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"CIVIL ENGINEERING"
FOR THE HP-41

SC-2

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CIVIL ENGINEERING

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02248C

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PROGRAM DESCRIPTION I

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Program Title BEAM DESIGN

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Program Description, Equations, Variables THIS PROGRAM HELPS TO FIND THE BEAM REQ'D TO SUPPORT GIVEN LOADS IMPISED FOR ANY OF THESE THREE CONDITIONS: SIMPLY SUPPORTED BEAMS, BEAMS FIXED AT ONE END SUPPORTED AT OTHER, AND BEAMS FIXED AT BOTH ENDS. TO ACHIEVE THIS, THE PROGRAM CALCULATES THE SUPPORT REACTIONS AND STATIC FUNCTIONS (SHEAR, MOMENT, SLOPE, AND DEFLECTION) FOR THE ENTIRE BEAM. LOADINGS MAY BE DISTRIBUTED LOADS, POINT LOADS, AND/OR MOMENTS. STATIC FUNCTIONS ARE CALCULATED BASED ON THE SMALLEST DISTANCE BETWEEN TWO SUCCESSIVE POINTS EITHER d_{MAX} (IMPOSED BY USER) OR d_i (DISTANCE BETWEEN TWO LOADS). LOCATION OF AND MAGNITUDE OF MAXIMUM MOMENT M AND MAXIMUM DEFLECTION y ARE CALCULATED BASED ON d_{MAX} . THEREFORE THE SMALLER d_{MAX} USED THE MORE ACCURATE THE CALCULATION. BASED ON MAX y A REQ'D MOMENT OF INERTIA I AND SECTION MODULOUS S ARE CALCULATED TO SATISFY DESIGN LIMITATIONS. AFTER CHOOSING AN I AND S BASED UPON PREVIOUS CALCULATIONS, USER INSERTS BEAM SPECIFICATIONS AS REQ'D TO FINALIZE BEAM DESIGN. THE FINAL CALCULATIONS ARE USED FOR FINDING DEFLECTIONS, MOMENTS, SECTION MODULOUS, UNSUPPORTED LENGTHS, AND ADDITIONAL DEFL. OF BEAM DUE TO APPLIED LIVE LOADS. FROM THIS THE BEAMS ARE EITHER APPROVED OR DISAPPROVED.

Necessary Accessories 41CV OR 41C W/QUAD MODULE, CARD READER, & PRINTER (OPTIONAL)

Operating Limits and Warnings SEE PAGE 2

Reference(s) AISC STEEL CONSTRUCTION MANUAL EIGHTH EDITION

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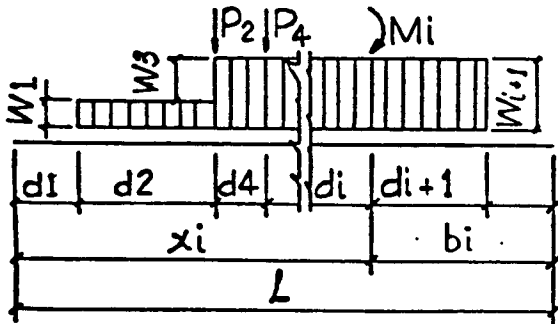
OPERATING LIMITS AND WARNINGS:

WHEN DISTRIBUTED LOADS EXIST, THE COMPUTED DEFLECTION Y_i WILL DIFFER SLIGHTLY FROM THE ACTUAL VALUES DUE TO THE INTEGRAL VALUES BEING APPROXIMATED. SO FOR $d_{MAX} = L/4$ THE MAXIMUM ERROR IS ABOUT $Y_{MAX} / 1.0024$ AND FOR SAY $d_{MAX} = 1.0$ THE MAXIMUM ERROR IS ABOUT $Y_{MAX} / 1.00007$. THEREFORE FOR $d_{MAX} < L/4$ THE ACCURACY WILL BE INCREASED. THE VALUE OF d_{MAX} MUST BE LIMITED IN SIZE TO 3 DECIMAL PLACES SINCE THE 4TH PLACE IS USED TO IDENTIFY THE LOAD TYPE.

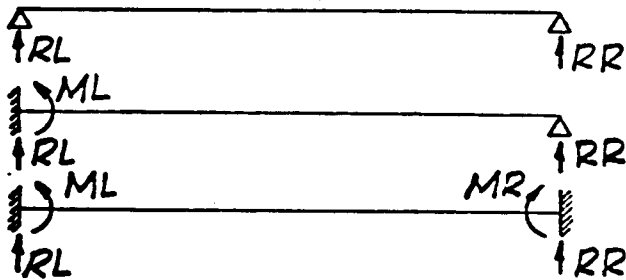
THIS PROGRAM IS LIMITED TO ONLY 9 SEPARATE LOADINGS AND DISTANCES SIMPLY DUE TO THE LACK OF STORAGE.

THE SMALLER THE d_{MAX} , THE LONGER IT TAKES FOR THE PROGRAM TO RUN.

LOADING SCHEME AND NOTATION



BEAM TYPES AND SUPPORT REACTIONS

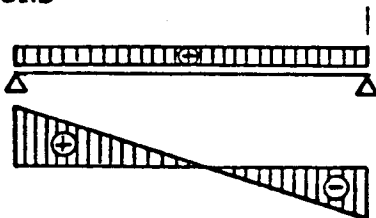


SIGN CONVENTIONS FOR LOADS AND SUPPORT REACTIONS



SIGN CONVENTIONS FOR STATIC FUNCTIONS

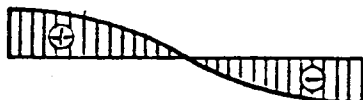
SHEAR (Q)



MOMENT (M)



SLOPE (S)



DEFL. (Y)

SUPPORT REACTIONS:

$$R_L = -\sum W_i b_i^2 / 2L - P_i b_i / L + \sum M_i / L - (M_L + M_R) / L$$

$$R_R = -\sum W_i b_i - \sum P_i - R_L$$

FOR BEAMS FIXED AT ONE END:

$$M_L = -3KL / L$$

FOR BEAMS FIXED AT BOTH ENDS:

$$M_L = -2(2KL + KR) / L$$

$$M_R = -2(2KR + KL) / L$$

SLOPE LEFT FOR SIMPLY SUPPORTED BEAMS:

$$S_L = KL / EI$$

$$KL = \sum W_i b_i^2 (2L^2 - b_i^2) / 24L + \sum P_i b_i (L^2 - b_i^2) / 6L + \sum M_i L (L^2 - 3b_i^2) / 6$$

$$KR = \sum W_i b_i^2 (b_i - 2L)^2 / 24L + \sum P_i x_i (x_i^2 - L^2) / 6L + \sum M_i L (L^2 - 3x_i^2) / 6$$

STATIC FUNCTIONS WILL BE COMPUTED BY NUMERICAL INTEGRATION USING SIMPSON'S RULE. THE SPACING BETWEEN TWO SUCCESSIVE POINTS, d_i IS SUBDIVIDED INTO TWO PARTS.

THE INTERMEDIARY VALUES OF FUNCTIONS WILL BE NOTED WITH m.

STATIC FUNCTIONS TO THE LEFT OF COMPUTATION POINTS:

$W_{i,L} = W_{i-1,R} = W_m$ (BETWEEN 2 SUCCESSIVE POINTS $W = \text{CONSTANT}$)

SHEAR: $Q_{i,L} = -Q_{i-1,R} - (W_{i-1,R} + 4W_m + W_{i,L})di/6$

$Q_m = -Q_{i-1,R} - (W_{i-1,R} + W_m)di/4$

MOMENT: $M_{i,L} = M_{i-1,R} + (Q_{i-1,R} + 4Q_m + Q_{i,L})di/6$

$M_m = M_{i-1,R} + (Q_{i-1,R} + Q_m)di/4$

SLOPE: $S_{i,L} = S_{i-1,R} - (M_{i-1,R} + 4M_m + M_{i,L})di/6EI$

$S_m = S_{i-1,R} - (M_{i-1,R} + M_m)di/6EI$

DEFL: $Y_{i,L} = Y_{i-1,R} + (S_{i-1,R} + 4S_m + S_{i,L})di/6$

STATIC FUNCTIONS TO THE RIGHT OF COMPUTATION POINT:

$W_{i,R} = W_{i,L} + W_i$

$Q_{i,R} = Q_{i,L} - P_i$

$M_{i,R} = M_{i,L} + M_i$

$S_{i,R} = S_{i,L}$

$Y_{i,R} = Y_{i,L}$

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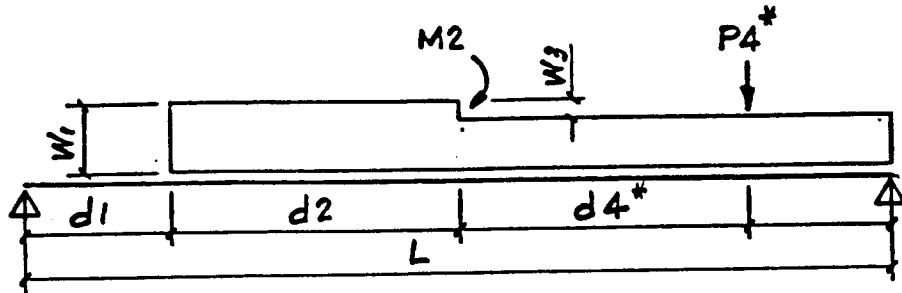
PROGRAM DESCRIPTION II

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Sample Problem (Sketch if Desired)

EXAMPLE: 1

BEAM SIMPLY SUPPORTED



$$L = 12'-0$$

$$d1 = 2'-0 \quad W1 = 10 \text{ K/FT}$$

$$d2 = 4'-0 \quad M2 = 8 \text{ FT-K}$$

$$d3 = 0 \quad W3 = -2 \text{ K/FT}$$

$$*d4 = 4'-0 \quad P4 = 3 \text{ K}$$

SOLUTION: * ASSUME THAT P4 IS A LIVE LOAD

Input	Function	Display	Comments
	XEQ A	L=?	BEAM LENGTH
12	R/S	d1=?	DISTANCE 1
2	R/S	LOAD? (:W::P::M:)	TYPE LOAD 1
10	[C]	d2=?	DISTANCE 2
4	R/S	LOAD? (:W::P::M:)	TYPE LOAD 2
8	[E]	d3=2	DISTANCE 3
0	R/S	LOAD? (:W::P::M:)	TYPE LOAD 3
-2	[C]	d4=?	DISTANCE 4
-	R/S	BEAM? (0,1,2)	TYPE OF CONNECTION
0	R/S	>---< L=12.000	
		X=2.000 W1=10.000	
		X=6.000 M2=8.000	
		X=6.000 W3=-2.000	
		RL=-38.000	
		ML=8.000	
		RP=-58.000	
		MR=8.000	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ Q,M,S,Y)	
-	XEQ Q	X=0.000 Q=38.000	SHEAR EXCLUDING LIVE LOAD
		X=1.000 Q=38.000	
		X=2.000 Q=38.000	
		X=3.000 Q=28.000	
		X=4.000 Q=18.000	
		X=5.000 Q=8.000	
		X=6.000 Q=-2.000	
		X=7.000 Q=-10.000	
		X=8.000 Q=-18.000	
		X=9.000 Q=-26.000	
		X=10.000 Q=-34.000	
		X=11.000 Q=-42.000	
		X=12.000 Q=-50.000	

(CONTINUATION PAGE)

Input	Function	Display	Comments
-	XEQ M	X=0.000 M=0.000 X=1.000 M=38.000 X=2.000 M=76.000 X=3.000 M=109.000 X=4.000 M=132.000 X=5.000 M=145.000 X=6.000 M=148.000 X=6.000 M=156.000 X=7.000 M=150.000 X=8.000 M=136.000 X=9.000 M=114.000 X=10.000 M=84.000 X=11.000 M=46.000 X=12.000 M=0.000 MAXIMUM M 156.000 AT X=6.000	MOMENT EXCLUDING LIVE LOAD
-	XEQ S	X=0.000 S=585.778 X=1.000 S=566.778 X=2.000 S=509.778 X=3.000 S=416.444 X=4.000 S=295.111 X=5.000 S=155.778 X=6.000 S=8.444 X=7.000 S=-145.222 X=8.000 S=-288.889 X=9.000 S=-414.556 X=10.000 S=-514.222 X=11.000 S=-579.889 X=12.000 S=-603.556	SLOPE EXCLUDING LIVE LOAD
-	XEQ Y	E=29000.000 I=1.000 X=0.000 Y=0.000 X=1.000 Y=34.527 X=2.000 Y=66.790 X=3.000 Y=94.553 X=4.000 Y=115.870 X=5.000 Y=129.372 X=6.000 Y=134.284 X=7.000 Y=130.183 X=8.000 Y=117.183 X=9.000 Y=96.119 X=10.000 Y=68.302 X=11.000 Y=35.520 X=12.000 Y=0.036 MAXIMUM Y 134.284/I AT X=6.000	DEFLECTIONS EXCLUDING LIVE LOADS
(NOW RERUN PROGRAM INCLUDING ALL LIVE LOADS)			

(CONTINUATION PAGE)

Input	Function	Display	Comments
***	XEQ =A	L=?	IGNORE SINCE LENGTH DOES NOT CHANGE, THIS STEP WAS TO SF04 ONLY.
4	XEQ B	d4=?	DISTANCE 4
4	R/S	LOAD? (:W::P::M:)	TYPE LOAD 4
3	[D]	d5=?	DISTANCE 5
-	R/S	BEAM? (0,1,2)	TYPE OF CONNECTIONS
0	R/S)---(L=12.000	
		X=2.000 W1=10.000	
		X=6.000 M2=8.000	
		X=6.000 W3=-2.000	
		X=10.000 P4=3.000	
		RL=-30.500	
		ML=0.000	
		RP=-52.500	
		MP=0.000	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ O.M.S.Y)	
-	XEQ Q	X=0.000 Q=30.500	SHEAR INCLUDING LIVE LOAD
		X=1.000 Q=30.500	
		X=2.000 Q=30.500	
		X=3.000 Q=28.500	
		X=4.000 Q=18.500	
		X=5.000 Q=0.500	
		X=6.000 Q=-1.500	
		X=7.000 Q=-9.500	
		X=8.000 Q=-17.500	
		X=9.000 Q=-25.500	
		X=10.000 Q=-33.500	
		X=10.000 Q=-36.500	
		X=11.000 Q=-44.500	
		X=12.000 Q=-52.500	
-	XEQ M	X=0.000 M=0.000	MOMENT INCLUDING LIVE LOAD
		X=1.000 M=30.500	
		X=2.000 M=77.000	
		X=3.000 M=110.500	
		X=4.000 M=134.000	
		X=5.000 M=147.500	
		X=6.000 M=151.000	
		X=6.000 M=159.000	
		X=7.000 M=153.500	
		X=8.000 M=140.000	
		X=9.000 M=110.500	
		X=10.000 M=89.000	
		X=11.000 M=40.500	
		X=12.000 M=0.000	
		MAXIMUM M	
		159.000 AT X=6.000	

*** NOTE: EITHER SF04, XEQ B OR XEQ =A TO RERUN PROGRAM TO INCLUDE LIVE LOADS. IF VERYFEW LIVE LOADS ARE ADDED SF04, XEQ B IS QUICKER THAN XEQ . BE SURE dn NUMBER IS INPUTED PRIOR TO XEQ B.

(CONTINUATION PAGE)

Input	Function	Display	Comments
-	XEQ S	X=0.000 S=597.444 X=1.000 S=578.194 X=2.000 S=528.444 X=3.000 S=425.861 X=4.000 S=382.778 X=5.000 S=161.194 X=6.000 S=11.111 X=7.000 S=-145.886 X=8.000 S=-293.222 X=9.000 S=-423.139 X=10.000 S=-527.556 X=11.000 S=-596.972 X=12.000 S=-621.889	SHEAR INCLUDING LIVE LOADS
-	XEQ Y	E=29000.000 I=1.000 X=0.000 Y=0.000 X=1.000 Y=35.217 X=2.000 Y=68.140 X=3.000 Y=96.584 X=4.000 Y=118.333 X=5.000 Y=132.228 X=6.000 Y=137.383 X=7.000 Y=133.346 X=8.000 Y=120.282 X=9.000 Y=98.756 X=10.000 Y=70.289 X=11.000 Y=36.588 X=12.000 Y=0.036 MAXIMUM Y 137.383/I AT X=6.000 TRY I>228.971 TRY S>79.500	DEFLECTIONS INCLUDING LIVE LOADS
			BEAM MINIMUM REQUIREMENTS WHEN LIVE LOADS APPLIED
	XEQ H	BEAM?	
W21 X	R/S	WT?	
44	R/S	I?	
843	R/S	S?	
81.6	R/S	D/AF?	
7.050	R/S	BF?	
6.5	R/S	TF?	
.451	R/S	RT?	
1.59	R/S	BEAM W21 X 44	
		E=29000.000 I=643.000 S=81.600 D/AF=7.050 BF=6.500 TF=0.451 RT=1.590	

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Input	Function	Display	Comments
		YB=0.000	
		YB=0.163 AT 6.000	
		YLa=0.400	
		YL=0.004 AT 6.000	
		MMB=159.000 AT 6.000	
		L=12.000	
		Fb=17.055	
		MMA=115.973	
		MMB EXCEEDS ALLOWABLE	
		SX = 111.874	
		SX EXCEEDS ALLOWABLE	
		TRY S>111.874	SPAN IS TO GREAT TO BE UNSUPPORTED
		LU=6.863	
		Fb=22.000	
		MMA=149.600	
		MMB EXCEEDS ALLOWABLE	
		SX = 86.727	
		SX EXCEEDS ALLOWABLE	
		TRY S>86.727	SPAN IS TO GREAT TO BE SUPPORTED AT LU
		LC=6.572	
		Fb=24.000	
		MMA=163.200	
		SX = 79.500	SPAN IS OK TO BE SUPPORTED AT LC

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PROGRAM DESCRIPTION II

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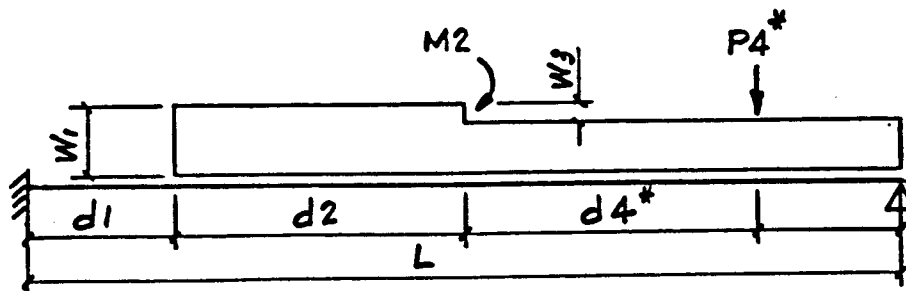
Sample Problem (Sketch if Desired)

EXAMPLE: 2

FIXED AT ONE END

SUPPORTED AT OTHER

***SF03



L = 12'-0

d1 = 2'-0 W1 = 10 K/FT

d3 = 0 W3 = -2K/FT

d2 = 4'-0 M2 = 8 FT-K

*d4 = 4'-0 P4 = 3K

SOLUTION: * ASSUME THAT P4 IS A LIVE LOAD

Input	Function	Display	Comments
12	XEQ A	L=?	BEAM LENGTH
2	R/S	d1=?	DISTANCE 1
10	R/S	LOAD? (:W::P::M:)	TYPE LOAD 1
4	[C]	d2=?	DISTANCE 2
8	R/S	LOAD? (:W::P::M:)	TYPE LOAD 2
0	[E]	d3=?	DISTANCE 3
-2	R/S	LOAD? (:W::P::M:)	TYPE LOAD 3
-	[C]	d4=?	DISTANCE 4
1	R/S	BEAM? (0,1,2)	TYPE OF CONNECTION
	R/S	1--< L=12.000	
		X=2.000 W1=10.000	
		X=6.000 M2=8.000	
		X=6.000 W3=-2.000	
		RL=-58.284	
		ML=-146.444	
		RR=-37.796	
		MR=0.000	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ Q,M,S,Y)	
-	XEQ Q		SHEAR EXCLUDING LIVE LOAD
-	XEQ M		MOMENT " " "
		MAXIMUM M	MAX M
		146.444 AT X=0.000	
-	XEQ S		SLOPE " " "
-	XEQ Y		DEFL " " "
		E=29000.000	
		I=1.000	
		MAXIMUM Y	MAX Y
		58.071/I AT X=7.000	
(NOW RERUN PROGRAM INCLUDING ALL LIVE LOADS)			

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Input	Function	Display	Comments
		YBa=0.600	
		YB=0.071 AT 7.000	
		YL=0.400	
		YL=0.002 AT 7.000	
		MNB=149.361 AT 0.000	
		L=12.000	
		Fb=17.055	
		MMA=115.973	
		MMS EXCEEDS ALLOWABLE	
		SX = 105.892	
		SX EXCEEDS ALLOWABLE	
		TRY S>105.892	SPAN IS TO GREAT TO BE UNSUPPORTED
		LU=6.863	
		Fb=22.000	
		MMA=149.600	
		SX = 81.478	SPAN IS OK TO BE SUPPORTED AT LU
		LC=6.572	
		Fb=24.000	
		MMA=163.200	
		SX = 74.681	SPAN IS OK TO BE SUPPROTED AT LC

(CONTINUATION PAGE)

Input	Function	Display	Comments
***	XEQ -a	L=?	IGNORE SINCE LENGTH DOES NOT CHANGE, THIS STEP WAS TO SF04 ONLY.
4	XEQ B	d4=?	DISTANCE 4
4	R/S	LOAD? (:W::P::M:)	TYPE LOAD 4
3	[D]	d5=?	DISTANCE 5
-	R/S	BEAM? (0,1,2)	TYPE OF CONNECTIONS
/		I--(L=12.000	
		X=2.000 W1=10.000	
		X=6.000 W2=8.000	
		X=6.000 W3=-2.000	
		X=10.000 P4=3.000	
		RL=-50.547	
		ML=-149.361	
		PR=-40.053	
		MR=0.000	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ Q,M,S,Y)	SHEAR INCLUDING LIVE LOAD
-	XEQ Q		MOMENT
-	XEQ M	MAXIMUM M 149.361 AT X=0.000	MAX M
-	XEQ S		SLOPE
-	XEQ Y	E=29000.000 I=1.000	DEFL
		MAXIMUM Y 59.798/1 AT X=7.000	MAX Y
		TRY I>99.664	MIN I AND S REQ'D FOR
		TRY S>74.681	CALCULATIONS
	XEQ H	BEAM?	
W21 X	R/S	WT?	
44	R/S	I?	
843	R/S	S?	
81.6	R/S	D/AF?	
7.050	R/S	BF?	
6.5	R/S	TF?	
.451	R/S	RT?	
1.59	R/S	BEAM W21 X 44	
		E=29000.000	
		I=843.000	
		S=81.600	
		D/AF=7.050	
		BF=6.500	
		TF=0.451	
		RT=1.590	

*** NOTE: EITHER SF04, XEQ B OR XEQ -A TO RERUN PROGRAM TO INCLUDE LIVE LOADS. IF VERYFEW LIVE LOADS ARE ADDED SF04, XEQ B IS QUICKER THAN XEQ -A. BE SURE dn NUMBER IS INPUTED PRIOR TO XEQ B.

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PROGRAM DESCRIPTION II

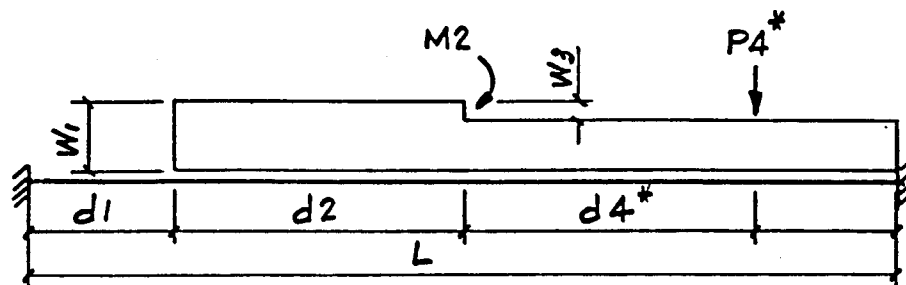
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Sample Problem (Sketch if Desired)

EXAMPLE: 3

BEAM FIXED AT BOTH ENDS

***SF03



L = 12'-0

d1 = 2'-0 W1 = 10 K/FT

d3 = 0 W3 = -2K/FT

d2 = 4'-0 M2 = 8 FT-K

*d4 = 4'-0 P4 = 3K

SOLUTION: * ASSUME THAT P4 IS A LIVE LOAD

Input	Function	Display	Comments
	XEQ A	L=?	BEAM LENGTH
12	R/S	d1=?	DISTANCE 1
2	R/S	LOAD? (:W::P::M:)	TYPE LOAD 1
10	[C]	d2=?	DISTANCE 2
4	R/S	LOAD? (:W::P::M:)	TYPE LOAD 2
8	[E]	d3=?	DISTANCE 3
0	R/S	LOAD? (:W::P::M:)	TYPE LOAD 3
-2	[C]	d4=?	DISTANCE 4
-	R/S	BEAM? (0,1,2)	TYPE OF CONNECTION
2	R/S	I---I L=12.000	
		X=2.000 W1=10.000	
		X=6.000 M2=8.000	
		X=6.000 W3=-2.000	
		RL=-37.259	
		ML=-94.667	
		RR=-50.741	
		MR=103.556	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ Q,M,S,Y)	
-	XEQ Q		SHEAR EXCLUDING LIVE LOAD
-	XEQ M		MOMENT " " "
		MAXIMUM M	MAX M
-	XEQ S	103.556 AT X=12.000	
-	XEQ Y		SLOPE " " "
			DEFL " " "
		E=29000.000	
		I=1.000	
		MAXIMUM Y	MAX Y
		27.932/I AT X=6.000	
(NOW RERUN PROGRAM INCLUDING ALL LIVE LOADS)			

(CONTINUATION PAGE)

Input	Function	Display	Comments
***	XEQ A	L=?	IGNORE SINCE LENGTH DOES NOT CHANGE, THIS STEP WAS TO SF04 ONLY.
4	XEQ B	d4=?	DISTANCE 4
4	R/S	LOAD? (:W::P::M:)	TYPE LOAD 4
3	[D]	d5=?	DISTANCE 5
-	R/S	BEAM? (0,1,2)	TYPE OF CONNECTIONS
2		I---I L=12.000	
		X=2.000 W1=10.000	
		X=6.000 M2=8.000	
		X=6.000 W3=-2.000	
		X=10.000 F4=3.000	
		RL=-37.481	
		ML=-95.500	
		RR=-53.519	
		HR=107.722	
		d.MAX=3.000?	
1	R/S	ST.FN.? (XEQ Q,M,S,Y)	SHEAR INCLUDING LIVE LOAD
-	XEQ Q		MOMENT " " "
-	XEQ M		MAX M
		MAXIMUM M	
		107.722 AT X=12.000	
-	XEQ S		SLOPE " " "
-	XEQ Y		DEFL " " "
		E=29000.000	
		I=1.000	
		MAXIMUM Y	MAX Y
		26.399/1 AT X=6.000	
		TRY 1/47.332	MIN I AND S REQ'D FOR CALCULATIONS
		TRY 3/53.861	
	XEQ H	BEAM?	
W18 X	R/S	WT?	
35	R/S	I?	
510	R/S	S?	
57.6	R/S	D/AF?	
6.94	R/S	BF?	
6.0	R/S	TF?	
.425	R/S	RT?	
1.49	R/S	BEAM	
		W18 X 35	
		E=29000.000	
		I=510.000	
		S=57.600	
		D/AF=6.940	
		BF=6.000	
		TF=0.425	
		RT=1.490	

*** NOTE: EITHER SF04, XEQ B OR XEQ -A TO RERUN PROGRAM TO INCLUDE LIVE LOADS. IF VERY FEW LIVE LOADS ARE ADDED SF04, XEQ B IS QUICKER THAN XEQ -A BE SURE dn NUMBER IS INPUTED PRIOR TO XEQ B.

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(CONTINUATION PAGE)

[illegible]

GLOSSARY OF TERMS

W - UNIFORMLY DISTRIBUTED LOAD, K/FT
P - CONCENTRATED LOAD, KIPS
M - IMPLIED MOMENT, K-FT
dn - DISTANCE FROM END OF BEAM OR LOAD TO NEXT LOAD, FT
X1 - DISTANCE FROM LEFT END TO POINT OF EXECUTION, FT
b1 - DISTANCE FROM POINT OF EXECUTION TO RIGHT END, FT
L - LENGTH OF BEAM, FT
RL - REACTION AT LEFT SUPPORT, KIPS
ML - MOMENT AT LEFT SUPPORT, K-FT
RR - REACTION AT RIGHT SUPPORT, KIPS
MR - MOMENT AT RIGHT SUPPORT, K-FT
Q - SHEAR
M - MOMENT
S - SLOPE
Y - DEFLECTION
SL - SLOPE AT LEFT SUPPORT, IN
KL - CONSTANT AT LEFT SUPPORT
KR - CONSTANT AT RIGHT SUPPORT
BEAM - SHAPE AND DEPTH OF BEAM, EX. W21_X
WT - WEIGHT OF BEAM EX. 44
E - MODULUS OF ELASTICITY, 29,000 KSI
I - MOMENT OF INERTIA
S - SECTION MODULOUS
D/AF - DEPTH OF BEAM/AREA OF THE FLANGE
BF - FLANGE WIDTH
TF - FLANGE THICKNESS
RT - RADIUS OF GYRATION, (FOR CHANNEL RT = 0)
YBa - DEFLECTION OF BEAM ALLOWABLE DUE TO 1/240 OF SPAN
YB - MAX. DEFLECTION OF BEAM
YLa - DEFLECTION OF BEAM ALLOWABLE W/LIVE LOAD DUE TO 1/360 OF SPAN
YL - MAX. DEFLECTION OF BEAM DUE TO LIVE LOAD
MMB - MAX. MOMENT OF BEAM AT X
MMA - MAX. MOMENT OF BEAM ALLOWABLE
Fb - ALLOWABLE BENDING STRESS
SX - MIN. SECTION MODULOUS REQUIRED
LU - MAX UNBRACED LENGTH OF COMPRESSION FLANGE @ Fb = 22 KSI
LC - MAX UNBRACED LENGTH OF COMPRESSION FLANGE @ Fb = 24 KSI
LIVE LOADS - LOADS APPLIED TO THE BEAM THAT ARE NOT PERMANENT

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				SIZE: (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	INITIALIZE PROGRAM		XEQ BEAM	A? OR \Rightarrow A?
2a	BEAM WITH LIVE LOAD EXCLUDED		XEQ A	L=?
2b	BEAM WITH LIVE LOAD INCLUDED		XEQ \neg a	L=?
3	BEAM LENGTH	L	R/S	d1=?
4	SPACING BETWEEN LOADS	d1	R/S	LOAD? (:W::P::M
5	LOADS W,P, OR M	LOAD 1	C,D, OR E	d2=?
6	REPEAT STEPS 4 AND 5 UNTIL ALL DISTANCES AND LOADS ARE ENTERED			d _n +1=?
6a	THEN TO CLOSE OUT DATA INPUT	-	R/S	BEAM? (0,1,2)
7	TO DISPLAY LOADINGS, REACTIONS, AND END MOMENTS FOR BEAM	0,1,2*	R/S	d.MAX=L/4?
8	INTERVALS OF COMPUTATION (a OR b)			
8a	FOR d.MAX L/4	-		
8b	FOR INCREASED PRECISION d.MAX L/4	d.MAX	R/S	ST.FN.? (XEQ Q,M
9	STATIC FUNCTION CALCULATION **			
9a	SHEAR	-	XEQ Q	Xi=_Qi=_
9b	MOMENT	-	XEQ M	Xi=_Mi= MAX M AT X=_
9c	SHEAR	-	XEQ S	Xi=_Si=_
9d	DEFLECTION	-	XEQ Y	E=29,000 I=1 Xi=_Yi= MAX Y AT X=_
	(DISPLAY STOPS HERE IF STEP 2a WAS EXECUTED. CONTINUE WITH STEP 11)			
	(DISPLAY STOPS HERE IF STEP 2b WAS EXECUTED. CONTINUE WITH STEP 11)			TRY I > ____ TRY S > ____
10	REPEAT STEPS 2 THRU 9 STARTING WITH STEP 2b			
11	INPUT BEAM DATA AS REQ'D BY I AND S CALCULATES STEP 11a			

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				SIZE: (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
	OR IF DATA PREVIOUSLY ENTERED IS STILL GOOD THEN GOTO STEP 11b			
11a	DATA INPUT AND BEAM CALCULATIONS	-	XEQ H	BEAM?
1)	BEAM	LNN_X	R/S	WT?
2)	BEAM WEIGHT	NN	R/S	I?
3)	MOMENT OF INERTIA	Ix-x	R/S	S?
4)	SECTION MODULOUS	Sx-x	R/S	D/AF?
5)	DEPTH/AREA OF FLANGE	d/af	R/S	BF?
6)	FLANGE WIDTH	bf	R/S	TF?
7)	FLANGE THICKNESS	tf	R/S	RT?
8)	RADIUS OF GYRATION	rT	R/S	VARIES
	(IF GOOD: NO FURTHER OPERATIONS REQ'D)			
	(IF BAD: PROGRAM SUGGESTS CHANGES, USER MUST REPEAT STEP 11a)			TRY I > ____
				TRY S > ____
11b	BEAM CALCULATIONS		XEQ F	VARIES
	(IF GOOD: NO FURTHER OPERATIONS REQ'D)			TRY I > ____
	(IF BAD: PROGRAM SUGGESTS CHANGES, USER MUST REPEAT STEP 11a)			TRY S > ____
	* THESE FIGURES REPRESENT THE TOTAL NUMBER OF FIXED ENDS OF THE BEAM. (IF THERE IS ONE FIXED END, IT MUST BE PLACED ON THE LEFT END.)			
	** NOTE: Q, M, S, & Y MAY BE EXECUTED IN ANY ORDER BUT FOR THIS PROGRAM TO BE USED TO ITS MAXIMUM XEQ Q THEN M AND XEQ S THEN Y, BUT ALL FOUR MUST BE DONE BEFORE CONTINUING TO STEP 10.			
	***SF03 TO OMIT DISPLAY OR PRINTING OF Xi AND STATIC FUNCTION.			

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL "BEA			46	3		
M"				47	LBL 06		LOAD IDENTIFIER
02	"A? OR a			48	1 E4		
?"				49	/		
03	AVIEW			50	RCL Z		
04	STOP			51	FIX 3		
05	LBL a			52	RND		
06	SF 04			53	+		
07	GTO 00			54	STO IND		
08	LBL A			06			
09	CF 04			55	ISG 06		
10	LBL 00			56	STOP		
11	CF 29			57	X<>Y		
12	"L=?"			58	STO IND		
13	PROMPT			06			
14	STO 10			59	RCL 09		
15	4			60	RCL 08		
16	/			61	X<=Y?		
17	STO 12			62	ISG 08		
18	1			63	CLA		
19	STO 08			64	X=Y?		
20	STO 09			65	ISG 09		
21	LBL 06		DATA INPUT	66	CLA		
22	FIX 0			67	1		
23	RCL 08			68	-		
24	2			69	X=Y?		
25	*			70	ISG 09		
26	38			71	CLA		
27	+			72	X<=Y?		
28	STO 06			73	GTO 06		
29	"d"			74	0		
30	ARCL 08			75	1/X		
31	"t=?"			76	LBL B		CORRECTION
32	CF 22			77	STO 08		
33	PROMPT			78	GTO 06		
34	FC? 22			79	LBL 07		
35	GTO 07			80	"BEAM?<0		
36	"LOAD?<:			1,2>"			
W::P::M:"				81	PROMPT		
37	"t>"			82	LBL I		
38	PROMPT			83	STO 18		
39	LBL C		DISTRIBUTED	84	ADV		
40	1		LOAD	85	ΣREG 11		
41	GTO 06			86	CLΣ		
42	LBL D		CONCENTRAITED	87	GTO IND		
43	2		LOAD	18			
44	GTO 06		IMPLIED MOMENT	88	LBL 00		
45	LBL E			89	">---<"		SIMPLE BEAM

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TEP/ JNE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
90	GTO 07			136	"FW"		DISPLAY OF
91	LBL 01			137	GTO 07		DATA
92	"I---<"		FIXED ONE END	138	LBL 04		
93	GTO 07			139	"FP"		
94	LBL 02			140	GTO 07		
95	"I---I"		FIXED BOTH ENDS	141	LBL 05		
96	LBL 07			142	"FM"		
97	RCL 10			143	LBL 07		COMPUTES SUPPORT
98	"L L="			144	.5		REACTIONS AND
99	FIX 3			145	STO 03		SLOPE AT LEFT
100	ARCL X			146	1		END
101	AVIEW			147	STO 04		
102	ADV			148	3		
103	STO 00			149	STO 05		
104	RCL 09			150	FIX 0		
105	2			151	ARCL 08		
106	*			152	"L="		
107	37			153	RCL 00		
108	+			154	2		
109	1 E3			155	/		
110	/			156	RCL 00		
111	40			157	RCL IND		
112	+			158	FIX 3		
113	STO 19			159	ARCL X		
114	.3			160	AVIEW		
115	STO 03			161	GTO IND		
116	LBL 16			07			
117	ISG 08			162	LBL 03		
118	RCL IND			163	*		
119	ENTER↑			164	LBL 04		
120	FIX 3			165	ST- 15		RR
121	RND		LOAD TYPE	166	*		
122	ST- 00		IDENTIFIER	167	CHS		
123	ST+ 11			168	LBL 05		
124	MOD			169	RCL 10		
125	1 E4			170	/		
126	*			171	ST+ 12		RL
127	2			172	6		
128	+			173	/		
129	STO 07			174	RCL 00		
130	ISG 19			175	X↑2		
131	"X="			176	RCL IND		
132	ARCL 11			07			
133	"L "			177	*		
134	GTO IND			178	RCL 10		
07				179	X↑2		
135	LBL 03			180	-		

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
181	*			225	*		
182	STO 01			226	STO 02		KR
183	GTO IND			227	RCL 01		
184	♦LBL 00		SIMPLE SUPPORTS	228	2		
185	ST+ 14		SL	229	*		
186	GTO 07			230	-		
187	♦LBL 01		FIXED ONE END	231	2		
188	3			232	*		
189	*			233	RCL 10		
190	RCL 10			234	/		
191	/			235	ST+ 13		ML
192	ST- 13		ML	236	RCL 01		
193	GTO 07			237	RCL 02		
194	♦LBL 02		FIXED BOTH ENDS	238	2		
195	1			239	*		
196	STO 03			240	-		
197	RCL 10			241	2		
198	X↑2			242	*		
199	RCL 11			243	RCL 10		
200	X↑2			244	/		
201	-			245	ST- 16		MR
202	4			246	♦LBL 07		
203	/			247	ISG 19		
204	RCL 11			248	GTO 16		
205	RCL IND			249	RCL 12		
19				250	RCL 16		
206	GTO IND			251	RCL 13		
07				252	+		
207	♦LBL 03			253	RCL 10		
208	X<>Y			254	/		
209	RDN			255	+		
210	♦LBL 04			256	STO 12		
211	*			257	ST- 15		
212	♦LBL 05			258	ADV		
213	CHS			259	"RL"		DISPLAY OF
214	RCL 10			260	RCL 12		SUPPORT REACTION
215	/			261	XEQ 15		AND MOMENTS
216	6			262	"ML"		
217	/			263	RCL 13		
218	RCL 11			264	XEQ 15		
219	X↑2			265	"RR"		
220	RCL IND			266	RCL 15		
07				267	XEQ 15		
221	*			268	"MR"		
222	RCL 10			269	RCL 16		
223	X↑2			270	XEQ 15		
224	-			271	RCL 10		
				272	4		

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
273	/			320	STO 01		
274	"d.MAX="			321	ΣREG 02		
275	ARCL X			322	CLΣ		
276	"t?"			323	ΣREG 11		
277	PROMPT			324	STO 02		
278	LBL J			325	0		
279	STO 21			326	STO 11		
280	"ST.FN.?"			327	RCL 19		
281	<XEQ Q,M"			328	FRC		
282	PROMPT			329	40		
283	LBL "Q"		SHEAR FUNCTION	330	+		
284	1			331	STO 19		
285	SF 05			332	RCL 12		
286	SF 08			333	CHS		
287	CF 07			334	STO 04		
288	CF 06			335	RCL 13		
289	GTO 07			336	STO 05		
290	LBL "M"		MOMENT FUNCTION	337	RCL 14		
291	2			338	STO 06		
292	SF 05			339	FC? 00		
293	CF 08			340	GTO 08		
294	GTO 07			341	"E"		
295	LBL "S"		SLOPE FUNCTION	342	RCL 22		
296	3			343	XEQ 15		
297	CF 05			344	"I"		
298	SF 08			345	1		
299	CF 06			346	XEQ 15		
300	CF 07			347	ADV		
301	GTO 07			348	LBL 08		
302	LBL "Y"		DEFLECTION	349	FC? 03		
303	4		FUNCTION	350	XEQ 13		
304	CF 05			351	RCL IND		
305	CF 08			19			
306	LBL 07		INITIALIZES FOR	352	RND		
307	STO 18		COMPITATION OF	353	LBL 19		
308	CF 00		STATIC FUNCTIONS	354	X=0?		
309	CF 02			355	GTO 11		
310	4			356	STO 20		
311	X=Y?			357	RCL 21		
312	GTO 07			358	X>Y?		
313	SF 00		FOR DEFL.	359	X<>Y		
314	29 E03			360	ST- 20		
315	STO 22			361	ST+ 11		
316	LBL 07			362	RCL 03		
317	ADV			363	STO 15		
318	0			364	STO 16		
319	STO 00			365	3.1		
				366	STO 17		

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
367	RCL	18		412	GTO	14	
368	STO	08		413	RCL	IND	
369	R↑			19			
370	XEQ	17		414	ISG	19	
371	♦LBL	10	NUMERICAL	415	ENTER↑		
372	CHS		INTEGRATION	416	FIX	3	
373	RCL	15		417	RND		
374	4			418	MOD		
375	*			419	1 E4		
376	RCL	16		420	*		
377	RCL	IND		421	2		
17				422	+		
378	+			423	STO	17	
379	+			424	4		
380	*			425	X=Y?		
381	6			426	SF	01	
382	/			427	RCL	IND	
383	ISG	17		19			
384	X<>	IND		428	FS?C	01	
17				429	CHS		
385	ST+	IND	STATIC FUNCTION	430	XEQ	17	
17			LEFT	431	ST+	IND	STATIC FUNCTION
386	X<>	16		17			RIGHT
387	RCL	15		432	XEQ	07	
388	+			433	ISG	19	
389	X<>Y			434	GTO	11	
390	4			435	SF	02	
391	/			436	FC?	03	
392	*			437	XEQ	12	
393	RCL	16		438	RCL	10	
394	+			439	RCL	11	
395	STO	15		440	-		
396	RDN			441	X=0?		
397	DSE	08		442	GTO	14	
398	GTO	10		443	GTO	19	
399	XEQ	07		444	♦LBL	17	
400	FS?	03		445	RCL	18	
401	GTO	22		446	3		
402	RCL	11		447	+		
403	FRC			448	RCL	IND	
404	X=0?			X			
405	GTO	22		449	STO	23	
406	XEQ	13		450	R↑		
407	♦LBL	22		451	R↑		
408	RCL	20		452	RTN		
409	GTO	19		453	♦LBL	07	
410	♦LBL	11		454	FS?	06	
411	FS?C	02		455	GTO	00	

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
456	FS?	07	FINDS EITHER	499	RCL 23		
457	GTO	01	M MAX OR Y MAX	500	RCL IND		
458	FC?	08	AND THEIR LOC.	17			
459	RTN		DEPENDING ON	501	X<=Y?		
460	RCL	18	ACCURACY INPUTED	502	RTN		
461	3		AS .d.MAX	503	XEQ 22		
462	+			504	RTN		
463	RCL IND			505	LBL 23		
X				506	X<>Y		
464	RCL 23			507	XEQ 21		
465	*			508	1		
466	X=0?			509	ST- IND		
467	X>0?			Y			
468	RTN			510	R↑		
469	SF 07			511	R↑		
470	XEQ 21			512	RTN		
471	RCL 11			513	LBL 22		
472	STO IND			514	FS? 05		
Y				515	GTO 01		
473	RTN			516	1728		
474	LBL 01			517	*		
475	FS? 08			518	RCL 22		
476	RTN			519	/		
477	XEQ 21			520	STO 27		
478	RCL 11			521	RTN		
479	RCL IND			522	LBL 01		
Y				523	STO 25		
480	X=Y?			524	RTN		
481	RTN			525	LBL 21		
482	SF 06			526	24		
483	RCL 18			527	2		
484	3			528	FS? 05		
485	+			529	CLX		
486	RCL IND			530	+		
X				531	RTN		
487	RCL 23			532	LBL 11		
488	X>Y?			533	RCL IND		
489	XEQ 23			19			
490	X<>Y			534	FS? 03		
491	XEQ 22			535	GTO 01		
492	RTN			536	X=0?		
493	LBL 00			537	XEQ 12		
494	XEQ 21			538	LBL 01		
495	RCL 11			539	RCL IND		
496	RCL IND			19			
Y				540	RND		
497	X=Y?			541	GTO 19		
498	RTN			542	LBL 12		

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
543	RCL	17		588	SF	12	DISPLAYS
544	RCL	18		589	-MAXIMUM		M MAX OR Y MAX
545	3			-			
546	+			590	FS?	05	
547	X=Y?			591	GTO	01	
548	RTN			592	-F Y-		
549	♦LBL	13	DISPLAYS Xi AND	593	AVIEW		
550	-X=		STATIC FUNCTION	594	CF	12	
551	ARCL	11		595	CLA		
552	-F -			596	RCL	27	
553	RCL	18		597	ARCL	X	
554	3			598	-F/I AT		
555	+			X=			
556	RCL	IND		599	ARCL	26	
X				600	AVIEW		
557	FC?	00		601	GTO	00	
558	GTO	IND		602	♦LBL	01	
18				603	RCL	25	
559	RCL	22		604	RCL	13	
560	/			605	ABS		
561	1728			606	X<=Y?		
562	*			607	GTO	02	
563	GTO	IND		608	STO	25	
18				609	0		
564	♦LBL	01		610	STO	24	
565	-F0-			611	♦LBL	02	
566	GTO	05		612	RCL	25	
567	♦LBL	02		613	RCL	05	
568	-FM-			614	ABS		
569	GTO	05		615	X<=Y?		
570	♦LBL	03		616	GTO	02	
571	-FS-			617	STO	25	
572	GTO	05		618	RCL	10	
573	♦LBL	04		619	STO	24	
574	-FY-			620	♦LBL	02	
575	♦LBL	05		621	-F M-		
576	FC?	21		622	AVIEW		
577	TONE	.6		623	CF	12	
578	-F=			624	CLA		
579	RND			625	ARCL	25	
580	ARCL	X		626	-F AT X=		
581	AVIEW			-			
582	RTN			627	ARCL	24	
583	♦LBL	14		628	AVIEW		
584	CF	02		629	♦LBL	00	
585	FC?C	06		630	FS?	05	
586	STOP			631	STOP		
587	CF	07		632	RCL	27	

Note: Refer to "HP-41C OWNER'S HANDBOOK AND PROGRAMMING GUIDE" for specific information on keystrokes. The Function Index is found at the very back of the Handbook. Refer to Appendix E in 67 or 97 "OWNER'S HANDBOOK AND PROGRAMMING GUIDE" for exact keystrokes.

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
633	FC?	04		681	STO 37		
634	GT0	04		682	"RT?"		
635	ST+	28		683	PROMPT		
636	CF	00		684	STO 38		
637	RCL	10		685	LBL F		TESTES BEAM
638	20			686	SF 00		AGAINST LOADING
639	/			687	SF 01		CONDITIONS
640	XEQ	21		688	XEQ 18		
641	PSE			689	CLA		
642	RCL	25		690	ADV		
643	2			691	SF 12		
644	/			692	"BEAM"		DISPLAYS DATA
645	"TRY S>"		DISPLAYS S MIN	693	AVIEW		OF BEAM TESTED
646	ARCL X		AND I MIN REQ'D	694	CLA		
647	AVIEW			695	ARCL 31		
648	STOP			696	"I "		
649	LBL 04			697	ARCL 32		
650	CHS			698	AVIEW		
651	STO 28			699	CF 12		
652	STOP			700	ADV		
653	LBL 15			701	"E="		
654	"I="			702	ARCL 22		
655	ARCL X			703	AVIEW		
656	AVIEW			704	"I="		
657	RTN			705	ARCL 33		
658	LBL H		STORES BEAM	706	AVIEW		
659	"BEAM?"		DATA INPUTED	707	"S="		
660	AON			708	ARCL 34		
661	PROMPT			709	AVIEW		
662	ASTO 31			710	"D/AF="		
663	"WT?"			711	ARCL 35		
664	PROMPT			712	AVIEW		
665	ASTO 32			713	"BF="		
666	ADFF			714	ARCL 36		
667	"I?"			715	AVIEW		
668	PROMPT			716	"TF="		
669	STO 33			717	ARCL 37		
670	"S?"			718	AVIEW		
671	PROMPT			719	"RT="		
672	STO 34			720	ARCL 38		
673	"D/AF?"			721	AVIEW		
674	PROMPT			722	ADV		
675	STO 35			723	RCL 10		
676	"BF?"			724	20		
677	PROMPT			725	/		
678	STO 36			726	"YBa="		
679	"TF?"			727	ARCL X		
680	PROMPT						

00

PROGRAM LISTING

□ 67 □ 97 ■ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
728	AVIEW			776	AVIEW		
729	RCL 27			777	GTO 00		
730	RCL 33			778♦	LBL 26		
731	/			779	XEQ 18		
732	"YB="			780♦	LBL 00		
733	ARCL X			781	ADV		
734	"F AT "			782	CLA		
735	ARCL 26			783	SF 12		
736	AVIEW			784	ARCL 29		
737	X<=Y?			785	"F"		
738	GTO 00			786	ARCL 30		
739	"YB "			787	AVIEW		
740	XEQ 09			788	CF 12		
741	LASTX			789	"Fb="		
742	*			790	ARCL 39		
743	X<>Y			791	AVIEW		
744	XEQ 21			792	RCL 39		
745♦	LBL 00			793	RCL 34		
746	RCL 10			794	*		
747	30			795	12		
748	/			796	/		
749	"YLa="			797	"MMA="		
750	ARCL X			798	ARCL X		
751	AVIEW			799	AVIEW		
752	RCL 28			800	RCL 25		
753	ABS			801	X<=Y?		
754	RCL 33			802	GTO 02		
755	/			803	"MMB "		
756	"YL="			804	XEQ 09		
757	ARCL X			805	AVIEW		
758	"F AT "			806♦	LBL 02		
759	ARCL 26			807	RCL 39		
760	AVIEW			808	/		
761	X<=Y?			809	12		
762	GTO 01			810	*		
763	"YL"			811	"SX = "		
764	XEQ 09			812	ARCL X		
765	AVIEW			813	AVIEW		
766	X<>Y			814	RCL 34		
767	RCL 28			815	X<>Y		
768	X<>Y			816	X<=Y?		
769	/			817	GTO 01		
770	XEQ 21			818	"SX "		
771♦	LBL 01			819	XEQ 09		
772	"MMB="			820	AVIEW		
773	ARCL 25			821	RCL 25		
774	"F AT "			822	12		
775	ARCL 24			823	*		

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□ 67 □ 97 ■ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
824	RCL 39			870	ASTO 29		
825	/			871	31.7		
826	"TRY S>"			872	RCL 36		
827	ARCL X			873	RCL 37		
828	AVIEW			874	/		
829	♦LBL 01			875	X>Y?		
830	FC?C 01			876	GTO 00		
831	FS?C 00			877	2		
832	GTO 26			878	/		
833	STOP			879	10.8		
834	♦LBL 09			880	X<>Y		
835	"EXCEED			881	X>Y?		
836	S "			882	GTO 02		
837	RTN			883	24		
838	♦LBL 21			884	STO 39		
839	/			885	GTO 05		
840	"TRY I>"			886	♦LBL 00		
841	ARCL X			887	2		
842	AVIEW			888	/		
843	RTN			889	♦LBL 02		
844	♦LBL 18			890	-.432		
845	RCL 36			891	*		
846	12.67			892	28.44		
847	*			893	+		
848	12			894	STO 39		
849	/			895	GTO 05		
850	556			896	♦LBL 01		
851	RCL 35			897	RCL 30		
852	/			898	RCL 10		
853	12			899	X<=Y?		
854	/			900	X<>Y		
855	FC? 00			901	STO 30		
856	GTO 00			902	"L="		
857	X<=Y?			903	ASTO 29		
858	X<>Y			904	♦LBL 03		
859	STO 30			905	RCL 38		
860	FS? 01			906	X=0?		
861	GTO 01			907	GTO 02		
862	"LU="			908	53.23		
863	ASTO 29			909	RCL 30		
864	GTO 03			910	12		
865	♦LBL 00			911	*		
866	X>Y?			912	RCL 38		
867	X<>Y			913	/		
868	STO 30			914	X<=Y?		
869	"LC="			915	GTO 04		
				916	119		
				917	X<>Y		

CALCULATES
UNSUPPORTED
LENGTHS
L, LU, & LC

PROGRAM LISTING

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☐ 67 ☐ 97 ☒ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
918	X<=Y?			51			
919	GT0 03						
920	X↑2						
921	1.7 E05						
922	X<>Y						
923	/						
924	ST0 39						
925	GT0 05						
926	◆LBL 03						
927	X↑2			60			
928	-1181						
929	/						
930	24						
931	+						
932	ST0 39						
933	GT0 05						
934	◆LBL 02						
935	1 E03						
936	RCL 30						
937	/			70			
938	RCL 35						
939	/						
940	ST0 39						
941	GT0 05						
942	◆LBL 04						
943	22						
944	ST0 39						
945	◆LBL 05						
946	RCL 25			80			
947	X<>Y						
948	/						
949	END						
40				90			
50				00			

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS			STATUS	
00 bi	50 d6		* SIZE 40+	TOT. REG. 25
01 KL	51 LOAD 6		ENG	FIX x SCI ON x OFF
02 KR	52 d7		DEG x	RAD GRAD
03 Wi	53 LOAD 7		* 2 REG. REQ'D FOR EACH LOAD	
04 Oi			FLAGS	
05 Mi			#	INIT S/C
06 Si			SET INDICATES	
07 Yi			CLEAR INDICATES	
08 COUNTER			00 C	FOR Y, L LC LU
09 TOTAL LOADS			01 C	USED, L LC LU
10 L			02 C	USED
11 xi			03 C	NO DISPLAY
12 RL			04 C	INCL. LIVE LOAD NO LIVE LOAD
13 ML			05 C	FOR Q OR M FOR S OR Y
14 SL			06 C	MAG. OF M OR Y
15 RR			07 C	LOC. OF Q OR S=0
16 MR			08 C	FOR Q OR S FOR M OR Y
17 POINTER				
18 POINTER				
19 MEMORY COUNTER				
20 di				
21 d MAX				
22 E 29,000 KSI				
23 PREVIOUS Q OR S				
24 LOC. WHEN Q=0				
25 M MAX				
26 LOC. WHEN S=0				
27 Y MAX				
28 ΔY (LL-NL)				
29 L, LC, OR LU				
30 VALUE OF R29				
31 BEAM				
32 WT. OF BEAM				
33 I				
34 S				
35 D/AF				
36 BF				
37 TE				
38 RT				
39 FB				
40 d1			ASSIGNMENTS	
41 LOAD 1			FUNCTION	KEY
42 d2			FUNCTION	KEY
43 LOAD 2			FUNCTION	KEY
44 d3			FUNCTION	KEY
45 LOAD 3			FUNCTION	KEY
46 d4			FUNCTION	KEY
47 LOAD 4			FUNCTION	KEY
48 d5			FUNCTION	KEY
49 LOAD 5			FUNCTION	KEY

PROGRAM REGISTERS NEEDED: 252

ROW 1 (1: 2)



ROW 2 (2: 8)



ROW 3 (8: 15)



ROW 4 (16: 26)



ROW 5 (27: 33)



ROW 6 (34: 36)



ROW 7 (36: 39)



ROW 8 (40: 48)



ROW 9 (48: 55)



ROW 10 (56: 65)



ROW 11 (66: 76)



ROW 12 (76: 80)



ROW 13 (80: 85)



ROW 14 (86: 91)



ROW 15 (92: 95)



ROW 16 (95: 100)



ROW 17 (101: 110)



ROW 18 (111: 118)



ROW 19 (118 : 125)



ROW 20 (126 : 133)



ROW 21 (133 : 139)



ROW 22 (140 : 148)



ROW 23 (148 : 157)



ROW 24 (157 : 165)



ROW 25 (166 : 176)



ROW 26 (177 : 186)



ROW 27 (187 : 197)



ROW 28 (198 : 208)



ROW 29 (209 : 220)



ROW 30 (221 : 233)



ROW 31 (234 : 245)



ROW 32 (245 : 253)



ROW 33 (254 : 261)



ROW 34 (262 : 267)



ROW 35 (267 : 274)



ROW 36 (274 : 278)



ROW 37 (278 : 280)	
ROW 38 (280 : 281)	
ROW 39 (282 : 287)	
ROW 40 (288 : 293)	
ROW 41 (293 : 298)	
ROW 42 (299 : 304)	
ROW 43 (304 : 312)	
ROW 44 (312 : 318)	
ROW 45 (319 : 328)	
ROW 46 (329 : 339)	
ROW 47 (339 : 345)	
ROW 48 (346 : 352)	
ROW 49 (353 : 360)	
ROW 50 (361 : 367)	
ROW 51 (368 : 377)	
ROW 52 (377 : 386)	
ROW 53 (386 : 397)	
ROW 54 (397 : 403)	

ROW 55 (404 : 408)



ROW 56 (409 : 416)



ROW 57 (417 : 426)



ROW 58 (426 : 432)



ROW 59 (432 : 438)



ROW 60 (439 : 446)



ROW 61 (447 : 455)



ROW 62 (456 : 463)



ROW 63 (464 : 472)



ROW 64 (472 : 480)



ROW 65 (481 : 489)



ROW 66 (489 : 496)



ROW 67 (496 : 504)



ROW 68 (505 : 513)



ROW 69 (513 : 519)



ROW 70 (520 : 527)



ROW 71 (528 : 536)



ROW 72 (537 : 543)



ROW 73 (544 : 552)

ROW 74 (552 : 559)

ROW 75 (559 : 565)

ROW 76 (565 : 572)

ROW 77 (572 : 578)

ROW 78 (579 : 587)

ROW 79 (588 : 591)

ROW 80 (591 : 597)

ROW 81 (598 : 600)

ROW 82 (601 : 609)

ROW 83 (610 : 618)

ROW 84 (619 : 625)

ROW 85 (626 : 630)

ROW 86 (630 : 637)

ROW 87 (638 : 645)

ROW 88 (645 : 651)

ROW 89 (652 : 659)

ROW 90 (659 : 663)

ROW 91 (664 : 670)



ROW 92 (671 : 676)



ROW 93 (676 : 681)



ROW 94 (682 : 687)



ROW 95 (688 : 693)



ROW 96 (694 : 701)



ROW 97 (701 : 707)



ROW 98 (707 : 712)



ROW 99 (713 : 717)



ROW 100 (718 : 725)



ROW 101 (726 : 731)



ROW 102 (732 : 735)



ROW 103 (735 : 741)



ROW 104 (742 : 749)



ROW 105 (749 : 756)



ROW 106 (756 : 760)



ROW 107 (761 : 767)



ROW 108 (768 : 773)



ROW 109 (774 : 778)

ROW 110 (779 : 786)

ROW 111 (786 : 792)

ROW 112 (793 : 798)

ROW 113 (799 : 804)

ROW 114 (804 : 811)

ROW 115 (811 : 818)

ROW 116 (818 : 824)

ROW 117 (825 : 830)

ROW 118 (830 : 835)

ROW 119 (835 : 836)

ROW 120 (836 : 840)

ROW 121 (840 : 846)

ROW 122 (846 : 853)

ROW 123 (854 : 861)

ROW 124 (862 : 868)

ROW 125 (869 : 873)

ROW 126 (873 : 881)

ROW 127 (882 : 890)



ROW 128 (890 : 894)



ROW 129 (895 : 902)



ROW 130 (903 : 908)



ROW 131 (909 : 916)



ROW 132 (916 : 922)



ROW 133 (923 : 929)



ROW 134 (930 : 936)



ROW 135 (936 : 944)



ROW 136 (944 : 949)



Program Title *RETAINING WALL LOADS*Media Manufactured in *USA*
Software, Product of *USA*Contributor's Name *LAWRENCE BUSACK*Address *1925 HILL ROAD*City *MONACA*State/Country *PA*Zip Code *15061*

Program Description, Equations, Variables *PROGRAM CALCULATES THE RESULTANT FORCE AGAINST A WALL CAUSED BY BOTH THE SOIL ITSELF AND A UNIFORM SURCHARGE LOAD. THE SURCHARGE CAN BE OF ANY WIDTH AND CAN BE APPLIED AT ANY DISTANCE FROM THE WALL. EITHER ACTIVE OR PASSIVE SOIL PRESSURE CAN BE SPECIFIED. ADDITIONALLY AFTER THE WALL IS EVALUATED, THE PRESSURE AT ANY DEPTH CAN BE CALCULATED. NO PRINTER IS USED.*

Necessary Accessories

Operating Limits and Warnings *THE SOIL BACKFILL IS ASSUMED TO BE FREE DRAINING*

Reference(s) *JARQUIO, RAMON TOTAL LATERAL SURCHARGE PRESSURE DUE TO STRIP LOAD, JOURNAL OF THE GEOTECHNICAL ENGINEERING DIVISION, AMERICAN SOCIETY OF CIVIL ENGINEERS, NEW YORK, NEW YORK OCTOBER 1981*

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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01154C

1 Aug 18

NOTE TO USER

Program is intentionally written to exclude the printer.

PROGRAM DESCRIPTION I

Program Title

Contributor's Name

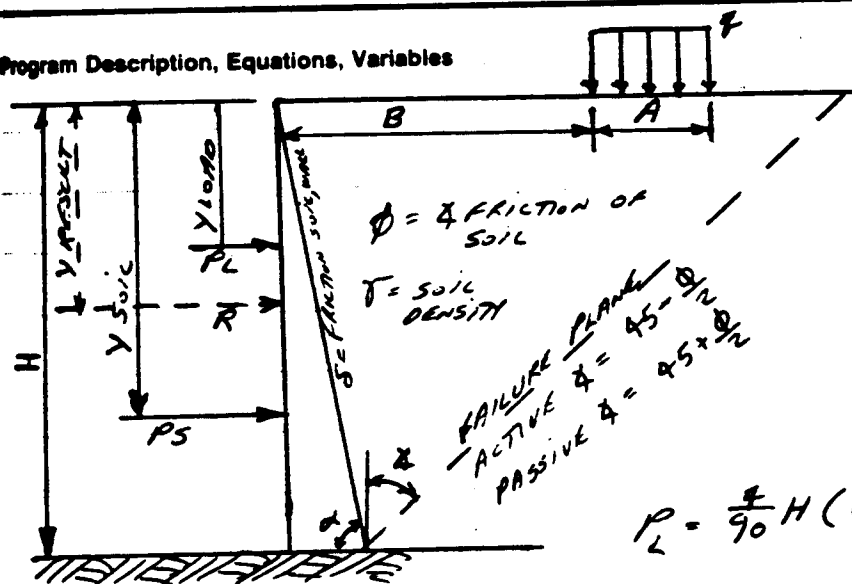
Address

City

State/Country

Zip Code

Program Description, Equations, Variables



$$\theta_1 = \tan^{-1} \left(\frac{b}{h} \right)$$

$$\theta_2 = \tan^{-1} \left(\frac{a+b}{h} \right)$$

$$P_L = \frac{\gamma}{90} H (\theta_2 - \theta_1)$$

$$Y_L = \frac{H^2 (\theta_2 - \theta_1) + (a+b)^2 (90 - \theta_2) - b^2 (90 - \theta_1) - 57.3 ah}{2h (\theta_2 - \theta_1)}$$

Necessary Accessories

Operating Limits and Warnings

Reference(s) PROGRAM HP 3095D RETAINING WALL - SOIL PRESSURES

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(CONTINUATION PAGE)

FOR ACTIVE SOIL PRESSURE

$$M = \left[\frac{\sin(\phi + \delta) \sin \phi}{\sin(\alpha - \delta) \sin \alpha} \right]^{1/2}$$

$$P_s = \frac{1}{2} \gamma H^2 K_a$$

$$K_a = \frac{\sin^2(\alpha + \phi)}{[\sin^2 \alpha \sin(\alpha - \delta)](1 + M)^2}$$

$$y_s = \frac{2H}{3}$$

FOR PASSIVE SOIL PRESSURE

$$N = \left[\frac{\sin(\phi + \delta) \sin \phi}{\sin(\alpha + \delta) \sin \alpha} \right]^{1/2}$$

$$P_s = \frac{1}{2} \gamma H^2 K_p$$

$$K_p = \frac{\sin^2(\alpha - \phi)}{[\sin^2 \alpha \sin(\alpha + \delta)](1 - N)^2}$$

$$y_s = \frac{2H}{3}$$

$$\text{RESULTANT PRESSURE } R = P_L + P_S$$

$$\text{RESULTANT LOCATION } = y_R = \frac{P_L y_L + P_S y_S}{P_L + P_S}$$

* ERROR CONDITIONS

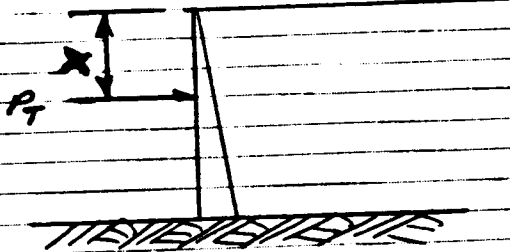
IF Δ EXTENDS BEYOND THE FAILURE PLANE
DISPLAY "BEYOND ACTIVE/PASSIVE ZONE"

IF A EXTENDS BEYOND THE FAILURE PLANE,
REDUCE A TO BE WITHIN FAILURE PLANE AND
DISPLAY "PARTIALLY BEYOND ACTIVE/PASSIVE ZONE"

$$A_{\text{CORRECTED}} = H \tan\left(45 - \frac{\phi}{2}\right) - b \quad \text{FOR ACTIVE ZONE}$$

$$A_{\text{CORRECTED}} = H \tan\left(45 + \frac{\phi}{2}\right) - b \quad \text{FOR PASSIVE ZONE}$$

(CONTINUATION PAGE)

PRESSURE AT ANY DEPTH

X = DISTANCE FROM TOP OF WALL TO PRESSURE

P_T = TOTAL PRESSURE ON WALL AT DISTANCE X

P_{XS} = PRESSURE CAUSED BY SOIL

P_{XL} = PRESSURE CAUSED BY SURCHARGE LOAD

$$P_T = P_{XS} + P_{XL}$$

$$P_{XS} = \delta H K$$

$$P_{XL} = \frac{2q}{\pi} \left\{ \frac{1}{57.3} \left[\tan^{-1} \left(\frac{a+b}{x} \right) - \tan^{-1} \left(\frac{b}{x} \right) \right] - \frac{(a+b)x}{(a+b)^2 + x^2} + \frac{bx}{b^2 + x^2} \right\}$$

ERROR MESSAGES

IF $X > H$ DISPLAY "DISTANCE BELOW WALL"

VARIABLES:

H = HEIGHT OF WALL

ϕ = INTERNAL FRICTION OF SOIL, DEGREES

δ = FRICTION BETWEEN SOIL AND WALL, DEGREES

α = ANGLE OF BACK SIDE OF RETAINING WALL, DEGREES

γ = DENSITY OF SOIL, lbs/ft^3

q = UNIFORM SURCHARGE LOAD, lbs/ft^2

A = WIDTH OF SURCHARGE LOAD, ft

B = DISTANCE FROM BACK OF WALL TO THE SURCHARGE LOAD, ft

P_L = LOAD ON WALL CAUSED BY SURCHARGE LOAD, lbs

Y_L = DISTANCE FROM TOP OF WALL TO APPLICATION OF LOAD, ft

P_S = LOAD ON WALL CAUSED BY SOIL, lbs

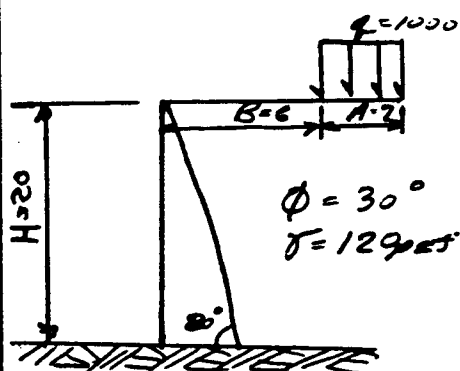
Y_S = DISTANCE FROM TOP OF WALL TO APPLICATION OF SOIL LOAD, ft

R = RESULTANT LOAD, lbs

Y_R = DISTANCE FROM TOP OF WALL TO APPLICATION OF RESULTANT LOAD, ft

PROGRAM DESCRIPTION II

Sample Problem (Sketch if Desired)



A WALL IS 20 FEET HIGH WITH A BACKSLOPE OF 80°. THE WALL IS BACKFILLED WITH SOIL AT A UNIT WEIGHT OF 120 pcf. THE FRICTION ANGLE IS 30°. THE FRICTION BETWEEN SOIL AND WALL IS 20°. A LOAD OF 1000 pcf IS APPLIED OVER A 7 FOOT WIDE AREA 6 FEET BEHIND THE WALL. FIND THE LOADS FOR BOTH ACTIVE AND PASSIVE SOIL PRESSURE, ALSO FIND THE PRESSURE AT 5 AND 10 FEET BELOW THE TOP OF WALL

SOLUTION:

Input	Function	Display	Comments
	XEQ "WALL"	WALL LOAD	
		HEIGHT? 0.00	
HEIGHT = 20	20 R/S	L SOIL? 0.00	
L SOIL = 30	30 R/S	L WALL? 0.00	
L WALL = 20	20 R/S	L WALSL? 0.00	
L WALSL = 80	80 R/S	DENSE? 0.00	
DENSITY = 120	120 R/S	LOAD? 0.00	
LOAD = 1000	1000 R/S	WALDIS? 0.00	
WALDIST = 6	6 R/S	LOADWID? 0.00	
LOADWIDTH = 7	7 R/S	DATA OK Y/N	IF DATA HAS BEEN CORRECTLY ENTERED ENTER Y - PROGRAM WILL CONTINUE
			IF DATA HAS BEEN INCORRECTLY ENTERED ENTER N - PROGRAM WILL GO BACK TO HEIGHT?
			IF INPUT IS CORRECT ENTER R/S, IF INCORRECT ENTER NEW INPUT

(CONTINUATION PAGE)

INPUT	FUNCTION	DISPLAY
	R/S	DENSE? 120.00 NO CHANGE, ENTER R/S
	R/S	LOAD? 1,000.00 NO CHANGE, ENTER R/S
	R/S	WALDIS? 6.00 NO CHANGE, ENTER R/S
	R/S	LOADWID? 7.00 NO CHANGE, ENTER R/S
		DATA OK Y/N DATA IS OK, ENTER Y
Y R/S	ACT/PASS?	FOR PASSIVE SOIL PRESSURES ENTER PASS
PASS R/S		R = 110,433.72 } OVERALL RESULTANT
R/S		Y RESULT = 13.17 }
R/S		PL = 3627.69 } PORTION OF RESULTANT CREATED BY SURCHARGE
R/S		Y LOAD = 8.42 }
R/S		PS = 106,806.02 } PORTION OF RESULTANT CREATED BY SOIL
R/S		Y SOIL = 13.33 }
R/S		K = 4.45 COEFFICIENT OF PASSIVE SOIL PRESSURE
		WALPRES Y/N
Y R/S		DISTANCE?
DISTANCE = 5	5 R/S	PRES = 2,978.46 WALL PRESSURE AT 5 FEET
		NUPRES Y/N
Y R/S		DISTANCE?
DISTANCE = 10	10 R/S	PRES = 5,552.01 WALL PRESSURE AT 10 FEET
	R/S	NUPRES Y/N
	N R/S	NUWALL Y/N
AS A SECOND PROBLEM ASSUME THE SAME WALL WITH NO SURCHARGE LOAD THEREFORE ENTER Y		

(CONTINUATION PAGE)

INPUT	FUNCTION	DISPLAY
Y R/S	ACT/PASS?	CHOOSE BETWEEN ACTIVE OR PASSIVE SOIL PRESSURE
ACT R/S		PARTIALLY BEYOND ACTIVE ZONE
		$R = 12,001.36$ } OVERALL RESULTANT
R/S	$Y_{RESULT} = 12.05$	
R/S	$PL = 2,955.72$	} PORTION OF RESULTANT CAUSED BY SURCHARGE LOAD
R/S	$Y_{LOAD} = 8.13$	
R/S	$PS = 9,045.64$	} PORTION OF RESULTANT CAUSED BY SOIL
R/S	$Y_{SOIL} = 13.33$	
R/S	$K = 0.38$	COEFFICIENT OF ACTIVE SOIL PRESSURE
R/S	WALPRES Y/N	ENTER Y TO CALCULATE PRESSURES AT 5' & 10' BELOW TOP OF WALL
Y R/S	DISTANCE?	DISTANCE BELOW WALL IS 5'
5 R/S	$PRES = 489.22 \text{ lbs/ft}^2$	PRESSURE AT 5 FEET
R/S	NUPRES Y/N	ENTER Y TO CALCULATE PRESSURE AT 10 FEET BELOW WALL
Y R/S	DISTANCE?	
DISTANCE = 10	10 R/S	$PRES = 619.67 \text{ lbs/ft}^2$ AT 10 FEET BELOW WALL
R/S	NUPRES Y/N	ENTER N TO CONTINUE PROGRAM
N R/S	NUWALL Y/N	SINCE PASSIVE SOIL PRESSURE RESULTS ARE ALSO DESIRED ENTER Y TO RETURN TO INPUT SECTION OF PROGRAM.
Y R/S	HEIGHT? 20.00	HEIGHT IS THE SAME, THEREFORE NO CHANGE IS REQUIRED, ENTER R/S
R/S	L SOIL? 30.00	NO CHANGE, ENTER R/S
R/S	L WALL? 20.00	NO CHANGE, ENTER R/S
R/S	L WALSL? 80.00	NO CHANGE, ENTER R/S

(CONTINUATION PAGE)

INPUT	FUNCTION	DISPLAY	
	Y R/S	HEIGHT? 20.00	OK, ENTER R/S
	R/S	L SOIL? 30.00	
	R/S	L WALL? 20.00	
	R/S	L WALSL? 80.00	
	R/S	DENSE? 120.00	
	R/S	LOAD? 1000.00	LOAD IS NOW 0
0	R/S	DATA OK Y/N	DATA IS OK, ENTER Y
	Y R/S	ACT/PASS?	EVALUATE ONLY THE ACTIVE CASE
	ACT R/S	PS = 9,045.64	} SINCE NO SURCHARGE IS APPLIED ONLY SOIL RESULTS ARE SHOWN
	R/S	Y SOIL = 13.33	
	R/S	K = 0.38	
	R/S	WALPRES Y/N	
	Y R/S	DISTANCE?	
DISTANCE = 5.5	R/S	PRES = 226.14	PRESSURE FROM SOIL PRESSURE ONLY
	R/S	NUPRES Y/N	
	Y R/S	DISTANCE?	
DISTANCE = 10	10 R/S	PRES = 452.28	
	R/S	NUPRES Y/N	
	N R/S	NUWALL Y/N	ALL CALCULATIONS ARE COMPLETE, ENTER N R/S
	N R/S	WALL LOAD HEIGHT? 0.00	

USER INSTRUCTIONS

SIZE:
(HP-41C)

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	LOAD PROGRAM			
2			REQ "WALL"	WALL LOAD
2A				HEIGHT? 0.00*
3	ENTER HEIGHT, ft		R/S	L SOIL? 0.00*
4	ENTER SOIL FRICTION ϕ , DEG.		R/S	L WALL? 0.00*
5	ENTER WALL FRICTION δ , DEG.		R/S	L WALSL? 0.00*
6	ENTER BACKSLOPE OF WALL α , DEG		R/S	DENSE? 0.00*
7	ENTER SOIL DENSITY γ , lbs/ft ³		R/S	LOAD? 0.00*
8	ENTER APPLIED SURCHARGE, q, lbs/ft ²		R/S	
	IF SURCHARGE IS ZERO (SKIP TO STEP 9)		R/S	DATA OK Y/N
	IF SURCHARGE IS NOT ZERO		R/S	WALDIS? 0.00*
8A	ENTER DISTANCE FROM LOAD TO POINT OF APPLICATION, ft		R/S	LOADWID? 0.00*
8B	ENTER WIDTH OF LOAD, ft		R/S	DATA OK Y/N
9	IF DATA IS OK ENTER "Y" PROGRAM GOES TO STEP 10		R/S	ACT/PASS?
	IF DATA IS NOT OK, ENTER "N", PROGRAM RETURNS TO STEP 2A			

* AFTER FIRST USE OF PROGRAM, 0.00 IS REPLACED BY
CURRENT VALUE OF DATA

USER INSTRUCTIONS

				SIZE: (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
10	IF ACTIVE SOIL PRESSURE IS TO BE USED		"ACT" R/S	*
	IF PASSIVE SOIL PRESSURE IS TO BE USED		"PASS" R/S	*
	* IF ERROR MESSAGES ARE NEEDED THEY WILL BE DISPLAYED FIRST THEN PROGRAM GOES TO STEP <u>11</u> MESSAGES:			
	① PARTIALLY BEYOND ACTIVE ZONE ② BEYOND ACTIVE ZONE ③ PARTIALLY BEYOND PASSIVE ZONE ④ BEYOND PASSIVE ZONE			
	* IF NO SURCHARGE LOAD HAS BEEN ENTERED NO ERROR MESSAGES WILL BE DISPLAYED. PROGRAM SKIPS TO STEP <u>15</u>			
11				R = ⊗
12			R/S	YRESULT = ⊗
13			R/S	PL = ⊗
14			R/S	YLOAD = ⊗
15			R/S	PS = ⊗

USER INSTRUCTIONS

SIZE:
(HP-41C)

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
16			R/S	$\gamma_{SOIL} = *$
17			R/S	$K = *$
	$*$ CURRENT VALUE IS DISPLAYED			
18	IF WALL PRESSURES ARE DESIRED ENTER "Y" PROGRAM GOES TO STEP <u>19</u>		R/S	WALL PRES Y/N
	IF NO WALL PRESSURES ARE DESIRED ENTER "N" PROGRAM GOES TO STEP <u>21</u>		Y R/S	DISTANCE? -
			N R/S	NO WALL Y/N
19	ENTER DISTANCE, X, BELOW WALL		R/S	DISTANCE? \leftarrow PRES = $*$
	$*$ CURRENT VALUE IS DISPLAYED			
20	IF ADDITIONAL WALL PRESSURES ARE DESIRED ENTER "Y" PROGRAM RETURNS TO STEP <u>19</u>		R/S	NO PRES Y/N
			Y R/S	DISTANCE?

USER INSTRUCTIONS

				SIZE: (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
	IF NO ADDITIONAL WALL PRESSURES ARE DESIRED ENTER "N" PROGRAM GOES TO STEP <u>21</u>		N R/S	NU WALL Y/N
21	IF ADDITIONAL PROBLEMS ARE TO BE RUN ENTER "Y" PROGRAM GOES TO STEP <u>2A</u>		Y R/S	HEIGHT? *
	* DISPLAYS CURRENT VALUE			
	IF NO ADDITIONAL PROBLEMS ARE TO BE RUN ENTER "N" PROGRAM GOES TO STEP 2		N R/S	WALL LOAD HEIGHT? 0.00

PROGRAM LISTING

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
*01	LBL WALL		INITIALIZE	51	LOADWID?		
*	LBL00		PROGRAM		XEQ12		
	CF21		AND DISPLAY		GTO 07		
	CL RG			*	LBL12		GENERALIZED
	WALL		TITLE		ARCL IND 20		INPUT
	AVIEW		TURN OFF		AVIEW		PROGRAM
	PSE		PRINTER		RCL IND 20		
	LOAD				SDP		
	AVIEW				STD IND 20		
10	PSE			60	RTN		
*	LBL 01		CLEAR FLAGS	*	LBL 07		ASK IF DATA
*	LBL IN		FOR NEW		DATA OK Y/N?		IS OK OR
	CF 01		RUN		AON		DOES IT NEED
	CF 02				PROMPT		TO BE CHANGED
	CF 03				AOFF		
	CF 04				ASTO X		
	0				N		
	STD 20				ASTO Y		
20	HEIGHT?				X=Y?		
	XEQ 12			70	GTO 01		CHOOSE BETWEEN
	1				ACT/PASS?		EITHER THE
	STD 20				AON		ACTIVE OR
	L SOIL?				PROMPT		PASSIVE SOIL
	XEQ 12				AOFF		STATE
	2				ASTO X		
	STD 20				PASS		
	L WALL?				ASTO Y		
	XEQ 12				X=Y?		
	3				SF 03		
30	STD 20			80	FS? 04		IF NO LOAD BYPASS
	L WALSL?				GTO 08		LOAD SURCHARGE
	XEQ 12				45		
	4				RCL 01		
	STD 20				2		
	DENSE?				/		
	XEQ 12				FS? 03		
	5				CHS		
	STD 20				-		
	LOAD?				TAN		
40	XEQ 12			90	RCL 00		IF $A \geq H \tan(45 - \frac{\phi}{2}) - b$
	XL=0?			*	RCL 06		ALL LOAD IS WITHIN ACTIVE
	SF 04				-		ZONE
	FS 04				RCL 07		IF $A \geq H \tan(45 + \frac{\phi}{2}) - b$
	GTO 07				X > Y?		ALL LOAD IS WITHIN PASSIVE
	6				SF 01		ZONE
	STD 20				FS? 01		IF NOT TOTALLY WITHIN ZONE
	WALDIS?				XL > Y		REDUCE TO BE WITHIN ZONE
	XEQ 12				XL 0?		REDUCE TO BE WITHIN ZONE
	7						
50	STD 20			100	SF 02		

PROGRAM LISTING

87 ☐ 97 ☒ 41C

STEP/	KEY ENTRY	KEY CODE	COMMENTS	STEP/	KEY ENTRY	KEY CODE	COMMENTS
LINE		(87/97 only)		LINE		(87/97 only)	
901	FS? 02		IF BEYOND ZONE	151	RCL 09		
	67 08		SKIP LOADS CAL		RCL 08		
	STD 10		ONLY 50% LOAD -		-		
	RCL 06				RCL 00		
	+		$\theta_2 = \tan^{-1} \left(\frac{a+b}{h} \right)$		X		
	RCL 00				Z		
	/				X		
	ATAN				/		
	STD 09				STD 12		
110	RCL 06			*60	LCL 08		
	RCL 00		$\theta_1 = \tan^{-1} \left(\frac{b}{h} \right)$		RCL 01		
	/				RCL 02		
	ATAN				+		
	STD 08				SIN		
	-				RCL 01		
	RCL 00				SIN		
	X		$\rho_L = \frac{r}{90} h (\theta_2 - \theta_1)$		X		
	RCL 05				RCL 03		
	X				RCL 02		
120	90			170	FS? 03		
	/				CHS		
	STD 11				-		
	RCL 09				SIN		
	RCL 08				/		
	-				RCL 03		
	RCL 00				SIN		
	X ²				/		
	X				5X		
	RCL 10				FS? 03		
130	RCL 06			180	CHS		
	+				1		
	X ²				+		
	90				X ²		
	RCL 09				RCL 03		
	-				RCL 02		
	X				FS? 03		
	+				CHS		
	90				-		
	RCL 08				SIN		
140	-			190	X		
	RCL 06				RCL 03		
	X ²				SIN		
	X				X ²		
	-				X		
	RCL 10				RCL 03		
	RCL 00				RCL 01		
	X				FS? 03		
	57.3				CHS		
	X			200	+		
150	-						

$$M = \left[\frac{\sin(\phi + \delta) \sin \phi}{\sin(\alpha - \delta) \sin \alpha} \right]^{1/2} \text{ ACTIVE ZONE}$$

$$N = \left[\frac{\sin(\phi + \delta) \sin \phi}{\sin(\alpha + \delta) \sin \alpha} \right]^{1/2} \text{ PASSIVE ZONE}$$

$$K_a = \frac{\sin^2(\alpha + \phi)}{\sin^2 \alpha \sin(\alpha - \delta) (1 + M)^2}$$

$$K_p = \frac{\sin^2(\alpha - \phi)}{\sin^2 \alpha \sin(\alpha + \delta) (1 - N)^2}$$

PROGRAM LISTING

□ 67 □ 97 ☒ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
201	SIN			251	STOP		INFO
	X ²				YLOAD=		
	X				ARCL12		
	STD13				AVIEW		
	RCL00				STOP		
	STD15		$P_s = \frac{1}{2} TH^2 K$	*	LBL10		
	X ²				PS=		DISPLAY
	X				ARCL14		
	RCL04				AVIEW		SOIL
210	X		$Y_s = \frac{2H}{3}$	260	STOP		RESULTS
	2				Y SOIL=		
	STX15				ARCL15		
	/				AVIEW		
	STD14				STOP		
	3				K=		
	STD15				ARCL13		
	FS?04		IF NO LOAD, SHOW		AVIEW		
	GTO10		ONLY SOIL RESULTS		STOP		
	FS?02		IF BEYOND ZONE		WALPRES Y/N		PROVIDE OPTION
220	GTO09		SHOW ONLY SOIL AND	270	AON		OF CALCULATION
	RCL11		DISPLAY ERROR		PROMPT		WALL PRESSURE
	STD16				AOFF		AT DEPTH
	RCL12				ASTOX		
	X				N		
	RCL14				ASTOY		
	ST+16				X=Y?		
	RCL15				GTO04		
	X				* LBL06		ENTER DEPTH
	+				DISTANCE?		BELOW WALL
230	RCL16			280	PROMPT		
	/				STD18		
	STD17				RCL00		IF BELOW WALL
	FS?01				XLO?		DISPLAY MESSAGE
	XEQ05		IF ONLY PARTIALLY		GTO02		
*	LBL09		BEYOND ZONE SHOW		FS?02		IF BEYOND ZONE
	FS?02		ALL RESULTS		0		BYPASS
	XEQ03		IF BEYOND ZONE		FS?02		SURCHARGE
	FS?02		SHOW ONLY SOIL		SP19		PRESSURES
	GTO10		AND DISPLAY ERROR		FS?02		
240	R=		DISPLAY	290	GTO11		
	ARCL16		RESULTANT		FS?04		IF NO LOAD
	AVIEW		INFORMATION		0		BYPASS
	STOP				FS?04		SURCHARGE
	YRESULT=				STD19		PRESSURES
	ARCL17				FS?04		
	AVIEW				GTO11		
	STOP				RCL10		
	PL=		DISPLAY		RCL06		
	ARCL11		SURCHARGE		+		
250	AVIEW			300	STD19		

PROGRAM LISTING

67 □ 97 41C

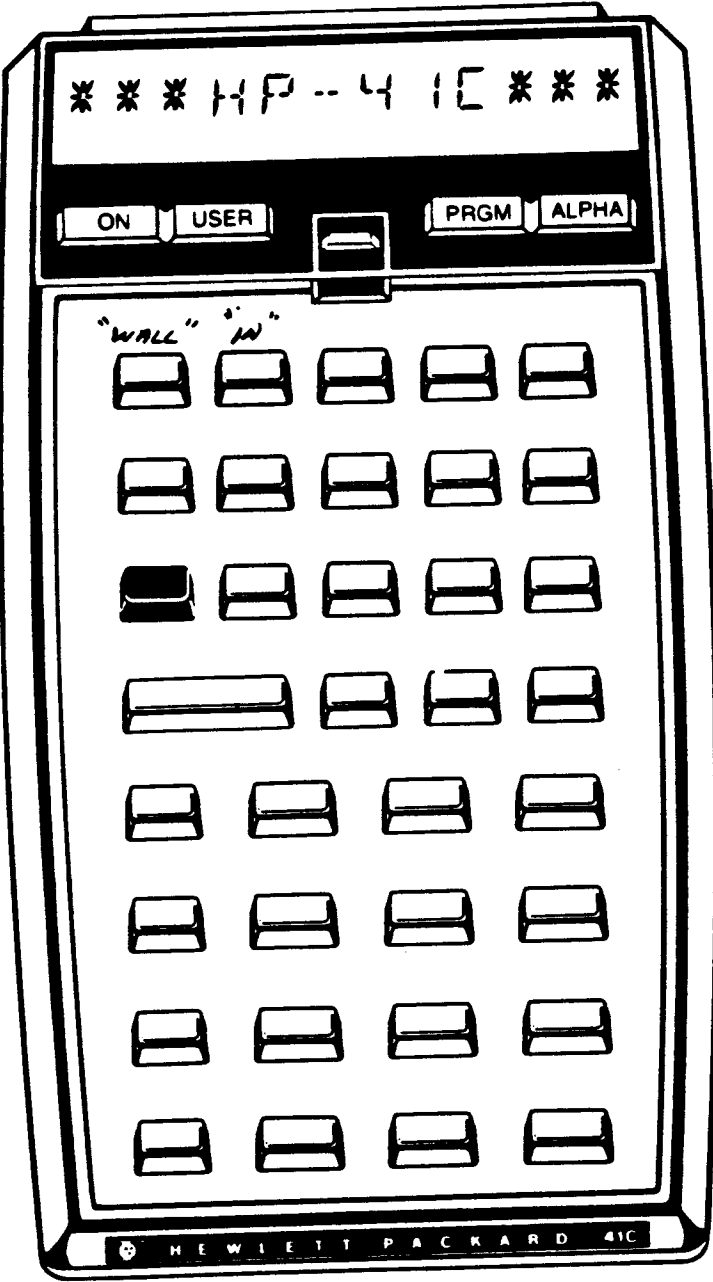
STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
301	RCL 18			351	PROMPT		ARE DESIRED
	/				ROFF		
	ATAN				ASTD X		
	RCL 06				Y		
	RCL 18				ASTD Y		
	ATAN				X=Y?		
	57.3				GTO 06		
310	/			*	LBL 04		ASK IF
	RCL 19				NUMALL Y/N		PROGRAM IS
	RCL 18			360	AON		TO BE REPEATED
	X				PROMPT		
	RCL 19				ROFF		
	X ²				ASTD X		
	RCL 18				Y		
	X ²				ASTD Y		
	+				X=Y?		
	/				GTO 01		
320	-				GTO 00		
	RCL 06			*	LBL 05		
	RCL 18			370	PARTIALLY		
	X				AVIEW		
	RCL 06				PSE		
	X ²			*	LBL 03		
	RCL 18				BEYOND		
	X ²				AVIEW		
	+				PSE		
	/				ACTIVE		
330	+				FS? 03		
	RCL 05				CLA		
	X			380	FS? 03		
	PI				PASSIVE		
	/				AVIEW		
	2				PSE		
	X				ZONE		
	SD 19				AVIEW		
	* LBL 11				PSE		
	RCL 18				RTN		
340	RCL 04			*	LBL 02		
	X				DISTANCE		
	RCL 13			390	AVIEW		
	X				PSE		
	ST+19				BELOW		
	PRES=				AVIEW		
	ARCL 19				PSE		
	AVIEW				WALL		
	STOP				AVIEW		
	NUMRES Y/N				PSE		
350	AON				GTO 06		
				399	END		
				00			

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

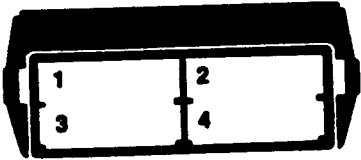
DATA REGISTERS		STATUS		
<u>INPUT</u>	<u>OUTPUT</u>	SIZE 21 ENG DEG X	TOT. REG. FIX 2 RAD SCI GRAD	USER MODE ON OFF
00 H = HEIGHT	08 θ_1	FLAGS # INIT S/C SET INDICATES CLEAR INDICATES		
01 ϕ = \angle SOIL	09 θ_2			
02 δ = \angle WALL	10 A CORRECTED	01 C PARTIALLY BEYOND WITHIN ZONE ZONE 02 C BEYOND ZONE WITHIN ZONE 03 C PASSIVE ZONE ACTIVE ZONE 04 C NO LOAD LOAD		
03 α = \angle WALSL	11 PL			
04 γ = DENSE	12 Y LOAD	ASSIGNMENTS FUNCTION KEY FUNCTION KEY "WALL" LBL00 "IN" LBL01 NO LOAD-WALL PRESS LBL11 DATA OK LBL10 ERROR-BEYOND ZONE LBL02 SOIL ROAD LBL04 ERROR-BEYOND ZONE LBL03 NO RESULTANT LBL05 ERROR-PARTIALLY BEYOND ZONE LBL05 NO RESULTANT LBL10 DATA INPUT LBL12 NEW WALL LBL04 WALL PRESSURE LBL06		
05 q = LOAD	13 K			
06 B = WALDIS	14 PS			
07 A = LOADWID	15 Y SOIL			
	16 R			
	17 Y RESULT			
	18 X = DISTANCE			
	19 P_r = PRES			
	20 DATA LOADER			

KEYBOARD CARD LABELING

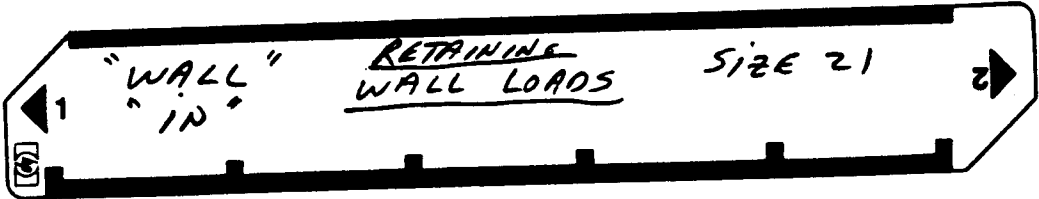
KEYBOARD



SYSTEM
CONFIGURATION



CARD



TRAINING WALL LOADS

USERS' LIBRARY
PROGRAM NUMBER: 01154C

PAGE 1
OF 4

PROGRAM REGISTERS NEEDED: 109

ROW 1 (1 : 5)

ROW 2 (6 : 10)

ROW 3 (11 : 15)

ROW 4 (16 : 19)

ROW 5 (20 : 23)

ROW 6 (24 : 27)

ROW 7 (28 : 31)

ROW 8 (32 : 35)

ROW 9 (36 : 39)

ROW 10 (40 : 43)

ROW 11 (44 : 47)

ROW 12 (48 : 51)

ROW 13 (52 : 55)

ROW 14 (56 : 59)

ROW 15 (60 : 63)

ROW 16 (64 : 67)

ROW 17 (68 : 71)

ROW 18 (72 : 75)

ROW 19 (95 : 96)

ROW 20 (96 : 104)

ROW 21 (105 : 117)

ROW 22 (118 : 129)

ROW 23 (130 : 140)

ROW 24 (141 : 150)

ROW 25 (151 : 163)

ROW 26 (164 : 175)

ROW 27 (176 : 186)

ROW 28 (187 : 198)

ROW 29 (199 : 211)

ROW 30 (212 : 219)

ROW 31 (220 : 229)

ROW 32 (230 : 236)

ROW 33 (237 : 242)

ROW 34 (243 : 246)

ROW 35 (247 : 252)

ROW 36 (253 : 258)

ROW 37 (268 : 283)

ROW 38 (284 : 299)

ROW 39 (300 : 314)

ROW 40 (315 : 329)

ROW 41 (330 : 344)

ROW 42 (345 : 359)

ROW 43 (360 : 374)

ROW 44 (375 : 389)

ROW 45 (390 : 404)

ROW 46 (405 : 419)

ROW 47 (420 : 434)

ROW 48 (435 : 449)

ROW 49 (450 : 464)

ROW 50 (465 : 479)

ROW 51 (480 : 494)

ROW 52 (495 : 509)

ROW 53 (510 : 524)

ROW 54 (525 : 539)

ROW 55 (377 : 381)



ROW 56 (381 : 387)



ROW 57 (388 : 392)



ROW 58 (392 : 396)



ROW 59 (397 : 399)



168C

PROGRAM DESCRIPTION I

Page 1 of 16

Program Title SLOPE STABILITY ANALYSIS
Contributor's Name D. Holmes Media Manufactured in USA
Address 827 15th Street Software, Product of USA
Bettendorf State/Country Iowa Zip Code 52722

Program Description, Equations, Variables

1. This program computes the safety factor, F , for slope stability analyses using the ordinary method of slices (OMS) and Bishop's modified F (submerged slopes).

2. The user must draw the shape of the slide mass and divide into vertical slices. See table below for number of slices vs. number of memory modules

Necessary Accessories	No. of Slices	No. of Mem. Mod.
Operating Limits and Warnings <u>None</u>	3	0
	19	1
	35	2
	51	3
	66	4

Reference(s) 1/ "Stability of Earth Slopes by Method of Slices," Evans, Leonard T., program # A3993D
2/ Bishop, A.W., "The Use of the Slip Circle in the Stability Analysis of Slopes," Geotechnique, Vol. 4, 1955, pp. 7-17
3/ Terzaghi, Karl and Peck, Ralph B., Soil Mechanics in Engineering Practice, John Wiley & Sons, N.Y., 1967, pp. 242-247.

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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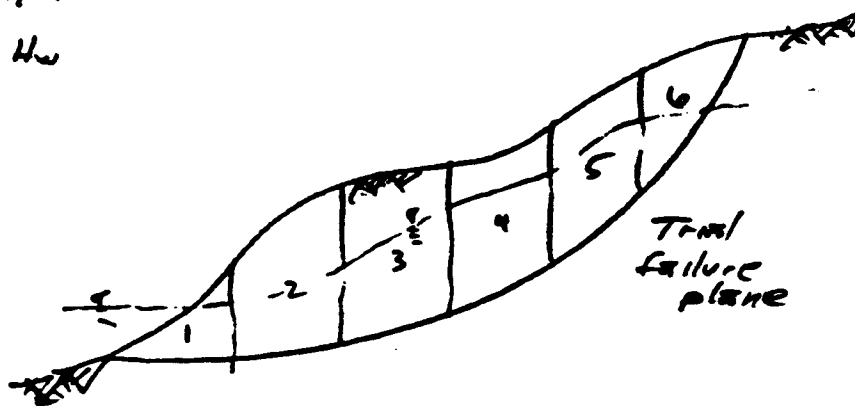
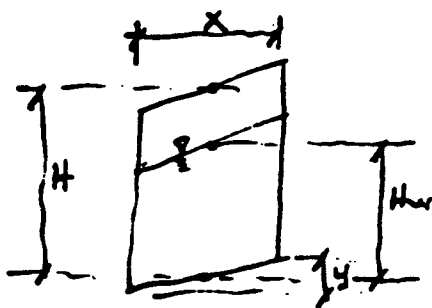
3. The following equation is used for both the OMS F and BSHP F.

$$F = \frac{\sum_{i=1}^n c x_i + (W_i \beta - u_i x_i) \tan \phi}{\cos \alpha \left[1 + \frac{\tan \alpha_i \tan \phi}{F} \right]} \quad (1) \text{ Ref 1}$$

$$\sum_{i=1}^n W_i \sin \alpha$$

where,

- γ : Soil unit weight "W"
- c : cohesion
- ϕ : friction angle of soil
- x : slice width
- y : rise of slice base
- H : height of slice at center
- H_w : height of static water table
- α : $\tan^{-1} y/x$
- γ_w : unit weight of water (62.4 lb/ft³)
- $W_i = \gamma H_i x_i$
- $u = \gamma_w H_w$



4. Ordinary Method of Slices (OMS).

a. Program solves equation (1) with the following:

$$\beta = \cos^2 \alpha$$

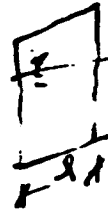
$$\delta = 0$$

b. Equation (1) is based on the following:
(non submerged slopes)

$$F = \frac{1}{\sum W_i \sin \alpha} \sum [c'l + \tan \phi' (W_i \cos \alpha - ul)]$$

where,

$$l = \frac{x}{\cos \alpha}$$



(2)

Equation 9
Ref 2/

and
Equation 35.22
Ref 3/
with $m = 1$

5. Bishop's F (submerged slopes)

a. Program solves (1) with the OMS F as the initial F and iterates until $|F_{\text{new}} - F_{\text{old}}| \leq .001$. The following conditions are set:

$$\beta = \delta = 1$$

b. Equation (1) as modified by β and δ is based on:

$$F = \frac{1}{\sum (W_1 + W_2) \sin \alpha} \sum \left[\frac{c'b + \tan \phi' (W_1 + W_2 - bu_s + (X_n - X_{n+1}))}{\cos \alpha (1 + \frac{\tan \phi' \tan \alpha}{F})} \right] \quad (3)$$

Equation 22
Ref 2/
and
Equation 35.22
Ref 3/
with $m = 1$

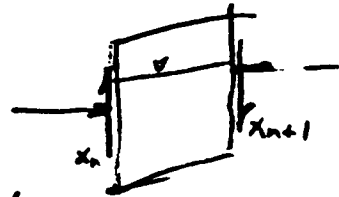
where,

$$x = b$$

$$(X_n^{\Delta x_n} - X_{n+1}) = 0$$

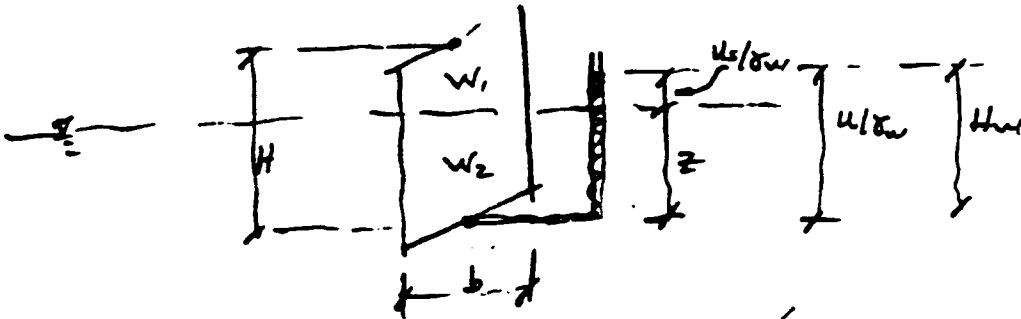
The exclusion
of Δx_n does not
significantly affect accuracy on circular arcs.

Consideration should be given to Δx_n if significant deviation from a circular failure arc.



C. Equation verification.

(1) Submerged slope, excess pore pressures



$$w_1 = (H - z)b\gamma = Hb\gamma - zb\gamma$$

$$w_2 = z\gamma_b b = zb(\gamma - \gamma_w) = zb\gamma - zb\gamma_w$$

$$bu_s = b\gamma_w(H_w - z) = b\gamma_w H_w - b\gamma_w z$$

$$w_1 + w_2 - bu_s = Hb\gamma - b\gamma_w H_w = w_1 - u_i x_i$$

(2) Non-submerged slopes, $H_w \geq 0$.

$$z = 0$$

$$w_1 = Hb\gamma$$

$$w_2 = 0$$

$$bu_s = b\gamma_w H_w$$

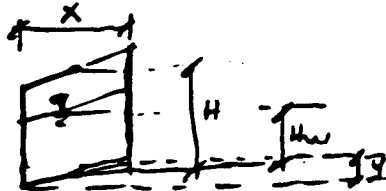
$$w_1 + w_2 - bu_s = Hb\gamma - b\gamma_w H_w = w_1 - u_i x_i$$

PROGRAM DESCRIPTION II

Sample Problem (Sketch If Desired)

Slide Data

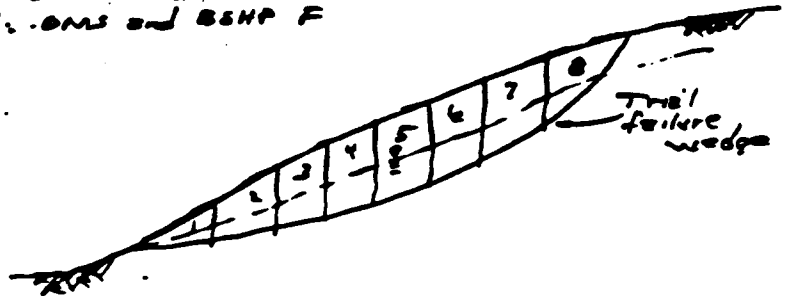
Slide No.	X	Y	H	H _w
1	5	-1.0	3	1
2	5	0	2	3
3	6	0.9	12	4
4	5	1.8	13	5
5	4	2	12	5
6	4	2.6	10	4
7	4	3.8	7	2
8	4	6	3	0

Problem 1

Given: 8 slices in Soil type I
Find: OMS and BSHP F

Problem 2

Given: Slices #1-6 in Soil type I and #7-8 in Soil II
Find: OMS and BSHP F

Soil I

$\phi = 25^\circ$
 $C = 200 \text{ psf}$
 $\gamma = \gamma_w = 125 \text{ pcf}$

Soil II

$\phi = 37^\circ$
 $C = 50 \text{ psf}$
 $\gamma = \gamma_w = 130 \text{ pcf}$

SOLUTION:

Input	Function	Display	Comments
<u>Problem 1</u>	[USER]		
	[XEQ] SIZE ***		See User instruction #6
	[XEQ] CLR6		Clears all flags for new data
	[XEQ] # 2		
	[XEQ] SLOPE	I XL = ?	
5	[R/S]	I YL = ?	
-1.0	[R/S]	I HL = ?	
3	[R/S]	I HWL = ?	
1	[R/S]	I XZ = ?	
5 etc		!	
		I XB = ?	
4	[R/S]	I YB = ?	
6	[R/S]	I HB = ?	
3	[R/S]	I HWB = ?	
6	[R/S]	I X9 = ?	
	[R/S]	I PHI? (P)	
25	[R/S]	I C? (C)	
200	[R/S]	I W? (W)	
125	[R/S]	I X9 = ?	
	[R/S]	I PHI?	
	[R/S]	VER I: A - II: B	Verify Soil I data, LBLA, etc.
	[R/S]	(Soil I verify)	Program verifies Soil I data
	[R/S]	VER II: B	Verify Soil II, LBLB
	[R/S]	OMS-BSHP: C	For OMS F and Bishop F, LBLC
	[R/S]	OMS F = 1.7003	
	[R/S]	1.7946	
	[R/S]	1.8039	
	[R/S]	BSHP F = 1.8048	

Program Description II

(CONTINUATION PAGE)

Input	Function	Display	Comments
Problem 2	[XEQ] CLR6		
	[XEQ] 00		
	[XEQ] SLOPE	I X1. = ?	
5 etc	[R6]	etc	
		!	
		II HW6. = ?	
4	[R6]	I X7. = ?	
	[R6]	I PHI? (0)	
25	[R6]	I C = ?	
200	[R6]	I W = ? (8)	
125	[R6]	II X7. = ?	
4	[R15]	II Y7. = ? etc	
		!	
		II X9. = ?	
	[R6]	II PHI = ?	
37	[R6]	II C = ?	
50	[R6]	II W = ?	
120	[R6]	YER I: A - II: B	Verify Soil I data, LBL A, etc.
	[A]	(Soil I data)	
	[B]	(Soil II data)	
		DMS - BSHP: C	
	[C]	DMS F = 1.6008	
		1.7340	
		1.7520	
		1.7537	
		BSHP F: 1.7639	

See output for Problem #2 on next page.

Program Description II (continued)

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Problem #2		Output		
XEQ -SLOPE-		II Y7.=?	3.8	RUN
I X1.=?	5.	II H7.=?	7.	RUN
I Y1.=?	-1.	II MW7.=?	2.	RUN
I H1.=?	3.	II X8.=?	4.	RUN
I MW1.=?	1.	II Y8.=?	6.	RUN
I X2.=?	5.	II H8.=?	3.	RUN
I Y2.=?	0.	II MW8.=?	0.	RUN
I H2.=?	7.	II X9.=?		RUN
I MW2.=?	3.	II PHI=?	37.	RUN
I X3.=?	6.	II C=?	50.	RUN
I Y3.=?	.9	II W=?	130.	RUN
I H3.=?	12.	VER I:A-II:B		
I MW3.=?	4.		XEQ A	
I X4.=?	5.	I X1.=5.0		
I Y4.=?	1.8	I Y1.=-1.0		
I H4.=?	13.	I H1.=3.0		
I MW4.=?	5.	I MW1.=1.0		
I X5.=?	4.	I X2.=5.0		
I Y5.=?	2.	I Y2.=0.0		
I H5.=?	12.	I H2.=7.0		
I MW5.=?	5.	I MW2.=3.0		
I X6.=?	4.	I X3.=6.6		
I Y6.=?	2.6	I Y3.=0.9		
I H6.=?	10.	I H3.=12.0		
I MW6.=?	4.	I MW3.=4.0		
I X7.=?		I X4.=5.0		
I PHI?	25.	I Y4.=1.8		
I C=?	200.	I H4.=13.0		
I W=?	125.	I MW4.=5.0		
II X7.=?	4.	I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.0		
		I Y1.=-1.0		
		I H1.=3.0		
		I MW1.=1.0		
		I X2.=5.0		
		I Y2.=0.0		
		I H2.=7.0		
		I MW2.=3.0		
		I X3.=6.6		
		I Y3.=0.9		
		I H3.=12.0		
		I MW3.=4.0		
		I X4.=5.0		
		I Y4.=1.8		
		I H4.=13.0		
		I MW4.=5.0		
		I X5.=4.0		
		I Y5.=2.0		
		I H5.=12.0		
		I MW5.=5.0		
		I X6.=4.0		
		I Y6.=2.6		
		I H6.=10.0		
		I MW6.=4.0		
		I PHI=25.0		
		I C=200.0		
		I W=125.0		
		END SOIL I		
		VER II:B		
			XEQ B	
		II X7.=4.0		
		II Y7.=3.0		
		II H7.=7.0		
		II MW7.=2.0		
		II X8.=4.0		
		II Y8.=6.0		
		II H8.=3.0		
		II MW8.=?		
		II X9.=?		
		II PHI=?		
		II C=?		
		II W=?		
		VER I:A-II:B		
			XEQ A	
		I X1.=5.		

USER INSTRUCTIONS

 SIZE: See step
(HP-41C) 6

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Enter program, set USER,			
2.	For new data entry,		[XEQ] CLR6	
			[XEQ] 22	
3.	Begin program, enter data as prompted. Must have at least two slices.		[XEQ] SLOPE	
4.	If input error discovered during Soil I data verification (LA), [RLS], [RCL] 26 for direct register address (integer portion of address only) of incorrect entry. [RCL] direct address and verify that entry displayed is incorrect entry. If the entry recalled is not the one desired, manually recall one or two registers before the above direct address. Once incorrect entry is verified, enter new value, [STO] correct direct address. [LA] for reverification			
5.	If input error discovered during Soil II data verification, (LB), [RLS], [RCL] 27 for direct address of incorrect entry and follow remaining			

User Instructions
(Continuation)

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instructions as per paragraph
#4

6.	<u>Number of Memory Modules</u>	<u>No. of Slices</u>	<u>SIZE</u>
	0	3	062
	1	19	126
	2	35	190
	3	51	254
	4	66	317

PROGRAM LISTING

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STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS
01	LBL	"SLO PE"		41	LBL	01	
02	FIX	1		42	CLA		
03	CF	22		43	LBL	05	
04	CF	10		44	CLA		
05	0.10001			45	ARCL	IND 20	
06	STO	20		46	ISG	20	
07	1.00401			47	FIX	0	
08	STO	14		48	ARCL	13	
09	50.30001			49	ARCL	12	
10	STO	28		50	CF	22	
11	1.10001			51	PROMPT		
12	STO	13		52	FS?C	22	
13	"I X"			53	GTO	02	
14	ASTO	IND 20	Data input	54	GTO	03	
15	ISG	20		55	LBL	02	
16	"I Y"			56	FIX	1	
17	ASTO	IND 20		57	STO	IND 28	
18	ISG	20		58	FS?	04	Data input
19	"I H"			59	GTO	18	
20	ASTO	IND 20		60	RCL	28	
21	ISG	20		61	STO	11	
22	"I HW"			62	SF	04	
23	ASTO	IND 20		63	LBL	18	
24	ISG	20		64	ISG	28	
25	"II X"			65	ISG	14	
26	ASTO	IND 20		66	GTO	01	
27	ISG	20		67	LBL	00	
28	"II Y"			68	ISG	13	
29	ASTO	IND 20		69	FS?	01	
30	ISG	20		70	GTO	04	
31	"II H"			71	GTO	06	
32	ASTO	IND 20		72	LBL	06	
33	ISG	20		73	0.10001		
34	"II HW"			74	STO	20	
35	ASTO	IND 20		75	1.00401		
36	ISG	20		76	STO	14	
37	"=?"			77	GTO	01	
38	ASTO	12		78	LBL	03	
39	0.10001			79	FS?	05	
40	STO	20		80	GTO	19	
				81	RCL	28	
				82	STO	18	
				83	SF	05	

PROGRAM LISTING

007 007 041C

STEP/ LINE	KEY ENTRY	KEY CODE (07/07 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (07/07 only)	COMMENTS
84	LBL 19		<i>Data input</i>	132	LBL 17		<i>Data input</i>
85	FS? 01			133	STO 08		
86	GTO 08			134	-II C=?		
87	SF 01			135	PROMPT		
88	RCL 13			136	STO 09		
89	STO 29			137	-II W=?		
90	-I PHI?			138	PROMPT		
91	PROMPT			139	STO 10		
92	STO 15			140	LBL 09		
93	-I C=?			141	-VER I:A		
94	PROMPT				-II:B		
95	STO 16			142	AVIEW		<i>LBL A verifies S.O.I data</i>
96	-I W=?			143	STOP		
97	PROMPT			144	LBL A		
98	STO 17			145	1.10001		
99	GTO 04			146	STO 22		
100	LBL 04			147	-=-		
101	FS? 02			148	ASTO 19		
102	GTO 07			149	1.00401		
103	SF 02			150	STO 21		
104	4.10001			151	RCL 11		
105	STO 20			152	STO 26		
106	CLA		<i>Data input</i>	153	LBL 11		<i>LBL A verifies S.O.I data</i>
107	1.00401			154	0.10001		
108	STO 14			155	STO 20		
109	GTO 05			156	LBL 10		
110	LBL 07			157	CLA		
111	4.10001			158	ARCL IND	20	
112	STO 20			159	ISG 20		
113	1.00401			160	FIX 0		
114	STO 14			161	ARCL 22		
115	GTO 05			162	FIX 1		
116	LBL 08		<i>Data input</i>	163	ARCL 19		<i>LBL A verifies S.O.I data</i>
117	FS? 03			164	ARCL IND	26	
118	GTO 13			165	AVIEW		
119	RCL 28			166	PSE		
120	STO 23			167	ISG 26		
121	SF 03			168	ISG 21		
122	LBL 13			169	GTO 10		
123	FS? 06			170	RCL 18		
124	GTO 09			171	INT		
125	SF 06			172	RCL 26		
126	-II PHI= ?"		<i>Data input</i>	173	INT		<i>LBL A verifies S.O.I data</i>
127	PROMPT			174	X=Y?		
128	FS?C 22			175	GTO 12		
129	GTO 17			176	ISG 22		
130	SF 10			177	1.00401		
131	GTO 09			178	STO 21		
				179	GTO 11		

PROGRAM LISTING

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STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS
180	LBL 12			224	ISG 27		
181	-I PHI=-			225	AVIEW		
182	ARCL 15			226	PSE		
183	AVIEW			227	ISG 25		
184	PSE			228	GTO 14		
185	-I C=-			229	RCL 23		
186	ARCL 16			230	INT		
187	AVIEW			231	RCL 27		
188	PSE			232	INT		
189	-I W=-			233	X=Y?		
190	ARCL 17			234	GTO 15		
191	AVIEW			235	ISG 24		
192	PSE			236	1.00401		
193	-END SOI			237	STO 25		
	L I-			238	GTO 16		
194	AVIEW			239	LBL 15		
195	PSE			240	-II PHI=-		
196	-VER II:						
	B-			241	ARCL 08		
197	AVIEW			242	AVIEW		
198	STOP			243	PSE		
199	LBL B			244	-II C=-		
200	RCL 18			245	ARCL 09		
201	STO 27			246	AVIEW		
202	RCL 23			247	PSE		
203	INT			248	-II W=-		
204	RCL 27			249	ARCL 10		
205	INT			250	AVIEW		
206	X=Y?			251	PSE		
207	GTO 20			252	LBL 20		
208	RCL 29			253	-END SOI		
209	STO 24				L II-		
210	1.00401			254	AVIEW		
211	STO 25			255	PSE		
212	LBL 16			256	-OMS-BSH		
213	4.10001				P: C-		
214	STO 20			257	AVIEW		
215	LBL 14			258	STOP		
216	CLA			259	LBL a		
217	ARCL IND			260	CF 00		
	20			261	CF 01		
218	ISG 20			262	CF 02		
219	FIX 0			263	CF 03		
220	ARCL 24			264	CF 04		
221	FIX 1			265	CF 05		
222	ARCL 19			266	CF 06		
223	ARCL IND			267	CF 07		
	27			268	CF 08		
				269	CF 09		
				270	CF 10		
				271	STOP		

PROGRAM LISTING

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STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS
272	LBL C			313	LBL 21		
273	0			314	FS? 00		
274	STO 41			315	GTO 24		
275	STO 42			316	SF 00		
276	CF 00			317	LBL 22		
277	CF 07			318	RCL 15		
278	CF 08			319	STO 34		
279	CF 09			320	RCL 16		
280	LBL 30			321	STO 35		
281	FS? 04			322	RCL 17		
282	GTO 27			323	STO 36		
283	GTO 09			324	GTO 23		
284	LBL 27			325	LBL 29		
285	FS? 08			326	SF 09		
286	GTO 28			327	FS? 10		
287	RCL 11			328	GTO 34		
288	STO 28			329	LBL 24		
289	SF 08			330	RCL 08		
290	LBL 28			331	STO 34		
291	RCL IND			332	RCL 09		
		28		333	STO 35		
292	STO 30			334	RCL 10		
293	ISG 28			335	STO 36		
294	RCL IND			336	GTO 23		
		28		337	LBL 23		
295	STO 31			338	FS? 07		
296	ISG 28			339	GTO 26		
297	RCL IND			340	1		
		28		341	STO 37		
298	STO 32			342	RCL 31		
299	ISG 28			343	RCL 30		
300	RCL IND			344	/		
		28		345	ATAN		
301	STO 33			346	STO 38		
302	ISG 28			347	COS		
303	RCL 23			348	X↑2		
304	RCL 28			349	STO 39		
305	X=Y?			350	0		
306	GTO 29			351	STO 40		
307	LBL 34			352	GTO 25		
308	RCL 28						
309	RCL 18						
310	X<=Y?						
311	GTO 21						
312	GTO 22						

LBL C
computes
OMS F,
then
BSHP's F
using
equation
#1

LBL C
(con't)

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PROGRAM LISTING

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
353	LBL	26	LBL C (cont)	400	RCL	36	LBL C (cont)
354	1			401	RCL	32	
355	STO	39		402	*		
356	STO	40		403	RCL	30	
357	RCL	31		404	*		
358	RCL	30		405	RCL	38	
359	/			406	SIN		
360	ATAN			407	*		
361	STO	38		408	ST+	42	
362	GTO	25		409	FS?	09	
				410	GTO	31	
				411	GTO	30	
363	LBL	25		412	LBL	31	
364	RCL	36		413	RCL	41	
365	RCL	32		414	RCL	42	
366	*			415	/		
367	RCL	30		416	STO	37	
368	*			417	FS?	07	
369	RCL	39		418	GTO	32	
370	*			419	SF	07	
371	62.4			420	RCL	37	
372	RCL	33		421	STO	43	
373	*			422	FIX	4	
374	RCL	30		423	OMS F=-		
375	*			424	ARCL	37	
376	-			425	AVIEW		
377	RCL	34		426	PSE		
378	TAN			427	0		
379	*			428	STO	41	
380	RCL	35		429	STO	42	
381	RCL	30		430	CF	00	
382	*			431	CF	08	
383	+			432	CF	09	
384	RCL	40		433	GTO	30	
385	RCL	34					
386	TAN			434	LBL	32	
387	*			435	1 E-3		
388	RCL	38		436	CLA		
389	TAN			437	ARCL	37	
390	*			438	AVIEW		
391	RCL	37		439	PSE		
392	/			440	RCL	37	
393	1			441	RCL	44	
394	+			442	-		
395	RCL	38		443	ABS		
396	COS			444	X<=Y?		
397	*			445	GTO	33	
398	/						
399	ST+	41					

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PROGRAM LISTING

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097 041C

[illegible]

01168C

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS			
00	"I" X ₁	50	X ₁ for Soil I	SIZE	TOT. REG. 152	USER MODE	
01	"I" Y ₁	51	Y ₁	ENG	FIX 4 SCI	ON X OFF	
02	"I" H ₁	52	H ₁	DEG: X	RAD	GRAD	
03	"I" HW ₁	53	HW ₁				
04	"II" X ₁						
05	"II" Y ₁						
06	"II" H ₁						
07	"II" HW ₁						
08	Φ ₁ storage						
09	C ₁ storage						
10	B ₁ storage						
11	USED						
12	"="						
13	USED						
14	USED						
15	Φ ₁ storage						
16	C ₁ storage						
17	B ₁ storage						
18	USED						
19	"="						
20	USED						
21	USED						
22	USED						
23	USED						
24	USED						
25	USED						
26	USED						
27	USED						
28	USED						
29	USED						
30	USED X ₁						
31	USED Y ₁						
32	USED H ₁						
33	USED HW ₁						
34	USED Φ ₁						
35	USED C ₁						
36	USED Y ₁						
37	OMS F & BSHP F						
38	α ₁						
39	β						
40	δ						
41	USED						
42	USED						
43	OMS F ₁						
44	USED						
45	OPEN						
46	OPEN						
47	OPEN						
48	OPEN						
49	OPEN						

SLOPE STABILITY ANALYSIS

USERS' LIBRARY
PROGRAM NUMBER: 01168C

PAGE 1
OF 5

PROGRAM REGISTERS NEEDED: 151

ROW 1 (1 : 3)



ROW 2 (4 : 7)



ROW 3 (7 : 9)



ROW 4 (9 : 13)



ROW 5 (13 : 18)



ROW 6 (18 : 22)



ROW 7 (22 : 27)



ROW 8 (27 : 31)



ROW 9 (31 : 35)



ROW 10 (35 : 39)



ROW 11 (39 : 47)



ROW 12 (47 : 54)



ROW 13 (54 : 60)



ROW 14 (61 : 68)



ROW 15 (68 : 73)



ROW 16 (73 : 77)



ROW 17 (77 : 83)



ROW 18 (84 : 90)



ROW 19 (90 : 93)

ROW 20 (94 : 98)

ROW 21 (99 : 104)

ROW 22 (104 : 108)

ROW 23 (109 : 113)

ROW 24 (113 : 118)

ROW 25 (118 : 125)

ROW 26 (125 : 128)

ROW 27 (129 : 134)

ROW 28 (134 : 137)

ROW 29 (138 : 141)

ROW 30 (141 : 145)

ROW 31 (145 : 148)

ROW 32 (148 : 154)

ROW 33 (154 : 161)

ROW 34 (162 : 168)

ROW 35 (169 : 177)

ROW 36 (177 : 181)

ROW 37 (181 : 185)

ROW 38 (185 : 191)

ROW 39 (192 : 194)

ROW 40 (195 : 199)

ROW 41 (199 : 207)

ROW 42 (207 : 210)

ROW 43 (211 : 214)

ROW 44 (215 : 222)

ROW 45 (222 : 229)

ROW 46 (230 : 236)

ROW 47 (236 : 240)

ROW 48 (240 : 244)

ROW 49 (244 : 248)

ROW 50 (249 : 253)

ROW 51 (253 : 256)

ROW 52 (256 : 261)

ROW 53 (261 : 267)

ROW 54 (268 : 275)

ROW 55 (275 : 281)



ROW 56 (282 : 287)



ROW 57 (288 : 294)



ROW 58 (294 : 300)



ROW 59 (301 : 307)



ROW 60 (307 : 313)



ROW 61 (313 : 319)



ROW 62 (320 : 325)



ROW 63 (326 : 332)



ROW 64 (333 : 339)



ROW 65 (339 : 346)



ROW 66 (347 : 354)



ROW 67 (355 : 362)



ROW 68 (362 : 369)



ROW 69 (369 : 376)



ROW 70 (377 : 385)



ROW 71 (385 : 395)



ROW 72 (395 : 403)



ROW 73 (404 : 411)



ROW 74 (411 : 417)



ROW 75 (418 : 423)



ROW 76 (423 : 429)



ROW 77 (429 : 435)



ROW 78 (435 : 442)



ROW 79 (443 : 450)



ROW 80 (450 : 456)



ROW 81 (456 : 460)



ROW 82 (460 : 460)



PROGRAM DESCRIPTION I

Program Title MASONRY WALL ANALYSIS
 Contributor's Name MARTIN N. POHLL
 Address 567 W. Shaw Avenue
 City FRESNO State/Country CALIF. Zip Code 93704

Source of Program Material in USA
 Source of Program Material of USA

Program Description, Equations, Variables

ANALYZES A SOLID GROUTED CONCRETE MASONRY WALL FOR COMBINED AXIAL AND
 BENDING LOADS IN ACCORDANCE WITH UNIFORM BUILDING CODE CRITERIA. PRINTER
 OUTPUT HIGHLY ANNOTATED FOR USE AS FINAL STRUCTURAL CALCULATIONS.

EQUATIONS: $NP = A_s N / b d$ VARIABLES: $P =$ AXIAL LOAD

$$K = \sqrt{(NP)^2 + 2NP} - NP$$

 $M =$ BENDING MOMENT

$$J = 1 - K/3$$

 $V =$ SHEAR

$$R = 1 - (H/40T)^3$$

 $T =$ THICKNESS

$$f_v = V / b J d$$

 $d =$ DEPTH

$$f_a = P / b T, F_a = 0.2 F'_c R$$

 $H =$ HEIGHT

$$f_b = 2M / (d^2 b j K), F_b = F'_m / 3$$

 $F'_c =$ ALLOW. COMPRESSION

$$\text{COMBINED} = f_a / F_a + f_b / F_b$$

 $N =$ MODULAR RATIO

BAR SIZE & BAR SPACING

Necessary Accessories PRINTER, MEMORY MODULEOperating Limits and Warnings DO NOT USE FOR REINFORCING BAR SIZE GREATER THAN #8.DOES NOT CONSIDER COMPRESSIVE REINFORCEMENT.Reference(s) INTERNATIONAL CONFERENCE OF BUILDING OFFICIALS,"UNIFORM BUILDING CODE", 1979 EDITION.

The program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses the program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

NEITHER HP NOR THE CONTRIBUTOR MAKES ANY EXPRESS OR IMPLIED WARRANTY OF ANY KIND WITH REGARD TO THIS PROGRAM MATERIAL, INCLUDING, BUT NOT LIMITED TO, THE IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A PARTICULAR PURPOSE. NEITHER HP NOR THE CONTRIBUTOR SHALL BE LIABLE FOR INCIDENTAL OR CONSEQUENTIAL DAMAGES IN CONNECTION WITH OR ARISING OUT OF THE FURNISHING, USE OR PERFORMANCE OF THIS PROGRAM MATERIAL.

Sample Problem (Sketch If Desired)

CANTILEVER RETAINING WALL

P = 1500 lbs/ft (includes wall weight)

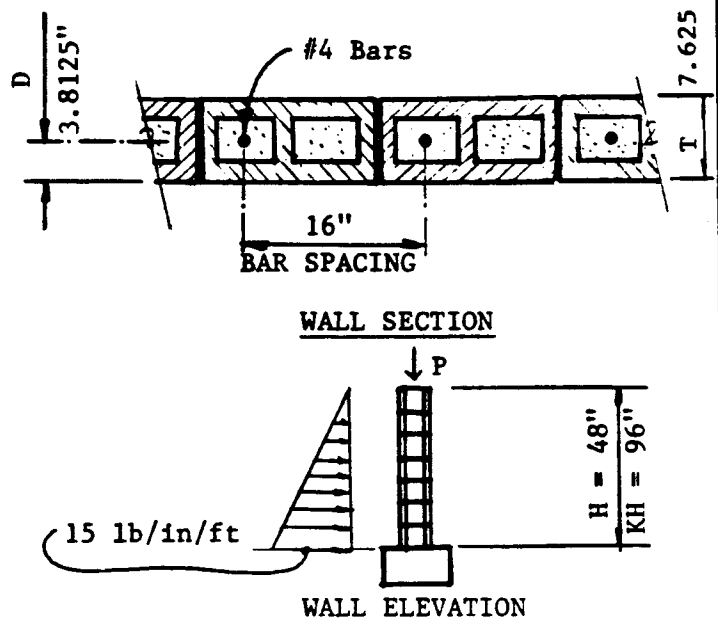
$$M = \frac{15(48)^2}{6} = 5760 \text{ in. lb/ft}$$

$$V = \frac{15(48)}{2} = 360 \quad \text{lb/ft}$$

ASSUME NO INSPECTION:

$$F'_c = 750 \text{ psi}$$

N = 40

**SOLUTION:**

Input	Function	Display	Comments
	XEQ MAS2	UNITS: IN-LBS	
	R/S	PER FT. BASIS	(Assuming
	R/S	P = 0.0	All registers were cleared prior
1500	R/S	M = 0.0	to execution)
5760	R/S	V = 0.0	
360	R/S	T = 0.0	
7.625	R/S	d = 0.0	
3.8125	R/S	H = 0.0	
96	R/S	BAR SIZE = 0.0	
4	R/S	BAR SPACING 0.0	
16	R/S	F↑c = 0.0	
750	R/S	N = 0.0	
40	R/S		
		SEE NEXT PAGE	PRINTER OUTPUT GIVEN ON NEXT PAGE
			TRY REVISED DATA
	LBL B	P=1500.000	
	R/S	M=5760.000	
	R/S	V=360.000	
	R/S	T=7.625	
	R/S	d=3.813	Revise d
5.375	R/S	H=96.000	
	R/S	BAR SIZE=4.000	
	R/S	BAR SPACING=16.000	Revise Bar spacing
32	R/S	F↑c=750.000	
	R/S	N=40.000	
		SEE NEXT PAGE	Printer output on next page

2420C PROGRAM DESCRIPTION II

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Sample Problem (Sketch if Desired)

$$A_s = \frac{\left(\frac{\text{BAR SIZE}}{8}\right)^2 \pi}{4 \left(\frac{\text{BAR SPACE}}{12}\right)}$$

$$NP = \frac{A_s N}{bd}$$

WHERE $b = 12"$

$$K = \sqrt{(NP)^2 + 2NP} - NP$$

$$J = 1 - K/3$$

$$R = 1 - \left(\frac{H}{40T}\right)^3$$

ACTUAL SHEAR STRESS

$$fv = \frac{V}{bJd}$$

ACTUAL COMPRESSIVE STRESS

$$fa = \frac{P}{bT}$$

ALLOWABLE COMPRESSIVE STRESS

$$Fa = 0.2 F'c R$$

ACTUAL BENDING STRESS

$$fb = \frac{2M}{d^2bjk} \quad \frac{2M}{d^2bjk}$$

ALLOWABLE BENDING STRESS

$$Fb = \frac{F'm}{3}$$

COMBINED STRESSES

$$\text{COMBINED} = \frac{fa}{Fa} + \frac{fb}{Fb}$$

ACTUAL STEEL TENSILE STRESS

$$fs = \frac{M}{AsJd}$$

ACTUAL BOND STRESS

$$\Sigma o = \frac{(\text{BAR SIZE}) \pi}{8 (\text{BAR SPACING}/12)}$$

$$fu = \frac{V}{\Sigma o JD}$$

SOLUTION:

PRINTER OUTPUT FROM INITIAL DATA

MASONRY WALL
units: in-lbs
per ft basis
solid grout
P = 1500
M = 5760
V = 360
T = 7.625
d = 3.813
H = 96.000
H/T = 12.590
R = 0.969
Ftc = 750.0
N = 40.0
NP = 0.1288
K = 0.3948
J = 0.8684

MAS STRESS

fv = 9.06
fa = 16.39
Fa = 145.32
fb = 192.65
Fb = 250.00
COMBINED
axial = 0.11
bend = 0.77
total = 0.88

STEEL STRESS

NO 4 at 16
As = 0.15
fs = 11814
Σo = 1.178
fu = 92.3

PRINTER OUTPUT FROM REVISED DATA

MASONRY WALL
units: in-lbs
per ft basis
solid grout
P = 1500
M = 5760
V = 360
T = 7.625
d = 5.375
H = 96.000
H/T = 12.590
R = 0.969
Ftc = 750.0
N = 40.0
NP = 0.0457
K = 0.2600
J = 0.9133

MAS STRESS

fv = 6.11
fa = 16.39
Fa = 145.32
fb = 139.95
Fb = 250.00
COMBINED
axial = 0.11
bend = 0.56
total = 0.67

STEEL STRESS

NO 4 at 32
As = 0.07
fs = 15935
Σo = 0.589
fu = 124.5

024200 USER INSTRUCTIONS

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Instructions assume all registers initially cleared

SIZE:
(HP-41C) 021

STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	ENTER THE PROGRAM		XBQ MAS2	P = 0.0
2.	INPUT VARIABLE DATA AS REQUESTED BY CALCULATOR (BASED ON ONE FOOT LENGTH OF WALL):			
	P = AXIAL LOAD	lbs/ft	R/S	M = 0.0
	M = BENDING MOMENT	in-lbs/ft	R/S	V = 0.0
	V = SHEAR	lbs/ft	R/S	T = 0.0
	T = WALL THICKNESS	inches	R/S	d = 0.0
	d = EFFECTIVE DEPTH (COMPRESSIVE FACE TO REBAR CENTROID)	inches	R/S	H = 0.0
	H = UNSUPPORTED HEIGHT OR LENGTH OF WALL (USE KH FOR OTHER THAN PINNED END CONDITIONS)	inches	R/S	BAR SIZE = 0.0
	BAR SIZE = DIAMETER ÷ 8	inches	R/S	BAR SPACING = 0.0
	BAR SPACING	inches	R/S	F _{tc} = 0.0
	F' _c = ALLOWABLE MASONRY COMPRESSIVE STRESS	psi	R/S	N = 0.0
	N = MODULAR RATIO	none	R/S	See Program Description for Output
3	IF YOU WANT TO RERUN WITH REVISED DATA,		LBL B	P- (current value
				⋮
	Revise only those variables you want	new value	R/S	Same as above
	to change or		R/S	

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STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL "MAS			43	12		
	2"			44	*		
02	SF 12			45	STO 11		
03	SF 21			46	RCL 10		
04	SF 27			47	*		$NP = \frac{As \cdot N}{bd}$
05	"UNITS: I			48	RCL 05		
	N-LBS"			49	/		WHERE b = 12"
06	AVIEW			50	12		
07	"PER FT			51	/		
	BASIS"			52	STO 12		
08	AVIEW			53	X↑2		
				54	RCL 12		
09	LBL B			55	2		
10	1			56	*		
11	STO 00			57	+		
12	FIX 3			58	SQRT		
13	"P= "			59	RCL 12		
14	XEQ 01			60	-		$K = \sqrt{(NP)^2 + 2NP} - NP$
15	"M= "			61	STO 13		
16	XEQ 01		INPUT VARIABLES	62	3		
17	"V= "			63	/		
18	XEQ 01			64	1		$J = 1 - K/3$
19	"T= "			65	-		
20	XEQ 01			66	CHS		
21	"d= "			67	STO 14		
22	XEQ 01			68	RCL 06		
23	"H= "			69	RCL 04		
24	XEQ 01			70	/		
25	"BAR SIZ			71	40		
	E= "			72	/		
26	XEQ 01			73	3		
27	"BAR SPA			74	Y↑X		
	CING= "			75	1		$R = 1 - \left(\frac{H}{40T}\right)^3$
28	XEQ 01			76	-		
29	"F↑c = "			77	CHS		
30	XEQ 01			78	STO 15		
31	"N= "			79	ADV		
32	XEQ 01			80	ADV		
33	RCL 07			81	FIX 0		
34	8			82	"MASONRY		
35	/				WALL"		
36	X↑2		$As = \frac{\left(\frac{BAR \ SIZE}{8}\right)^2 \pi}{4 \left(\frac{BAR \ SPACE}{12}\right)}$	83	AVIEW		
37	PI			84	SF 13		
38	*			85	"UNITS: I		
39	4				N-LBS"		
40	/			86	AVIEW		
41	RCL 08			87	"PER FT		
42	/				BASIS"		

PROGRAM LISTING

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
88	AVIEW			135	-NP= "		
89	-SOLID G			136	FIX 4		
ROUT-				137	RCL 12		
90	AVIEW			138	ARCL X		
91	CF 13			139	AVIEW		
92	-P = "			140	-K = "		
93	RCL 01			141	RCL 13		
94	ARCL X			142	ARCL X		
95	AVIEW			143	AVIEW		
96	-M = "			144	-J = "		
97	RCL 02			145	RCL 14		
98	ARCL X			146	ARCL X		
99	AVIEW			147	AVIEW		
100	-V = "			148	FIX 2		
101	RCL 03			149	ADV		
102	ARCL X			150	-MAS STR		
103	AVIEW		PRINT INPUT DATA	ESS-			
104	-T = "			151	AVIEW		
105	FIX 3			152	SF 13		
106	RCL 04			153	-FV = "		MASONRY STRESSES
107	ARCL X			154	RCL 03		ACTUAL SHEAR STRESS
108	AVIEW			155	RCL 05		
109	-d = "			156	/		$f_v = \frac{V}{bJd}$
110	RCL 05			157	12		
111	ARCL X			158	/		
112	AVIEW			159	RCL 14		
113	-H = "			160	/		WHERE b = 12"
114	RCL 06			161	ARCL X		
115	ARCL X			162	AVIEW		
116	AVIEW			163	-FA = "		
117	-H/T= "			164	RCL 01		ACTUAL COMPRESSIVE STRESS
118	RCL 04			165	RCL 04		
119	/			166	/		$f_a = \frac{P}{bT}$
120	ARCL X			167	12		
121	AVIEW			168	/		WHERE b = 12"
122	-R = "			169	STO 16		
123	RCL 15			170	ARCL X		
124	ARCL X			171	AVIEW		
125	AVIEW			172	CF 13		
126	-F'c= "			173	-Fa = "		
127	FIX 1			174	RCL 09		
128	RCL 09			175	RCL 15		
129	ARCL X			176	*		
130	AVIEW			177	.2		ALLOWABLE COMPRESSIVE STRESS
131	-N = "			178	*		$F_a = 0.2 F'c R$
132	RCL 10			179	STO 17		
133	ARCL X			180	ARCL X		
134	AVIEW						

PROGRAM LISTING

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
181	AVIEW			225	AVIEW		
182	SF 13			226	ADV		
183	"FB = "			227	CF 13		
184	RCL 02			228	"STEEL S		
185	2				TRESS"		
186	*			229	AVIEW		
187	RCL 05			230	FIX 0		
188	X↑2			231	"NO"		
189	/			232	ACA		
190	12			233	RCL 07		
191	/			234	ACX		
192	RCL 13			235	SF 13		
193	/			236	"AT"		
194	RCL 14			237	ACA		
195	/			238	RCL 08		
196	STO 18			239	ACX		
197	ARCL X			240	PRBUF		
198	AVIEW			241	CF 13		
199	CF 13			242	FIX 2		
200	"Fb = "			243	"A"		
201	RCL 09			244	ACA		
202	3			245	SF 13		
203	/			246	"S = "		
204	STO 19			247	ACA		
205	ARCL X			248	RCL 11		
206	AVIEW			249	ACX		
207	"COMBINE			250	PRBUF		
	D"			251	SF 13		
208	AVIEW			252	FIX 0		
209	SF 13			253	"FS = "		
210	"AXIAL =			254	RCL 02		
	"			255	RCL 11		
211	RCL 16			256	/		
212	RCL 17			257	RCL 14		
213	/			258	/		
214	ARCL X			259	RCL 05		
215	AVIEW			260	/		
216	"BEND =			261	ARCL X		
	"			262	AVIEW		
217	RCL 18			263	"Σ0 = "		
218	RCL 19			264	RCL 07		
219	/			265	RCL 08		
220	ARCL X			266	/		
221	AVIEW			267	12		
222	"TOTAL =			268	*		
	"			269	8		
223	+			270	/		
224	ARCL X			271	PI		

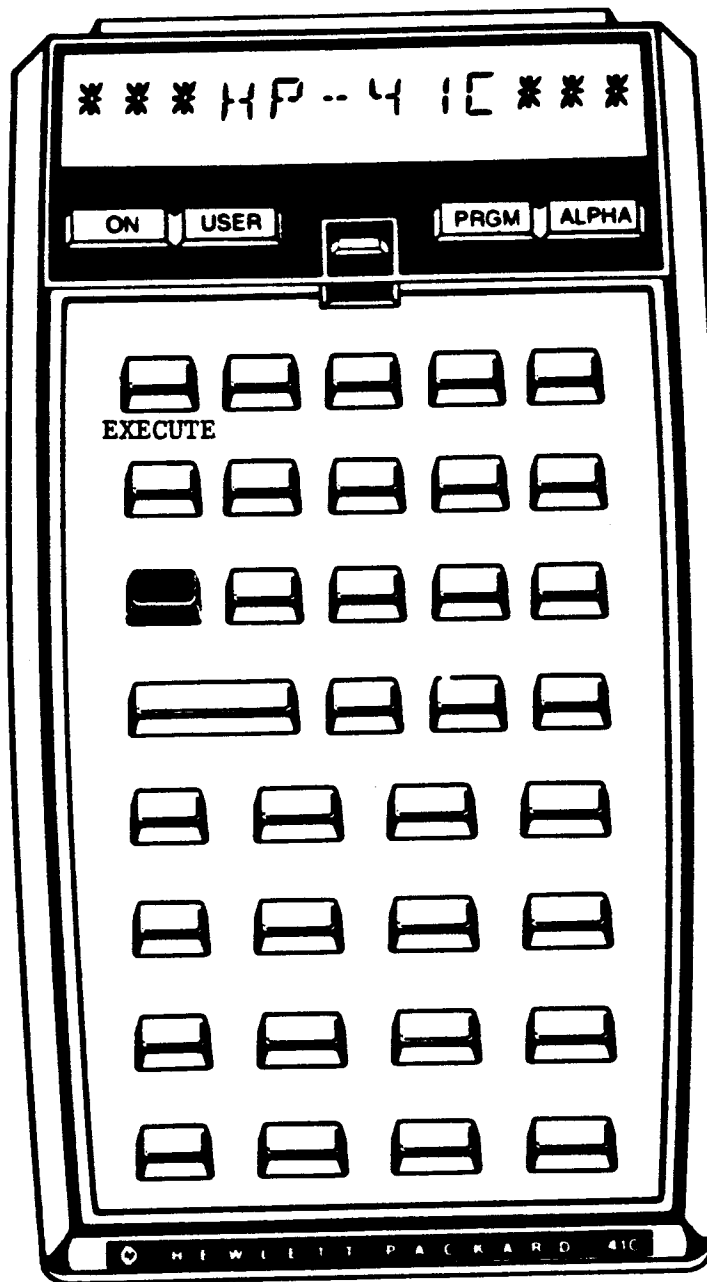
PROGRAM LISTING

□ 67 □ 97 □ 41C

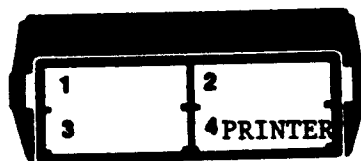
STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
272	*			51			
273	STO 20						
274	FIX 3						
275	ARCL X						
276	AVIEW						
277	-FU = -						
278	RCL 03						
279	RCL 14						
280	/			60			
281	RCL 05						
282	/		ACTUAL BOND STRESS				
283	RCL 20						
284	/		$\Sigma O = \frac{(\text{BAR SIZE}) \pi}{8 (\text{BAR SPACING}/12)}$				
285	FIX 1						
286	ARCL X						
287	AVIEW		$f_u = \frac{V}{\Sigma O JD}$				
288	CF 13						
289	RTN						
290	LBL 01			70			
291	CF 22						
292	ARCL IND						
00							
293	PROMPT						
294	FS? 22						
295	STO IND						
00							
296	1						
297	ST+ 00			80			
298	RTN						
299	.END.						
40				90			
50				00			

KEYBOARD CARD LABELING

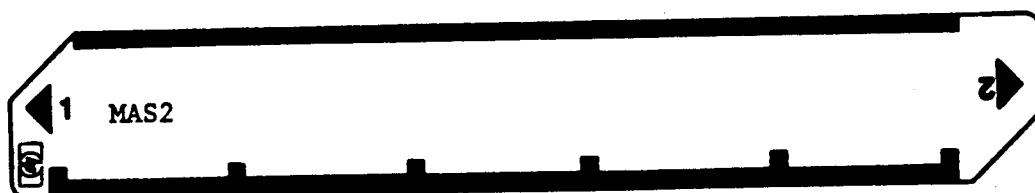
KEYBOARD



SYSTEM
CONFIGURATION



CARD



PROGRAM REGISTERS NEEDED: 99

ROW 1 (1:4)	
ROW 2 (4:5)	
ROW 3 (5:7)	
ROW 4 (7:13)	
ROW 5 (14:17)	
ROW 6 (17:21)	
ROW 7 (21:25)	
ROW 8 (25:26)	
ROW 9 (27:27)	
ROW 10 (27:30)	
ROW 11 (30:37)	
ROW 12 (38:49)	
ROW 13 (50:61)	
ROW 14 (62:73)	
ROW 15 (74:83)	
ROW 16 (83:85)	
ROW 17 (86:86)	
ROW 18 (87:88)	

ROW 19 (88 : 90)	
ROW 20 (90 : 96)	
ROW 21 (97 : 101)	
ROW 22 (101 : 107)	
ROW 23 (108 : 114)	
ROW 24 (114 : 118)	
ROW 25 (118 : 125)	
ROW 26 (125 : 130)	
ROW 27 (131 : 136)	
ROW 28 (136 : 141)	
ROW 29 (142 : 148)	
ROW 30 (149 : 151)	
ROW 31 (151 : 157)	
ROW 32 (158 : 164)	
ROW 33 (164 : 173)	
ROW 34 (173 : 179)	
ROW 35 (180 : 184)	
ROW 36 (185 : 196)	

ROW 37 (187 : 201)



ROW 38 (202 : 208)



ROW 39 (208 : 211)



ROW 40 (211 : 217)



ROW 41 (217 : 221)



ROW 42 (221 : 225)



ROW 43 (225 : 229)



ROW 44 (229 : 233)



ROW 45 (234 : 240)



ROW 46 (241 : 247)



ROW 47 (247 : 252)



ROW 48 (253 : 259)



ROW 49 (260 : 266)



ROW 50 (267 : 276)



ROW 51 (276 : 283)



ROW 52 (284 : 292)



ROW 53 (292 : 300)



ROW 54 (300 : 300)



D782C

PROGRAM DESCRIPTION I

Page / of 14

Program Title 36 BEAMS
Contributor's Name Michel Walsh
Address 824 rue principale
City St-Léonard de Portneuf State/Country Québec Zip Code GOA-4A0

Program Description, Equations, Variables Can resolve any one span strait beam,
without axial force, elastically.

V Shear

M Flexural Moment

EIT Slope of deformed beam time "EI"

EIY Deflection of deformed beam, time "EI"

See reference for equations.

For a discontinuity of a function (like a concentrated load for shear), evaluation of it at discontinuity give the value of the function at the left.

Necessary Accessories Cases with many loads need memory module.

Operating Limits and Warnings "EI" (Young modulus time Inertia) must be constant.

Reference(s) ROARK and YOUNG, "Formulas for Stress and Strain", 5^o ed., McGraw Hill.

This program has been verified only with respect to the numerical example given in Program Description // User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material

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Program Title

Contributor's Name

Address

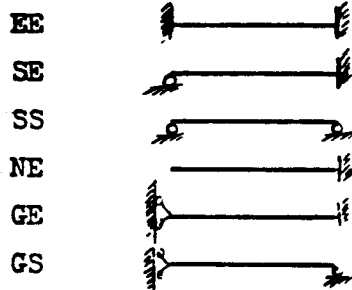
City

State/Country

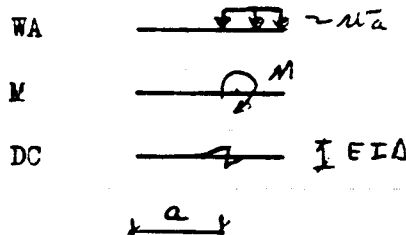
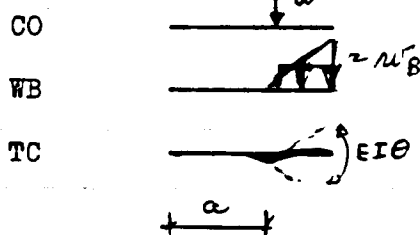
Zip Code

Program Description, Equations, Variables

The "codes" for the end restrain are as follow:



and for the six loading-cases: (they are written for EE)



Program use superposition to resolve the non-"EE" case (i.e.: SE is simply EE with an appropriate moment added to SE, obtaining so EE).

Necessary Accessories

Operating Limits and Warnings

WB can't be zero. Subroutine SE don't be erase

if you use SS or NE. Subroutine GE must don't be erase if you use GS.

Round-off errors can give such as a 10 as "EII" instead of a zero theoretic.

Don't forgot: it's EI time Y and not Y itself...

Reference(s)

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007820 USER INSTRUCTIONS

Page 3 of 14

				SIZE: Variable. (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Enter subprog. that you need. "BEAM" and "Q" must be enter. Also, "CO", "WA", "TB", "X", "TC", "DC" if it's a load acting on the beam. You can clear of memory the loads-prog. ("CO", "WA", ...) you don't need. Also you can clear end-restrain-code ("SE", "SS", ...) if it's not your case (see "warning" of PROG. DESC. I)			
2.	SIZE. If you want register 08 (R08) for your own use, write 9 in line 03 of "BEAM" and il line 11 of "FF". If you want also R09, write 10 in line 03 of "BEAM" (the same number must appear in line 11 of "FF"), and so on... If you want, say, i registers for your own, and you have j loads, size must be: $8 + i + 3j = n$ (Your registers are R08 to R(7+i) if i is greater than zero).		SIZE n	
3.	INITIALISATION for a (new) case:		XEQ'BEAM	L:
4.	Input length	L	R/S	END: alpha
5.	Input "END RESTRAIN CODE"	code	R/S	a
6.	Input "a"-length (Write negative number for out, going then to 10.)	a	R/S	C-CH: alpha
7.	Input "LOADING-CODE" for load at (or beginning at) the "a"-distance	code	R/S	VALUE
8.	Input numerical value of the "load"	value	R/S	a
9.	Repeat 5. to 8. as you want.			

007820 USER INSTRUCTIONS

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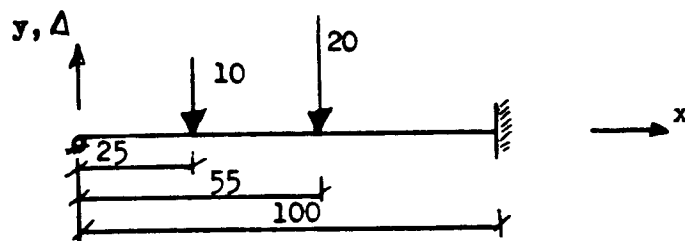
				SIZE: (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
10.	You can, here, clear all programs and then, enter "FF". Now, if you want EIX(x),EIT(x),M(x), or V(x), you execute "FF":	(No ".END." statement are written on magnetics cards, so, change "RTN" by "END" if you want "CLP".)		
11.	0 for EIX; 1 for EIT; 2 for M; 3 for V	code	XEQ'FF R/S	C-FCT: X:
12.	Input X value to obtain fct(X)	x-value	R/S	result X:
13.	For a new X (same fct) repeat 12. For a new fct, goto step 10. Note that if you want "FF" in a prog of your mind (i.e.: to find max.) without interruption: Put X in RO5 Set flag 00 Put 0,-1,-2 or -3 in RO6 to obtain, respectively EIX,EIT,M or V Use XEQ'GG instead of XEQ'FF and then, the result isn't "pause" and is return in the X-STACK. (Stack is perturbed) Remember, the same number must appear in line 03 of "BEA'" and in line 11 of "FF" .			
			(No END statement on mag.card, so number of line is different if loaded from mag. cards.)	

0782C PROGRAM DESCRIPTION II

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Sample Problem (Sketch if Desired)

1



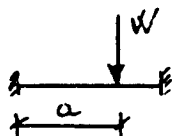
Find $EI\Delta$ at $x = \frac{1}{2}l = 50$ and at $x = 40$
 $EI\theta$ at $x = 0$
 and $V(x = 0)$.

OLUTION:

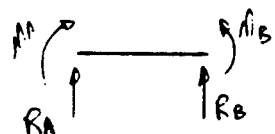
Input	Function	Display	Comments
			Since we have two loads, and no need of own-reg., size must be $8 + 23 = 31$ 14
14 14	XEQ'SIZE'		
	XEQ'BEAM'		I suppose enough space.
100	R/S	L:	Input length
SE	R/S	END alpha	It's SE
25	R/S	a	The first CO is at 25
CO	R/S	C-CH alpha	It's COncentrated load
10	R/S	W	It's intensity is 10 units
55	R/S	a	We have effectively another load.
20	R/S	C-CH alpha	COncentrated, again
1 chs	R/S	a	No more loads, put negative one.
	XEQ'FF'	C-FCT alpha	Input are finished. Goto computation.
0	R/S	X	Deflection, first, say...
50	R/S	-240846	at 50
		X	so, downward (-)
			(if the PAUSE isn't suff. to read the answer, press chs twice)
40	R/S	-246420	
		X	No more value for deflection.
	XEQ'FF'	C-FCT	For rotation, say
1	R/S	X	at simple support
0	R/S	-9084.375	(i.e.: clockwise (-))
			no more for rotation...
	XEQ'FF'	C-FCT	For shear, it's 3
3	R/S	X	at simple support
0	R/S	11.4919	
nb: evaluated shear at $x = 25.0001$, it's		$x = 25$ will give 11.4919	11.4919 and at (See page 1)

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL 'CO		Concentrated load	51	LBL 'M		Moment load
	REL IND 07		first disp. reg.		RCL 05		
1					RCL IND 07		first disp. reg.
	ST+ 07			3			
	*			*			
	'W			-			
	PROMPT			LAST x			
	CHS			RCL 05			
	STO IND 07			2			
10	RCL 05			60	*		
	X ↑ 2			-			
	/			RCL 05			
	RCL 05			RCL IND 07			
	RCL Z			ST* Z			
	*			-			
	LAST x			ST* Z			
	X <> Z			RCL IND 07			
	X ↑ 2			*			
20	*			RCL 05			
	ST+ 04			RCL 05			
	RCL T			X ↑ 2			
	/			ST/ T			
	*			ST/ Z			
	ST+ 02			/			
	X <> Y			6			
	/			*			
	RCL 05			1			
30	RCL 05			ST+ 07			
	RCL T			RDN			
	2			'M			
	*			PROMPT			
	+			ST* Z			
	*			ST* T			
	CHS			ST+ IND 07			
	ST+ 03			*			
	RCL 07			ST- 03			
	1			RIN			
40	+			ST+ 04			
	3			RDN			
	STO IND Y			ST- 02			
	2			1			
	ST+ 07			ST+ 07			
	RIN			2			
	END			STO IND 07			
				X <> Y			
				ST+ 07			
				RIN			
				END			
50				00			

Concentrated load
first disp. reg.

$$a \neq 0$$



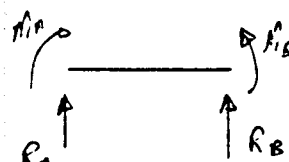
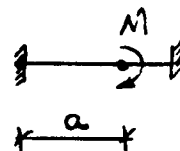
$$R_A = \frac{W(l-a)^2(l+2a)}{l^3}$$

$$M_A = -\frac{Wa(l-a)^2}{l^2}$$

$$M_B = \frac{Wa^2(3l-2a)}{l^3}$$

$$EI\theta_A = EI\theta_B = 0$$

since code is
written for TEE

Moment load
first disp. reg.

$$R_A = -\frac{6Ma(l-a)}{l^3}$$

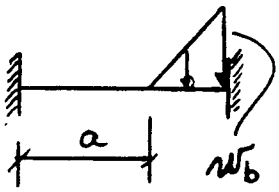
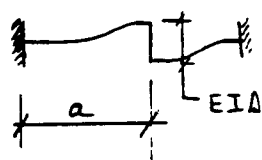
$$M_A = -\frac{M}{l^2}(l-a)(l-3a)$$

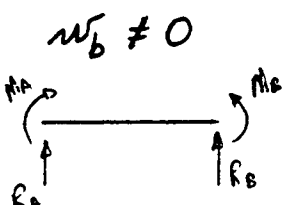
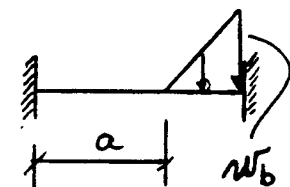
$$M_B = \frac{M}{l^2}a(3l-2l)$$

$$EI\theta_A = EI\theta_B = 0$$

(1) No end sta-
tement on mag. card.

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	Lbl 'WB			51	RCL Z		
	RCL 05				ST + 03		
	RCL IND 07				RCL 05		
	-				*		
	STO 06				-		
	X ↑ 2				+		
	Last x				ST - 04		
	*				1		
	RCL IND 07				ST + 07		
10	3		$W_b \neq 0$	60	RCL 06		
	*				1/x		
	RCL 05				ST-IND 07		
	2				1		
	*				ST + 07		
	+				5		
	X < > Y				STO IND 07		
	*				1		
	Last X				ST + 07		
	3				RTN		
20	ST / Z			70	END		
	RDN			01	LBL 'DC		
	RCL 05				1		
	3				ST + 07		
	*				RCL 05		
	RCL IND 07				1/x		
	+				ENTER ↑		
	RCL IND 07				X ↑ 2		
	+				*		
	*				LAST X		
30	20			80	- 6		
	ST / Z				ST * Y		
	/				ST * Z		
	RCL 05				RDN		
	/				2		
	RCL 05				ST * Z		
	X ↑ 2				RDN		
	ST / Z				'EIY		
	/				PROPT		
	RCL 06				STO IND 07		
40	X ↑ 2			20	STO * 2		
	6				*		
	/				ST + 04		
	'WB				ST - 02		
	PROPT				RDN		
	ST * T				ST + 03		
	ST * Z				2		
	ST * Y				ST + 07		
	ST / 06				RTN		
	X < > T			29	END		
50	ST - 02			00			



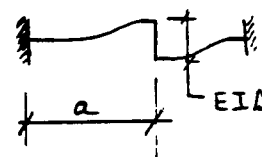
$$R_A = \frac{W_b}{20l^3} (l-a)^3 (3l+2a)$$

$$M_A = -\frac{W_b}{60l^2} (l-a)^3 (2l+3a)$$

$$M_B = R_A l + M_A - \frac{W_b}{6} (l-a)^2$$

$$EI\theta_A = EI\theta_B = 0$$

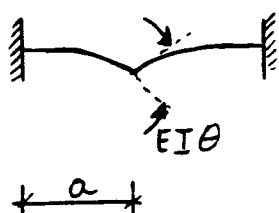

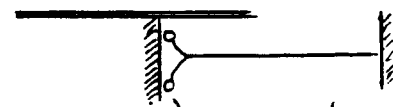
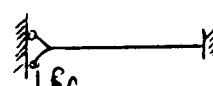

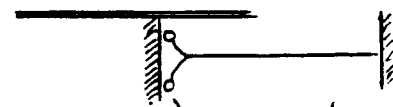
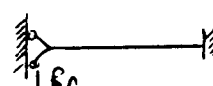

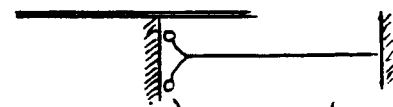
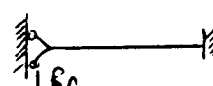

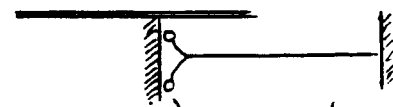
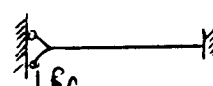

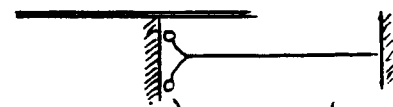
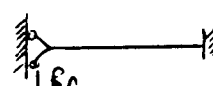
since code is
written for EE case.



$$R_A = \frac{12 EI \Delta}{l^3}$$

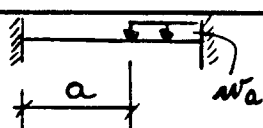
$$M_A = -\frac{6 EI \Delta}{l^2} = -M_B$$

067 097 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL*TC		 <p>Externally created notation</p> $R_A = \frac{6EI\theta}{l^3}(l-2a)$ $M_A = \frac{2EI\theta}{l^2}(3a-2l)$ $M_B = \frac{2EI\theta}{l^2}(l-3a)$ <p>"Encastre" Beam</p> 	02	XEQ*Q		<p>General (common) input exit if $a < 0$</p> <p>XEQ* Loading code</p>  <p>Translation can occur, but no rotation: "Guided" Elimination of R_A:</p>  $M_A = M_A + \frac{R_A l}{2}$ $EI\theta_A = 0$ $EI\theta_A = -\frac{R_A l^2}{12}$ <p>Guided Simply supported</p> <p>Elimination of R_B</p> $R_A = 0 \quad EI\theta_A = 0$ $M_A = M_A - R_B$ $EI\theta_A = EI\theta_A + \frac{R_B l^2}{2}$
	RCL 05			01	RTN		
	RCL IND 07			01	END		
3	*				LBL*Q		
	*				'a =		
	PROMPT				X < 0?		
	RTN				STO IND 07		
	'C-CH:			07	AON		
	PROMPT				ASTO X		
	RCL 05				AOFF		
10	*		<p>Externally created notation</p> $R_A = \frac{6EI\theta}{l^3}(l-2a)$ $M_A = \frac{2EI\theta}{l^2}(3a-2l)$ $M_B = \frac{2EI\theta}{l^2}(l-3a)$ <p>"Encastre" Beam</p> 		XEQ IND X		<p>General (common) input exit if $a < 0$</p> <p>XEQ* Loading code</p>  <p>Translation can occur, but no rotation: "Guided" Elimination of R_A:</p>  $M_A = M_A + \frac{R_A l}{2}$ $EI\theta_A = 0$ $EI\theta_A = -\frac{R_A l^2}{12}$ <p>Guided Simply supported</p> <p>Elimination of R_B</p> $R_A = 0 \quad EI\theta_A = 0$ $M_A = M_A - R_B$ $EI\theta_A = EI\theta_A + \frac{R_B l^2}{2}$
	RCL IND 07				GTO*Q		
	2			14	END		
	*			01	LBL*GE		
	RCL 05				XEQ*Q		
	RCL 05			03	RCL 03		
	/				RCL 05		
	RCL 05				*		
	X ↑ 2				/		
	ST/ T				ST + 02		
20	ST/ Z		<p>Externally created notation</p> $R_A = \frac{6EI\theta}{l^3}(l-2a)$ $M_A = \frac{2EI\theta}{l^2}(3a-2l)$ $M_B = \frac{2EI\theta}{l^2}(l-3a)$ <p>"Encastre" Beam</p> 		ST- 04		<p>General (common) input exit if $a < 0$</p> <p>XEQ* Loading code</p>  <p>Translation can occur, but no rotation: "Guided" Elimination of R_A:</p>  $M_A = M_A + \frac{R_A l}{2}$ $EI\theta_A = 0$ $EI\theta_A = -\frac{R_A l^2}{12}$ <p>Guided Simply supported</p> <p>Elimination of R_B</p> $R_A = 0 \quad EI\theta_A = 0$ $M_A = M_A - R_B$ $EI\theta_A = EI\theta_A + \frac{R_B l^2}{2}$
	/				6		
	2				/		
	ST * Z				RCL 05		
	ST * T			13	X ↑ 2		
	*				*		
	3				ST- 00		
	*				STO 03		
	1				RTN		
	ST + 07			19	END		
30	*		<p>Externally created notation</p> $R_A = \frac{6EI\theta}{l^3}(l-2a)$ $M_A = \frac{2EI\theta}{l^2}(3a-2l)$ $M_B = \frac{2EI\theta}{l^2}(l-3a)$ <p>"Encastre" Beam</p> 	01	LBL*GS		<p>General (common) input exit if $a < 0$</p> <p>XEQ* Loading code</p>  <p>Translation can occur, but no rotation: "Guided" Elimination of R_A:</p>  $M_A = M_A + \frac{R_A l}{2}$ $EI\theta_A = 0$ $EI\theta_A = -\frac{R_A l^2}{12}$ <p>Guided Simply supported</p> <p>Elimination of R_B</p> $R_A = 0 \quad EI\theta_A = 0$ $M_A = M_A - R_B$ $EI\theta_A = EI\theta_A + \frac{R_B l^2}{2}$
	'EIT				XEQ*GE		
	PROMPT				RCL 04		
	ST * 2			04	ST- 02		
	ST * T				RCL 05		
	STO IND 07				X ↑ 2		
	*				*		
	ST- 03				/		
	RDN				ST + 00		
40	ST + 02				CL X		
	RDN		<p>Externally created notation</p> $R_A = \frac{6EI\theta}{l^3}(l-2a)$ $M_A = \frac{2EI\theta}{l^2}(3a-2l)$ $M_B = \frac{2EI\theta}{l^2}(l-3a)$ <p>"Encastre" Beam</p> 		STO 04		<p>General (common) input exit if $a < 0$</p> <p>XEQ* Loading code</p>  <p>Translation can occur, but no rotation: "Guided" Elimination of R_A:</p>  $M_A = M_A + \frac{R_A l}{2}$ $EI\theta_A = 0$ $EI\theta_A = -\frac{R_A l^2}{12}$ <p>Guided Simply supported</p> <p>Elimination of R_B</p> $R_A = 0 \quad EI\theta_A = 0$ $M_A = M_A - R_B$ $EI\theta_A = EI\theta_A + \frac{R_B l^2}{2}$
	ST + 04				RTN		
	1				RTN		
	ST + 07			14	END		
	STO IND 07						
	ST + 07						
	RTN						
	END						
60	LBL*EE						

Note: No "End" statement on magnetic cards.
Replaced by "RTN" statement.

☐ 67 ☐ 97 ☒ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL'WA		 $R_A = \frac{W_a (l-a)^2 (l+a)}{2l^3}$ $M_A = \frac{-W_a (l-a)^2 (l+3a)}{12l^2}$ $M'_B = R_A l + M_A = \frac{-W_a (l-a)^2}{2}$	51	X < > T		
	RCL 05				ST + 03		
	RCL IND 07				RCL 05		
	-				*		
	X ↑ 2				+		
	LAST X				CHS		
	*				ST + 04		
	RCL IND 07				1		
10	*			60	RCL 07		
	RCL 05				+		
	+				4		
	X < > Y				STO IND Y		
	*				ST + 07		
	LAST X			66	END		
	ST/ Z			01	LBL'SS		
	RDN				XEQ'SE		
	RCL 05				RCL 04		
20	RCL IND 07			04	RCL 05		
	+				/		
	*				ST- 03		
	2				RCL 05		
	ST/ Z				X ↑ 2		
	RCL 05				*		
	X ↑ 2				6		
	ST/ Z				/		
	/				ST + 01		
30	RCL 05			14	CL X		
	/				STO 04		
	RCL 05				RTN		
	RCL IND 07			16	END		
	X ↑ 2			01	LBL'NE		
	2				XEQ'SE		
	/				RCL 03		
	PBA				RCL 05		
	PROMPT				X ↑ 2		
40	ST * Y				*		
	ST * Z				2		
	ST * T			08	/		
	STO L				ST + 01		
	CL X				1.5		
	ST + 07				/		
	X < > T				RCL 05		
	ST- 02				*		
	LAST X				ST- 00		
50	ST-IND 07				CL X		
					STO 03		
					RTN		
				18	END		

"S"implify
simplified
Elimination of M_B
from TSE:
 $R_A = R_A = M_B / l$
 $M_A = 0$ $EIG_A = 0$
 $EIG_B = EIG_A - \frac{M_B l}{6}$

"N"othing "Encas"
= Encas
Elimination of R_A
from TSE
 $R_A = 0$ $M_A = 0$
 $EIG_A = -R_A l^3 / 3EI$
 $EIG_B = EIG_A + \frac{R_A l^2}{2EI}$

67 ☐ 97 ☒ 41C

REP/	KEY ENTRY	KEY CODE	COMMENTS	STEP/	KEY ENTRY	KEY CODE	COMMENTS
LINE		(67/97 only)		LINE		(67/97 only)	
01	LBL 'BEAM		<i>initialisation for a new case</i>	51			
	CLRG						
	8						
	STO 07						
	'L:						
	PROMPT						
	STO 05						
	'END:						
	AON						
10	PROMPT			60			
	ASTO X						
	Aoff						
	XEQ IND X						
	LEL 00						
	STOP						
	'XEQ ?						
	AVIEW						
	GTO 00						
	END						
20				70			
01	LBL 'SE		<i>Simplex "E" nested supported</i>				
	XEQ 'Q						
	RCL 02						
	2						
	/						
	ST + 04		<i>elimination of M_P from TEE</i>				
	2						
	/						
	RCL 05						
80	* ST + 01			80			
	RCL 02						
	1.5						
	* RCL 05						
	/						
	ST + 03						
	CL X						
	STO 02						
90	RTN			90			
	END						
50				00			

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	LBL'FF		Compute	51	RCL IND 04		
	'C-ECT:		EIY(4) if $\delta=0$		RCL 06		
	PROMPT		EIG(4) $\delta=-1$		+		
	CHS		M(4) $\delta=-2$		X < 0?		
	STO 06		V(4) $\delta=-3$		GTO 06		
	LBL 08				LAST X		
	'X=		Manually:		FACT		
	PROMPT		XEQ TFF		/		
10	STO 05		and enter 181	60	1		
	LBL'GG		corresponding to		ST- 04		
	8		let you want.		*		
	STO 04		In subroutine:		RCL IND 04		
	RCL 05		Set flag 00		*		
	X < 0?		put δ in R06		+		
	RTN		put X in R05		2		
	2		XEQ TGG		LEL 03		
	RCL 06				ST+ 04		
	ABS				RCL 04		
20	X > Y?			70	RCL 07		
	GTO 09				X > Y?		
	1 E 3				GTO 00		
	/				R ↑		
	3				FS ? 00		
	+				RTN		
	0				PSE		
	LBL 04				GTO 08		
	RCL 06				LBL 09		
	RCL Z				3		
	+				X = Y?		
30	INT			80	GTO 01		
	FACT				0		
	1/X				GTO 05		
	RCL IND T				CL X		
	*				3		
	+				GTO 03		
	RCL 05				LBL 06		
	*				RCL T		
	DSE Y				1		
	GTO 04				GTO 03		
40	RCL IND Y				LBL 00		
	+				R ↑		
	LBL 05				GTO 05		
	RCL 05				LBL 01		
	RCL IND 04				RCL 03		
	X < 0?				GTO 05		
	GTO 02				98	END	
	2						
	ST+ 04						
50	CL X			00			

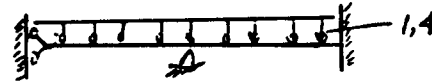
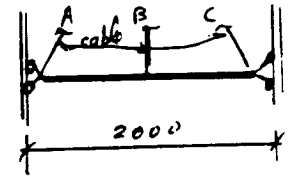
Note: $\langle K \rangle^0 = 1$ if $K > 0$
 $\quad \quad \quad = 0$ if $K \leq 0$
 $\langle K \rangle^m = \langle K \rangle^0 K^m$

Sample Problem (Sketch if Desired)

#2.

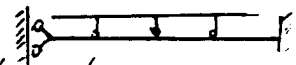
A guided on rails platform is normally suspended by 3 cables. Suppose cable A is now loose or broken, we want know deflection at this end if a uniform load of 1.4 is apply. Suppose, for demonstration, inextensible cables.

Since end C is guided + translation restrained, it's become an encastred end. So, our model is then:



It's a two spans beam.

Let us consider middle support as redundant. Central reaction is then temporarily remove and we have causing a deflection at center, Δ_0 . But central support act as a concentrated force, upward. If reaction is 1 (one), we have



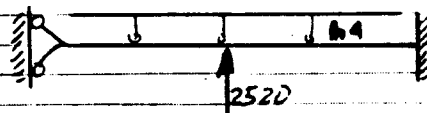
SOLUTION: an upward deflection Δ_1 . It's well know, then, that

Input	Function	Display	Comments
reaction, P , is and then, knowing which is one of our "36 Beams".		$-\Delta_0 \div \Delta_1$ central reaction	we obtain:
1- Compute Δ_1			
XEQT BEAM	R/S	L:	2 loads
2000	R/S	END:	so size 14
GE	R/S	$\alpha =$	is the minimum
1000	R/S	C-CH:	$14 = 8 + 2 \times 3$
CO	R/S	W:	Since P is upward.
1 CHS	R/S	$\alpha =$	
1 CHS	R/S	C-FCT:	so, upward deflection.
0	XEQT FF	X=	
1000	R/S	X=	
	R/S	X=	
2- Compute Δ_0			
XEQT BEAM	R/S	L:	
2000	R/S	END:	
GE	R/S	$\alpha =$	
W/A	R/S	C-CH:	
1.4	R/S	W/A:	
1 CHS	R/S	$\alpha =$	
0	XEQT FF	C-FCT:	
1000	R/S	X=	
	R/S	X=	
	R/S	X=	

(CONTINUATION PAGE)

So, $P = 2520 =$ true reaction, at central support
(inextensible cable)

3- We now compute



("Hard-user" only: Since almost loads are already entered, we will ask: there is a way to, add loads without begin at zero, as nothing was already worked in. Answer is yes:

- Restore length in R05; Put 0 in R04
- Give the first register disposable for new loads in R07
($8 + i + 3 =$ already enter loads since last XEQT BCAM)
(# of registers reserved to you)
- XEQT Code of restrain.

Here: $2000 \text{ STO } 05 \quad 0 \text{ STO } 04$
 ~~$2000 \text{ STO } 07$~~
XEQT GE

For the net trace of all INPUT option: (Re-begin at zero)

XEQT BCAM	L:	2000
R/S	CND:	GE
R/S	a =	0
R/S	C-CH:	WA
R/S	WA:	1.4
R/S	a =	1000
here, hard-user reformed us	C-CH:	CD
R/S	W:	2520 CHS (upward)
R/S	a =	1 CHS

XEQT FF	C-ECT	0
R/S	X =	

Let us verify at $X = 1000$

R/S	-60	1000
-----	-----	------

since it's about (-60 for hard-user, don't ask me why?)
zero (EY = -60)

(Round-off errors don't give exactly 0) $y = 0$

and now, at $X = 0$

R/S	X:	0
	-9,333 E10	

Evidently, since EY at $X = 0$ is always in R00:

RCL 00 -9,333 E10 is also good.

PROGRAM REGISTERS NEEDED: 21

ROW 1 (1 : 2)



ROW 2 (3 : 10)



ROW 3 (10 : 20)



ROW 4 (21 : 30)



ROW 5 (31 : 40)



ROW 6 (40 : 49)



ROW 7 (50 : 60)



ROW 8 (61 : 70)



ROW 9 (71 : 80)



ROW 10 (81 : 89)



ROW 11 (90 : 98)



ROW 12 (98 : 98)



PROGRAM REGISTERS NEEDED: 95

ROW 1 (1 : 7)



ROW 2 (8 : 18)



ROW 3 (19 : 28)



ROW 4 (29 : 38)



ROW 5 (39 : 48)



ROW 6 (49 : 54)



ROW 7 (55 : 65)



ROW 8 (65 : 69)



ROW 9 (70 : 80)



ROW 10 (81 : 85)



ROW 11 (86 : 95)



ROW 12 (95 : 101)



ROW 13 (102 : 113)



ROW 14 (114 : 124)



ROW 15 (125 : 134)



ROW 16 (135 : 143)



ROW 17 (144 : 150)



ROW 18 (150 : 160)



ROW 19 (160 : 168)



ROW 20 (168 : 176)



ROW 21 (177 : 184)



ROW 22 (184 : 192)



ROW 23 (192 : 196)



ROW 24 (197 : 203)



ROW 25 (204 : 211)



ROW 26 (211 : 216)



ROW 27 (216 : 225)



ROW 28 (226 : 235)



ROW 29 (235 : 242)



ROW 30 (243 : 254)



ROW 31 (255 : 263)



ROW 32 (264 : 270)



ROW 33 (271 : 279)



ROW 34 (279 : 284)



ROW 35 (284 : 289)



ROW 36 (290 : 295)



ROW 37 (296 : 300)

ROW 38 (301 : 305)

ROW 39 (310 : 315)

ROW 40 (318 : 325)

ROW 41 (326 : 332)

ROW 42 (332 : 341)

ROW 43 (342 : 351)

ROW 44 (352 : 361)

ROW 45 (362 : 372)

ROW 46 (373 : 379)

ROW 47 (380 : 390)

ROW 48 (391 : 399)

ROW 49 (400 : 409)

ROW 50 (409 : 417)

ROW 51 (418 : 424)

PROGRAM DESCRIPTION I

Program Title TRUSS DEFORMATIONContributor's Name Paulo de Salles MourãoAddress Rua Eng. Amaro Lanari 110/201City Belo Horizonte State/Country MG, BRASIL Zip Code 30000

Program Description, Equations, Variables 1) For a loaded truss, it is of interest to get the elastic line for both superior and inferior polygonals of the structure, that is, respective joints' strains under elastic deformation, which is the program's goal, restrictive to the more important vertical displacements.

As everybody knows, there are classical types of trusses that received particular names, such as Warren, Pratt, Howe. Notwithstanding the standardization, they can vary to a certain extent, and non typical designs can vary widely. For this reason, it is difficult to combine a vast range of application with a high degree of program's automation. So we decided to sacrifice some on the last one, in order to maintain an wide applicability, that includes all standard trusses and great number of non typical ones, without redundant members.

2) The sacrifice doesn't go as far as requiring reentering of data as such. However, references to data are provided in such a way that the user will furnish them to the 41C, as oriented by the display, opportunely.

3) Now, let us present the chief variables of the program
(see continuation page 2)

Necessary Accessories 2 memory modules

Operating Limits and Warnings 30 angles and 20 sides limit the size of the structure for one straightforward run, but since subsequent runs can always be done, there is no total limitation.

Reference(s) Theory of Structures, by Timoshenko and Young
Ed. McGraw-Hill Book Company, Inc.

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses the program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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PROGRAM DESCRIPTION I

- 3-1) Angle , as symbolized by the 41C sign : \angle . Refers to the angle between two concurrent bars , not to the angle of the bar about X axis , which will also play a role , and will be referred to as angle (\angle) about X . For practical reasons only the angle unit is the degree with decimal fractions .
- 3-2) Unitary stress acting on a bar , positive if tension , negative if compression . Will be called 'S' , from sigma .
- 3-3) Fictitious loads symbolized 'FP' are the main findings from the program , they come from the sum of adjacent angles variation in each desired joint . So , they have no physical dimension.
- 3-4) The vertical strains , symbolized 'ST', being final outputs .

- 4) Consider now a triangle , whose vertices were numbered 1,2,3, meaning that such numbers became references for respective angles. (Such references match the registers that contain the angles). The sides were numbered 42, 43, 44 , but instead of standing for lengths of the sides , such references apply to 'S' variables (3-2, above.)

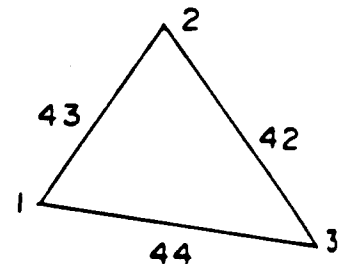


Fig 1

- 4-1) If we prefix the symbol of a variable with the letter 'R' , we symbolize the reference to such variable . In this way, 'RS' stands for a reference to the variable sigma , and 'R \angle ' signifies a reference to the variable angle . As stated before , such references are numbers that match registers where the variables are stored .

- 4-2) Figure 2 shows a joint 'J' where 3 triangles concur . As this joint is being treated in program's running, the user will be invited to make entries , and besides what will appear in the display to orient him, her, the following simple rules must be obeyed :

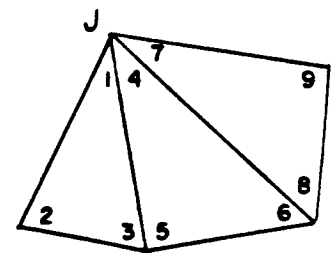


Fig 2

- 4-2-1) Couples of angle and sigma references will be called for , frequently, respective to the elements of a triangle .

First rule :Entered an angle reference ,its counterpart is always the opposite side sigma reference .

see continuation page 3

CONTINUATION PAGE
PROGRAM DESCRIPTION I

Example : In fig 1 the couples are :
1-42 2-44 3-43

4-2-2) A joint (knot) J is being considered (fig 2). In the case illustrated three triangles are to be computed (may be one to several). The order of triangle treatment is not relevant, but of course it is easier to follow a sequence, as :
1-2-3, 4-5-6, 7-8-9,
or the reverse, but not either beginning or finishing with the middle triangle.
On the other hand, it is mandatory to begin each triangle with the angle contiguous to the joint in question (for fig 2, 1 in the first, 4 in the second, 7 in the third triangle.) For the other 2 couples in each triangle the order is irrelevant, but again it helps to adopt a rule; for example, counter-clockwise, we'd get the sequences cited above.
After the n triangles have been processed, and the program asks for elements of the n+1 triangle (nonexistent), enters zero and run - the next joint will be ready.

- 5) The searched vertical strains are due mainly to the variation of the angles between bars, but if inclined bars are present, there is part due to variation of respective lengths. See in next item 6 how to consider this. Referring again to fig 1, variation of angle 1 is a function of angles 2 and 3, and the unitary variation of each side; if we call DL the variation of a length L, we can write :
$$DL/L = S/E$$
, being E the module of elasticity, supposed constant. The second member will be used.
Now, the formula for angle variation. According to the reference, we can write for the variation $D\angle 1$ of angle 1 in fig 1 :

$$E(D\angle 1) = (S_{42} - S_{44})\cotan(2) + (S_{42} - S_{43})\cotan(3)$$

It is not necessary to write similar equations for the other 2 angles, because only 1 angle in each triangle will be considered at a time.
For each joint, respective $D\angle$ will be treated as the fictitious load (FP) there applied, and after all of them have been computed, they are input in the last part for desired strains gathering.

- 6) In case of inclined bars, besides the effects described in (5), there will be strains due to variation in the length of the bars, and we can apply the same fictitious loads concept, considering at bars' ends two equal FP with opposite signs.

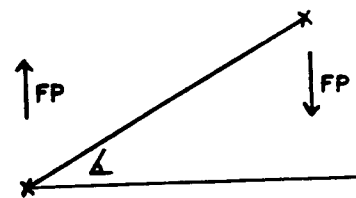


Fig 3

see continuation page 4

PROGRAM DESCRIPTION I

In each inclined bar , the intensity of FP is :

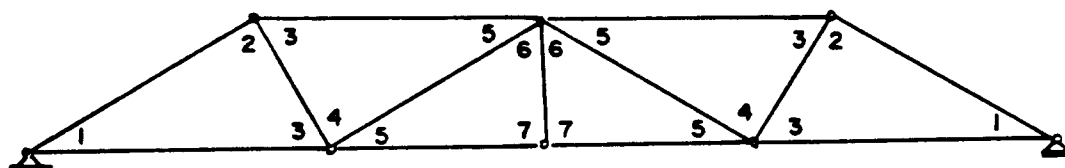
$$FP = (S/E)\tan(\Delta) \quad \Delta = \text{angle about } X$$

If Δ is positive , as in fig 3 , the sign of FP depends on the sign of S . For a compressed bar , S is negative , and so is FP . It is necessary to state to which FP applies this negative sign : it is to the left FP , so the right FP is positive . A positive FP leads to a positive strain , that is , a strain going down , for this is the natural tendency of a joint in a load structure . Lbl S (reminding of slope) takes care of these calculations , and for clarity to the user the FP value displayed is preceded by the reminder "TO RIGHT", meaning that the FP sign applies to the right element . Summarizing : If FP is displayed with positive sign , the situation matches fig 3 ; and if negative sign , invert fig 3 .

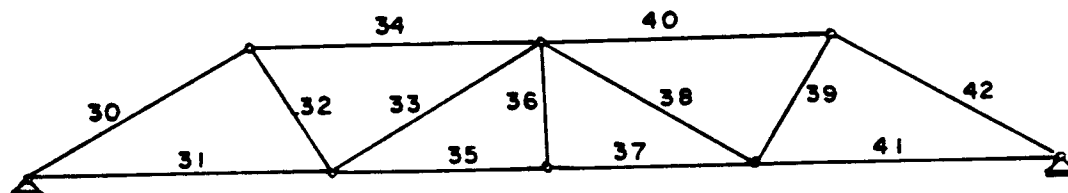
- 7) After determining all FP , we consider them as concentrated loads applied on a simply supported beam that matches the truss , as long as abscissas are concerned. The bending moment that results at each joint abscissa , equals respective strain. Related computations are performed in Lbl T , that asks as inputs each FP and respective abscissa . Then , strains are output currently from left to right , at each R/S command .
- 8) How to reference an entire truss ? Very simply :
 Number angles "ad libitum" from 1 to 30 (if more angles , see 9)
 Equal angles must receive same number .
 Then , number sides in same way , from 31 to 50 (if more , see 9)
 Such numbers will stand for sigma (S) in the bars , not lenght.
 The program will prompt for angles , first , which must be entered according to the numeration. No more angles , enters 0 , run , and the program prompts for 'S', that will be entered in similar way , and so for the conclusion .
- 9) If the truss exceeds program's capacity , run in first part how many joints as possible , then renumber the remainder of the truss , and make another independent run for determining lacking FP . The last part , Lbl T , can take simultaneously 20 FP and abscissas . If 2 or more runs are necessary , the results must be superposed (in this last part).
- 10) Vertical bars at ends - If in pg 5 truss ref.30 and ref.42 bars were vertical ones , at Lbl S 90 could not be angle entry , but with adequate precision we'd entry with ATAN H, being H the height (1645). This ensure to be 1 mm the X of FP near left support , and similarly for right support . Another option is introducing a fictitious moment equal to vertical bar's strain at respective end but this doesn't make use of program's facilities .

Sample Problem (Sketch if Desired)

The truss below was numbered for angles and 'S' values. Respective values are given in page 6 table. Find the elastic lines of both superior and inferior polygonals of the truss.



Angles



S

Take $E=206000 \text{ N/mm}^2$

OLUTION: We assume the program loaded in the 41C, and SIZE C60 covered

Input	Function	Display	Comments
	XEQ ELTRUSS	E	Call the program
206000	R/S	END ENTRIES	Enter E and run
		WITH ZERO	Advice about going on
		ANGLE ENTRY	What will be entered now
		4 1	Angle ref. 1 enter, run
31	R/S	4 2	Angle ref. 2 enter, run
88	R/S	4 3	Similarly ...
61	R/S	4 4	Similarly ...
89	R/S	4 5	Similarly ...
30	R/S	4 6	Similarly ...
60	R/S	4 7	Similarly ...
90	R/S	4 8	No 8th angle, enter 0, run
0	R/S	SIGMA ENTRY	Next variable entry, the
		S 30	1st is referenced by '30'.
53.22	CHS R/S	S 31	As each reference appears
45.62	R/S	S 32	in display, respective
10.76	R/S	S 33	value is keyed in and runs
18.82	CHS R/S	S 34	(See S table, pg 6)
50.84	CHS R/S	S 35	
67.13	R/S	S 36	
FEF CHS 20	R/S	S 37	As a zero value would ter-
67.13	R/S	S 38	minate the entry, enter
5.18	CHS R/S	S 39	in its place a tiny value.
13.25	R/S	S 40	
62.65	CHS R/S	S 41	
55.90	R/S	S 42	
65.22	CHS R/S	S 43	Nonexistent, enter 0, run
0	R/S	ABOVE JOINT?	Asks situation of joint,
		Y OR N	Y=ABOVE, N=BELOW
Y	R/S	KNOT N 1	First, above
		TRIANGLE N 1	Knot, triangle, and refe-
		R 4 RS 1	rence entries are given
			User must review 4-2 item
			See continuation pg 7

'S' table Unit : N/mm²

R	S
30	-53.22
31	45.62
32	10.76
33	-18.82

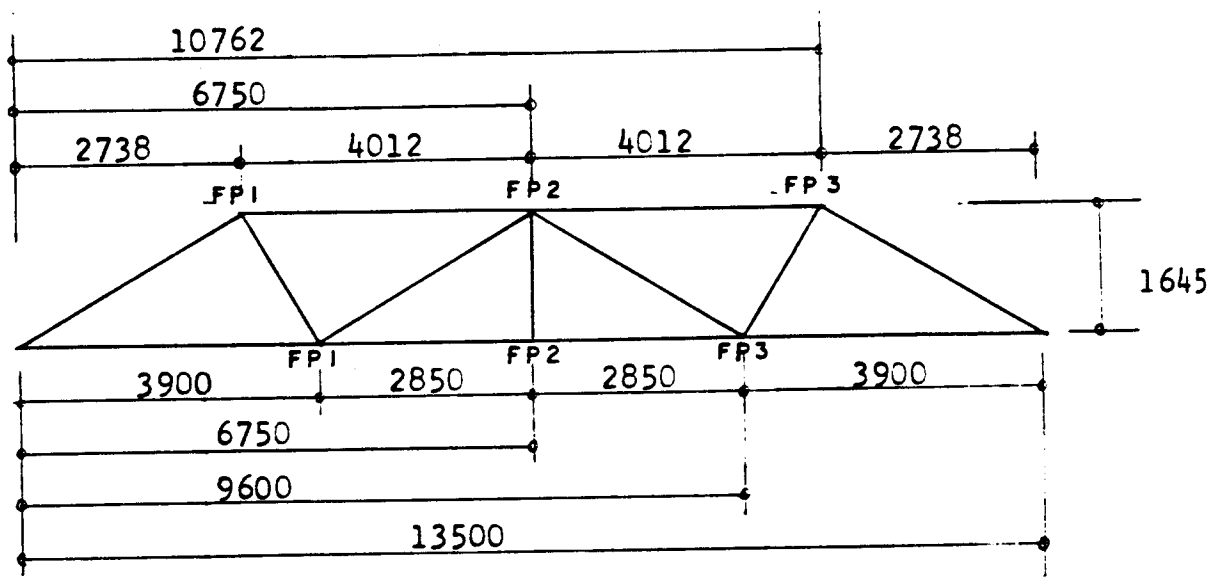
R	S
34	-50.84
35	67.13
36	0.00
37	67.13

R	S
38	-5.18
39	13.25
40	-62.65
41	55.90
42	-65.22

Angle table
Unit : deg.

R	Δ
1	31
2	88
3	61
4	89

R	Δ
5	30
6	60
7	90



TRUSS measurements - abscissas of the knots
Unit : mm

Determined FP table

	principal	additional	sum		principal
FP1	0.001159	0.000155	0.001314	FP1	0.001192
FP2	0.001705	-	0.001705	FP2	0.001398
FP3	0.001575	0.000190	0.001765	FP3	0.001665

S U P E R I O R

I N F E R I O R

Input	Function	Display	Comments
2 31 1	ENTER R/S ENTER	2 R Δ RS 2	Enter couple of Δ and S references, according to 4-2 item, thrice for each triangle. This comment will repeat as comment 1. Second triangle of same knot will be considered Comment 1 Third triangle is referenced As nonexistent, enter 0, ... First FP1 is displayed, and second knot is announced Comment 1
32 3 30	R/S ENTER R/S	R Δ RS 3 TRIANGLE N 2 R Δ RS 1	
3 33	ENTER R/S	R Δ RS 2	
4 34 5	ENTER R/S ENTER	R Δ RS 3	
32 0	R/S R/S	TRIANGLE N 3 R Δ RS 1 FP1=0.001159 KNOT N 2 TRIANGLE N 1 R Δ RS 1	
5 32 3	ENTER R/S ENTER	R Δ RS 2	
33 4 34	R/S ENTER R/S	R Δ RS 3 TRIANGLE N 2 R Δ RS 1	
6 35	ENTER R/S	R Δ RS 2	
5 36 7	ENTER R/S ENTER	R Δ RS 3	
33 6 37 7 38	R/S ENTER R/S ENTER R/S	TRIANGLE N 3 R Δ RS 1 R Δ RS 2 R Δ RS 3	
5 36	ENTER R/S	TRIANGLE N 4 R Δ RS 1	Fourth triangle, knot 2
5 39 4	ENTER R/S ENTER	R Δ RS 2	Comment 1
40 3 38	R/S ENTER R/S	R Δ RS 3 TRIANGLE N 5 R Δ RS 1	Fifth triangle is required As nonexistent, enter 0, run, and FP2 is shown. Third joint will be treated Comment 1
0	R/S R/S	FP2=0.001705 KNOT N 3 TRIANGLE N 1 R Δ RS 1	
			see continuation pg 8

Input	Function	Display	Comments
3	ENTER	3	Entering elements of knot N 3 , TRIANGLE N 1
38	R/S	R Δ RS 2	
5	ENTER	5	
39	R/S	R Δ RS 3	Comment 1 Second triangle
4	ENTER	4	
40	R/S	TRIANGLE N 2	
		R Δ RS 1	Comment 1
2	ENTER	2	
41	R/S	R Δ RS 2	
3	ENTER	3	Third triangle , nonexistent Now are complete FP due to angle variation for superior polygonal, and for the other effect (item 6), call Lbl S. For 1st inclined bar , enter S and run . Now, asks angle Call it and run Position of FP for sign
42	R/S	R Δ RS 3	
1	ENTER	1	
39	R/S	TRIANGLE N 3	Now, run for the other bar
		R Δ RS 1	
0	R/S	FP3=0.001575	
	XEQ S	S	Call the stress, and run The angle is 180-41
	RCL 30	-53.220000	
	R/S	ANGLE ABOUT X	
	RCL 01	31.000000	FP is positive, since the point is to the left of bar. Now we can return to Lbl 04 for the inferior polygonal Of course , N First knot will be treated
	R/S	TO RIGHT	
		FP=1.5523E-4	
	XEQ S	S	Comment 1
	RCL 42	-6.5220 01	
	R/S	ANGLE ABOUT X	
180	RCL 01	3,1000 01	Passes to 2nd triangle
	-	1,4900 02	
	R/S	TO RIGHT	
		FP=-1.9023E-4	Comment 1
	XEQ 04	ABOVE JOINT?	
		Y OR N	
N	R/S	KNOT N 1	Passes to 3rd triangle
		TRIANGLE N 1	
		R Δ RS 1	
3	ENTER	3	Comment 1
30	R/S	R Δ RS 2	
2	ENTER	2	
31	R/S	R Δ RS 3	Comment 1
1	ENTER	1	
32	R/S	TRIANGLE N 2	
		R Δ RS 1	Comment 1
4	ENTER	4	
34	R/S	R Δ RS 2	
5	ENTER	5	Comment 1
32	R/S	R Δ RS 3	
3	ENTER	3	
33	R/S	TRIANGLE N 3	Comment 1
		R Δ RS 1	
5	ENTER	5	
36	R/S	R Δ RS 2	Comment 1
7	ENTER	7	
33	R/S	R Δ RS 3	

see continuation pg 9

ELTROSS

Input	Function	Display	Comments
6 35	ENTER R/S	6 TRIANGLE N 4 R Δ RS 1	Nonexistent Enter 0 , run FP1 output . Run again , Announces 2nd joint
0	R/S R/S	FP1=0.001192 KNOT N 2 TRIANGLE N 1 R Δ RS 1	
7 33	ENTER R/S	7 R Δ RS 2	
6 35 5	ENTER R/S ENTER	6 R Δ RS 3 5	Second triangle of 2nd KNOT
36	R/S	TRIANGLE N 2 R Δ RS 1	
7 38	ENTER R/S	7 R Δ RS 2	
5 36	ENTER R/S	5 R Δ RS 3	Comment 1
6 37	ENTER R/S	6 TRIANGLE N 3 R Δ RS 1	
0	R/S R/S	FP2=0.001398 KNOT N 3 TRIANGLE N 1 R Δ RS 1	
5 36	ENTER R/S	5 R Δ RS 2	Passes to 2nd triangle
6 37 7	ENTER R/S ENTER	6 R Δ RS 3 7	
38	R/S	TRIANGLE N 2 R Δ RS 1	
4 40	ENTER R/S	4 R Δ RS 2	Comment 1
3 38	ENTER R/S	3 R Δ RS 3	
5 39	ENTER R/S	5 TRIANGLE N 3 R Δ RS 1	
3 42 1	ENTER R/S ENTER	3 R Δ RS 2 1	Comment 1
39 2	R/S ENTER	R Δ RS 3 2	
41	R/S	TRIANGLE N 4 R Δ RS 1	
0	R/S	FP3=0.001665	Nonexistent Enter 0 , run FP3 output Since no inclined bars are present, Lbl S doesn't apply

For table of determined FP , see page 6

See continuation page 10

Input	Function	Display	Comments
13500 2738	XEQ T R/S ENTER	L TOTAL X FP 1 2738	For getting strains , XEQ T Enter Truss lenght and run First superior polygonal
.001314 6750 .001705	R/S ENTER R/S	X FP 2 6750 X FP 3	Page 6 helps data entry Entering 2nd abscissa ,and FP
10762 .001765 0	ENTER R/S R/S	10762 X FP 4 STRAINS	Third and last X and FP Nonexistent, enter 0 and run Advice that strains will follow
	R/S R/S	ST1=6.18232 ST2=9.96953 ST3=6.91627	Strain related to X1. Run again Strain in the middle. Run Strain related to X3 .
13500 3900	XEQ T R/S ENTER	L TOTAL X FP 1 3900	Return to T for inferior pol. Make similar entries
.001192 6750 .001398	R/S ENTER R/S	X FP 2 6750 X FP 3	Asks 2nd X and FP Third X and FP
9600 .001665 0	ENTER R/S R/S	9600 X FP 4 STRAINS	Nonexistent, enter 0 and run Results will be shown First one , run
	R/S R/S	ST1=7.90781 ST2=10.28940 ST3=8.68669	Again Completing the output .

In practice , of course , the precision of five decimal digits is illusory ,and additional strains will be produced by other factors .
. So , rounding off the values, the results are :

Vertical strains ,superior polygonal : 6.2 , 10.0 , 6.9 mm
inferior 7.9 , 10.3 , 8.7 mm

Comments regarding program's effectiveness

It cannot be denied that this program's execution requires substantial amount of user's guidance . However, as stated in page 1 this is the price to pay for assuring vast range of application . As truss configurations vary widely, it is not possible ,keeping the generalization , to avoid instructions necessary to face distinct truss arrangements , even if mass storage were to be employed . On the other hand , the execution is far from cumbersome , very easy to grasp , thoroughly signaled , and he or she who has ever calculated truss strains using a Williot-Mohr diagram or equivalent process , will consider using this program a very convenient way .

USER INSTRUCTIONS

				SIZE: 060 (HP-41C)
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1	Enter the program , check status		XEQ ELTRUSS	E
2	Call the program		R/S	END ENTRIES WITH ZERO
3	Enter the module of elasticity	E		ANGLE ENTRY Δ 1
				Δ 2
4	Enter angle numbered 1	Δ 1	R/S	Δ 3
	enter angle numbered 2	Δ 2	R/S	Δ 4
	enter angle numbered 3	Δ 3	R/S	
5	when a nonexistent angle is asked enter zero , run	0	R/S	SIGMA ENTRY S 30
				S 31
6	Enter sigma numbered 30	S 30	R/S	S 32
	enter sigma numbered 31	S 31	R/S	S 33
	enter sigma numbered 32	S 32	R/S	
7	when a nonexistent S is asked enter zero and run	0	R/S	ABOVE JOINT? Y OR N
				KNCT N 1
8	Enter Y if it is superior joint	Y	R/S	TRIANGLE N 1 R Δ RS 1
				R Δ
9	Enter 1st pair R Δ , RS (Review 4-2) (page 2)	R Δ	ENTER	R Δ RS 2
	enter 2nd pair	RS	R/S	R Δ
	enter 3rd pair	R Δ	ENTER	R Δ RS 3
		RS	R/S	R Δ
				TRIANGLE N 2 R Δ RS 1
10	Repeat step 9 for triangle n 2			TRIANGLE N X
11	When a nonexistent triangle is announced			R Δ RS 1
12	Enter zero and run , FP1 is shown run again	0	R/S R/S	FP1=() KNCT N 2
13	Next joint will be considered			TRIANGLE N 1
14	Repeat step 9 for this triangle			R Δ RS 1
	Repeat step 9 for subsequent triangles , then step 11 to 13			KNCT N Y TRIANGLE N 1 R Δ RS 1
15	After treating all joints ,XEQ S for inclined bars, if present .		XEQ S	S
16	Enter stress in the bar	S	R/S	Δ ABOUT X
17	Enter angle about X Gives FP value (review item 6)	Δ	R/S	TO RIGHT FP=()
18	Repeat 15 to 17 for all inclined bars .			
19	Holding FP values , final compu- tations will follow in Lbl T		XEQ T	L TOTAL
20	Enter Truss lenght and run	L	R/S	X FP 1
21	Of 1st FP , abscissa and value	X FP	ENTER R/S	X X FP 2
22	Repeat 21 for subsequent pairs		R/S	STRAINS
23	When nonexistent one ,enter 0,run At each run, next strain is shown	0		ST 1=()

PROGRAM LISTING

□ 67 □ 97 □ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (67/97 only)	COMMENTS
01	<u>LBL ELTRUSS</u>			51	X=Y?		
	CLRG				SF 00		Flag 00 is set
	"E"		Elasticity		AOFF		
	PROMPT		module		<u>LBL 05</u>		
	STO 59				1		
	"END ENTRIES"		How to leave		ST+00		Preparation
	" WITH ZERO"		entry loops		0		
	XEQ 06				STO 58		
	1				"KNOT N "		Knot(joint) ,
10	STO 00		Angle entry	60	ARCL 00		is referred
	"ANGLE ENTRY"		loop		XEQ 06		by number
	XEQ 06				0		
	FIX 0				STO 51		
	<u>LBL 11</u>				<u>LBL 07</u>		
	"Z "				1		Triangle is
	ARCL 00				ST+51		also control-
	PROMPT				"TRIANGLE N "		led by num-
	X=0?				ARCL 51		ber
	GTO 12				XEQ 06		
20	STO IND 00		Storage	70	1.003		Reg. 52 will
	1				STO 52		control verti-
	ST+00				<u>LBL 08</u>		ces of trian-
	GTO 11				"RZ RS "		gle loop
	<u>LBL 12</u>				ARCL 52		References for
	"SIGMA ENTRY"		Sigma entry		PROMPT		angles and
	XEQ 06		loop		X=0?		Stresses are
	30				GTO 15		asked.
	STO 00				XEQ IND 52		Calls subrou-
	<u>LBL 13</u>				ISG 52		-tines (see
30	"S"			80	GTO 08		01 - 02 - 03)
	ARCL 00				XEQ 10		
	PROMPT				GTO 07		
	X=0?				<u>LBL 15</u>		
	GTO 04				"="		
	STO IND 00		Storage		ASTO X		Will display
	1				RCL 58		calculated
	ST+00				FC?00		"FP" matched
	GTO 13				CHS		to knot's
	<u>LBL 04</u>				RCL 59		number
40	CF 00		Preparation	90	/		
	FIX 0				"FP"		
	0				ARCL 00		
	STO 00				ARCL Y		
	"ABOVE JOINT?"		Asks position		FIX 6		
	" Y OR N"		of joint		ARCL X		
	AON				PROMPT		
	PROMPT				FIX 0		
	ASTO X				GTO 05		
	"Y"		If above ...		<u>LBL 06</u>		Display
50	ASTO Y			00	AVIEW		subroutine

PROGRAM LISTING

167 ☐ 97 ☒ 41C

STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS	STEP/ LINE	KEY ENTRY	KEY CODE (87/87 only)	COMMENTS
101	PSE			51	PROMPT		
	RTN				LBL 1		
	LBL 01		The three		"L TOTAL"		To enter whole
	STO 53		subroutines		PROMPT		truss lenght
	RTN		01, 02, 03		STO 51		
	LBL 02		position		LBL 21		
	STO 55		adequately		1		Preparation
	RDN		angles and		STO 53		
	STO 54		sigmas for		31		
10	RTN		each triangle	60	STO 54		
	LBL 03		being		0		
	STO 57		processed		STO 52		
	RDN				STO 55		
	STO 56				FIX 0		
	RTN				LBL 22		
	LBL 10		This		"X FP"		Loop :
	RCL IND 56		subroutine		ARCL 53		abscissas and
	XEQ 14		calculates		PROMPT		fictitious
	RCL IND 53		angle		X=0?		loads entry
20	RCL IND 55		variation	70	GTO 23		
	-		as function		STO IND 54		
	*		of other		X \geq Y		
	RCL IND 54		angles		STO IND 53		
	XEQ 14		and sigmas		CHS		
	RCL IND 53				RCL 51		Left reaction
	RCL IND 57				+		is figured
	-				*		
	*				RCL 51		
	+				/		and
30	ST+58			80	ST+52		accumulated
	RTN				1		
	LBL 14		Figures		ST+53		
	TAN		cotangent		ST+54		
	1/X		of angle		GTO 22		
	RTN				LBL 23		
	LBL S				"STRAINS"		Advice that
	"S"				XEQ 06		strains will
	PROMPT		For an incli-		1.1		follow, cal-
	"4 ABOUT X"		ned member,		STO 00		culated as
40	PROMPT		calculates	90	RCL 52		moments of
	TAN		respective		STO 30		fictitious
	*		"FP"		RCL 01		loads "FP"
	RCL 59				*		
	/				STO 55		
	CHS				XEQ 30		
	"TO RIGHT"		Position of		31		
	XEQ 06		FP matched		STO 54		
	"FP="		by its sign		LBL 24		
	SCI 4				RCL IND 54		
50	ARCL X			200	ST-30		

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS		STATUS			
Registers	Contents	SIZE	TOT. REG.	USER MODE	
00	Counter at input labels	060	134	ON	OFF
51	Triangle number control	ENG	FIX 0-6 SCI 4	ON	OFF
52	Triangle vertice number control	DEG x (mainly DEG)	BAD x GRAD x	any	
53	53-55-57 Current reference numbers for sigmas	FLAGS			
54	54-56 Current reference numbers for angles	# INIT S/C	SET INDICATES	CLEAR INDICATES	
55	(as asked in lbl 08, and stored in lbls. 01 to 03)	00 C	Above joint	Below joint	
56					
57					
58	Σ D 4				
59	E				
		ASSIGNMENTS			
		No			
		FUNCTION	KEY	FUNCTION	KEY

PROGRAM REGISTERS NEEDED: 74

ROW 1 (1:3)

ROW 2 (3:6)

ROW 3 (6:7)

ROW 4 (7:11)

ROW 5 (11:18)

ROW 6 (18:22)

ROW 7 (23:25)

ROW 8 (25:31)

ROW 9 (31:39)

ROW 10 (40:44)

ROW 11 (44:45)

ROW 12 (45:52)

ROW 13 (53:59)

ROW 14 (59:65)

ROW 15 (65:67)

ROW 16 (67:71)

ROW 17 (72:77)

ROW 18 (77:82)

ROW 19 (83 : 89)

ROW 20 (90 : 96)

ROW 21 (97 : 106)

ROW 22 (107 : 115)

ROW 23 (116 : 123)

ROW 24 (124 : 130)

ROW 25 (131 : 138)

ROW 26 (139 : 142)

ROW 27 (143 : 146)

ROW 28 (147 : 152)

ROW 29 (153 : 154)

ROW 30 (155 : 162)

ROW 31 (163 : 166)

ROW 32 (167 : 174)

ROW 33 (175 : 183)

ROW 34 (184 : 186)

ROW 35 (187 : 182)

ROW 36 (183 : 189)

ROW 37 (199 : 206)



ROW 38 (207 : 213)



ROW 39 (213 : 219)



ROW 40 (219 : 223)



