_{i=1}^n \tan^{-1} \frac{\omega - \omega_i}{-\sigma_i}$$

The normalized group delay is

$$t_g = \frac{d}{d\omega} \{\theta(\omega)\} = \sum_{i=1}^n \frac{\sigma_i}{\sigma_i^2 + (\omega - \omega_i)^2}$$

Example:

Plot the response of a 6-pole Butterworth band-pass filter with BW = 100, $f_0 = 800$. Make a logarithmic plot using steps of $2^{1/8}$ from 400 Hz to 1600 Hz.

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 016

[SF] 00

6 [STO] 00

800 [STO] 02

100 [STO] 03

400 [STO] 04

1600 [STO] 05

2 \sqrt{x} \sqrt{x} \sqrt{x} [STO] 06

[XEQ] [ALPHA] BODE [ALPHA]

Display:

?

3 [R/S]

0,1-?

1 [R/S]

T=0.027

[R/S]

L=161.536

[R/S]

MAG=-129.502

[R/S]

F=400.00

[R/S]

T=0.036

[R/S]

L=158.504

[R/S]

MAG=-121.591

[R/S]

F=436.203

[R/S]

T=0.051

[R/S]

L=154.506

[R/S]

MAG=-112.727

[R/S]

F=475.683

:

:

User Instructions

STEP	INSTRUCTIONS	INPUT	FUNCTION	SIZE: 016
				DISPLAY
1	Load program: for Butterworth for Chebyshev		[SF] 00 [CF] 00	
2	Store applicable data:			
	Filter order	n	[STO] 00	
	Pass band ripple	rip	[STO] 01	
	Cutoff frequency	f _o	[STO] 02	
	Band width	BW	[STO] 03	
	Minimum frequency	f ₁	[STO] 04	
	Maximum frequency	f ₂	[STO] 05	
	Frequency steps	Δf	[STO] 06	
3	Begin execution		[XEQ] BODE	?
4	Input filter type:			
	1-Low pass	1	[R/S]	0,1-?
	2-High pass	2	[R/S]	0,1-?
	3-Band pass	3	[R/S]	0,1-?
	4-Band elimination	4	[R/S]	0,1-?
5	Select: Linear	0	[R/S]	
	Logarithmic	1	[R/S]	T=
			[R/S]	A=
			[R/S]	MAG=
			[R/S]	F=
6	For next increment, continue to press [R/S].			

Program Listings

01♦LBL "BOD		52 P-R	gain
E"		53 RCL 13	normalization
02 FIX 3		54 +	
03 RCL 01	-----	55 RCL 08	
04 10		56 R-P	
05 /	Convert dB	57 X†2	
06 10†X	ripple to ε	58 X<>Y	
07 1		59 RDH	
08 -		60 /	time delay
09 SQRT		61 ST+ 09	
10 STO 01	-----	62 DSE 10	
11 1		63 GTO 08	
12 XEQ 09	Convert Hz to	64 RCL 04	-----
13 ST* 02	r/s	65 1	frequency
14 ST* 03		66 XEQ 09	
15 ST* 04		67 /	
16 ST* 05		68 RCL 11	
17 RCL 06		69 LOG	gain, dB
18 *		70 20	
19 STO 15	-----	71 *	
20 "?"	Store filter	72 RND	
21 PROMPT	type	73 RCL 12	
22 STO 14	-----	74 1	
23 "0, 1-?"	Set linear or	75 P-R	phase, degrees
24 PROMPT	logarithmic	76 DEG	
25 SF 01	increment	77 R-P	
26 X=0?		78 CLX	
27 CF 01		79 RCL 09	
28♦LBL E	-----	80 "T="	
29 0		81 XEQ 05	Display
30 STO 09	Initialize	82 "Δ="	
31 STO 12	registers	83 XEQ 05	
32 1		84 "MAG="	
33 STO 11		85 XEQ 05	
34 RCL 00		86 "F="	
35 STO 10		87 XEQ 05	
36 XEQ 07		88 RCL 05	-----
37♦LBL 08	Loop	89 RCL 04	Increment
38 RAD		90 FS? 01	
39 XEQ 06		91 GTO 00	
40 RCL 07	Compute s _k	92 RCL 15	
41 RCL 13		93 +	
42 +		94 GTO 03	
43 RCL 08	gain	95♦LBL 00	
44 R-P		96 RCL 06	
45 ST/ 11		97 *	
46 X<>Y		98♦LBL 03	
47 ST- 12	phase	99 STO 04	
48 RCL 08		100 X<=Y?	
49 RCL 07		101 GTO E	
50 R-P		102 RTN	
51 ST* 11		103♦LBL 07	

Program Listings

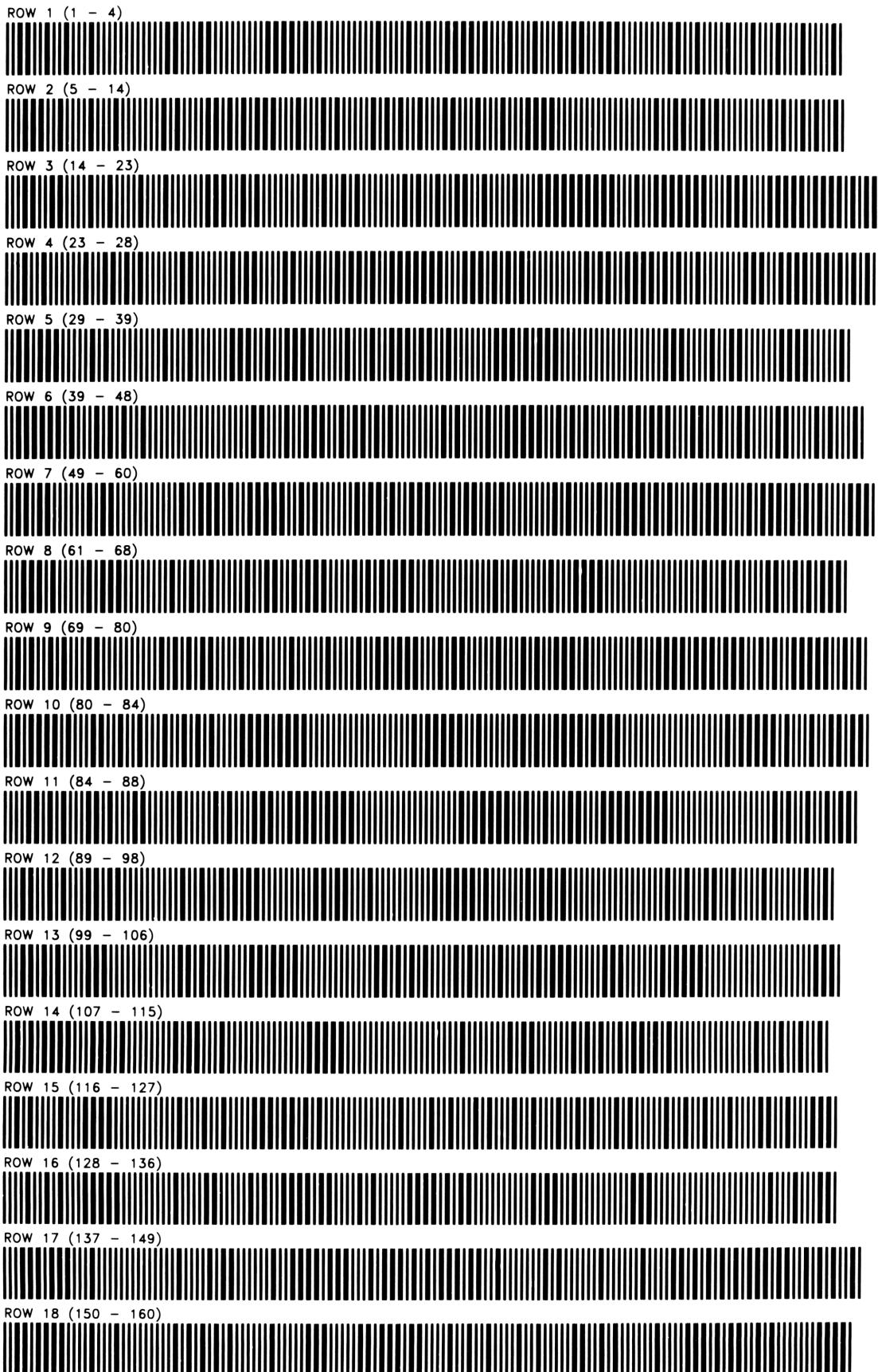
104 GTO IND		155 2
14	Compute ω_n	156 *
105+LBL 04		157 -
106 XEQ 03	BE	158 ST* 08
107 GTO 00		159 RDN
108+LBL 02		160 ST* 07
109 XEQ 01	HP	161 2
110+LBL 00		162 ST/ 08
111 1/X		163 ST/ 07
112 CHS		164 RTN
113 GTO 04		165+LBL 01
114+LBL 01	LP	166 RCL 10
115 RCL 04		167 2
116 RCL 02		168 *
117 /		169 1
118 GTO 04		170 -
119+LBL 03	BP	171 RCL 00
120 RCL 04		172 /
121 X↑2		173 XEQ 09
122 RCL 02		174 4
123 X↑2		175 /
124 -		176 1
125 RCL 04		177 P-R
126 /		178 STO 07
127 RCL 03		179 X<>Y
128 /		180 STO 08
129+LBL 04		181 RTN
130 STO 13		182+LBL 09
131 RTN		183 2
132+LBL 06		184 *
133 FS? 00		185 PI
134 GTO 01	Subroutine to	186 *
135 XEQ 01	compute s_k	187 RTN
136 1		188+LBL 05
137 RCL 01		189 ARCL X
138 1/X		190 AVIEW
139 R-P		191 STOP
140 X<>Y		192 RDN
141 RDN		193 RTN
142 LASTX		194 .END.
143 +		90
144 LN		
145 RCL 00		
146 /		
147 E↑X		
148 LASTX		
149 CHS		
150 E↑X		
151 +		
152 ENTER↑		
153 ENTER↑		
154 LASTX		00

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS			
Reg	Name	Value	Flags			
			#	INIT S/C	SET INDICATES	CLEAR INDICATES
00	N	50				
	ripple					
	cutoff frequency					
	Band width					
	fmin, ω_1					
05	fmax, ω_2	55				
	Δf					
	$\text{Im}\{\mathbf{s}_K\}$					
	$\text{Re}\{\mathbf{s}_K\}$					
	delay					
10	counter	60				
	$\pi H(j\omega) $					
	$\sum \theta(\omega)$					
	ω_n					
	$\frac{3}{4}$ filter type					
15	$\Delta \omega$	65				
20		70				
25		75				
30		80				
35		85				
ASSIGNMENTS						
			FUNCTION	KEY	FUNCTION	KEY
40		90				
45		95				

BODE PLOT OF BUTTERWORTH AND
CHEBYSHEV FILTERS
PROGRAM REGISTERS NEEDED: 40

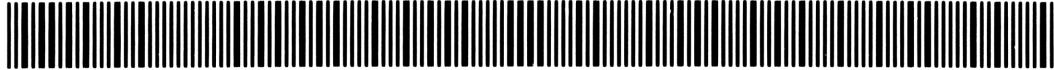
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BODE PLOT OF BUTTERWORTH AND
CHEBYSHEV FILTERS

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ROW 19 (161 - 171)



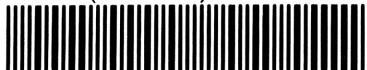
ROW 20 (172 - 182)



ROW 21 (183 - 194)

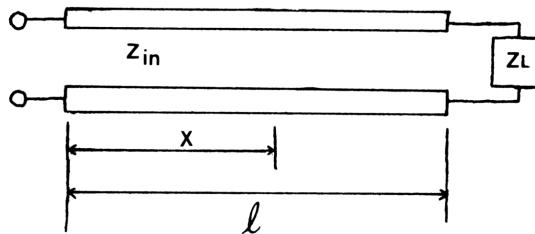


ROW 22 (194 - 194)



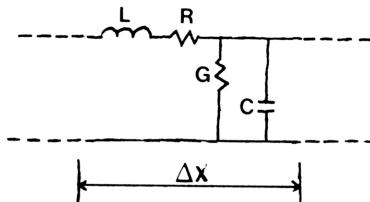
TRANSMISSION LINE CALCULATIONS

This program computes the input impedance of a lossy transmission line terminated in Z_L . The program provides an exact solution when the distributed line parameters $R_0 (\sqrt{L/C})$, R , and G are given, and it provides an approximate solution when R_0 , copper loss and dielectric loss are given.



The transmission line shown has a lumped model composed of elements L , C , R , and G . From this model the following equations can be derived:

MODEL



Equations:

$$R_0 = \sqrt{\frac{L}{C}}$$

$$r = \frac{R}{L} = \frac{vR}{R_0}$$

$$g = \frac{G}{C} = v R_0 G$$

$$\omega = 2\pi f$$

where

L = inductance/unit length

C = capacitance/unit length

G = conductance/unit length

R = resistance/unit length

v_r = relative phase velocity

$v = 3 \times 10^8 v_r$

f = frequency, Hz

and

$$\alpha = \frac{1}{\sqrt{2} v} \left[rg - \omega^2 + \sqrt{(r^2 + \omega^2)(g^2 + \omega^2)} \right]^{\frac{1}{2}}$$

$$\beta = \frac{1}{\sqrt{2} v} \left[\omega^2 - rg + \sqrt{(r^2 + \omega^2)(g^2 + \omega^2)} \right]^{\frac{1}{2}}$$

The approximate solution is

$$\text{Re}\{Z_0\} = R_0 \left[1 + \frac{1}{2} \left(\frac{\alpha_C - \alpha_D}{\beta_0} \right) \left(\frac{3\alpha_D + \alpha_C}{\beta_0} \right) \right]$$

$$\text{Im}\{Z_0\} = R_0 \left[\frac{\alpha_D - \alpha_C}{\beta_0} \right]$$

$$\alpha = \alpha_C + \alpha_D$$

$$\beta = \beta_0 \left[1 + \frac{1}{2} \left(\frac{\alpha_C - \alpha_D}{\beta_0} \right)^2 \right]$$

where

$$\alpha_C = \text{Copper loss, nepers/unit length} = \frac{1}{2} \frac{R}{R_0}$$

$$\alpha_D = \text{Dielectric loss, nepers/unit length} = \frac{1}{2} GR$$

$$\beta_0 = \frac{\omega}{v}$$

Then

$$Z_{in} = Z_0 \left(\frac{1 + \Gamma_L e^{-2\gamma\ell}}{1 - \Gamma_L e^{-2\gamma\ell}} \right)$$

where

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

ℓ = line length

Z_L = impedance of termination

Z_0 = characteristic impedance of line = $\text{Re}\{Z_0\} + j \text{Im}\{Z_0\}$

γ = propagation constant of line = $\alpha + j\beta$

Z_0 and γ are computed differently depending on which solution is selected.

$$\text{Re}\{Z_0\} = \frac{R_0}{\sqrt{2(g^2 + \omega^2)}} \left[rg + \omega^2 + \sqrt{(r^2 + \omega^2)(g^2 + \omega^2)} \right]^{\frac{1}{2}}$$

$$\text{Im}\{Z_0\} = \frac{\pm R_0}{\sqrt{2(g^2 + \omega^2)}} \left[-(rg + \omega^2) + \sqrt{(r^2 + \omega^2)(g^2 + \omega^2)} \right]^{\frac{1}{2}}$$

in which the + sign is chosen when $g \geq r$ and the - sign is chosen when $g < r$.

Example:

A transmission line has the following properties:

$$R = 1.2664 \Omega/\text{cm}$$

$$G = 0.000\ 041\ 87 \text{ Siemens/cm}$$

$$R_0 = 55 \Omega$$

$$v_T = 0.85$$

What is the input impedance of 3.5 cm of this line at 2 GHz if it is terminated in $Z_L = 75 \angle -30^\circ$?

Keystrokes :

[XEQ] [ALPHA] SIZE [ALPHA] 012

[XEQ] [ALPHA] LINE [ALPHA]

2 [EEX] 9 [R/S]

0.85 [R/S]

55 [R/S]

3.5 [R/S]

[XEQ] [ALPHA] EXACT [ALPHA]

0.00004187 [R/S]

1.2664 [R/S]

75 [R/S]

30 [CHS] [R/S]

[R/S]

Display:

F?

VR?

RO?

L?

G?

R?

ZL?

$\angle ZL = 28.48$

$ZIN = 48.01$

User Instructions

Program Listings

01♦LBL "LIN E" 02 FIX 2 03 "F?" 04 PROMPT 05 1 E10 06 / 07 STO 09 08 2 09 PI 10 * 11 * 12 STO 08 13 "VR?" 14 PROMPT 15 STO 02 16 "R0?" 17 PROMPT 18 STO 01 19 "L?" 20 PROMPT 21 STO 11 22 2 23 * 24 3 25 RCL 02 26 * 27 STO 03 28 / 29 STO 07 30 STOP 31♦LBL "EXA CT" 32 "G?" 33 PROMPT 34 "R?" 35 PROMPT 36 RCL 03 37 * 38 RCL 01 39 / 40 STO 05 41 RDN 42 RCL 01 43 * 44 ST* 03 45 RCL 08 46 RCL 05 47 R-P 48 SQRT 49 STO 05	Initialization	50 X<>Y 51 2 52 / 53 STO 06 54 RCL 08 55 RCL 03 56 R-P 57 SQRT 58 STO 03 59 X<>Y 60 2 61 / 62 STO 08 63 RCL 06 64 + 65 STO 04 66 RCL 06 67 RCL 08 68 - 69 STO 02 70 RCL 05 71 RCL 03 72 / 73 ST* 01 74 RCL 05 75 RCL 03 76 * 77 ST* 07 78 GTO "ZIN ----- Exact solution	50 X<>Y 51 2 52 / 53 STO 06 54 RCL 08 55 RCL 03 56 R-P 57 SQRT 58 STO 03 59 X<>Y 60 2 61 / 62 STO 08 63 RCL 06 64 + 65 STO 04 66 RCL 06 67 RCL 08 68 - 69 STO 02 70 RCL 05 71 RCL 03 72 / 73 ST* 01 74 RCL 05 75 RCL 03 76 * 77 ST* 07 78 GTO "ZIN ----- 79♦LBL "APP ROX" 80 "AD?" 81 PROMPT 82 "AC?" 83 PROMPT 84 X<>Y 85 STO 08 86 RDN 87 STO 03 88 RCL 11 89 RCL 02 90 RCL 09 91 PI 92 * 93 1.5 94 / 95 X<>Y 96 / 97 STO 06 98 *	Approximate solution
--	----------------	---	---	----------------------

Program Listings

99	2		149	PROMPT
100	*		150	STO 06
101	STO 07		151	RCL 04
102	RCL 08		152	RCL 07
103	10		153	P-R
104	LN		154	CHS
105	20		155	E↑X
106	/		156	STO 07
107	RCL 06		157	X<>Y
108	/		158	180
109	ST* 03		159	*
110	ST* 08		160	PI
111	RCL 08		161	/
112	RCL 03		162	STO 08
113	-		163	RCL 06
114	ENTER↑		164	RCL 02
115	STO 05		165	-
116	RCL 08		166	RCL 05
117	3		167	RCL 01
118	*		168	/
119	RCL 03		169	P-R
120	+		170	1
121	*		171	+
122	2		172	R-P
123	/		173	1/X
124	CHS		174	-2
125	1		175	*
126	+		176	X<>Y
127	R-P		177	CHS
128	ST* 01		178	X<>Y
129	X<>Y		179	P-R
130	STO 02		180	1
131	RCL 05		181	+
132	X↑2		182	R-P
133	2		183	RCL 07
134	/		184	*
135	1		185	1/X
136	+		186	X<>Y
137	RCL 03		187	RCL 08
138	RCL 08		188	-
139	+		189	CHS
140	R-P		190	X<>Y
141	ST* 07		191	P-R
142	X<>Y		192	1
143	STO 04		193	-
144	LBL "ZIN"	-----	194	R-P
"			195	1/X
145	"ZL?"	Calculate Zin	196	2
146	PROMPT		197	*
147	STO 05		198	X<>Y
148	"ZL?"		199	CHS

Program Listings

200	X<>Y		51		
201	P-R				
202	1				
203	+				
204	R-P				
205	RCL 01				
206	*				
207	X<>Y				
208	RCL 02				
209	+		60		
210	"ZIN= "				
211	ARCL X				
212	AVIEW	Display			
213	STOP				
214	X<>Y				
215	"ZIN= "				
216	ARCL X				
217	AVIEW				
218	STOP				
219	.END.		70		
20					
30			80		
40			90		
50			00		

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS									
00		50		SIZE	012	TOT. REG.	56	USER MODE					
				ENG		FIX	2	SCI		ON		OFF	X
				DEG		RAD		GRAD					
05	3v _r R ₀ G/R	55		FLAGS				CLEAR INDICATES					
				#	INIT S/C	SET INDICATES		CLEAR INDICATES					
				2	l	3v _r	w ¹						
				f ¹⁰ ¹⁰									
10		60		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
15		65		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
20		70		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
25		75		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
30		80		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
35		85		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
40		90		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					
45		95		ASSIGNMENTS				FUNCTION KEY					
				FUNCTION KEY				FUNCTION KEY					

TRANSMISSION LINE CALCULATIONS

PROGRAM REGISTERS NEEDED: 45

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ROW 1 (1 - 3)



ROW 2 (4 - 13)



ROW 3 (13 - 19)



ROW 4 (19 - 31)



ROW 5 (31 - 34)



ROW 6 (34 - 44)



ROW 7 (45 - 57)



ROW 8 (58 - 70)



ROW 9 (71 - 78)



ROW 10 (78 - 80)



ROW 11 (80 - 88)



ROW 12 (89 - 99)



ROW 13 (100 - 109)



ROW 14 (110 - 121)



ROW 15 (122 - 133)



ROW 16 (134 - 144)



ROW 17 (144 - 148)



ROW 18 (148 - 158)



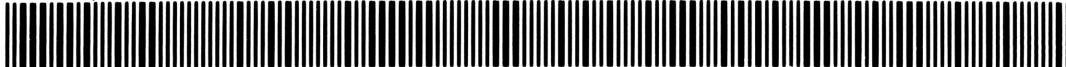
TRANSMISSION LINE CALCULATIONS

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ROW 19 (158 - 169)



ROW 20 (170 - 181)



ROW 21 (182 - 194)



ROW 22 (195 - 207)



ROW 23 (208 - 214)



ROW 24 (215 - 219)



TRANSMISSION LINE IMPEDANCE

This program computes high frequency characteristic impedance (Z_0) for five types of transmission lines.

Transmission line configuration

open two-wire line

Equation for Z_0

$$Z_0 = \frac{120}{\sqrt{\epsilon_r}} \ln \left(\frac{2D}{d} \right)$$

single wire near ground

$$Z_0 = \frac{138}{\sqrt{\epsilon_r}} \log \left(\frac{4h}{d} \right)$$

balanced wires near ground

$$Z_0 = \frac{276}{\sqrt{\epsilon_r}} \log \left\{ \frac{2D}{d} \left[1 + \left(\frac{D}{2h} \right)^2 \right]^{-\frac{1}{2}} \right\}$$

wires in parallel near ground

$$Z_0 = \frac{69}{\sqrt{\epsilon_r}} \log \left\{ \frac{4h}{d} \left[1 + \left(\frac{2h}{D} \right)^2 \right]^{\frac{1}{2}} \right\}$$

coaxial line

$$Z_0 = \frac{60}{\sqrt{\epsilon_r}} \ln \frac{D}{d}$$

Example 1:

Compute Z_0 of RG-218/U coaxial cable. ($D = .68$ in., $d = .195$ in., $\epsilon_r = 2.3$ (polyethylene)).

Keystrokes:

```
[XEQ] [ALPHA] SIZE [ALPHA] 004
.68 [ENTER↑] .195 [ENTER↑]
2.3 [XEQ] [ALPHA] [C] [ALPHA]
```

Display:

Z0=49.42

Example 2:

Compute Z_0 of open 2-wire line with $D = 6$ in., $d = .0808$ in., $\epsilon_r = 1$ (air).

Keystrokes:

```
6 [ENTER↑] .0808 [ENTER↑] 1 [XEQ] [ALPHA]
[OP] [ALPHA]
```

Display:

Z0=600.08

Example 3:

Compute Z_0 of an air line consisting of a single .1285 inch wire 6 inches from a ground plane.

Keystrokes:

```
.1285 [ENTER↑] 6 [ENTER↑] 1 [XEQ] [ALPHA]
[SW] [ALPHA]
```

Display:

Z0=313.44

User Instructions

				SIZE: 004
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Load program			
2	Compute impedance of open two-wire line.			
	Input: -wire spacing	D	[ENTER↑]	
	-wire diameter	d	[ENTER↑]	
	-relative permittivity	ϵ_r	[XEQ] OP	Z0=
3	Compute impedance of a single wire near ground. Input:			
	-wire diameter	d	[ENTER↑]	
	-wire height	h	[ENTER↑]	
	-relative permittivity	ϵ_r	[XEQ] SW	Z0=
4	Compute impedance of balanced wires near ground. Input:			
	-wire spacing	D	[ENTER↑]	
	-wire diameter	d	[ENTER↑]	
	-wire height	h	[ENTER↑]	
	-relative permittivity	ϵ_r	[XEQ] B	Z0=
5	Compute impedance of wires in parallel near ground. Input:			
	-wire spacing	D	[ENTER↑]	
	-wire diameter	d	[ENTER↑]	
	-wire height	h	[ENTER↑]	
	-relative permittivity	ϵ_r	[XEQ] P	Z0=
6	Compute impedance of coaxial line. Input:			
	-inside diameter of outer conductor	D	[ENTER↑]	
	-outside diameter of inner conductor	d	[ENTER↑]	
	-relative permittivity	ϵ_r	[XEQ] C	Z0=

Program Listings

01♦LBL "OF"		52 276	
02 STO 00		53 *	
03 RDN	Two wire line	54 RCL 00	
04 *		55 SQRT	
05 2		56 *	
06 *		57 GTO 05	
07 LN		58♦LBL "P"	
08 120		59 STO 00	
09 *		60 RDN	
10 RCL 00		61 STO 01	Wires in
11 SQRT		62 RDN	parallel near
12 *		63 STO 02	ground
13 GTO 05		64 RDN	
14♦LBL "SW"		65 STO 03	
15 STO 00		66 RCL 01	
16 RDN	Single wire	67 *	
17 4	near ground	68 1/X	
18 *		69 2	
19 *		70 *	
20 1/X		71 X†2	
21 LOG		72 1	
22 138		73 +	
23 *		74 SQRT	
24 RCL 00		75 RCL 01	
25 SQRT		76 *	
26 *		77 RCL 02	
27 GTO 05		78 *	
28♦LBL B		79 4	
29 STO 00		80 *	
30 RDN	Balanced wires	81 LOG	
31 STO 01	near ground	82 69	
32 RDN		83 *	
33 STO 02		84 RCL 00	
34 RDN		85 SQRT	
35 STO 03		86 *	
36 RCL 01		87 GTO 05	
37 *		88♦LBL C	
38 2		89 STO 00	Coaxial cable
39 *		90 RDN	
40 X†2		91 *	
41 1		92 LN	
42 +		93 60	
43 SQRT		94 *	
44 1/X		95 RCL 00	
45 2		96 SQRT	
46 *		97 *	
47 RCL 03		98♦LBL 05	
48 *		99 FIX 2	
49 RCL 02		100 "Z0="	Display
50 *		101 ARCL X	
51 LOG		102 AVIEW	

Program Listings

103 STOP		51	
104 .END.			
10		60	
20		70	
30		80	
40		90	
50		00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS			
00	εr	50	SIZE	004	TOT. REG.	24
	h		ENG		SCI	
	D		DEG		RAD	
	D (rounded)				GRAD	
05		55	FLAGS			
			#	INIT S/C	SET INDICATES	CLEAR INDICATES
10		60				
15		65				
20		70				
25		75				
30		80				
35		85				
			ASSIGNMENTS			
			FUNCTION		KEY	FUNCTION
40		90				KEY
45		95				

TRANSMISSION LINE IMPEDANCE

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PROGRAM REGISTERS NEEDED: 20

ROW 1 (1 - 8)



ROW 2 (8 - 14)



ROW 3 (14 - 24)



ROW 4 (25 - 35)



ROW 5 (36 - 48)



ROW 6 (49 - 58)



ROW 7 (58 - 67)



ROW 8 (68 - 80)



ROW 9 (81 - 90)



ROW 10 (91 - 100)



ROW 11 (100 - 104)



NOTES

NOTES

Hewlett-Packard Software

In terms of power and flexibility, the problem-solving potential of the HP-41 programmable calculator is nearly limitless. And in order to see the practical side of this potential, HP has different types of software to help save you time and programming effort. Every one of our software solutions has been carefully selected to effectively increase your problem-solving potential. Chances are, we already have the solutions you're looking for.

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To increase the versatility of your HP-41, HP has an extensive library of "Application Pacs". These programs transform your HP-41 into a specialized calculator in seconds. Included in these pacs are detailed manuals with examples, miniature plug-in Application Modules, and keyboard overlays. Every Application Pac has been designed to extend the capabilities of the HP-41.

You can choose from:

Aviation (Pre-Flight Only) 00041-15018
Clinical Lab 00041-15024
Circuit Analysis 00041-15024
Financial Decisions 00041-15004
Mathematics 00041-15003
Structural Analysis 00041-15021
Surveying 00041-15005
Securities 00041-15026

Statistics 00041-15002
Stress Analysis 00041-15027
Games 00041-15022
Home Management 00041-15023
Machine Design 00041-15020
Navigation 00041-15017
Real Estate 00041-15016
Thermal and Transport Science 00041-15019
Petroleum Fluids 00041-15039

Users' Library

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*Users' Library Solutions Books

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Home Construction Estimating 00041-90096
Lending, Saving and Leasing 00041-90086
Real Estate 00041-90136
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Geometry 00041-90084
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Mechanical Engineering 00041-90090
Solar Engineering 00041-90138
Calendars 00041-90145
Cardiac/Pulmonary 00041-90097
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Games 00041-90099
Optometry I (General) 00041-90143
Optometry II (Contact Lens) 00041-90144
Physics 00041-90142
Surveying 00041-90141
Time Module Solutions 00041-90395

*Some books require additional memory modules to accomodate all programs.

ELECTRICAL ENGINEERING

RC TIMING

FREQUENCY RESPONSE OF A TRANSFER FUNCTION

TRANSISTOR AMPLIFIER PERFORMANCE

CLASS A TRANSISTOR AMPLIFIER BIAS OPTIMIZATION

ACTIVE FILTER DESIGN

BUTTERWORTH FILTER DESIGN

CHEBYSHEV FILTER DESIGN

BODE PLOT OF BUTTERWORTH AND CHEBYSHEV FILTERS

TRANSMISSION LINE CALCULATIONS

TRANSMISSION LINE IMPEDANCE

