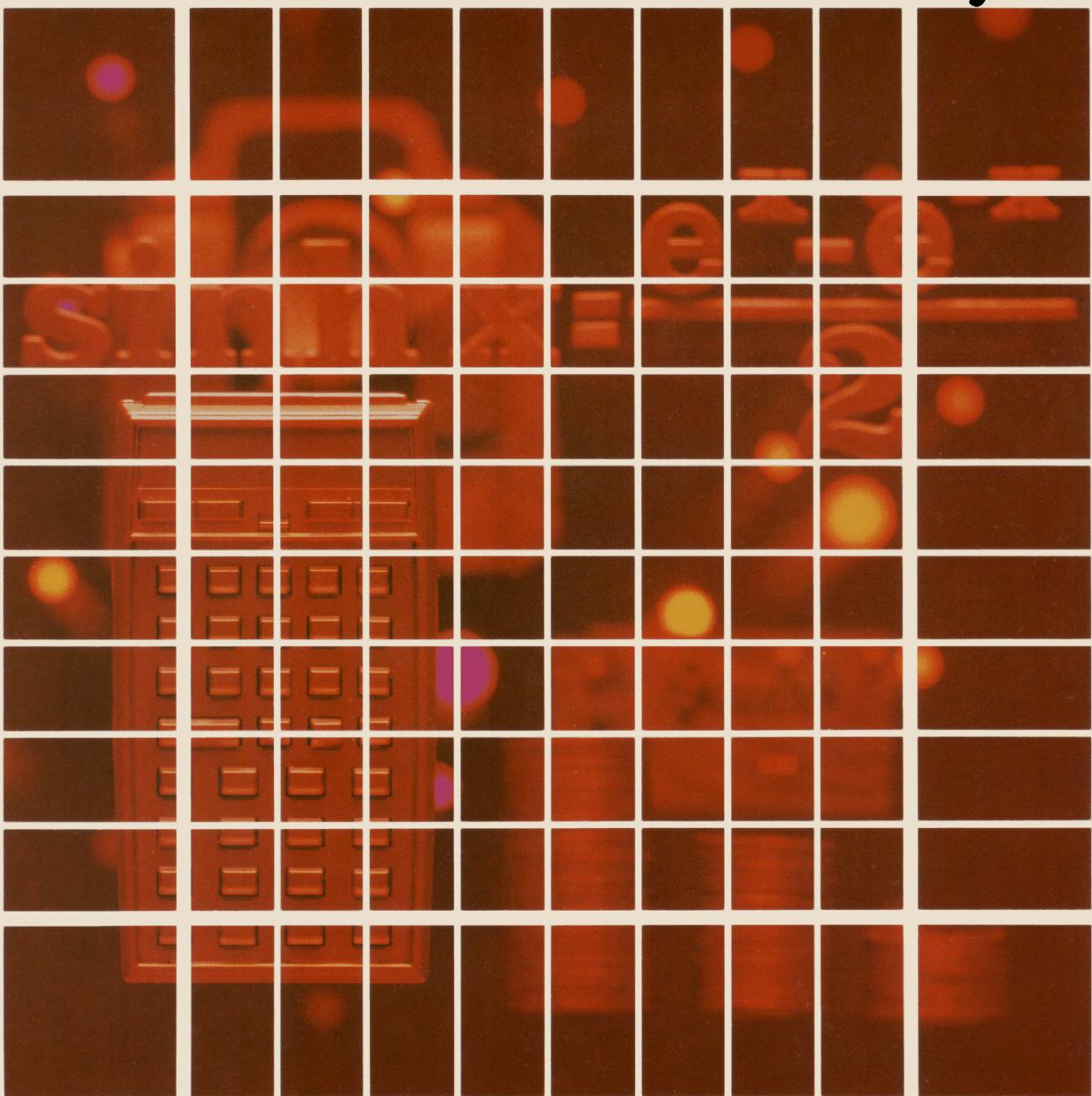


HEWLETT-PACKARD

HP-41C

**USERS'
LIBRARY SOLUTIONS
Structural Analysis**



NOTICE

The program material contained herein is supplied without representation or warranty of any kind. Hewlett-Packard Company therefore assumes no responsibility and shall have no liability, consequential or otherwise, of any kind arising from the use of this program material or any part thereof.

INTRODUCTION

This HP-41C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.

KEYING A PROGRAM INTO THE HP-41C

There are several things that you should keep in mind while you are keying in programs from the program listings provided in this book. The output from the HP 82143A printer provides a convenient way of listing and an easily understood method of keying in programs without showing every keystroke. This type of output is what appears in this handbook. Once you understand the procedure for keying programs from the printed listings, you will find this method simple and fast. Here is the procedure:

- At the end of each program listing is a listing of status information required to properly execute that program. Included is the SIZE allocation required. Before you begin keying in the program, press **XEQ ALPHA SIZE ALPHA** and specify the allocation (three digits; e.g., 10 should be specified as 010).

Also included in the status information is the display format and status of flags important to the program. To ensure proper execution, check to see that the display status of the HP-41C is set as specified and check to see that all applicable flags are set or clear as specified.

- Set the HP-41C to PRGM mode (press the **PRGM** key) and press **■ GTO □ □** to prepare the calculator for the new program.
- Begin keying in the program. Following is a list of hints that will help you when you key in your programs from the program listings in this handbook.
 - When you see " (quote marks) around a character or group of characters in the program listing, those characters are ALPHA. To key them in, simply press **ALPHA**, key in the characters, then press **ALPHA** again. So "SAMPLE" would be keyed in as **ALPHA "SAMPLE" ALPHA**.
 - The diamond in front of each LBL instruction is only a visual aid to help you locate labels in the program listings. When you key in a program, ignore the diamond.
 - The printer indication of divide sign is /. When you see / in the program listing, press **÷**.
 - The printer indication of the multiply sign is ×. When you see × in the program listing, press **×**.
 - The † character in the program listing is an indication of the **APPEND** function. When you see †, press **■ APPEND** in ALPHA mode (press **■** and the K key).
 - All operations requiring register addresses accept those addresses in these forms:
nn (a two-digit number)
IND nn (INDIRECT: **■**, followed by a two-digit number)
X, Y, Z, T, or L (a STACK address: **□** followed by X, Y, Z, T, or L)
IND X, Y, Z, T or L (INDIRECT stack: **■ □** followed by X, Y, Z, T, or L)

Indirect addresses are specified by pressing **■** and then the indirect address. Stack addresses are specified by pressing **□** followed by X, Y, Z, T, or L. Indirect stack addresses are specified by pressing **■ □** and X, Y, Z, T, or L.

Printer Listing	Keystrokes	Display
01♦LBL "SAM PLE"	■ LBL ALPHA SAMPLE ALPHA	01 LBL^T SAMPLE
02 "THIS IS A "	ALPHA THIS IS A ALPHA	02^T THIS IS A
03 "I-SAMPLE "	ALPHA ■ APPEND SAMPLE	03^T †-SAMPLE
04 AVIEW	■ AVIEW ALPHA	04 AVIEW
05 6		05 6
06 ENTER↑	ENTER*	06 ENTER ↑
07 -2	2 CHS	07 -2
08 /	÷	08 /
09 ABS	XEQ ALPHA ABS ALPHA	09 ABS
10 STO IND L	STO ■ □ L	10 STO IND L
11 "R3="	ALPHA R3= ■ ARCL 03	11^T R3=
12 ARCL 03	■ AVIEW	12 ARCL 03
13 AVIEW	ALPHA	13 AVIEW
14 RTN	■ RTN	14 RTN

S T R U C T U R A L A N A L Y S I S I

by E. FIERENS , ing.

Research and development dept. of N.V. Nobels-Peelman.

Docent Industriële Hogeschool Mechelen.

T A B L E O F C O N T E N T S

1. BEAM CALCULATION	2 : 13
This program calculates for a beam, charged with concentrated loads, a uniformly distributed load and support moments, the support reactions, the maximum moment, the moment of inertia and the section modulus for three kinds of steel.	
2. CONTINUOUS BEAM	14 : 28
This program calculates the support moments of a continuous beam with maximum 5 unequal fields.	
3. MAXIMUM MAXIMORUM BENDING MOMENT	29 : 40
This program calculates the maximum maximorum bending moment and its location for a load train and a uniformly distributed load.	
4. N-TRUSS GIRDER	41 : 56
This program calculates the member loads in an inclined N-truss girder loaded with uniformly distributed loads and longitudinal loads.	
5. CHARACTERISTICS OF COMPOSITE CROSS-SECTIONS	57 : 66
This program calculates the characteristics of a composite steel-concrete section.	

B E A M C A L C U L A T I O N

(Requires an additional memory module)

This program calculates for a supported beam of uniform section; charged with n concentrated loads P_i ($i = 1 \dots n$), a uniform distributed load q and support moments M_L and M_R :

- The required moment of Inertia I_m for a given deflection coefficient $m = F/l$.
- The support reactions L and R.
- The location X of the maximum field moment.
- The maximum field moment max.M or in the case : $M_S = (M_R \text{ or } M_L) > \text{max.M}$.
the greatest support moment M_S .
- The required section moduli SM_i ($i = 1/3$) for three admissible tensions $\sqrt{f_i}$ ($i = 1/3$) of three kinds of steel.
- The bending moments M_i and the shearing forces Q_i at the position of the concentrated loads P_i and at each desired location a_i (input : a_i ; $P_i = 0$).

Operating limits and warnings.

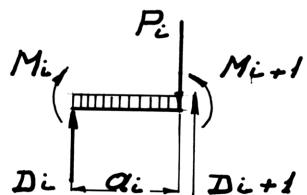
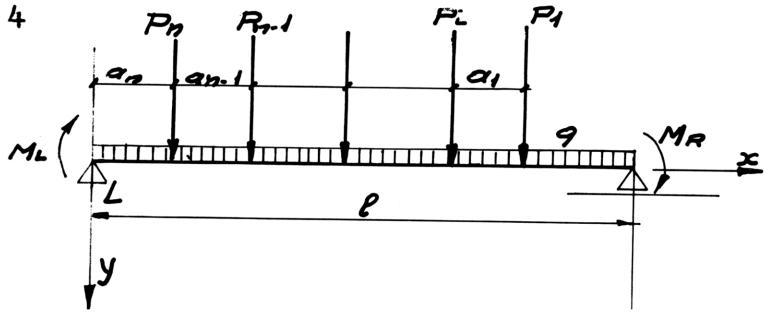
- To prevent the division by zero : $q \neq 0$
- In the case that the shearing force Q does not change of sign : max.M does not exist and M_S (M_L or M_R) is displayed and the section moduli are calculated accordingly.
- Mathematically it can be proved that for isostatic girders the maximum deflection and the deflection in the middle of the girder do not differ more than 2,5 % from each other.

When however the support moments M_L and M_R are important in comparison with the other loads and when those moments are working furthermore in opposite sense, it may occur that the elastica shows a deflection point, about in the middle of the span so that in this special case the calculated deflection is not a maximum.

For normal calculations the 41 C calculator works autonomically.

In the event that the moments and shear force line are to be calculated, the printer is required.

4



$P_i ; L ; R$: kN
$M_L ; M_R ; M$: kNm
q	: kN/m
$\ell ; \alpha_i$: m
I	: cm ⁴
SM	: cm ³
$E = 21000$: kN/cm ²

SUPPORT REACTIONS

$$R = \frac{q\ell}{2} + \frac{1}{\ell} \sum P_i x_i + \frac{M_L + M_R}{\ell}$$

$$L = q\ell + \sum P - R$$

$$\underline{\text{Deflection}} \quad F = y_{0,5\ell}$$

$$y_{0,5\ell} = F = \frac{1}{6EI} \left(\sum P_i x_i \frac{1}{2} \left(\ell^2 - \frac{\ell^2}{4} - x_i^2 \right) \right) + \frac{5}{384} \frac{q\ell^4}{EI} + \frac{(M_L - M_R)\ell^2}{6EI} \cdot \frac{3}{8} = \frac{\ell}{m}$$

$$F = \frac{1}{EI} \left[\frac{\ell^3}{72} \sum P_i \alpha_i (0,75 - \alpha_i^2) + \frac{9\ell^2}{76,8} + \frac{(M_L - M_R)}{16} \ell^2 \right] = \frac{\ell}{m}$$

$$I = \frac{m\ell^2}{E} \left[\frac{1}{12} \sum P_i \alpha_i (0,75 - \alpha_i^2) + \frac{9\ell}{76,8} + \frac{(M_L - M_R)}{16\ell} \right]$$

$$I = \frac{m\ell^2}{C} \left[\frac{1}{3} \left(\sum P_i \alpha_i (0,75 - \alpha_i^2) \right) + \frac{9\ell}{19,2} + \frac{M_L - M_R}{4\ell} \right] \text{ cm}^4$$

$$C = 8,4 \text{ kN/cm}^2$$

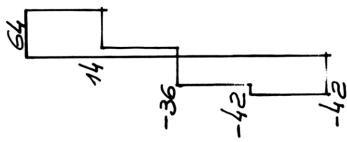
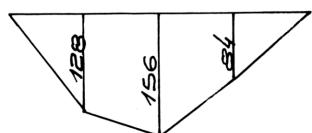
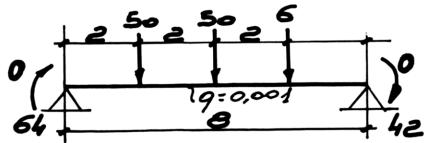
$$\frac{x}{\ell} \quad \begin{cases} \leq 0,5 \Rightarrow \alpha = \frac{x}{\ell} \\ > 0,5 \Rightarrow \alpha = 1 - \frac{x}{\ell} \end{cases}$$

Bending moments and shearing forces

$$\boxed{M_{i+1} = M_i + (D_i - 9\frac{\alpha_i}{2})\alpha_i}$$

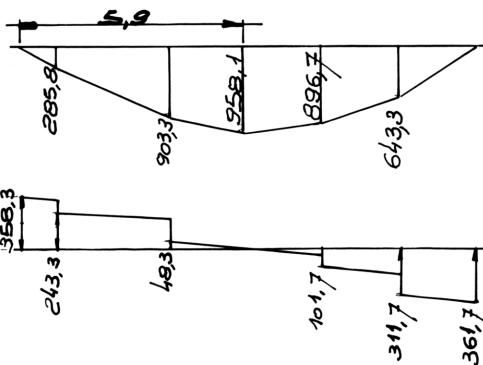
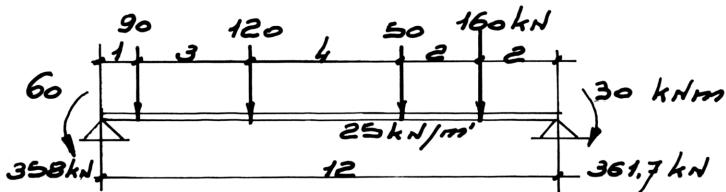
$$\boxed{D_{i+1} = D_i - 9\alpha_i - P_i}$$

$$\begin{aligned} D > 0 \quad \text{Sing}(D) = 1 \quad \} \quad \text{Sing}(D_i) + \text{Sing}(D_{i+1}) = 2 \Leftrightarrow & \text{ No sing change} \\ D < 0 \quad \text{Sing}(D) = -1 \quad \} \quad .. & = 0 \Leftrightarrow \text{ sing change} \end{aligned}$$

EXAMPLE 1Case I $\alpha' > \alpha$ 

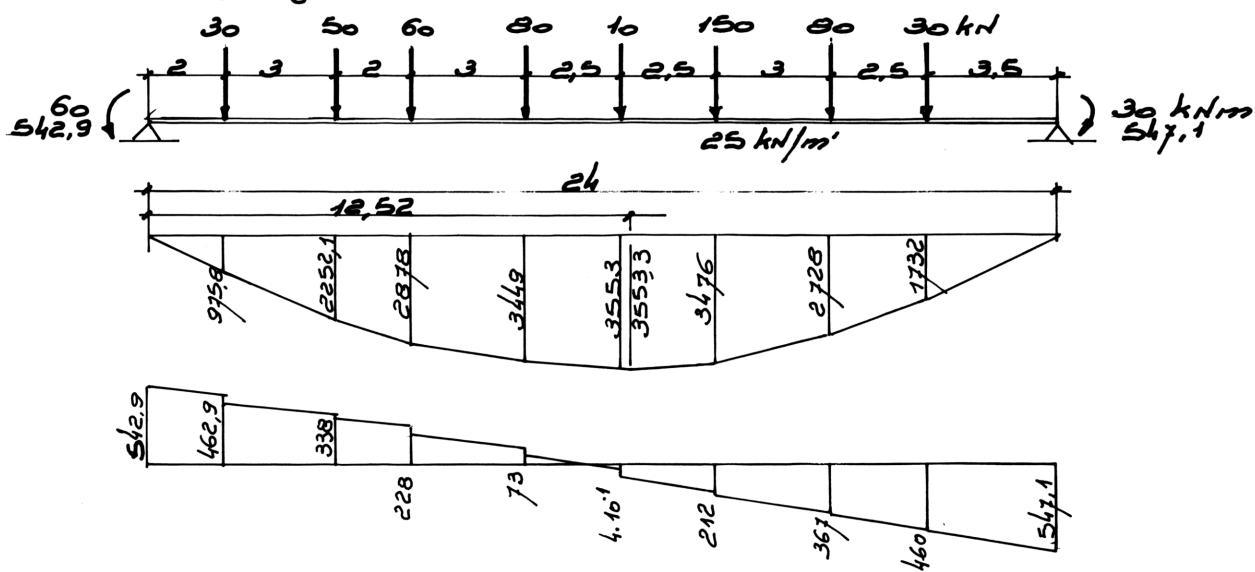
XEQ BEAM

SIGMA1=16,00
 SIGMA2=18,00
 SIGMA3=24,00
A
 F:L=300,00
B
 MOM.L=0,00
 MOM.R=0,00
 SPAN=6,00
 U,L.=1,00E-3
 N,P=3,00
 DIST,3.=2,00
 P3.=50,00
 DIST,2.=2,00
 P2.=50,00
 DIST,1.=2,00
 P1.=6,00
 I300.=16,858,
 SP:L=64,0R=42,0
 X=4,0
 MAX.M=156,0
 SM.16,0=975,1
 SM.18,0=866,7
 SM.24,0=650,0

EXAMPLE 2Case III $\alpha'_3 < \alpha_3$ 

A F:L=300,0
B MOM.L=-60,0
 MOM.R=30,0
 SPAN=12,0
 U,L.=25,0
 N,P=4,0
 DIST,4.=1,00
 P4.=90,00
 DIST,3.=3,00
 P3.=120,00
 DIST,2.=4,00
 P2.=50,00
 DIST,1.=2,00
 P1.=160,00
 I300.=175,347,
 SP:L=358,3R=361,7
 X=5,9
 MAX.M=950,1
 SM.16,0=5,937,2
 SM.18,0=5,272,1
 SM.24,0=3,958,6

E M 4, 286, Q 4, 243,
 M 3, 903, Q 3, 48,
 M 2, 897, Q 2,-102,
 M 1, 643, Q 1,-312,

EXAMPLE 3Case III $\alpha'_6 < \alpha_6$ B MOM.L=-60,

MOM.R=30,

SPAN=24,

U.L.=25,

N.P=8,

DIST.8.=2.00

P8.=30.00

DIST.7.=3.00

P7.=50.00

DIST.6.=2.00

P6.=60.00

DIST.5.=3.00

P5.=80.00

DIST.4.=2.50

P4.=10.00

DIST.3.=2.50

P3.=150.00

DIST.2.=3.00

P2.=80.00

DIST.1.=2.50

P1.=30.00

I300.=1.266.610,

SP:L=542.9 R=547.1

X=12.5

MAX.M=3.553.3

SM.16.0=22.208.4

SM.18.0=19.740.8

SM.24.0=14.885.6

F M 8, 976, 0 8, 463,

M 7, 2.252, 0 7, 338,

M 6, 2.878, 0 6, 228,

M 5, 3.449, 0 5, 73,

M 4, 3.553, 0 4, 4,-01

M 3, 3.476, 0 3,-212,

M 2, 2.728, 0 2,-367,

M 1, 1.732, 0 1,-460,

XEQ BEAM SIGMA1.=16.00

SIGMA2.=18.00

SIGMA3.=24.00

A F:L=300.00B MOM.L=600.00

MOM.R=300.00

SPAN=12.00

U.L.=0.10

N.P=3.00

DIST.3.=3.00

P3.=0.00

DIST.2.=3.00

P2.=0.00

DIST.1.=3.00

P1.=0.00

I300.=32.464.

SP:L=-74.4 R=75.6

MS=600.0

SM.16.0=3.750.0

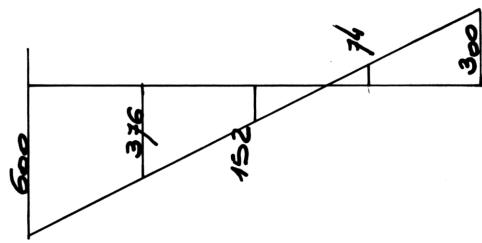
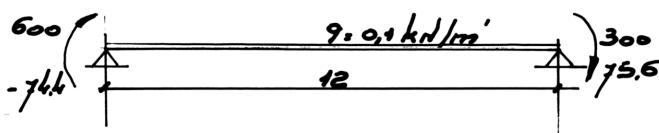
SM.18.0=3.333.3

SM.24.0=2.500.0

M 3, 376, 0 3,-75,

M 2, 152, 0 2,-75,

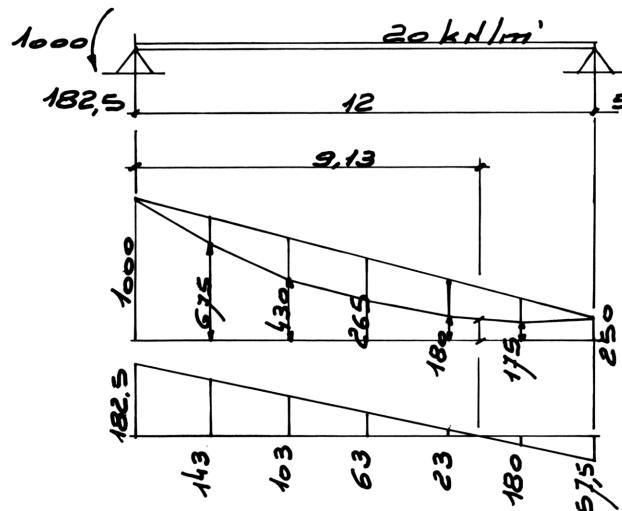
M 1,-74, 0 1,-75,

The display will show
NONEXISTENTEXAMPLE 4Case II $\alpha' > L$ 

EXAMPLE 5

7

Case III : $\alpha' < L$

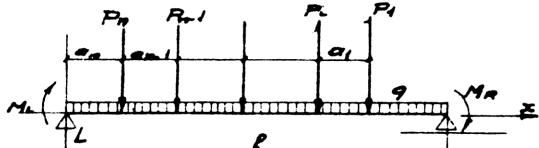


XEQ BEAM

SIGMA1,=16,00
 SIGMA2,=18,00
 SIGMA3,=24,00
 F:L=300,00
A
B MOM,L=-1,000,00
 MOM,R=250,00
 SPAN=12,00
 U.L.=20,00
 N.P=5,00
 DIST,5,=2,00
 P5,=0,00
 DIST,4,=2,00
 P4,=0,00
 DIST,3,=2,00
 P3,=0,00
 DIST,2,=2,00
 P2,=0,00
 DIST,1,=2,00
 P1,=0,00
 I300,=-69,643,
 SP:L=182,5R=57,5
 MS=1,000,0
 SM,16,0=6,250,0
 SM,18,0=5,555,6
 SM,24,0=4,166,7
F
 M 5,-675, 0 5, 143,
 M 4,-430, 0 4, 103,
 M 3,-265, 0 3, 63,
 M 2,-180, 0 2, 23,
 M 1,-175, 0 1,-18,

USER INSTRUCTIONS

PROGRAMMABLE
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Données Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
1	Load Program (user mode)		user	
2	Beginning execution and input data:		XEQ BEAM	SIGMA 1 =
3	Input : admissible tensions	σ_1 kN/cm ²	R/S	$\sigma_1 = \sqrt{\sigma_1}$
4		σ_2 "	R/S	$\sigma_2 = \sqrt{\sigma_2}$
5		σ_3 "	R/S	$\sigma_3 = \sqrt{\sigma_3}$
6			A	F:L =
7	Desired deflection coefficient :	$\alpha = F/L$	R/S	$F:L = \alpha$
8			B	MOM.L =
9	Left end moment	M_L kN m	R/S	$MOM.L = M_L$
10	Right end moment	M_R kN m	R/S	$MOM.R = M_R$
11	Beam span	L m	R/S	SPAN = L
12	Uniform distributed load	q kN/m	R/S	U.L = q
13	Number of concentrated loads	n	R/S	N.P = n
14	Distance	A_n m	R/S	DIST.n = A_n
15	Applied concentrated load	P_n kN	R/S	$P_n^n = P_n$
16	Repeat step 14 and 16 for	A_{n-1} m	R/S	DIST.n-1 = A_{n-1}
17	Each A_i and P_i ; $i = 1 \dots n$	P_{n-1} kN	R/S	$P_{n-1}^{n-1} = P_{n-1}$
18	Required moment of inertia	I_m^4		$I_m = I_r$
19	Support reactions	kN		SP.L=L. R=R
20	Position of the max.field moment	m		X = x
21	Max.bending moment in the field Or	kNm		MAX.M = M
22	The max. support moment	kNm		MS = M
23	Required section modul	cm ³		$SM.\sqrt{1} = SM_1$
24		"		$SM.\sqrt{2} = SM_2$
25		"		$SM.\sqrt{3} = SM_3$
26	Return to step 6			F:L =
27	If you want to print the bending moments and the shearing forces under each local load P_i		shearing MA N mode	
	Push	kNm ; kN	F	$M_{n,m} \dots Q_{n,q} \dots$
28	Return to step 6			MOM.L
29	For a new case go to step	2 : 6 or 8	[XEQ BEAM][A] or [B]	

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

9

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touchés Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touchés Tasti	Comments Kommentar Commentaires Commenti
01 LBL "BEA M"	XEQ BEAM		46 X=0?		
02 1.00301			47 GTO 04		
03 STO 00			48 XEQ 05		$n+1 \rightarrow REG.18$
04 LBL 00			49 LBL 02		$2n+1 \rightarrow REG.19$
05 RCL 00			50 FIX 0		
06 FIX 0			51 "DIST."		
07 "SIGMA"			52 ARCL 00		
08 ARCL X			53 XEQ 21		
09 XEQ 21			54 STO IND		$\alpha_i (i=1 \dots n)$
10 STO IND 00		$\sqrt{1}; \sqrt{2}; \sqrt{3}$	18		
11 ISG 00			55 ST+ 10		
12 GTO 00			56 RCL 10		
13 LBL A	A		57 RCL 07		
14 "F:L="		$m = F/l$	58 /		
15 PROMPT			59 STO 11		
16 XEQ 22			60 FIX 0		
17 STO 04			61 "P"		
18 LBL B	B		62 ARCL 00		
19 0			63 XEQ 21		$P_i (i=1 \dots n)$
20 STO 10			64 STO IND		
21 STO 12			19		
22 STO 13			65 ST+ 12		
23 STO 15			66 RCL 11		
24 CF 01			67 *		
25 CF 02			68 ST+ 13		
26 "MOM.L="			69 .5		
27 ASTO 05			70 RCL 11		
28 "MOM.R="			71 X<=Y?		
29 ASTO 06			72 GTO 03		
30 "SPAN="			73 1		
31 ASTO 07			74 -		
32 "U.L.="			75 CHS		
33 ASTO 08			76 LBL 03		
34 "N.P="			77 STO 14		
35 ASTO 09			78 X \times 2		
36 5.00901			79 .75		
37 STO 00			80 -		
38 LBL 01			81 CHS		
39 CLA			82 RCL 14		
40 ARCL IND 00			83 *		
41 PROMPT		$M_L; M_R; l; q; h$	84 RCL IND		
42 XEQ 22			19		
43 STO IND 00			85 *		
44 ISG 00			86 ST+ 15		
45 GTO 01			87 DSE 18		
			88 DSE 19		
			89 DSE 00		
			90 GTO 02		
			91 FIX 2		
			92 RCL 15		
			93 3		
			94 /		

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
95♦LBL 04			148	XEQ 22	R:4
96 RCL 08			149	XEQ 05	
97 RCL 07			150	RCL 05	
98 *			151	STO 13	
99 19.2			152	0	
100 /			153	STO 10	
101 +			154	STO 16	
102 RCL 05			155	RCL 09	
103 RCL 06			156	X=0?	
104 -			157	GTO 06	
105 4			158♦LBL 07		
106 /			159	RCL IND	
107 RCL 07					19
108 /			160	STO 15	
109 +			161	RCL IND	
110 RCL 07					18
111 X↑2			162	STO 14	
112 *			163	GTO 08	
113 8.4			164♦LBL 17		
114 /			165	RCL 16	
115 RCL 04			166	ST+ 13	
116 *			167	RCL 13	
117 FIX 0			168	STO IND	
118 "I"					18
119 ARCL 04			169	RCL 12	
120 "F="			170	STO IND	
121 ARCL X					19
122 XEQ 23			171	RCL 14	
123 RCL 08			172	ST+ 10	
124 RCL 07			173	DSE 18	
125 *			174	DSE 19	
126 2			175	DSE 00	
127 /			176	GTO 07	
128 RCL 05			177	FS? 01	
129 RCL 06			178	GTO A	CASE I a>a;
130 +			179	XEQ 09	
131 RCL 07			180	GTO A	CASE II a>b
132 /			181♦LBL 06		
133 +			182	SF 02	
134 RCL 13			183	RCL 07	
135 +			184	STO 14	
136 ENTER↑			185♦LBL 08		
137 ENTER↑			186	FS? 01	
138 RCL 08			187	GTO 13	
139 RCL 07			188	RCL 14	
140 *			189	RCL 12	
141 -			190	RCL 08	
142 ST- 12			191	/	
143 FIX 1			192	ABS	
144 "SP:L="					
145 ARCL 12					
146 "F=R="					
147 RCL Y					

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

11

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touchées Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touchées Tasti	Comments Kommentar Commentaires Commenti
193 X<=Y?	$\left \frac{D}{q} \right = a' \leq a_i$		242 XEQ 15		$ M_{FIELD} \leq Ms ?$
194 GTO 12			243 RCL 11		
195 GTO 13			244 RCL 10		
196 LBL 12			245 +		
197 STO 11			246 "X="		
198 XEQ 14			247 ARCL X		
199 XEQ 09			248 XEQ 23		
200 FS? 02			249 "MAX.M="		
201 GTO A			250 RCL 17		
202 LBL 13			251 XEQ 22		
203 FS? 02			252 LBL 10		
204 GTO 20			253 1.00301		
205 RCL 14			254 STO 11		
206 STO 11			255 FIX 1		
207 XEQ 14			256 LBL 16		
208 RCL 12			257 RCL 11		
209 SIGN			258 RCL 17		
210 RCL 11			259 RCL IND		
211 RCL 08			11		
212 *			260 /		
213 RCL 15			261 100		
214 +			262 *		
215 ST- 12			263 "SM."		
216 FS? 01			264 ARCL IND		
217 GTO 17			11		
218 X<>Y			265 "I="		
219 RCL 12			266 XEQ 22		
220 SIGN			267 ISG 11		
221 +			268 GTO 16		
222 X#0?			269 SF 01		
223 GTO 17			270 RTN		
224 RCL 16					
225 XEQ 09			271 LBL 14		
226 GTO 17			272 RCL 12		
227 LBL 09			273 RCL 11		
228 RCL 05			274 RCL 08		
229 ABS			275 *		
230 RCL 06			276 2		
231 ABS			277 /		
232 X>Y?			278 -		
233 GTO 19			279 RCL 11		
234 X<>Y			280 *		
235 LBL 19			281 STO 16		
236 RCL 13			282 RTN		
237 RCL 16					
238 +			283 LBL 05		
239 STO 17			284 RCL 09		
240 ABS			285 STO 00		
241 X<=Y?			286 19		
			287 +		
			288 STO 18		$n+19 \rightarrow REG.18$

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
289 RCL 00			333 ACX		
290 +			334 PRBUF		
291 STO 19		21+19 → REG. 19	335 DSE 18		
292 RTN			336 DSE 19		
293♦LBL 20			337 DSE 00		
294 0			338 GTO 18		
295 STO 13			339 GTO A		
296 XEQ 09			340 .END.		END OF PRINTING
297 GTO A			60		
298♦LBL 15					
299 RCL Y					
300 STO 17					
301 "MS= "					
302 RCL 17			65		
303 XEQ 22					
304 XEQ 10					
305 FS? 02					
306 GTO A					
307 GTO 13			70		
308♦LBL 21					
309 "I= "					
310 PROMPT					
311 FIX 2			75		
312♦LBL 22					
313 ARCL X					
314♦LBL 23					
315 AVIEW			80		
316 PSE					
317 RTN					
318♦LBL F					
319 XEQ 05					
320 FIX 0			85		
321♦LBL 18					
322 "M"					
323 ACX					
324 RCL 00					
325 ACX					
326 RCL IND					
18			90		
327 ACX					
328 " Q "					
329 ACX					
330 RCL 00					
331 ACX					
332 RCL IND					
19			00		

REGISTERS, STATUS, FLAGS

13

REGISTERBELEGUNG, FLAGS, BETRIEBSARTEN REGISTRES, INDICATEURS, MODES OPÉRATOIRES REGISTRI, MODI OPERATIVI, FLAGS

Registers Datenspeicher Registres de données Registri		Status Betriebsart Modes opératoires Modi operativi			
00 counter		Size 91 Total Reg. 110+2n	User Mode		
01	$\sqrt{1}$	Eng <input type="checkbox"/> Fix <input checked="" type="checkbox"/> Sci <input type="checkbox"/>	On <input checked="" type="checkbox"/>		
02	σ^2	Deg <input type="checkbox"/> Rad <input type="checkbox"/> Grad <input type="checkbox"/>	Off <input type="checkbox"/>		
03	σ^3				
05 m	M				
M	L				
M	R				
L					
q					
n					
10 $\sum a_i$	$\sum a_i$				
X/t	a _i				
$\sum P$	D _i				
$\sum P_x/L$	M _i				
15 $\sum P_d(0,75 - \alpha^2)$	a_{i+1}				
	a _i				
	P _i				
	$a(D - \frac{aq}{2})$				
	M _S or Max				
20 a-counter					
P-counter					
25	a_n	M _n			
	a_1	M ₁			
30	P_n	D _n			
	P_1	D ₁			
35	$n + 19$				
	$2n + 19$				
40					
45					
		Purpose Bedeutung Signification Scopo	Flags SET CLEAR		
00	max.M calculated				
01	n = 0				
02					
03					
04					
05					
06					
07					
08					
09					
10					
11	Audio execute				
12					
13					
14					
15					
16					
17					
18					
19					
20					
21	Printer Enable				
22	Number Input				
23	Alpha Input				
24	Range Ignore				
25	Error Ignore				
26	Audio Enable				
27	User Mode				
28	Decimal Point				
29	Digit Grouping				
Assignments Tastenbelegung / Assignations / Assegnamenti					
Function Funktion Fonction Funzione		Key Taste Touche Tasto	Function Funktion Fonction Funzione	Key Taste Touche Tasto	
Start of input " m = F/L MOM.L		A	Print M. and Q (Man. mode)		F
		B			

C O N T I N U O U S B E A M

(Requires an additional memory module)

This program calculates the support of a continuous beam with max.

5 unequal fields.

Each field i with a moment of inertia I_i and a span L_i is loaded with :

- an uniformly distributed load q_i
- any given number of local loads P_i
- external support moments M_L and M_R
- any given number of load factors R' and L' .

These factors may be calculated and inserted manually or by means of magnetic cards.

Note : The external support moments may be used as a random condition for the computation of continuous beams combined with cantilever beams (type GERBER).

Equation of three moments

$$\begin{bmatrix} a_{11} & a_{12} & 0 & 0 \\ a_{21} & a_{22} & a_{23} & 0 \\ 0 & a_{32} & a_{33} & a_{34} \\ 0 & 0 & a_{43} & a_{44} \end{bmatrix}$$

$$\begin{bmatrix} M_B \\ M_C \\ M_D \\ M_E \end{bmatrix} = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix}$$

\Rightarrow

reduced by elimination

$$\begin{bmatrix} a_{11} & a_{12} & 0 & 0 \\ 0 & b_{22} & a_{23} & 0 \\ 0 & 0 & b_{33} & a_{34} \\ 0 & 0 & 0 & b_{44} \end{bmatrix} \begin{bmatrix} M_B \\ M_C \\ M_D \\ M_E \end{bmatrix} = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix}$$

$$a_{11} = 2(L'_1 + L'_2)$$

$$a_1 = R_1 L'_1 + L_2 L'_2$$

$$a_{22} = 2(L'_2 + L'_3)$$

$$a_2 = R_2 L'_2 + L_3 L'_3$$

$$a_{33} = 2(L'_3 + L'_4)$$

$$a_3 = R_3 L'_3 + L_4 L'_4$$

$$a_{44} = 2(L'_4 + L'_5)$$

$$a_4 = R_4 L'_4 + L_5 L'_5$$

$$a_{12} = a_{21} = L'_2$$

$$L'_i = L_i : I_i ; \alpha_i = (P_a (L-a) : L^2)_i$$

$$a_{23} = a_{32} = L'_3$$

$$R_i = q L_i^2 / 4 + \sum_i \alpha_i (2L_i - a_i) + \sum R' + M_L$$

$$a_{34} = a_{43} = L'_4$$

$$L_i = q L_i^2 / 4 + \sum_i \alpha_i (L_i + a_i) + \sum L' + M_R$$

$$b_{22} = a_{22} - \frac{a_{12}^2}{a_{11}}$$

$$M_E = - b_4 : b_{44}$$

$$b_{33} = a_{33} - \frac{a_{22}^2}{b_{22}}$$

$$M_D = -(b_3 - a_{34} M_E) : b_{33}$$

$$b_{44} = a_{44} - \frac{a_{34}^2}{b_{33}}$$

$$M_C = -(b_2 - a_{23} M_D) : b_{22}$$

$$b_2 = a_2 - a_1 \frac{a_{12}}{a_{11}}$$

$$M_B = -(a_1 - a_{12} M_C) : a_{11}$$

$$b_3 = a_3 - b_2 \frac{a_{33}}{b_{22}}$$

$$b_4 = a_4 - b_3 \frac{a_{43}}{b_{33}}$$

$$\begin{bmatrix} a_{11} & a_{12} & 0 & 0 \\ a_{21} & a_{22} & a_{23} & 0 \\ 0 & a_{32} & a_{33} & a_{34} \\ 0 & 0 & a_{43} & a_{44} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \\ a_4 \end{bmatrix}$$

$a_{ij} = a_{ji}$

$$1) a_{11}a_{21}x_1 + a_{12}a_{21}x_2 = a_1a_{21}$$

$$2) a_{21}a_{11}x_1 + a_{22}a_{11}x_2 + a_{23}a_{11}x_3 = a_2a_{11}$$

$$(a_{12}^2 - a_{22}a_{11})x_2 - a_{23}a_{11}x_3 = a_1a_{21} - a_2a_{11}$$

$$(a_{22} - \frac{a_{12}^2}{a_{11}})x_2 + a_{23}x_3 = a_2 - a_1 \frac{a_{12}}{a_{11}}$$

b₂₂^{II}

b₂^{II}

$$2) b_{22}x_2 + a_{23}x_3 = b_2$$

$$3) a_{32}x_2 + a_{33}x_3 + a_{34}x_4 = a_3$$

$$2) b_{22}a_{32}x_2 + a_{23}a_{32}x_3 = b_2a_{32}$$

$$3) \underline{a_{32}b_{22}x_2 + a_{33}b_{22}x_3 + a_{34}b_{22}x_4 = a_3b_{22}}$$

$$(a_{23}^2 - a_{33}b_{22})x_3 - a_{34}b_{22}x_4 = b_2a_{32} - a_3b_{22}$$

$$(a_{33} - \frac{a_{23}^2}{b_{22}})x_3 + a_{34}x_4 = a_3 - b_2 \frac{a_{32}}{b_{22}}$$

$b_{33}^{||}$

$b_3^{||}$

$$3) b_{33}x_3 + a_{34}x_4 = b_3$$

$$4) a_{43}x_3 + a_{44}x_4 = a_4$$

$$3) b_{33}a_{43}x_3 + a_{34}a_{43}x_4 = b_3a_{43}$$

$$4) a_{43}b_{33}x_3 + a_{44}b_{33}x_4 = a_4b_{33}$$

$$(a_{34}^2 - a_{44}b_{33})x_4 = b_3a_{43} - a_4b_{33}$$

$$(a_{44} - \frac{a_{34}^2}{b_{33}})x_4 = a_4 - b_3 \frac{a_{43}}{b_{33}}$$

$b_{44}^{||}$

$b_4^{||}$

$$1) \begin{bmatrix} a_{11} & a_{12} & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} a_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix}$$

$$2) \begin{bmatrix} 0 & b_{22} & a_{33} & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} a_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix}$$

$$3) \begin{bmatrix} 0 & 0 & b_{33} & a_{34} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} a_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix}$$

$$4) \begin{bmatrix} 0 & 0 & 0 & b_{44} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} = \begin{bmatrix} a_1 \\ b_2 \\ b_3 \\ b_4 \end{bmatrix}$$

$$b_{rr} = a_{rr} - a_{r-1,r}^2 : b_{r-1,r-1}$$

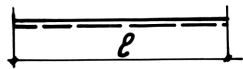
$$b_r = a_r - b_{r-1} \cdot \frac{a_{r,r-1}}{b_{r-1,r-1}}$$

$$\alpha = \frac{a}{l}$$

$$\beta = \frac{b}{l}$$

$$f = \frac{c}{l}$$

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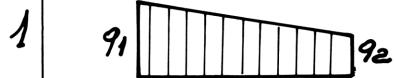


$$\frac{1}{6EI} \cdot L = \varphi_A$$

L

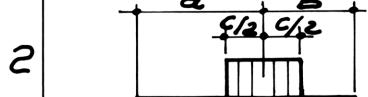
$$\varphi_B = -\frac{1}{6EI} \cdot R$$

R



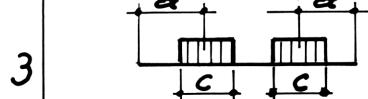
$$\frac{l^2}{60} (8q_1 + 7q_2)$$

$$\frac{l^2}{60} (7q_1 + 8q_2)$$



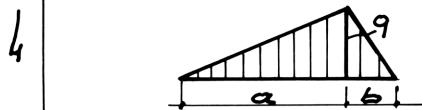
$$qbc(1 - \beta^2 - 0,25\gamma^2)$$

$$q \cdot a \cdot c (1 - \alpha^2 - 0,25\gamma^2)$$



$$qlc[3\alpha(1-\alpha) - 0,25\gamma^2]$$

$$qlc[3\alpha(1-\alpha) - 0,25\gamma^2]$$



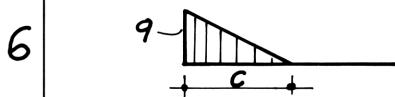
$$\frac{ql^2}{60} (1 + \beta)(\gamma - 3\beta^2)$$

$$\frac{ql^2}{60} (1 + \alpha)(\gamma - 3\alpha^2)$$



$$\frac{qc^2}{3} (2 - 2,25\gamma + 0,6\gamma^2)$$

$$\frac{qc^2}{3} (1 - 0,6\gamma^2)$$



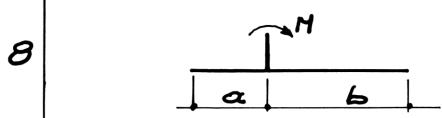
$$\frac{qc^2}{3} (1 - 0,75\gamma + 0,15\gamma^2)$$

$$\frac{qc^2}{6} (1 - 0,3\gamma^2)$$



$$\frac{ql^2}{4} [1 - \alpha^2(2 - \alpha)]$$

$$\frac{ql^2}{4} [1 - \alpha^2(2 - \alpha)]$$



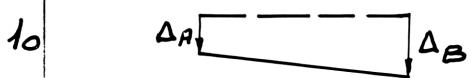
$$-M(1 - 3\beta^2)$$

$$M(1 - 3\alpha^2)$$



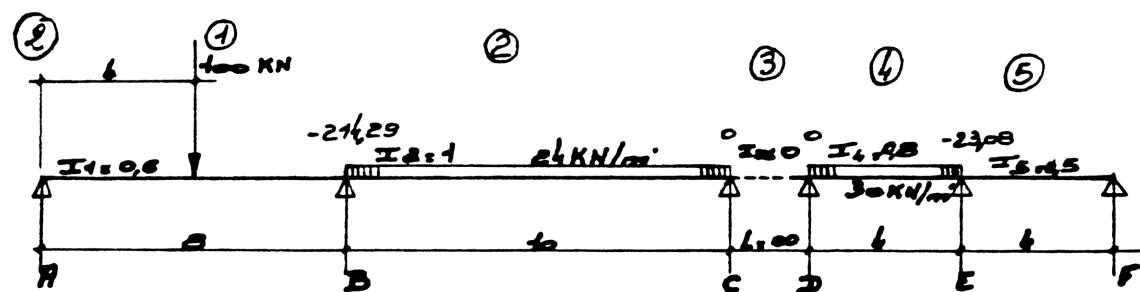
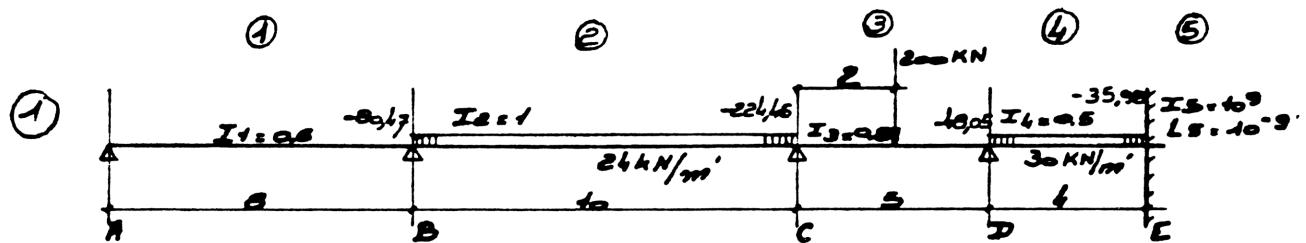
$$\frac{Pab}{l} (1 + \beta)$$

$$\frac{Pal}{l} (1 + \alpha)$$



$$\frac{GEI}{l^2} (\Delta_B - \Delta_A)$$

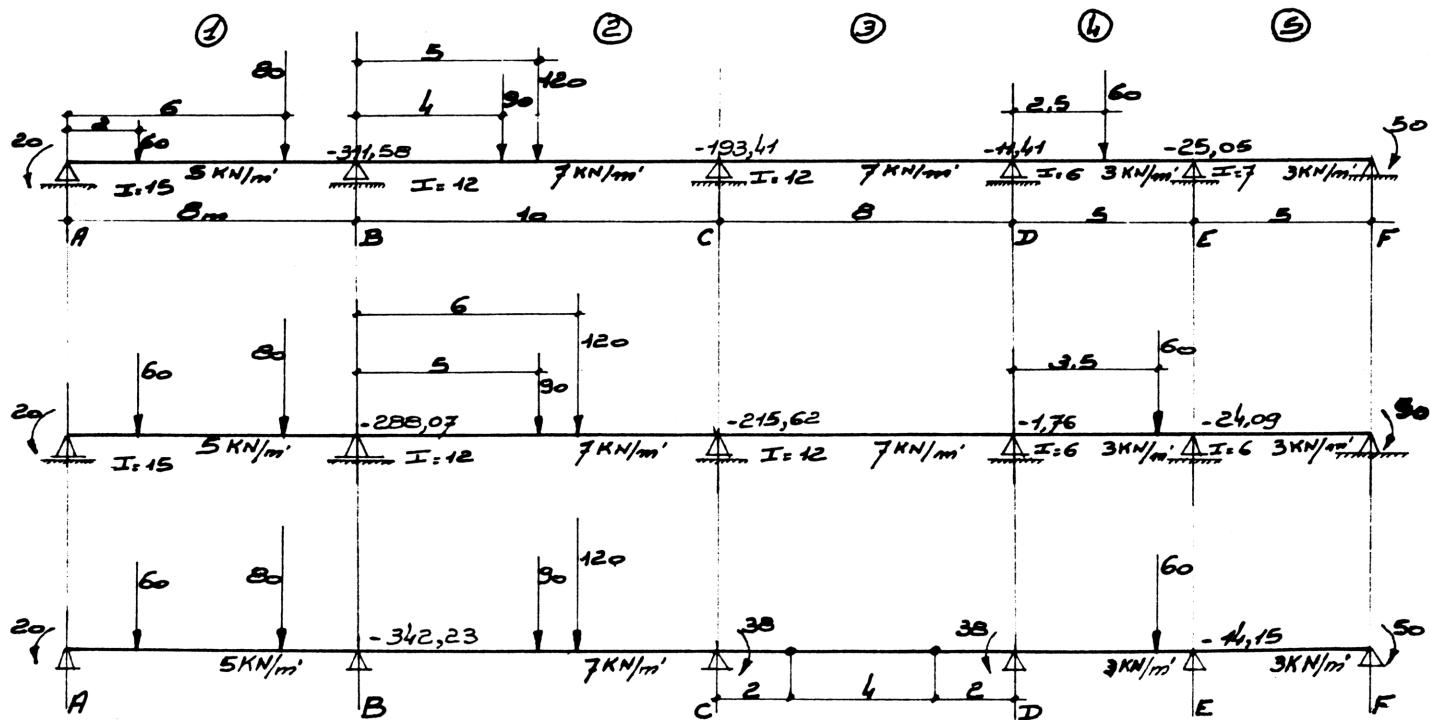
$$-\frac{GEI}{l^2} (\Delta_B - \Delta_A)$$

EXAMPLE 1

LBL	Case 1	LBL	Case 2
XEQ CB	F.N? = 1.00 I? = 0.60 L? = 8.00	A	F.N? = 1.00 I? = 0.60 L? = 8.00
B	F.N? = 2.00 I? = 1.00 L? = 10.00 UL? = 24.00		UL? = 0.00 X? = 4.00 P? = 100.00
B	F.N? = 3.00 I? = 1.00 L? = 5.00 X? = 2.00 P? = 200.00	B	F.N? = 2.00 I? = 1.00 L? = 10.00 UL? = 24.00
(c)		B	
B	F.N? = 4.00 I? = 0.50 L? = 4.00 UL? = 30.00	B	F.N? = 4.00 I? = 0.50 L? = 4.00 UL? = 30.00
B	F.N? = 5.00 I? = 1000000000. L? = 1.00E-9 ME = -35.98 MD = -48.05 MC = -224.46 MB = -80.47	E	ME = -23.08 MD = 1.07E-7 MC = -2.68E-7 MB = -214.29

EXAMPLE 2

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LBL

XEQ CB

$$F.N? = 1,00$$

$$I? = 15,00$$

$$L? = 8,00$$

$$UL? = 5,00$$

$$X? = 2,00$$

$$P? = 60,00$$

$$X? = 6,00$$

$$P? = 80,00$$

$$ML,R? = -20,00$$

$$MR,L? = 0,00$$

D

B

$$F.N? = 2,00$$

$$I? = 12,00$$

$$L? = 10,00$$

$$UL? = 7,00$$

$$X? = 4,00$$

$$P? = 90,00$$

$$X? = 5,00$$

$$P? = 120,00$$

B

B

$$F.N? = 3,00$$

$$I? = 12,00$$

$$L? = 8,00$$

$$UL? = 7,00$$

$$F.N? = 4,00$$

$$I? = 6,00$$

$$L? = 5,00$$

$$UL? = 3,00$$

$$X? = 2,50$$

$$P? = 60,00$$

B

B

$$F.N? = 5,00$$

$$I? = 7,00$$

$$L? = 5,00$$

$$UL? = 3,00$$

$$ML,R? = 0,00$$

D

E

$$MR,L? = -50,00$$

$$ME = -25,05$$

$$MD = -11,41$$

$$MC = -193,41$$

$$MB = -311,58$$

LBL
B

$$F.N? = 2,00$$

$$I? = 12,00$$

$$L? = 10,00$$

$$UL? = 7,00$$

$$X? = 5,00$$

$$P? = 90,00$$

$$X? = 6,00$$

$$P? = 120,00$$

$$F.N? = 4,00$$

$$I? = 6,00$$

$$L? = 5,00$$

$$UL? = 3,00$$

$$X? = 3,50$$

$$P? = 60,00$$

$$F.N? = 5,00$$

$$I? = 6,00$$

$$L? = 5,00$$

$$ME = -24,09$$

$$MD = 1,76$$

$$MC = -215,62$$

$$MB = -288,07$$

$$F.N? = 2,00$$

$$ML,R? = 0,00$$

$$MR,L? = -38,00$$

$$F.N? = 3,00$$

$$I? = 0,10$$

$$L? = 1,000,000,000,$$

$$UL? = 0,00$$

$$F.N? = 4,00$$

$$ML,R? = -38,00$$

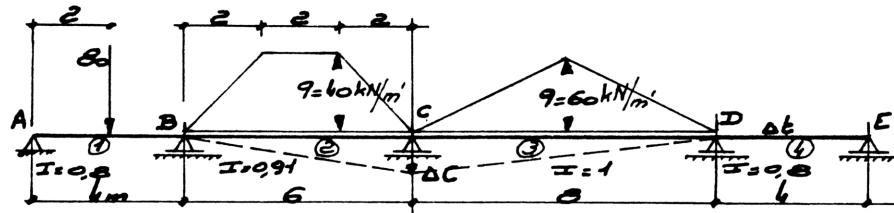
$$MR,L? = 0,00$$

$$ME = -14,15$$

$$MD = 1,27E-8$$

$$MC = -3,27E-8$$

$$MB = -342,23$$

EXAMPLE 31) Loads P and q:

$$\begin{cases} R_2 = L_2 = \frac{qL^2}{4} \left(1 - \frac{d^2}{L^2} (2-d) \right) = 60 \times \frac{6^2}{4} \left(1 - \left(\frac{2}{6} \right)^2 (2 - \frac{2}{6}) \right) = 293,3 \text{ kN} \\ R_3 = L_3 = \frac{5}{32} qL^2 = 5 \times 60 \times 6^2 : 32 = 500 \text{ kN} \end{cases}$$

2) Temperature difference in field 4 of $\Delta t = 60 - 66 = -30 \text{ grd.}$

$$\begin{array}{l} EI_4 = 24 \cdot 10^4 \text{ kNm}^2 \\ \alpha T = 10^{-5} \\ h = 60 \text{ cm} \end{array} \quad \begin{cases} R_4 = L_4 = 3EI_4 \alpha t \Delta t : h = 3 \times 24 \cdot 10^4 \times 10^{-5} \times 30 : 0,6 = 360 \\ \square \quad \text{---} \quad \Delta t \end{cases}$$

3) Displacement of support C: $\Delta C = 1 \text{ cm}$

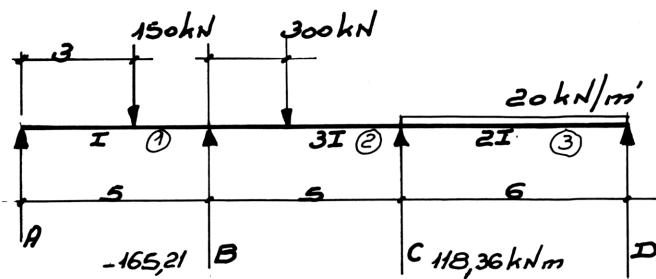
$$EI_2 = 0,91 \times 15 \times 10^4 \text{ kNm}^2$$

$$EI_1 = 1$$

$$R = -6EI(\Delta R - \Delta L) : L^2 \quad \begin{cases} R_2 = -6 \times 0,91 \times 15 \cdot 10^4 \times 0,01 : 6^2 = -227,5 & L_2 = 227,5 \\ R_3 = +6 \times 1 \times 15 \cdot 10^4 \times 0,01 : 6^2 = +140,6 & L_3 = -140,6 \end{cases}$$

$$L = -R$$

LBL	Case 1	LBL	Case 2	LBL	case 3
XEQCB	F.N? = 1,00 I? = 0,80 L? = 4,00 UL? = 0,00 X? = 2,00 P? = 00,00	A	F.N? = 1,00 I? = 0,80 L? = 4,00 UL? = 0,00	B	F.N? = 2,00 I? = 0,91 L? = 6,00 UL? = 0,00
B	F.N? = 2,00 I? = 0,91 L? = 6,00 ML,R? = 293,33 MR,L? = 293,33	B	F.N? = 2,00 I? = 0,91 L? = 6,00 UL? = 0,00	D	F.N? = 3,00 I? = 1,00 L? = 6,00 UL? = 0,00
D	F.N? = 3,00 I? = 1,00 L? = 6,00 ML,R? = 293,33 MR,L? = 293,33	B	F.N? = 3,00 I? = 1,00 L? = 6,00 UL? = 0,00	B	F.N? = 3,00 I? = 1,00 L? = 6,00 UL? = 0,00
B	F.N? = 4,00 I? = 0,80 L? = 4,00 ML,R? = 600,00 MR,L? = 600,00	D	F.N? = 4,00 I? = 0,80 L? = 4,00 UL? = 0,00 ML,R? = 360,00 MR,L? = 360,00	D	ML,R? = 140,63 MR,L? = -140,63 F.N? = 4,00 I? = 0,80 L? = 4,00 UL? = 0,00
E	ME=3,57E-8 MD=-128,44 MC=-182,55 MB=-57,38	E	ME=-7,89E-8 MD=-76,09 MC=22,29 MB=-6,34	E	ME=2,37E-8 MD=-85,34 MC=136,73 MB=-103,57

EXAMPLE 4

case a LBL XEQ CB F. N? = 1.00
 $I_2 = 1.00$
 $L_2 = 5.00$
 $UL_2 = 0.00$
 $X_2 = 3.00$
 $P_2 = 150.00$

F. N? = 2.00

$I_2 = 3.00$
 $L_2 = 5.00$
 $UL_2 = 0.00$
 $X_2 = 2.00$
 $P_2 = 300.00$

F. N? = 3.00

$I_2 = 2.00$
 $L_2 = 6.00$
 $UL_2 = 20.00$

$ME = 2.94E-9$
 $MD = -1.17E-8$

$MC = -118.36$

$MB = -165.21$

F. N? = 1.00

$I_2 = 1000000000.$

$L_2 = 1.00E-9$

F. N? = 2.00

$I_2 = 1.00$

$L_2 = 7.00$

$ML, R_2 = 39.20$

$MR, L_2 = 34.30$

F. N? = 3.00

$I_2 = 2.00$

$L_2 = 8.00$

$UL_2 = 6.00$

F. N? = 4.00

$I_2 = 1.00$

$L_2 = 7.00$

$ML, R_2 = 34.30$

$MR, L_2 = 39.20$

F. N? = 5.00

$I_2 = 1000000000.$

$L_2 = 1.00E-9$

$ME = -5.19$

$MD = -23.93$

$MC = -23.93$

$MB = -5.19$

F. N? = 1.00

$I_2 = 1.00$

$L_2 = 8.00$

$UL_2 = 4.00$

F. N? = 2.00

$I_2 = 1.20$

$L_2 = 6.00$

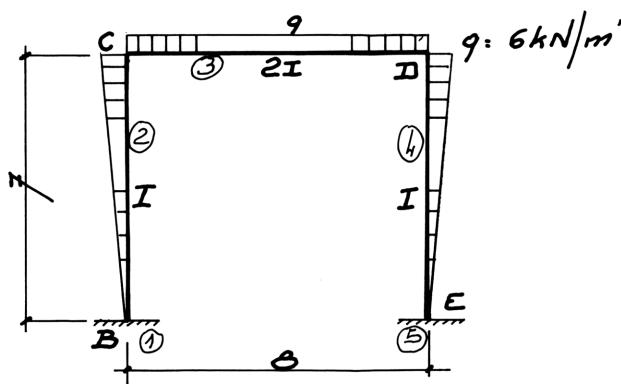
$ML, R_2 = -12.00$

$ME = 4.21E-10$

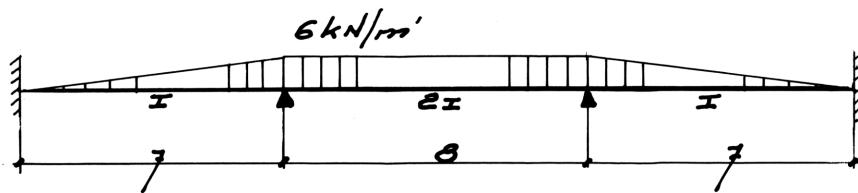
$MD = -1.68E-9$

$MC = 6.31E-9$

$MB = -19.69$



case b A



$$L_2 = \frac{7}{60} \cdot 6 \cdot 7^2 = 34.30 \text{ km}$$

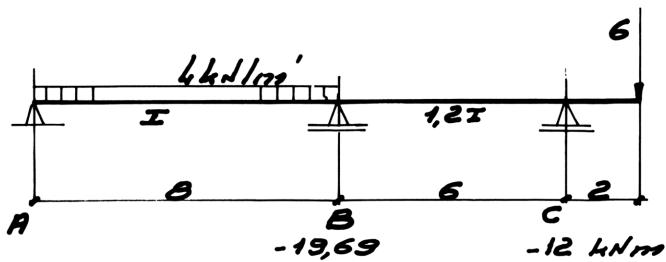
$$L_4 = R_2 = 39.20$$

$$R_2 = \frac{2}{15} \cdot 6 \cdot 7^2 = 39.20 \text{ kNm}$$

$$R_4 = L_2 = 34.30$$

E

case c A



Example 5 Extended program

REMARK : Optionally the program can be extended for direct calculation of the most occurring load factors (L : R).

In this example the program has been extended with the steps 235 : 309 to compute directly the load factors numbers : 1, 2 and 3 of the tabel.

$$L_a = 50 \times 8,5 \times 3 \left(1 - \left(\frac{8,5}{10}\right)^2 - 0,25\left(\frac{3}{10}\right)^2 \right) = 325,13 \quad R 16$$

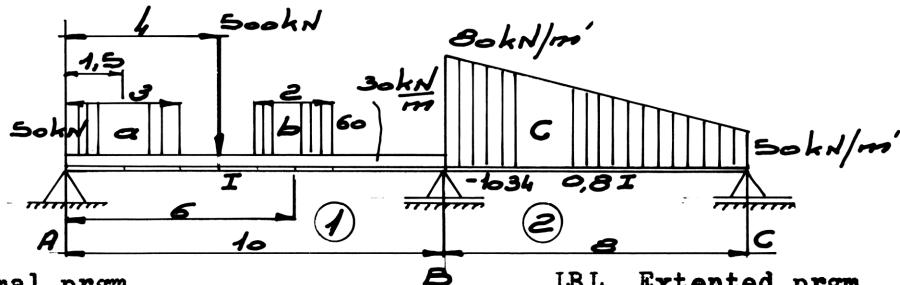
$$R_a = 50 \times 1,5 \times 3 \left(1 - \left(\frac{1,5}{10}\right)^2 - 0,25\left(\frac{3}{10}\right)^2 \right) = 214,88 \quad R 11$$

$$L_b = 60 \times 4 \times 2 \left(1 - \left(\frac{4}{10}\right)^2 - 0,25\left(\frac{3}{10}\right)^2 \right) = 398,40 \quad R 16$$

$$R_b = 60 \times 6 \times 2 \left(1 - \left(-\frac{6}{10}\right)^2 - 0,25\left(\frac{2}{10}\right)^2 \right) = 435,60 \quad R 11$$

$$L_c = \frac{8^2}{60} (8 \times 80 + 7 \times 50) = 1056 \quad R 17$$

$$R_c = \frac{8^2}{60} (7 \times 80 + 8 \times 50) = 1056 \quad R 12$$



LBL Normal prgm

A F.N? = 1,00

I? = 1,00

L? = 10,00

UL? = 30,00

X? = 4,00

P? = 500,00

D ML,R? = 214,88

MR,L? = 325,13

ML,R? = 435,60

MR,L? = 398,40

B F.N? = 2,00

I? = 0,00

L? = 8,00

D ML,R? = 1,024,00

MR,L? = 1,056,00

E ME=4,32E-10

MD=-1,73E-9

MC=6,49E-9

MB=-1,034,12

LBL Extended prgm

A F.N? = 1,00

I? = 1,00

L? = 10,00

UL? = 30,00

X? = 4,00

P? = 500,00

F X? = 1,50

C? = 3,00

Q? = 50,00

X? = 6,00

C? = 2,00

Q? = 60,00

B F.N? = 2,00

I? = 0,00

L? = 8,00

UL? = 0,00

G QL? = 80,00

QR? = 50,00

E ME=6,25E-10

MD=-2,50E-9

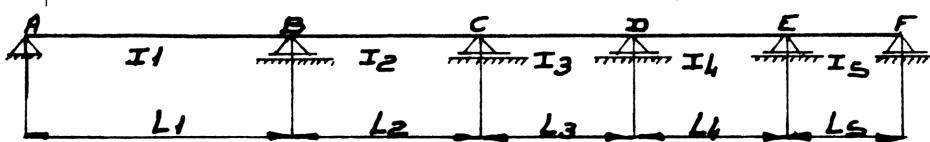
MC=9,37E-9

MB=-1,038,62

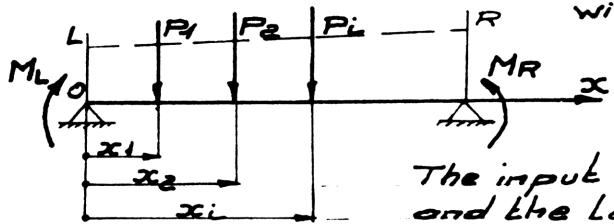
USER INSTRUCTIONS
PROGRAMMABLELAUF
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE

23

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Données Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
	CONTINUOUS BEAM CARDS		DISPLAY	PRINTER and DISPLAY
1	Enter program			<u>size</u>
2	Printer : used at option			<u>MAN.mode</u>
3	To start the execution or a new data input of another beam	print	<u>A or XEQCB</u>	<u>CLRG</u>
4	For each other field		<u>B</u>	
5	Input of the field number $i = 1 \dots 5$	F.N. ? i	R/S	<u>F.N.? = i</u>
6	Moment of inertia	I. ? I_i	R/S	<u>I.? = I_i</u>
7	Span	L. ? L_i	R/S	<u>L.? = L_i</u>
8	The uniformly distributed load	U.L.? q_i	R/S	<u>UL.? = q_i</u>
9	Input concentrated loads $i = 1 \dots n$		<u>C</u>	
10	Local coordinate	X.? x_i	R/S	<u>X.? = x_i</u>
11	The applied concentrated load	P.? P_i	R/S	<u>P.? = P_i</u>
12	Repeat step 10 and 11 for each concentrated load P_i applied in this field			
13	When the considered field i is loaded with external support moments or load factor	print	<u>D</u>	
14	Input of the left support moment and/or the load factor	ML,R ? m_{l_i}	R/S	<u>ML,R? = m_{l_i}</u>
15	Input of the right support moment and/or the left load factor	MR,L ? m_{r_i}	R/S	<u>MR,L? = m_{r_i}</u>
16	Repeat step 14 and 15 for each applied moment and/or load factor in this field	ML,R ?		
17	For each other field go to step 4			
18	Compute support moments		<u>E</u>	<u>M_E = ... M_D = ...</u>
19	Step 18 can be repeated; for a new case go to step 3			<u>M_C = ... M_B = ...</u>



*Indications of applied loads
with positive sign convention*



*The input sequence of the field numbers i
and the local loads in these fields is optional*

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
01♦LBL "CB"	A OR XEQ CB		47 /		
02 CLRG			48 RCL 23		
03 9.001			49 *		
04 STO 10			50 "P"		
05♦LBL 00			51 XEQ 10	Pi	
06 9 E9			52 *		
07 STO IND			53 STO 22		
10			54 RCL 24		
08 DSE 10			55 2		
09 GTO 00			56 *		
10♦LBL B	B		57 RCL 23		
11 SF 12			58 -		
12 "F.N"	FIELD NUMBER: i=1÷5		59 *		
13 XEQ 10			60 RCL 22		
14 CF 12			61 RCL 24		
15 STO 10			62 RCL 23		
16 10			63 +		
17 +			64 *		
18 STO 00			65 XEQ 01		
19 "I"	MOM. OF INERTIA: Ii		66 GTO C		
20 XEQ 10			67♦LBL D	D	
21 "L"			68 "ML,R"	SUPPORT MOM. OR	
22 XEQ 10			69 XEQ 10	LOAD FACTORS.	
23 STO 24			70 ENTER↑	ML OR R'	
24 X<>Y			71 "MR,L"	MR OR L'	
25 /			72 XEQ 10		
26 STO IND	SPAN : Li		73 X<>Y		
10			74 XEQ 01		
27 RCL 24			75 GTO D		
28 X↑2			76♦LBL E	E	
29 "UL"	UNIF. DISTR. LOAD: q_i		77 SF 00	COMPUTATION OF M	
30 XEQ 10			78 SF 12		
31 *			79 5		
32 4			80 STO 10		
33 /			81♦LBL 02	L'5 ÷ L'2	
34 ENTER↑			82 RCL IND		
35 STO IND			10		
00			83 DSE 10		
36 XEQ 04			84 GTO 19		
37 STO IND			85 GTO 03		
10			86♦LBL 19		
38 XEQ 09			87 RCL IND		
39♦LBL C	C		10		
40 RCL 24	CONCENTRATED LOADS		88 +		
41 "X"			89 2		
42 XEQ 10	X_i [i = 1÷n]		90 *		
43 STO 23			91 5		
44 -			92 ST+ 10		
45 RCL 24			93 RDN		
46 X↑2					

PROGRAM LISTING

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PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
94	STO IND 10	$a_4; a_3; a_2; a_1$	137	ENTER↑	
95	5		138	XEQ 07	
96	ST- 10		139	STO 08	b_{33}
97	GTO 02		140	RCL 09	
			141	RCL 08	
			142	RCL 04	
			143	ENTER↑	
			144	XEQ 07	b_{44}
100	STO 10		145	STO 09	
101	10		146	RCL 22	
102	+		147	RCL 06	
103	STO 00		148	RCL 21	
			149	RCL 02	
104	LBL 05		150	XEQ 07	
105	RCL IND 10		151	STO 22	
106	XEQ 04	$L'_i \quad (i = 5 \div 1)$	152	RCL 23	
107	RCL IND 10		153	RCL 07	
108	*	$L_i \quad (i = 5 \div 1)$	154	RCL 22	
109	XEQ 09		155	RCL 03	
110	RDN		156	XEQ 07	
111	DSE 00		157	STO 23	b_3
112	DSE 10		158	RCL 24	
113	GTO 18		159	RCL 08	
114	GTO 06		160	RCL 23	
			161	RCL 04	
115	LBL 18		162	XEQ 07	
116	RCL IND 10		163	RCL 09	
117	RCL IND 00		164	/	
118	*		165	CHS	
119	+		166	STO 24	
120	20		167	"ME"	$ME \Rightarrow REG. 24$
121	ST+ 10		168	XEQ 11	
122	RDN		169	RCL 08	
123	STO IND 10		170	RCL 23	
124	20		171	RCL 04	
125	ST- 10		172	RCL 24	
126	GTO 05	$a_4 \div a_1$	173	XEQ 08	
			174	STO 23	
127	LBL 06		175	"MD"	
128	RCL 07		176	XEQ 11	
129	RCL 06		177	RCL 07	
130	RCL 02		178	RCL 22	
131	ENTER↑		179	RCL 03	
132	XEQ 07		180	RCL 23	
133	STO 07		181	XEQ 08	
134	RCL 08		182	STO 22	
135	RCL 07		183	"MC"	
136	RCL 03		184	XEQ 11	

$Mc \Rightarrow REG. 22$

b_{22}

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
190 STO 21			234 PSE		
191 "MB"		<i>MB → REG.21</i>	235 .END.		
192 XEQ 11					
193 CF 12					
194 CF 00			55		
195 RTN					
196 *LBL 01					
197 ST+ IND					
00					
198 XEQ 04			60		
199 RDN					
200 ST+ IND					
10					
201 XEQ 09					
202 RTN			65		
203 *LBL 04					
204 15					
205 ST+ 10					
206 RDN			70		
207 RTN					
208 *LBL 07					
209 *					
210 X<>Y					
211 /			75		
212 -					
213 RTN					
214 *LBL 08					
215 *			80		
216 +					
217 X<>Y					
218 /					
219 CHS					
220 RTN			85		
221 *LBL 09					
222 15					
223 ST- 10					
224 RTN			90		
225 *LBL 10					
226 "F?" "					
227 PROMPT					
228 *LBL 11			95		
229 FIX 2					
230 "F="					
231 ARCL X					
232 AVIEW					
233 FS? 00			00		

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

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Line Zeile Ligne Linea	Keystrokes Tastenfolge Touchées Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touchées Tasti	Comments Kommentar Commentaires Commenti
228♦LBL 11			280	/	
229 FIX 2			281	-	
230 "F="			282	RTN	
231 ARCL X			283♦LBL G		G
232 AVIEW			284 "QL"		9e
233 FS? 00			285 XEQ 10		$L = \frac{R^2}{60^2} (89e + 79z)$
234 PSE		EXTENDED PROGRAM	286 STO 23		$R = \frac{L^2}{60^2} (79e + 89z)$
235 RTN			287 8		
236♦LBL F			288 *		
237 RCL 24			289 "QR"		9z
238 "X"			290 XEQ 10		$L = \frac{R^2}{60^2} (89e + 79z)$
239 XEQ 10			291 STO 22		$R = \frac{L^2}{60^2} (79e + 89z)$
240 STO 23			292 XEQ 13		
241 -			293 RCL 22		
242 "C"			294 8		
243 XEQ 10			295 *		
244 STO 21			296 RCL 23		
245 *			297 XEQ 13		
246 "Q"			298 XEQ 01		
247 XEQ 10			299 GTO G		
248 STO 22			300♦LBL 13		
249 *			301 ?		
250 XEQ 12			302 *		
251 RCL 24			303 +		
252 RCL 23			304 RCL 24		
253 -			305 X↑2		
254 RCL 24			306 *		
255 /			307 60		
256 X↑2			308 /		
257 -			309 END		
258 *					
259 XEQ 12					
260 RCL 23					
261 RCL 24					
262 /					
263 X↑2					
264 -					
265 RCL 22					
266 *					
267 RCL 23					
268 *					
269 RCL 21					
270 *					
271 XEQ 01					
272 GTO F					
273♦LBL 12					
274 1					
275 RCL 21					
276 RCL 24					
277 /					
278 X↑2					
279 4					
		$1 - 0.25 \left(\frac{C}{E} \right)^2$			
			85		
			90		
			95		
			00		

REGISTERS, STATUS, FLAGS
REGISTERBELEGUNG, FLAGS, BETRIEBSARTEN
REGISTRES, INDICATEURS, MODES OPÉRATOIRES
REGISTRI, MODI OPERATIVI, FLAGS

Registers Datenspeicher Registres de données Registri				Status Betriebsart Modes opératoires Modi operativi				
00	i+10			Size <u>25</u> Total Reg. <u>61</u>				User Mode
9E9	L ¹ L ² L ³ L ⁴ a ⁵ a ¹¹ a ²² a ³³ a ⁴⁴			Eng <input type="checkbox"/> Fix <input checked="" type="checkbox"/> Sci <input type="checkbox"/> Deg <input type="checkbox"/> Rad <input type="checkbox"/> Grad <input type="checkbox"/>				On <input checked="" type="checkbox"/> Off <input type="checkbox"/>
05				Purpose Bedeutung Signification Scopo				Flags
10	9,001	i	5	SET CLEAR				
R ₁				00	X	X		
R ₂				01				
R ₃				02				
R ₄				03				
R ₅				04				
L ₁				05				
L ₂				06				
L ₃				07				
L ₄				08				
L ₅				09				
P _i	b ₂			10				
X _i	b ₃			11	Audio execute			
L _i				12		XX		
25			M _B M _C M _D M _E	13				
30				14				
35				15				
40				16				
45				17				
				18				
				19				
				20				
				21	Printer Enable			
				22	Number Input			
				23	Alpha Input			
				24	Range Ignore			
				25	Error Ignore			
				26	Audio Enable			
				27	User Mode			
				28	Decimal Point			
				29	Digit Grouping			
Assignments Tastenbelegung / Assignations / Assegnamenti								
40			Function Funktion Fonction Funzione	Key Taste Touche Tasto	Function Funktion Fonction Funzione	Key Taste Touche Tasto		
45			Start = CLRG	A	Computation	E		
			Start input for		support moments			
			each other field	B				
			Input concentrated					
			loads	C				
			Input external					
			moment and factors	D				

M A X I M U M M A X I M O R U M B E N D I N G M O M E N T
(Requires an additional memory module)

This program calculates for a load train with n local loads P_i with a dynamic coefficient γ and an uniformly distributed load q :

- the left support reaction L
- the bending moment at any local load P_i
- the shear force just after any local load P_i
- the max. bending moment at each step Δ
- the max. bending moment and its location

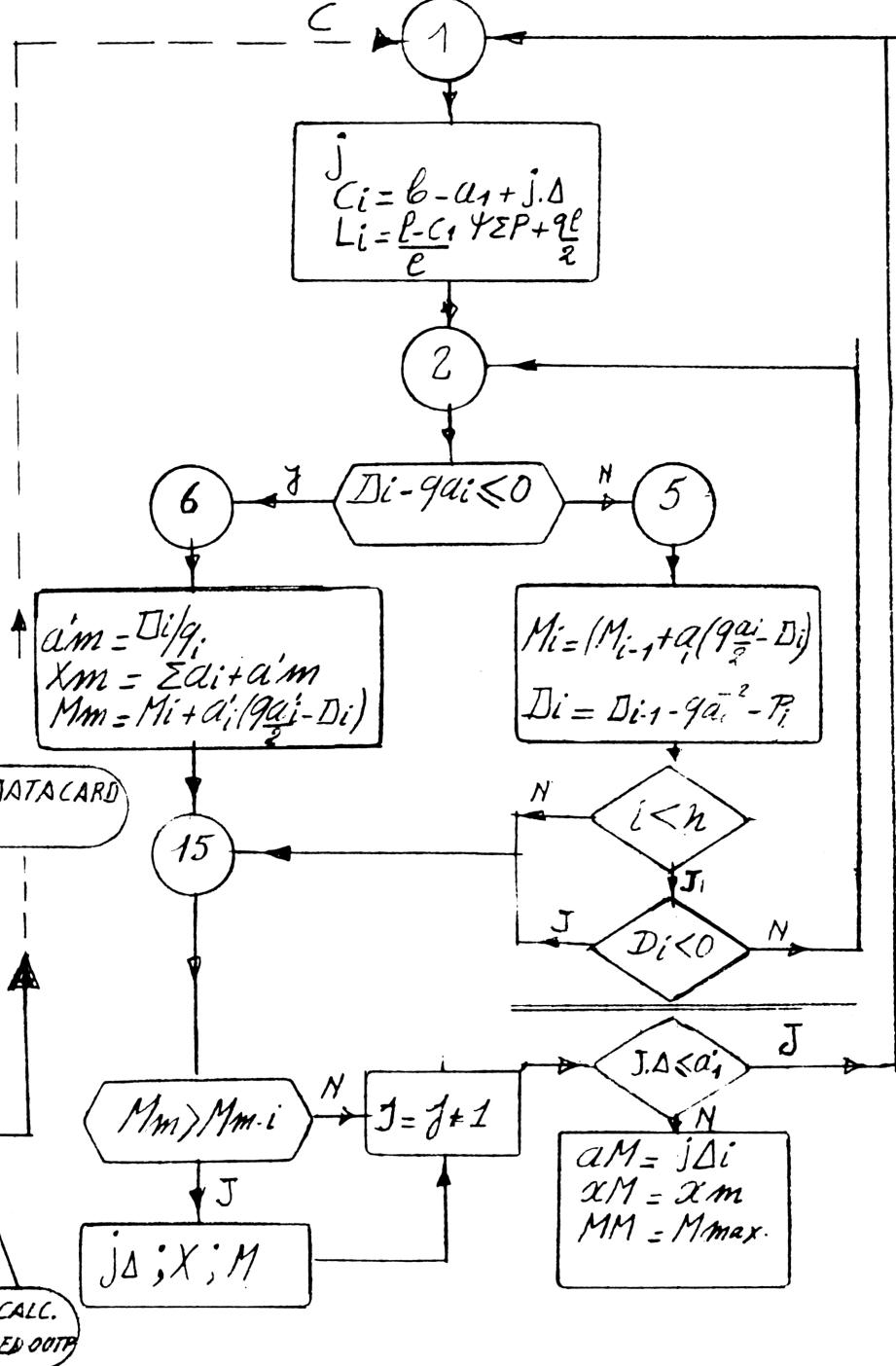
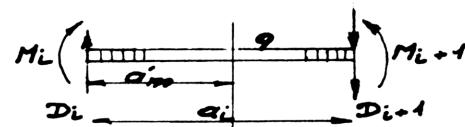
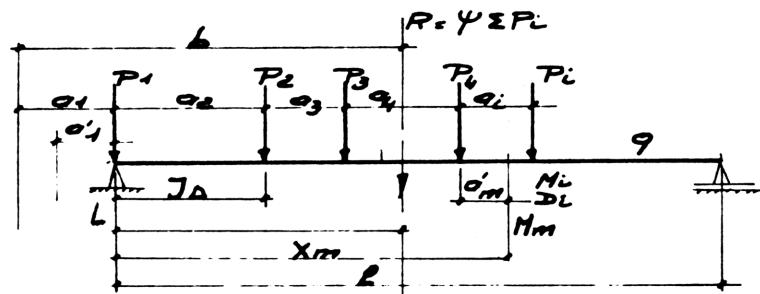
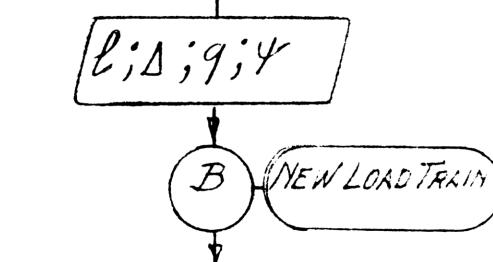
After the complete run (of n-steps) of the load train, this program gives the position $J\Delta$ of the train ; the max. maximorum moment and its location.

Note :

In this program it is possible to store data onto cards (for example : the load train) for later use.

CALCULATION OF THE MAXIMUM MAXIMUM BENDING MOMENT

(XEQM) A SF01 EXT. PAINT.

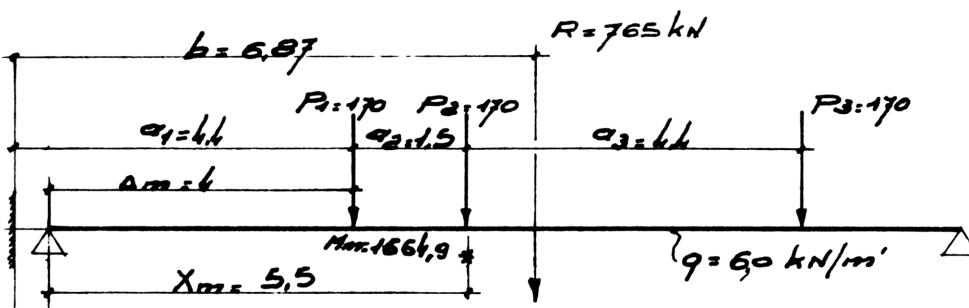
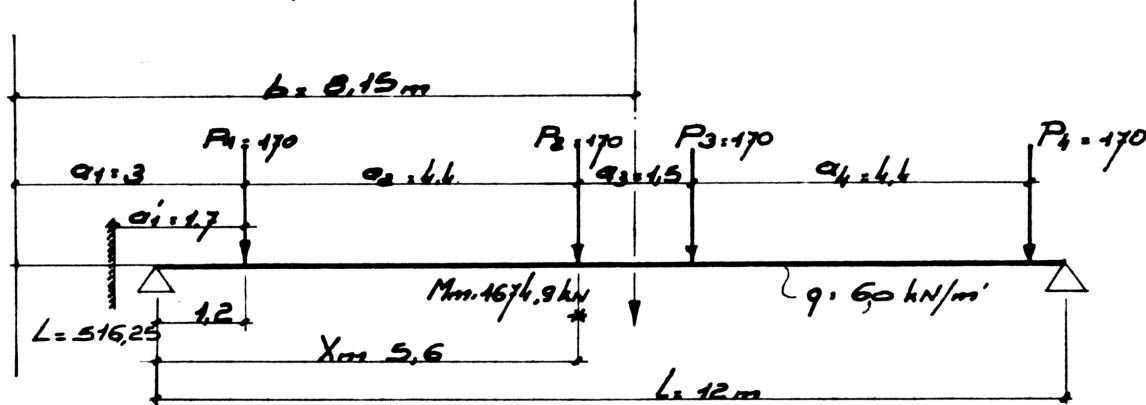


Example 1

$$\gamma = 1.5$$

$$\Delta = 0.2$$

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Example 2**A**

L=24.00
INC=1.00
UL=50.00
d=1.50
(B)
N=5.00
a=8.00
P=200.00
d.P=300.00
a=3.00
P=250.00
d.P=375.00
a=6.00
P=300.00
d.P=450.00
a=6.00
P=350.00
d.P=525.00
a=3.00
P=400.00
d.P=600.00
***(D)**
R=2.250.00
b=18.60
a1=6.00
X=14.63 M=10.522.27
X=12.75 M=10.364.06
X=12.38 M=9.003.52
aM=0.00
Xm=14.63
MM=10.522.27
N=0.00
MOMENT SHEAR
0.00 1.856.25
0.00 1.556.25
4.443.75 1.031.25
9.731.25 281.25
X=14.63 M=10.522.27
N=1.00
MOMENT SHEAR
0.00 1.762.50
1.737.50 1.412.50
5.750.00 887.50
10.175.00 137.50
X=12.75 M=10.364.06
N=2.00
MOMENT SHEAR
0.00 1.668.75
3.237.50 1.268.75
6.818.75 743.75
10.381.25 -6.25
N=3.00
MOMENT SHEAR
0.00 1.575.00
4.500.00 1.125.00
7.650.00 600.00
10.350.00 -150.00
N=4.00
MOMENT SHEAR
0.00 1.481.25
5.525.00 981.25
8.243.75 456.25
10.481.25 -293.75

SF01 C

N=5.00
MOMENT SHEAR
0.00 1.387.50
6.312.50 837.50
8.600.00 312.50
9.575.00 -437.50

N=6.00
MOMENT SHEAR
0.00 1.293.75
6.862.50 693.75
8.718.75 168.75
X=12.38 M=9.003.52
aM=0.00
Xm=14.63
MM=10.522.27

B

N=5.00
a=3.00
P=0.00
d.P=0.00
a=6.00
P=200.00
d.P=300.00
a=3.00
P=250.00
d.P=375.00
a=6.00
P=300.00
d.P=450.00
a=6.00
P=350.00
d.P=525.00
a=3.00
P=400.00
d.P=600.00
D? R/S

D? R/S

N=0.00
MOMENT SHEAR
0.00 1.987.50
0.00 1.687.50
7.762.50 337.50
8.550.00 -187.50

N=1.00
MOMENT SHEAR
0.00 1.846.63
1.815.63 998.63
7.906.25 240.63
8.403.13 -284.38

N=2.00**MOMENT SHEAR****0.00 993.75****1.887.50 893.75****7.906.25 143.75****X=13.88 M=8.112.89**

N=3.00

MOMENT SHEAR

0.00 946.88

2.615.63 796.88

7.762.50 46.88

X=12.94 M=7.784.47

N=4.00

MOMENT SHEAR

0.00 900.00

3.200.00 700.00

7.475.00 -50.00

N=5.00

MOMENT SHEAR

0.00 853.13

3.640.63 603.13

7.043.75 -146.88

N=6.00

MOMENT SHEAR

0.00 806.25

3.937.50 506.25

6.468.75 -243.75

aM=0.00

Xm=12.00

MM=8.550.00

B
N=4.00
a=6.00
P=0.00
d.P=0.00
a=9.00
P=200.00
d.P=300.00
a=3.00
P=250.00
d.P=375.00
a=6.00
P=300.00
d.P=450.00
a=6.00
P=350.00
d.P=525.00
a=3.00
P=400.00
d.P=600.00
D? R/S

N=0.00
MOMENT SHEAR
0.00 1.987.50
0.00 1.687.50
7.762.50 337.50
8.550.00 -187.50

N=1.00
MOMENT SHEAR
0.00 1.846.63
1.815.63 998.63
7.906.25 240.63
8.403.13 -284.38

N=2.00

MOMENT SHEAR

0.00 993.75

1.887.50 893.75

7.906.25 143.75

X=13.88 M=8.112.89

N=3.00

MOMENT SHEAR

0.00 946.88

2.615.63 796.88

7.762.50 46.88

X=12.94 M=7.784.47

N=4.00

MOMENT SHEAR

0.00 900.00

3.200.00 700.00

7.475.00 -50.00

N=5.00

MOMENT SHEAR

0.00 853.13

3.640.63 603.13

7.043.75 -146.88

N=6.00

MOMENT SHEAR

0.00 806.25

3.937.50 506.25

6.468.75 -243.75

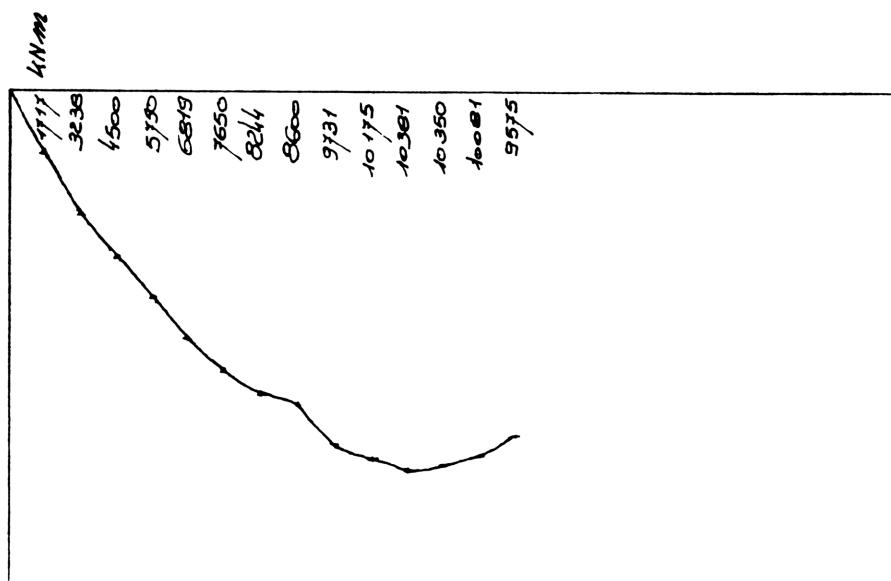
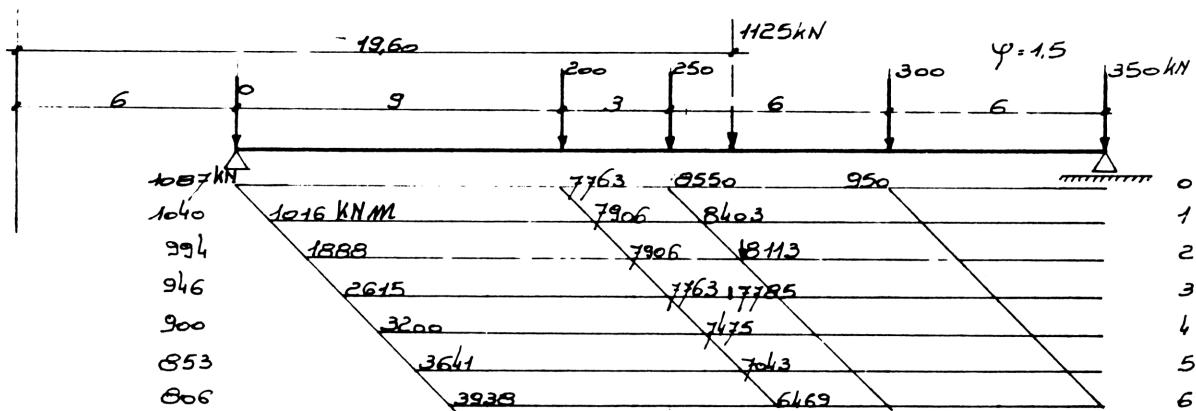
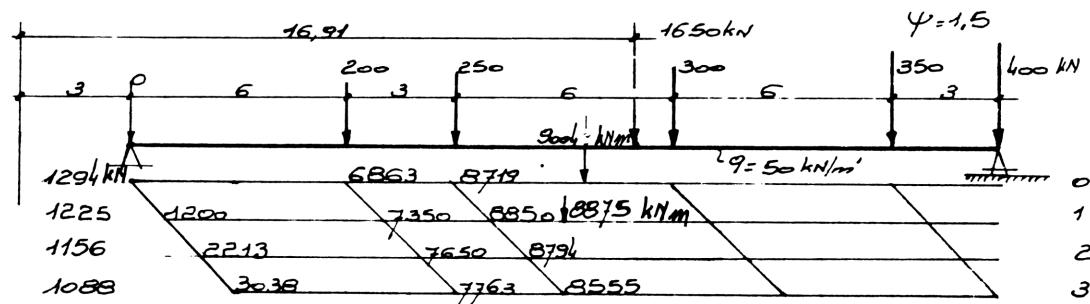
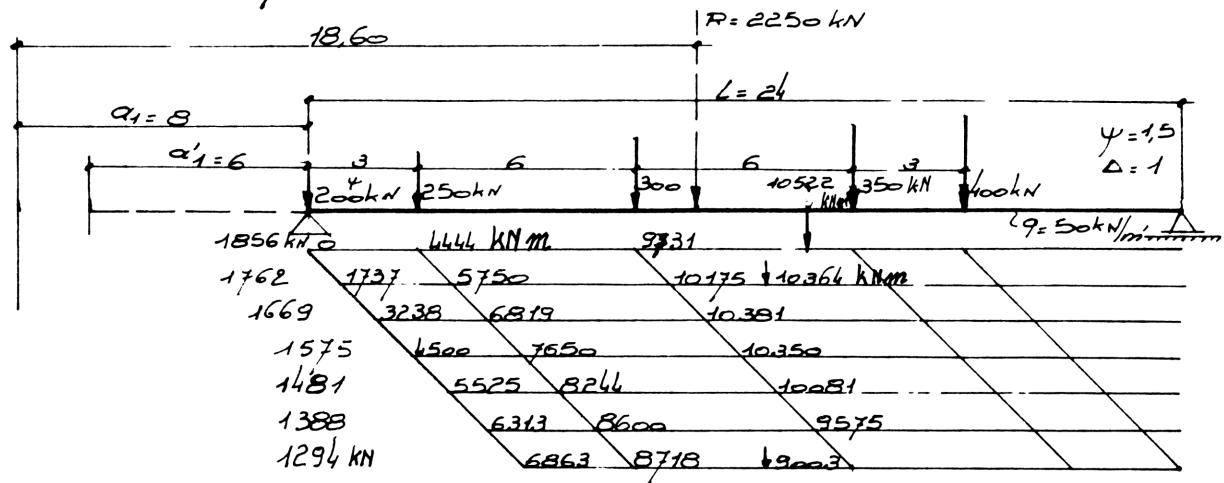
aM=0.00

Xm=12.00

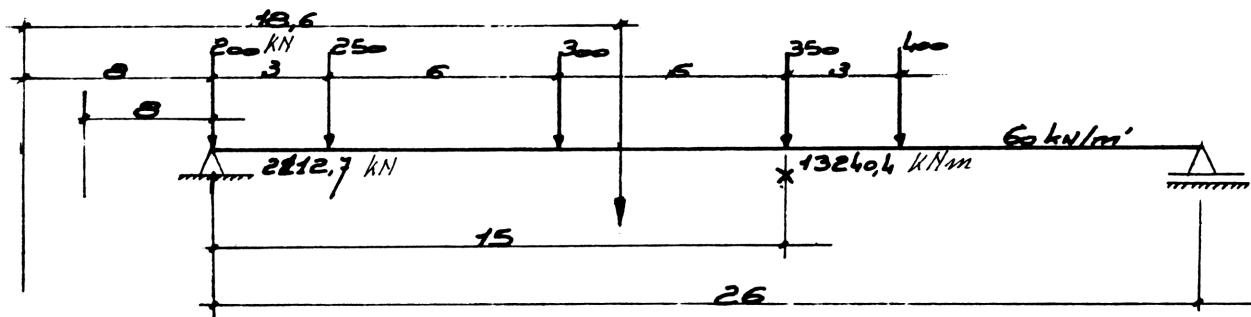
MM=8.550.00

***Note:**
STORE THE LOAD TRAIN FOR LATER USE
IN EXAMPLE 3
- ENTER 0.020 IN X-REGISTER
- XEQ WDTAX
- INSERT DATA CARD SIDES 1 AND 2
- PUSH R/S

Sketch example 2



Example 3



CALCULATE THE MAXIMUM MAXIMUM BENDING MOMENT FOR:

- L 26 24 22 m
- g 60 50 50 kN/m'

- LOAD TRAIN OF EXAMPLE 2 : USING DATA CARD

PUSH D D? DISPLAYED: INSERT DATA CARD SIDE 1 AND 2

LBL	LBL	LBL
CF01 A D(D?)R/S	A D(D?)R/S	A D(D?)R/S
L?=26,00 INC?=1,00 UL?=60,00 R=2.250,00 b=18,60 a1=8,00 X=15,02 M=13.067,32 X=13,58 M=12.954,99 X=12,13 M=12.967,47 X=13,87 M=11.617,47 X=12,42 M=11.154,99 aM=0,00 XM=15,00 MM=13.240,38	L?=24,00 INC?=1,00 UL?=50,00 R=2.250,00 b=18,60 X=14,63 M=10.522,27 X=12,75 M=10.364,06 X=12,38 M=9.003,52 X=10,56 M=8.606,25 aM=0,00 XM=14,63 MM=10.522,27	L?=22,00 INC?=1,00 R=2.250,00 b=18,60 X=11,82 M=8.666,74 X=12,64 M=7.816,94 X=10,59 M=7.304,18 aM=1,00 XM=10,00 MM=8.686,36

USER INSTRUCTIONS

PROGRAMMABLEAUF
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE

35

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Donnees Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
	MAXIMUM MAXIMORUM BENDING MOMENT		CF 28; SF 29	
		DISPLAY		PRINTER and DISPLAY
1	Enter program 2 cards			size 16+n CF 01
2	Printer : used at option			MAN. mode
3	If you want to print L ; M _i ; Q _i under each local load P _i at each step J			SF 01
4	To start the execution		<u>A or XEQMM</u>	
5	The span	L ? 1	R/S	L? = 1
6	The step	INC ? Δ	R/S	INC? = Δ
7	The uniformly distributed load	UL ? q	R/S	UL? = q
8	The dynamic coefficient	d ? γ	R/S	d ? = γ
9	Start of input of the load train		B	
10	The number of concentrated loads	N ? n	R/S	N ? = n
11	The distance	a ? a _i	R/S	a ? = a _i
12	The applied concentrated load	P ? P _i	R/S	P ? = P _i
13	Repeat step 11 and 12 for each input of a _i and P _i			
14	Insert data card sides 1 and 2 [Data card used at option]	D ?	XEQ WDTA	
15	If no data card is used Location of the resultant R The maximum admissible distance a ₁ a ₁ is only displayed in the case that a ₁ ≥ a _{max} .		R/S	R = P _i b = b a ₁ = a _{1 max} .
	Step number			N = j
	L : left support reaction			Moment shear
	M _i : the bending moment under P _i			0,00 L
	Q _i : the shear force just after P _i			M _i Q _i
	X : the coordinate of the location of the max. moment			M _i Q _i
	M : the maximum moment			
	X and M are only displayed in the case that the location of the maximum moment does not correspond with a local load			X =... M =...
	The coordinate of the load P _i in number of steps			aM = ... RG.9
	The coordinate of the maximum moment			xM = ... RG.8
	The max. maximorum bending moment			MM = ... RG.7
16	For a new load train go to step 9		<u>B</u>	
17	For repetition of the calculation after a complete run push		<u>C</u>	

USER INSTRUCTIONS

PROGRAMMABLE AUF INSTRUCTIONS D'EMPLOI NORME OPERATIVE

PROGRAM LISTING

37

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
01♦LBL "M"	XEQ M OR ASNA		51 "D?"		D= DATA CARD
02 "L"	L? = L		52 PROMPT		RIS: CONTINUE
03 XEQ 10			53 SF 02		
04 STO 10			54 RCL 00		
05 "INC"	INC? = A		55 RCL 02		
06 XEQ 10			56 RCL 01		
07 STO 11	UL? = 9		57 "R"		
08 "UL"			58 XEQ 11		
09 XEQ 10			59 /		
10 STO 12	d? = 4		60 "b"		
11 "d"			61 XEQ 11		
12 XEQ 10			62 STO 00		
13 STO 13			63 RDN		
14♦LBL B	B		64 RCL 10		
15 "N"	N? = n		65 X<=Y?		
16 XEQ 10			66 XEQ 08		
17 16015			67♦LBL C		C
18 +			68 0		
19 1 E3			69 STO 03		REPETITION
20 /			70 STO 07		CALCULATION
21 STO 14	16,015 + n.10 ⁻³ → 14		71♦LBL 01		
22 STO 15	" " " → 15		72 0		
23 0			73 STO 06		
24 STO 00			74 STO 05		
25 STO 01			75 RCL 03		
26 STO 02			76 RCL 00		
27♦LBL 00			77 +		
28 "a"	a? = a _i (i=1÷n)		78 XEQ 03		
29 XEQ 10			79 -		
30 ST+ 00			80 RCL 10		
31 E2			81 -		
32 *			82 CHS		
33 "P"	P? = P _i (i=1÷n)		83 RCL 10		
34 XEQ 10			84 /		
35 RCL 13			85 RCL 01		
36 *			86 *		
37 "d.P"	d.P = 4P _i		87 RCL 10		
38 XEQ 11			88 RCL 12		
39 ST+ 01			89 *		
40 E4			90 2		
41 /			91 /		
42 +			92 +		
43 STO IND 15			93 STO 04		
44 XEQ 09			94 RCL 14		
45 RCL 00			95 STO 15		
46 *			96 FS? 01		
47 ST+ 02			97 XEQ 13		
48 ISG 15			98 SF 00		
49 GTO 00			99♦LBL 02		
50♦LBL D	D		100 XEQ 12		
			101 ST+ 06		

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
102 RCL 12			152 SF 12		
103 *			153 RCL 09		
104 RCL 04			154 "aM"		$aM - jA \rightarrow 9$
105 X<=Y?			155 XEQ 11		
106 GTO 06			156 RCL 08		
107 XEQ 12			157 "XM"		
108 XEQ 05			158 XEQ 11		$XM - Xm \rightarrow 8$
109 XEQ 12			159 RCL 07		
110 RCL 12			160 "MM"		
111 *			161 XEQ 11		$MM - Max.M \rightarrow 7$
112 RCL 04			162 CF 12		
113 -			163 CF 02		
114 CHS			164 RTN		
115 RCL IND 15			165+LBL 03		
116 XEQ 09			166 RCL 16		
117 -			167 XEQ 07		
118 STO 04			168 RTN		
119 ISG 15		$D_i < 0$	169+LBL 04		
120 X<0?			170 RCL 05		
121 GTO 15			171 STO 07		
122 CF 00			172 RCL 06		
123 GTO 02			173 STO 08		
124+LBL 06			174 RCL 03		
125 XEQ 12			175 STO 09		
126 ST- 06			176 RTN		
127 RCL 04			177+LBL 09		
128 RCL 12			178 FRC		
129 /			179 E4		
130 ST+ 06			180 *		
131 XEQ 05		$X = \sum a_i - a_i + JA$	181 RTN		
132 "X="			182+LBL 08		
133 ARCL 06		$M = Mi + a'(ga' - Di)$	183 -		
134 "F M="			184 CHS		
135 ARCL 05			185 ST+ 00		
136 AVIEW			186 XEQ 03		
137 GTO 17			187 +		
138+LBL 15			188 "a1"		
139 FS? 01			189 XEQ 11		
140 XEQ 14			190 E2		
141+LBL 17			191 *		
142 RCL 05			192 RCL 16		
143 RCL 07			193 FRC		
144 X<=Y?			194 +		
145 XEQ 04			195 STO 16		
146 RCL 11			196 RTN		
147 ST+ 03			197+LBL 07		
148 XEQ 03			198 INT		
149 RCL 03			199 E2		
150 X<=Y?			200 /		
151 GTO 01					

PROGRAM LISTING

39

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

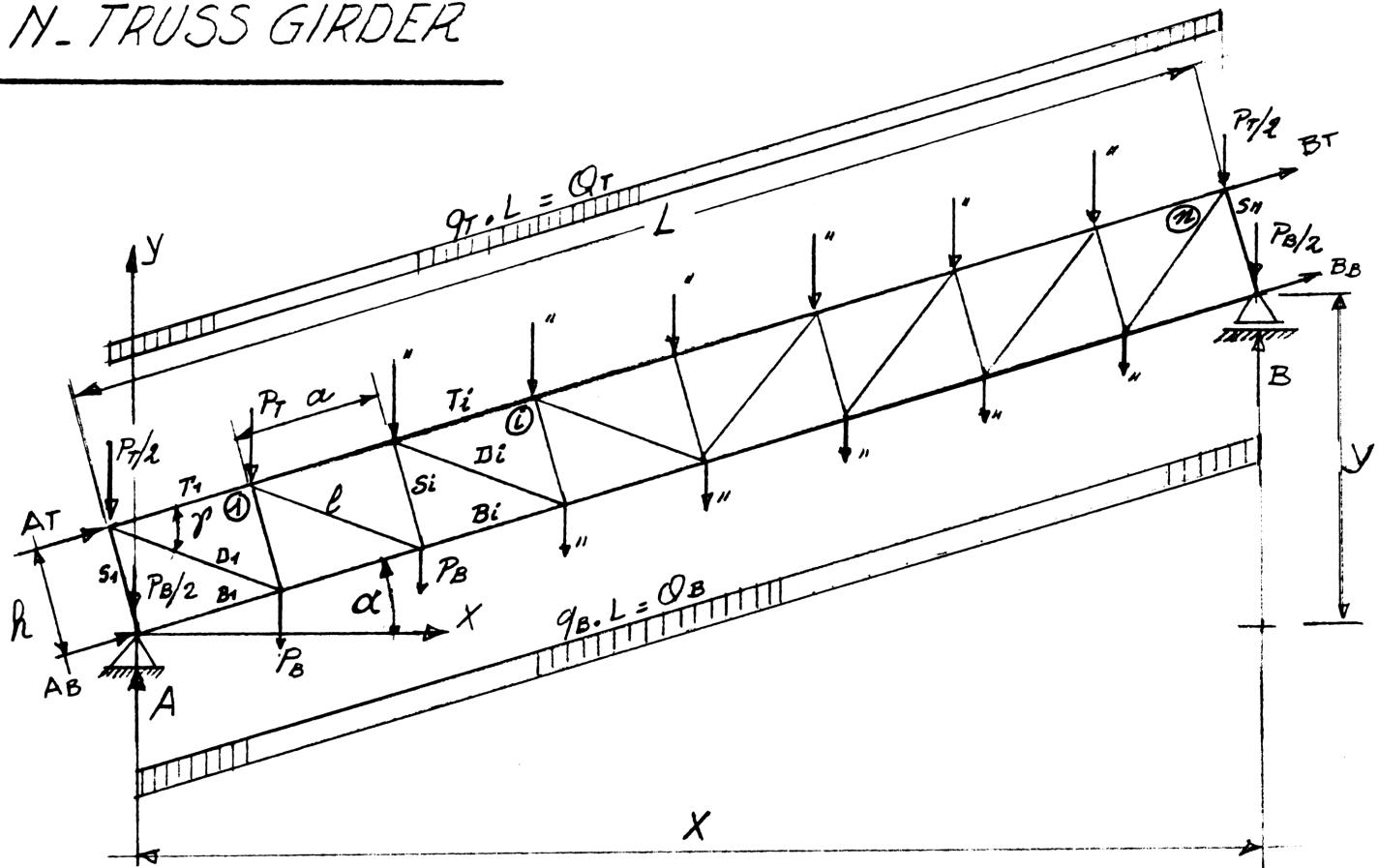
LISTATO DI PROGRAMMA

REGISTERS, STATUS, FLAGS
REGISTERBELEGUNG, FLAGS, BETRIEBSARTEN
REGISTRES, INDICATEURS, MODES OPÉRATOIRES
REGISTRI, MODI OPERATIVI, FLAGS

Registers Datenspeicher Registres de données Registri				Status Betriebsart Modes opératoires Modi operativi
00 0 Σa_i 0 $\gamma \sum p_i$ 0 $\gamma \sum b_i p_i$ 0 i 05 0 Σa_i 0 n 0 $\sum a_i - a_1$ MM xM aM				Size <u>16+11</u> Total Reg. <u>80+11</u> User Mode Eng <input type="checkbox"/> Fix <input type="checkbox"/> Sci <input type="checkbox"/> On <input checked="" type="checkbox"/> Deg <input type="checkbox"/> Rad <input type="checkbox"/> Grad <input type="checkbox"/> Off <input type="checkbox"/>
10 1 Δ q γ 16,015 15 16,015 (a,P) ₁ " " 2 " " 3 " " 4 20 " " 5 " " 6				Purpose Bedeutung Signification Scopo
				Flags
				SET CLEAR
00 X X No				
01 X X Extented output print				
02 X				
03				
04				
05				
06				
07				
08				
09				
10				
11 Audio execute				
12 X				
13				
14				
15				
16				
17				
25 18				
26 19				
27 20				
28 Printer Enable				
29 Number Input				
30 Alpha Input				
31 Range Ignore				
32 Error Ignore				
33 Audio Enable				
34 User Mode				
35 Decimal Point				X
36 Digit Grouping				X
Assignments Tastenbelegung/Assignations/Assegnamenti				
Function Funktion Fonction Funzione		Key Taste Touche Tasto	Function Funktion Fonction Funzione	Key Taste Touche Tasto
40 Start XEQ M		A		
41 Input new load		B		
42 train				
43 Repetition		C		
44 Data card		D		

N - TRUSS GIRDER

(Requires an additional memory module)

N-TRUSS GIRDER

Loads with positive sign convention

Requirements : n equal panels

$$\vec{A}_T + \vec{A}_B + \vec{B}_T + \vec{B}_B = 0$$

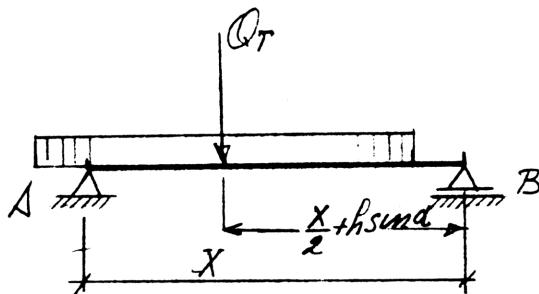
Input : Dimensions : Coordinates X and Y (m)Number of panels n Theoretical height h (m)

Loads : Uniformly distributed loads :

$$U.L.TOP = q_T \quad \text{and} \quad U.L.BOT. = q_B \quad (\text{kN/m})$$

Longitudinal loads : \vec{A}_B ; \vec{A}_T ; \vec{B}_T (kN)

<u>Output</u> : Length :	L (m)	Total load :	Q_T ; Q_B (kN)
Slope angle :	α ° (°)	Local load :	P_T ; P_B (kN)
Node distance :	a (m)	Support reaction : A ; B (kN)	
Diagonal length :	l (m)	Member loads :	T_i ; B_i ; D_i ; S_i (kN)



$$A = \frac{Q_T}{X} \left(-\frac{X}{2} + h \sin \alpha \right) + \frac{Q_B}{2} - \frac{h}{X} (A_T + B_T)$$

$$L = (X^2 + Y^2)^{1/2}$$

$$\alpha = \tan^{-1}(Y/X)$$

$$a = L/n$$

$$l = (a^2 + h^2)^{1/2}$$

$$\gamma = \tan(h/a)$$

$$Q_T = q_T \cdot L$$

$$P_T = Q_T/n$$

$$Q_B = q_B \cdot L$$

$$P_B = Q_B/n$$

$$A = \frac{Q_T + Q_B}{2} - \frac{h}{X} (A_T + B_T - Q_T \sin \alpha)$$

$$B = Q_T + Q_B - A$$

PANEL 1

$$T \begin{cases} -\frac{P_T}{2} \cos \alpha - D_1 \sin \gamma - S_1 = 0 \\ -\frac{P_T}{2} \sin \alpha - D_1 \cos \gamma - T_1 + A_T = 0 \end{cases}$$

$$B \begin{cases} -\frac{P_B}{2} + A \cos \alpha + S_1 = 0 \\ -\frac{P_B}{2} + A \sin \alpha + A_B + B_1 = 0 \end{cases}$$

$$S_1 = \left(\frac{P_B}{2} - A \right) \cos \alpha$$

$$B_1 = \left(\frac{P_B}{2} - A \right) \sin \alpha - A_B$$

$$D_1 = -\frac{1}{\sin \alpha} \left(\frac{P_T}{2} \cos \alpha + S_1 \right) < 0 \rightarrow GTI$$

$$T_1 = \frac{P_T}{2} \sin \alpha - D_1 \cos \gamma - A_T$$

PANEL 2 : (i - 1)

$$\begin{array}{l} T \left\{ \begin{array}{l} -P_T \cos \alpha - D_n \sin \gamma - S_n = 0 \\ -P_T \sin \alpha - D_n \cos \gamma + T_n - T_{n-1} = 0 \end{array} \right. \\ \\ B \left\{ \begin{array}{l} -P_B \cos \alpha - D_{n-1} \sin \gamma + S_n = 0 \\ -P_B \sin \alpha - D_{n-1} \cos \gamma - B_{n-1} + B_n = 0 \end{array} \right. \end{array} \quad \begin{array}{l} S_n = P_B \cos \alpha - D_{n-1} \sin \gamma \\ B_n = P_B \sin \alpha + D_{n-1} \cos \gamma + B_{n-1} \\ \\ D_n = -\frac{1}{\sin \gamma} (P_T \cos \alpha + S_n) < 0 \rightarrow GToi \\ T_n = P_T \sin \alpha - D_n \cos \gamma + T_{n-1} \end{array}$$

PANEL i

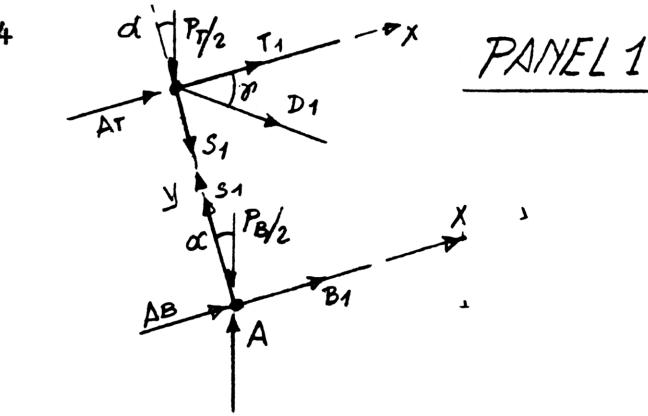
$$\begin{array}{l} T \left\{ \begin{array}{l} -P_T \cos \alpha - S_i = 0 \\ -P_T \sin \alpha - T_{i-1} + T_i = 0 \end{array} \right. \\ \\ B \left\{ \begin{array}{l} -P_B \cos \alpha + (D_{i-1} + D_i) \sin \gamma + S_i = 0 \\ -P_B \sin \alpha - (D_{i-1} - D_i) \cos \gamma - B_{i-1} + B_i = 0 \end{array} \right. \end{array} \quad \begin{array}{l} S_i = -P_T \cos \alpha \\ T_i = P_T \sin \alpha + T_{i-1} \\ \\ D_i = \frac{1}{\sin \gamma} (P_B \cos \alpha - S_i) - D_{i-1} \\ B_i = P_B \sin \alpha - (D_{i-1} - D_i) \cos \gamma + B_{i-1} \end{array}$$

PANEL i + 1 + n = m

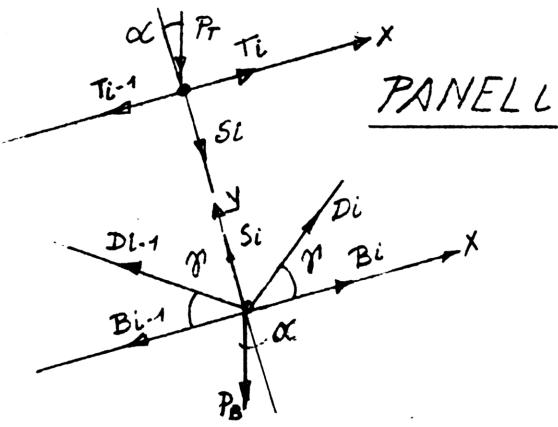
$$\begin{array}{l} T \left\{ \begin{array}{l} -P_T \cos \alpha - S_m - D_{m-1} \sin \gamma = 0 \\ -P_T \sin \alpha - D_{m-1} \cos \gamma - T_{m-1} + T_m = 0 \end{array} \right. \\ \\ B \left\{ \begin{array}{l} -P_B \cos \alpha + S_m + D_m \sin \gamma = 0 \\ -P_B \sin \alpha + D_m \cos \gamma - B_{m-1} + B_m = 0 \end{array} \right. \end{array} \quad \begin{array}{l} S_m = -P_T \cos \alpha - D_{m-1} \sin \gamma \\ B_m = P_B \sin \alpha - D_m \cos \gamma + B_{m-1} \\ \\ T_m = P_T \sin \alpha + D_{m-1} \cos \gamma + T_{m-1} \\ D_m = \frac{1}{\sin \gamma} (P_B \cos \alpha - S_m) \end{array}$$

PANEL n + 1 = l

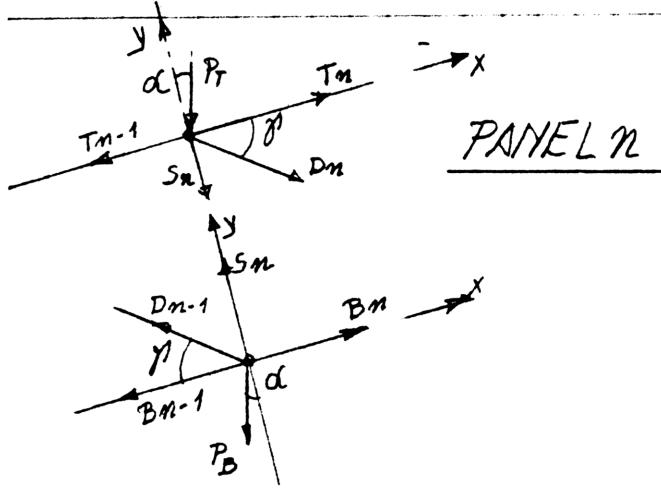
$$T - \frac{P_T}{2} \cos \alpha - S_m - D_m \sin \gamma = 0 \quad S_m = -(\frac{P_T}{2} \cos \alpha + D_m \sin \gamma)$$



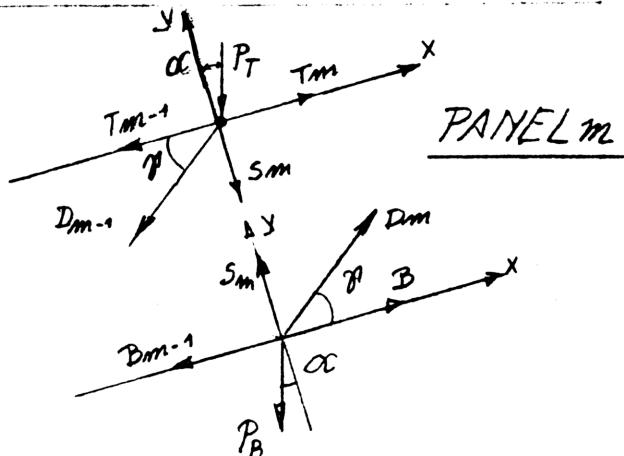
PANEL 1



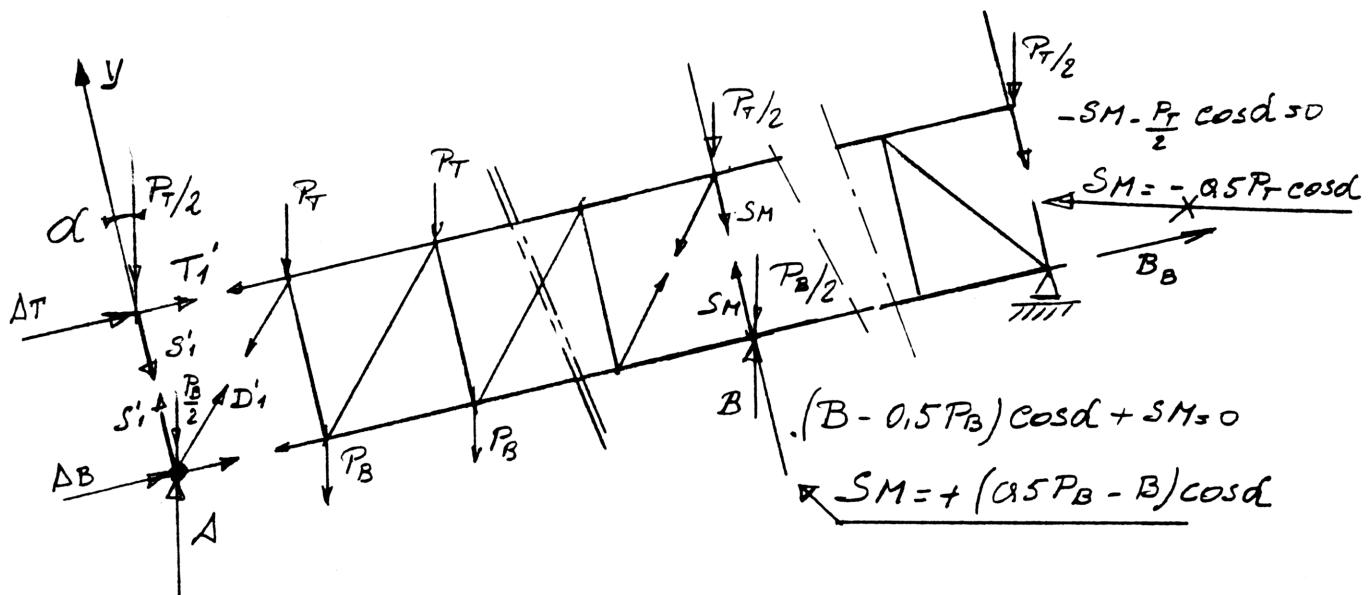
PANEL L



PANEL n



PANEL m



$$T \left\{ \begin{array}{l} -\frac{P_T}{2} \cos \alpha - S_1' = 0 \\ -\frac{P_T}{2} \sin \alpha - A_T + T_1' = 0 \end{array} \right.$$

$$B \left\{ \begin{array}{l} \left(-\frac{P_B}{2} + A\right) \cos \alpha + D_1' \sin \gamma + S_1' \\ \left(-\frac{P_B}{2} + A\right) \sin \alpha + D_1' \cos \gamma + B_1' + A_B = 0 \end{array} \right.$$

$$S_1' = -\frac{P_T}{2} \cos \alpha$$

$$T_1' = \frac{P_T}{2} \sin \alpha - A_T$$

$$D_1' = \left(\left(\frac{P_B}{2} - A\right) \cos \alpha - S_1'\right) \frac{1}{\sin \gamma}$$

$$B_1' = \left(\frac{P_B}{2} - A\right) \sin \alpha - D_1' \cos \gamma - A_B$$

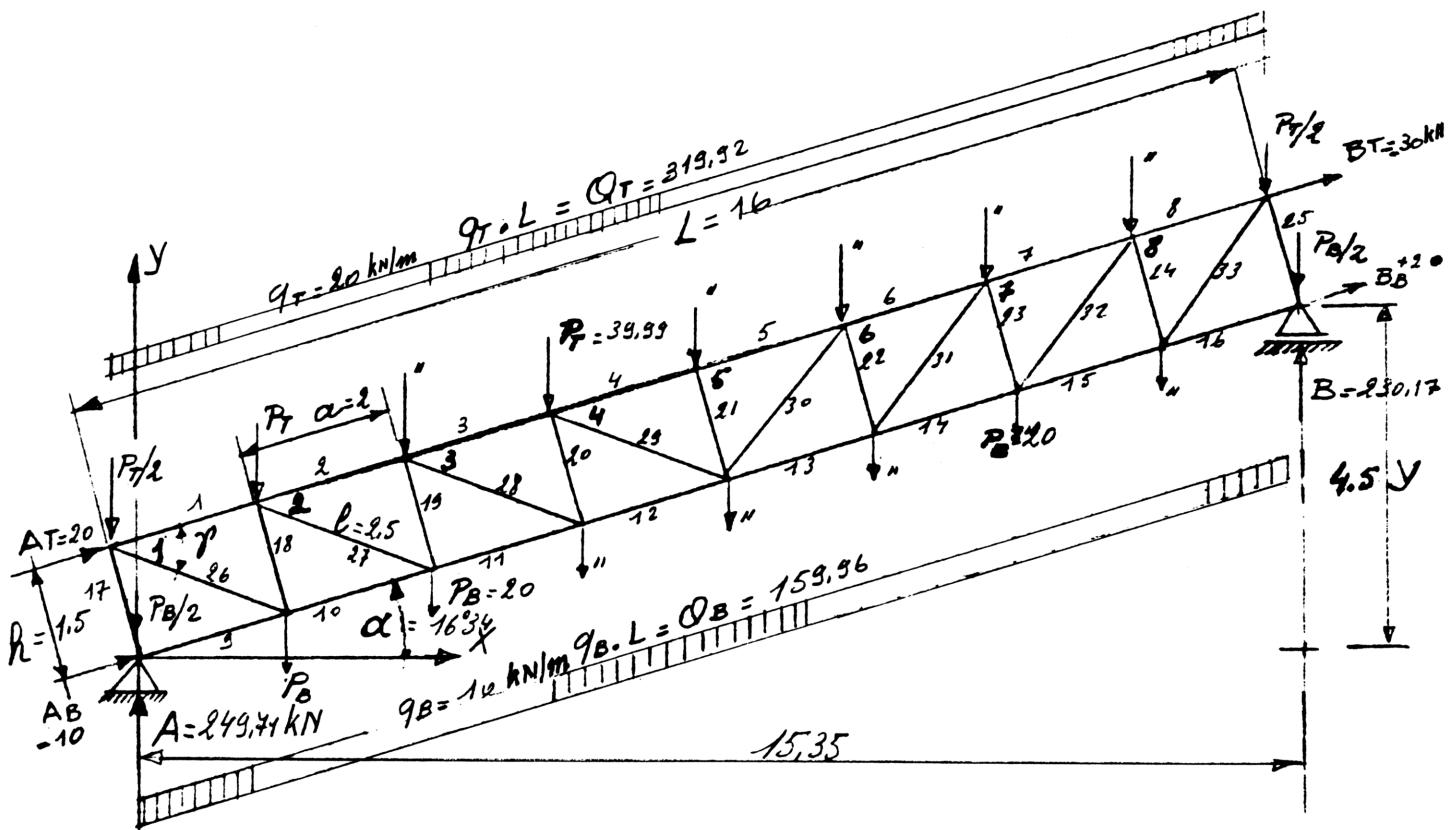
When the indication " DIAG.CH.OF INCL. " is printed before the first series ($i = 1$) this means that the first diagonal was compressed and tipped by the program.

However to have tensioned diagonals in that case the girder should be turned over (see e.g. 3 and 4)

In the case that a girder with equally directed diagonals should be calculated, this characteristic may be useful (see e.g. 3 and 4).

This program can also be applied to girders with different serial section lengths (see e.g. 5).

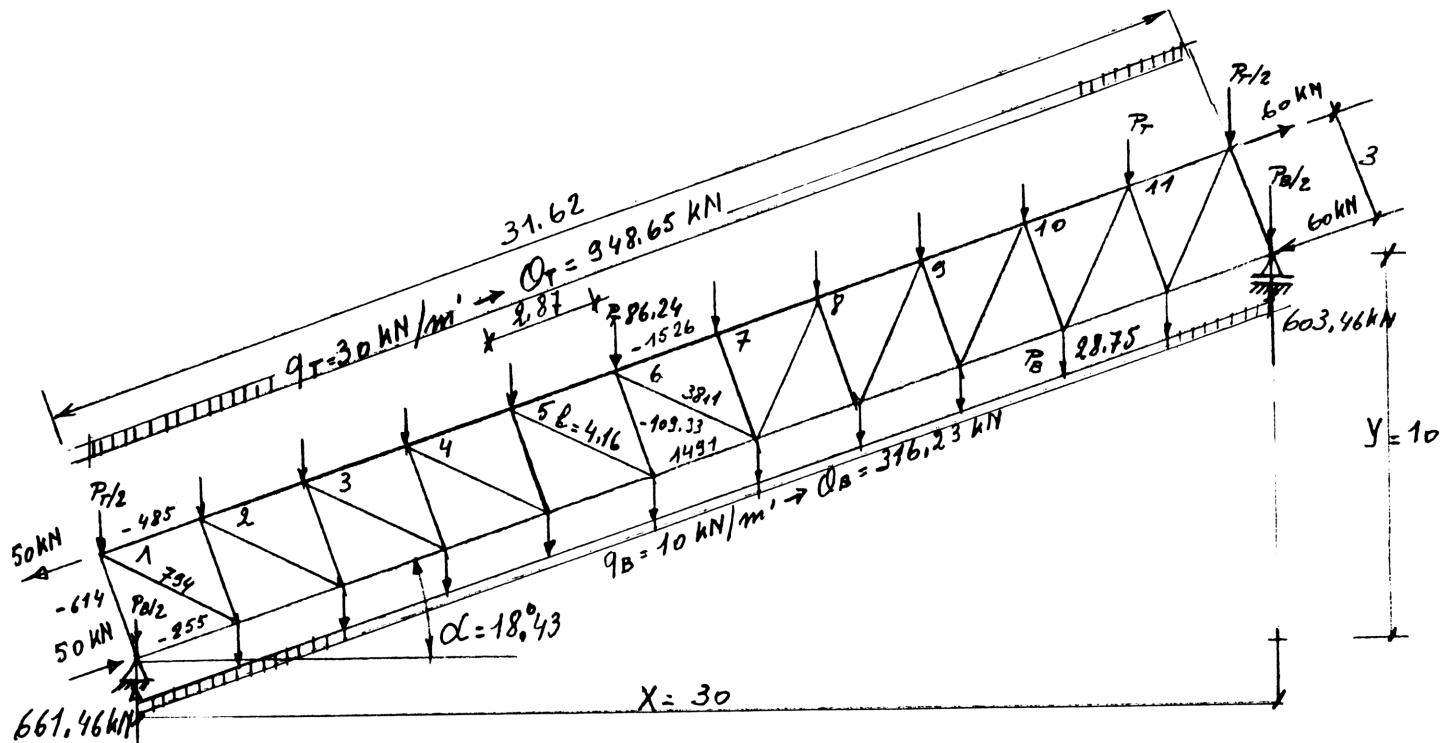
Example 1



$Y = 4.50 \times 2 15.35 Y = 4,$
 $50 X = 15.35$
 $\text{LENGTH} = 16.00$
 $\text{SLOPE} = 16.34$
 $\text{NUB.} = 8.00$
 $\text{TH. HEIGHT} = 1.50$
 $\text{CHORD, L} = 2.00$
 $\text{DIAG, L} = 2.50$
 $\text{U.L.TOP} = 20.00$
 $Q_T = 319.92 \text{ PT} = 39.99$
 $\text{U.L.BOT.} = 10.00$
 $Q_B = 159.96 \text{ PB} = 20.00$
 $AB = 10.00 \text{ AT} = 20.00$
 $BT = 30.00$

SUP. REACT:
 $A = 249.71$
 $B = 230.17$
 N TOPCH. BOTT. CH.
 DIAG. STAN.

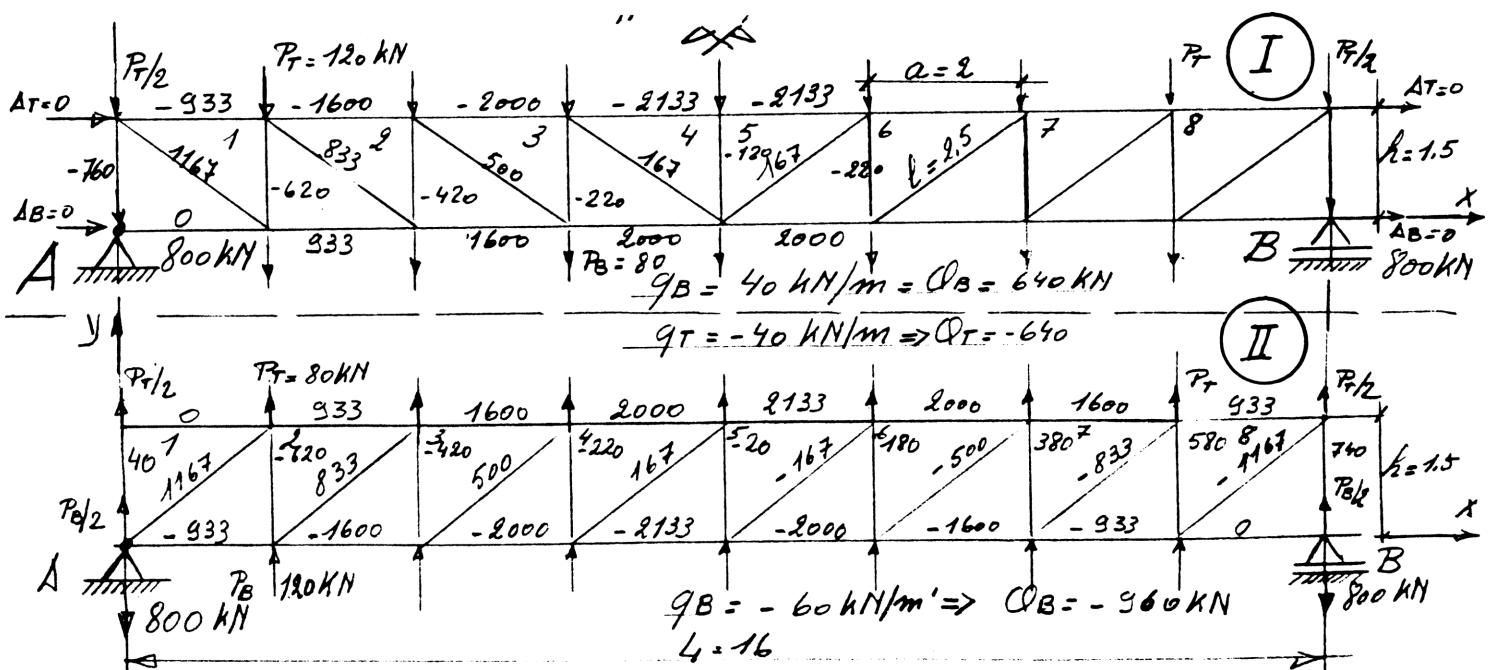
 1, -295.43 -57.44
 351.35 -230.03
 2, -488.51 229.25
 255.43 -191.66
 3, -684.86 439.20
 159.51 -134.10
 4, -644.47 572.42
 63.59 -76.53
 DIAG. CH. OF INCL.
 5, -633.22 603.05
 32.33 -38.38
 6, -596.11 506.07
 128.26 -57.78
 7, -482.26 332.37
 224.18 -115.34
 8, -291.68 81.94
 320.10 -172.90
 SM = -211.28



$Y = 10.00$ $X = 30.00$
 LENGTH = 31.62
 SLOPE = 18.43
 NUB. = 11.00
 TH. HEIGHT = 3.00
 CHORD, L = 2.87
 DIAG. L = 4.16
 U.L.TOP = 30.00
 QT = 948.68 PT = 86.24
 U.L.BOT. = 10.00
 QB = 316.23 PB = 28.75
 AB = 50.00 AT = -50.00
 BT = 60.00
 SUP. REACT:
 A = 661.46
 B = 603.46

N TOPCH. BOTT. CH.	DIAG. STAN.
1, -485.42 -254.63	793.57 -613.88
2, -902.66 303.52	642.48 -545.69
3, -1.215.37 757.13	491.38 -436.60
4, -1.423.53 1.106.20	340.29 -327.51
5, -1.527.16 1.350.73	189.20 -218.42
6, -1.526.25 1.490.72	38.10 -109.33
DIAG. CH. OF INCL.	
7, -1.498.98 1.448.00	112.99 -81.82
8, -1.393.53 1.274.38	264.08 -163.40
9, -1.183.55 996.22	415.17 -272.49
10, -869.02 613.52	566.27 -381.58
11, -449.96 126.28	717.36 -490.67
SM = -558.85	

Example 3



(I)

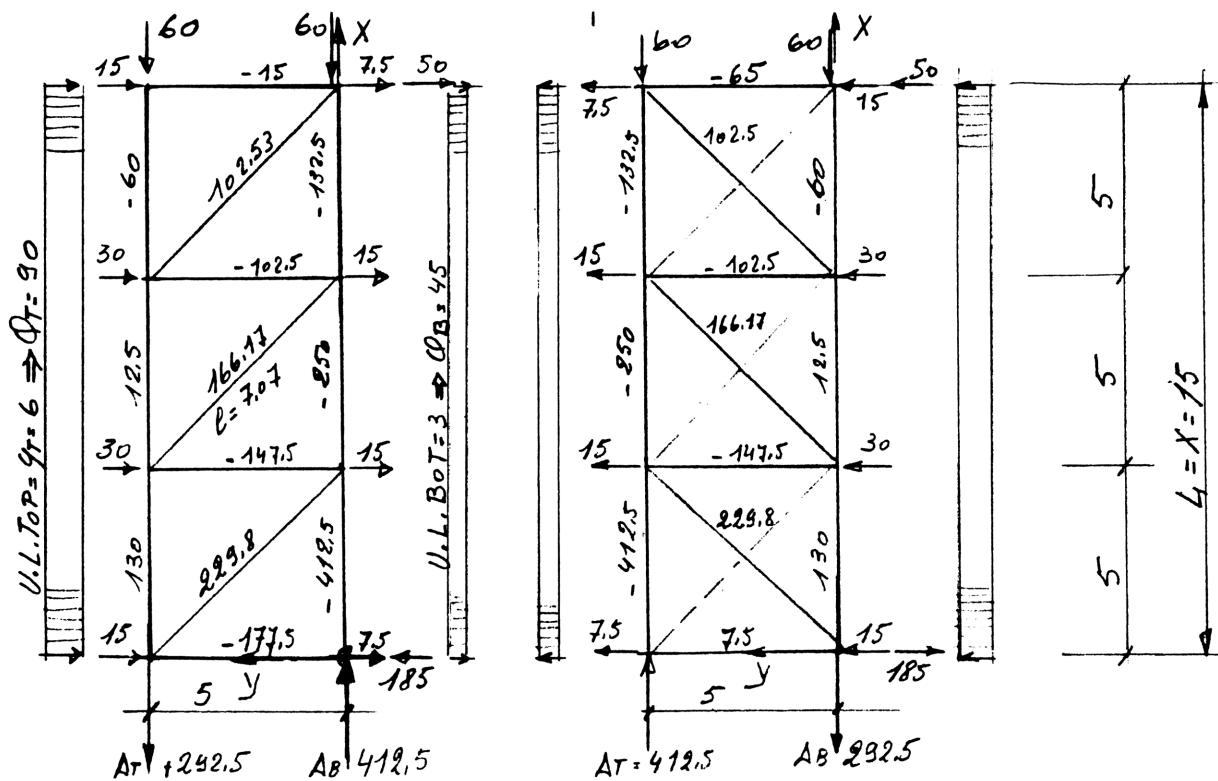
$Y ? 0,00 X ? 16,00$
 LENGTH = 16,00
 SLOPE = 0,00
 NUB. ? 8,00
 TH. HEIGHT ? 1,50
 CHORD. L = 2,00
 DIAG. L = 2,50
 U.L.TOP ? 60,00
 $QT = 960,00 PT = 120,00$
 U.L.BOT. ? 40,00
 $QB = 640,00 PB = 80,00$
 $AB ? 0,00 AT ? 0,00$
 $BT ? 0,00$
 SUP. REACT:
 $A = 800,00$
 $B = 800,00$
 N TOPCH. BOTT. CH.
 DIAG. STAN.

1, -933,33 0,00
 1,166,67 -760,00
 2, -1,600,00 933,33
 833,33 -620,00
 3, -2,000,00 1,600,00
 500,00 -420,00
 4, -2,133,33 2,000,00
 166,67 -220,00
 DIAG. CH. OF INCL.
 5, -2,133,33 2,000,00
 166,67 -120,00
 6, -2,000,00 1,600,00
 500,00 -220,00
 7, -1,600,00 933,33
 833,33 -420,00
 8, -933,33 -2,60E-6
 1,166,67 -620,00
 $SM = -760,00$

(II)

$Y ? 0,00 X ? 16,00$
 LENGTH = 16,00
 SLOPE = 0,00
 NUB. ? 8,00
 TH. HEIGHT ? 1,50
 CHORD. L = 2,00
 DIAG. L = 2,50
 U.L.TOP ? 40,00
 $QT = -640,00 PT = -80,00$
 U.L.BOT. ? -60,00
 $QB = -960,00 PB = -120,00$
 $AB ? 0,00 AT ? 0,00$
 $BT ? 0,00$
 SUP. REACT:
 $A = -800,00$
 $B = -800,00$
 N TOPCH. BOTT. CH.
 DIAG. STAN.

DIAG. CH. OF INCL.
 1, 0,00 -933,33
 1,166,67 40,00
 2, 933,33 -1,600,00
 833,33 -620,00
 3, 1,600,00 -2,000,00
 500,00 -420,00
 4, 2,000,00 -2,133,33
 166,67 -220,00
 5, 2,133,33 -2,000,00
 -166,67 -20,00
 6, 2,000,00 -1,600,00
 -500,00 180,00
 7, 1,600,00 -933,33
 -833,33 380,00
 8, 933,33 2,60E-6
 -1,166,67 580,00
 $SM = 740,00$



$$A_B = (90 + 45) \frac{15}{2 \times 5} + 50 \times \frac{15}{5} + 60 = 412.5$$

$$A_T = - - + = -292.5$$

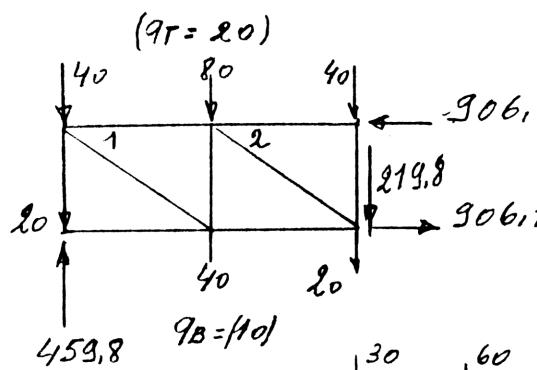
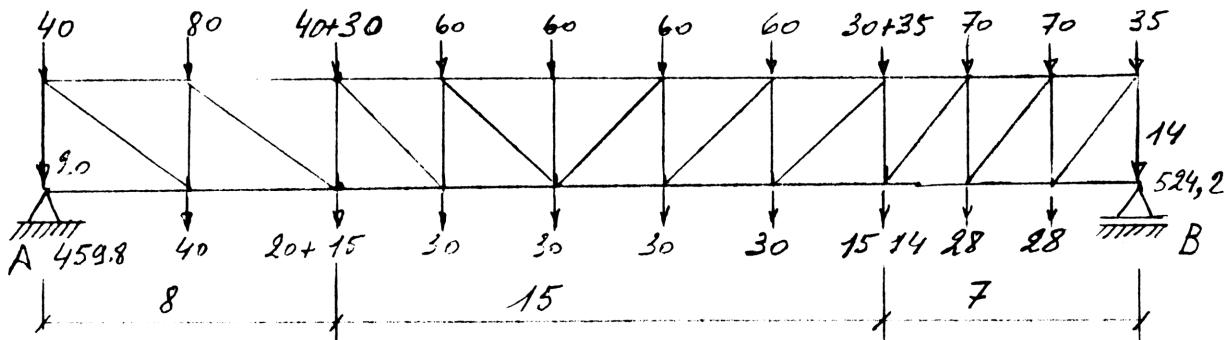
Y ? 0,00 X ? 15,00
 LENGTH = 15,00
 SLOPE = 0,00
 NUB. ? 3,00
 TH. HEIGHT ? 5,00
 CHORD. L = 5,00
 DIAG. L = 7,07
 U.L.TOP ? 6,00
 QT = 90,00 PT = 30,00
 U.L.BOT. ? 3,00
 QB = 45,00 PB = 15,00
 AB ? 412,50 AT ? -292,50
 BT ? -60,00
 SUP. REACT:
 A = 185,00
 B = -50,00
 N TOPCH. BOTT. CH.
 DIAG. STAN.

1, 130,00 -412,50
 229,81 -177,50
 2, 12,50 -250,00
 166,17 -147,50
 3, -60,00 -132,50
 102,53 -102,50
 SM = -15,00

Y ? 0,00 X ? 15,00
 LENGTH = 15,00
 SLOPE = 0,00
 NUB. ? 3,00
 TH. HEIGHT ? 5,00
 CHORD. L = 5,00
 DIAG. L = 7,07
 U.L.TOP ? -3,00
 QT = -45,00 PT = -15,00
 U.L.BOT. ? -6,00
 QB = -90,00 PB = -30,00
 AB ? -292,50 AT ? 412,50
 BT ? -60,00
 SUP. REACT:
 A = -185,00
 B = 50,00
 N TOPCH. BOTT. CH.
 DIAG. STAN.

DIAG. CH. OF INCL.
 1, -412,50 130,00
 229,81 7,50
 2, -250,00 12,50
 166,17 -147,50
 3, -132,50 -60,00
 102,53 -102,50
 SM = -65,00

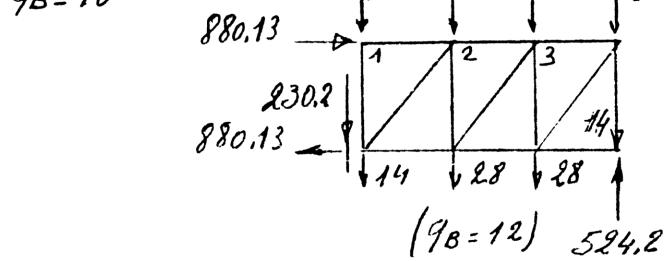
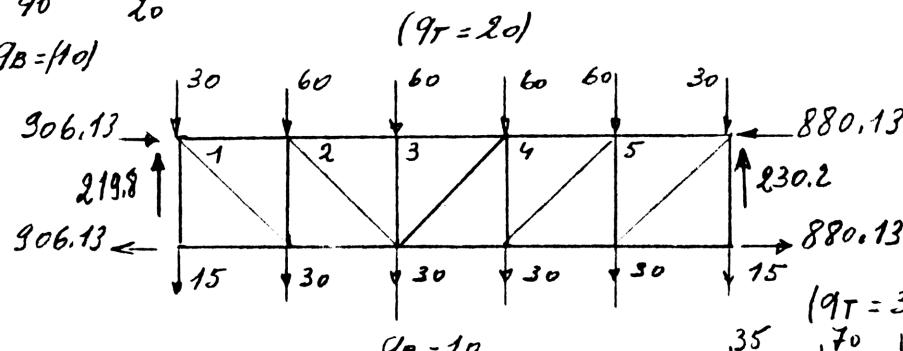
Example 5



$$A = \frac{1}{30} (240 \times 26 + 450 \times 14.5 + 294 \times 3.5) = 459.8$$

$$B = 240 + 450 + 294 - 459.8 = 524.2$$

$$BT = \frac{459.8 \times 8 - 240 \times 4}{3} = -906.13$$



Y ? 0,00 X ? 8,00

LENGTH = 8,00

SLOPE = 0,00

NUB. ? 2,00

TH. HEIGHT ? 3,00

CHORD. L = 4,00

DIAG. L = 5,00

U.L.TOP ? 20,00

QT = 160,00 PT = 80,00

U.L.BOT. ? 10,00

QB = 80,00 PB = 40,00

AB ? 0,00 AT ? 0,00

BT ? -906,13

SUP. REACT:

A = 459,80

B = -219,80

N TOPCH. BOTT. CH.

DIAG. STAN.

1, -533,06 0,00
666,33 -439,80
2, -906,13 533,06
466,33 -359,80
SM = -40,00

Y ? 0,00 X ? 15,00

LENGTH = 15,00

SLOPE = 0,00

NUB. ? 5,00

TH. HEIGHT ? 3,00

CHORD. L = 3,00

DIAG. L = 4,24

U.L.TOP ? 20,00

QT = 300,00 PT = 60,00

U.L.BOT. ? 10,00

QB = 150,00 PB = 30,00

AB ? -906,13 AT ? 906,13

BT ? -880,13

SUP. REACT:

A = 219,80

B = 230,20

N TOPCH. BOTT. CH.

DIAG. STAN.

1, -1080,93 906,13
247,20 -204,80
2, -1165,73 1.080,93
119,93 -144,80

DIAG. CH. OF INCL.

3, -1.165,73 1.160,53

7,35 -60,00

4, -1.160,53 1.065,33

134,63 -65,20

5, -1.065,33 880,13

261,91 -155,20

SM = -215,20

SUP. REACT:

A = -230,20

B = 524,20

N TOPCH. BOTT. CH.

DIAG. STAN.

DIAG. CH. OF INCL.

1, -880,13 662,98

353,71 -35,00

LENGTH = 7,00

477,86 -349,20

SLOPE = 0,00

3, -369,60 2,00E-7

NUB. ? 3,00

602,01 -447,20

TH. HEIGHT ? 3,00

SM = -510,20

CHORD. L = 2,33

DIAG. L = 3,80

U.L.TOP ? 30,00

QT = 210,00 PT = 70,00

U.L.BOT. ? 12,00

QB = 84,00 PB = 28,00

AB ? -880,13 AT ? 880,13

BT ? 0,00

USER INSTRUCTIONS

PROGRAMMABLEAUF
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE

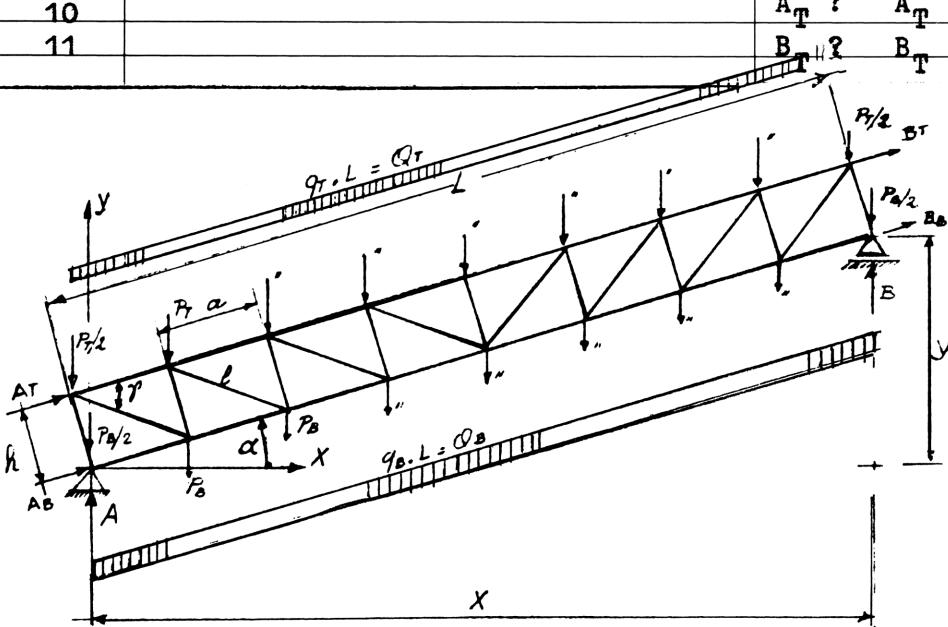
51

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Données Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
1	Load program N-Truss Girder 3 cards		XEQNG size 17	
2	Printer		MAN.mode	
	Beginning execution and data input	DISPLAY		PRINTER
3	Coordinates of B :	Y ? y R/S		
4		X ? x R/S	Y? y X? x m length =L m	
			slope = α deg	
5	Number of panels :	NUB ? n R/S		
6	Theoretical height: Chord length Diagonal length	TH.HEIGHT?h R/S chord.L = a m diag.L = l m	th.height? h m chord.L = a m diag.L = l m	
	Uniformly distributed loads :			
7	- on the top-chord	U.L.TOP ? q _T R/S	U.L.TOP? q _T kNm Q _T = q _T L kN P _T = Q _T / n kN	
8	- on the bottom-chord	U.L.BOT ? q _B R/S	U.L.BOT ? q _B kNm Q _B = q _B L kN P _B = Q _B / n kN	
	Longitudinal loads :			
9		A _B ? A _B R/S		
10		A _T ? A _T R/S	A _B ? A _B ? A _T ? A _T kN	
11		B _T ? B _T R/S	B _T ? B _T kN	
			Sup.react.:	
			A = R _A kN	
			B = R _B kN	
			N TOPCH. BOTT.CH. DIAG. STAN	

1	T ₁	B ₁ D ₁	S ₁	
2	T ₂	B ₂ D ₂	S ₂	

	T _n	B _n D _n	S _n	
			DIAG.CH.OF INCL.	
	T _i	B _i D _i	S _i	
	T _m	B _m D _m	S _m	

	When the diagonal is compressed, it is tipped in the other direction and the machine automatically continues the computation after printing			
	Member load in last stanchion SM			



When the diagonal is compressed, it is tipped in the other direction and the machine automatically continues the computation after printing

DIAG.CH.OF INCL.

i T_i B_i
D_i

m T_m B_m
D_m

SM

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
01 *LBL "NG"	XEQ NG		50 PRBUF		
02 SF 00			51 RCL 01		
03 CLRG			52 *		
04 CLA			53 STO 10		Q _T = q _T L
05 "Y ?"		Y-COORDINATE ?	54 "QT"		
06 XEQ 99			55 XEQ 98		
07 ENTER↑		X-COORDINATE ?	56 RCL 04		
08 " X ?"			57 /		
09 XEQ 99			58 STO 13		
10 STO 00			59 STO 11		
11 PRBUF	L		60 " PT"		P _T = Q _T /m
12 "LENGTH"			61 XEQ 98		
13 R-P			62 PRBUF		
14 STO 01			63 "U.L.BOT		q _{BOT} ?
15 XEQ 98			64 . ?"		
16 PRBUF			65 XEQ 99		
17 RDN			66 STO 09		
18 "SLOPE"	d		67 RCL 01		
19 XEQ 98			68 *		
20 STO 03			69 STO 12		
21 PRBUF			70 "QB "		Q _B = q _B L
22 RCL 01			71 XEQ 98		
23 "NUB. ?"			72 RCL 04		
24 XEQ 99			73 /		
25 STO 04			74 STO 16		
26 PRBUF			75 STO 15		
27 /			76 " PB"		
28 STO 05			77 XEQ 98		
29 "TH. HEI GHT ?"			78 PRBUF		
30 XEQ 99			79 RCL 03		
31 STO 14			80 1		
32 PRBUF			81 P-R		
33 RCL 05			82 STO 03		
34 "CHORD. L"	a = L/n		83 ST* 13		
35 XEQ 98			84 ST* 16		
36 PRBUF			85 RDN		
37 R-P			86 STO 02		
38 " DIAG. L"	b = (a ² +L ²) ^{1/2}		87 ST* 11		
39 XEQ 99			88 ST* 15		
40 PRBUF			89 "AB ?"		A _B ?
41 RDN			90 XEQ 99		
42 SIN			91 STO 06		
43 STO 07			92 RCL 12		
44 LASTX			93 RCL 10		
45 COS			94 +		
46 STO 08			95 STO 01		
47 " U.L.TO P ?"	q _{TOE} ?		96 2		
48 XEQ 99			97 /		
49 STO 09			98 " AT ?"		A _T ?
			99 XEQ 99		
			100 STO 05		
			101 PRBUF		
			102 "BT ?"		B _T ?

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

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Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
103 XEQ 99			152 +		
104 +			153 RCL 07		
105 RCL 10			154 /		
106 RCL 02			155 CHS		
107 *			156 X<0?		
108 -			157 GTO 03		D1<0
109 RCL 14			158 STO 01		
110 *			159 RCL 08		
111 RCL 00			160 *		
112 /			161 CHS		
113 -			162 RCL 11		
114 STO 09			163 2		
115 "SUP. RE ACT:"			164 /		
116 PRA			165 +		
117 SF 12		A	166 RCL 05		
118 "A"			167 -		
119 XEQ 98			168 STO 05		T1
120 PRBUF			169 RCL 15		
121 RCL 01			170 2		
122 -			171 /		
123 CHS			172 RCL 09		
124 "B"		B	173 RCL 02		
125 XEQ 98			174 *		
126 PRBUF			175 -		
127 CF 12			176 RCL 06		
128 "N TOPCH BOTT. "			177 -		
129 "I-CH."			178 STO 06		B1
130 PRA			179 XEQ 97		
131 "DIAG. S TAN."			180 *LBL 00		
132 ACA			181 RCL 16		
133 ADV			182 RCL 01		
134 "----- -----" -----"			183 RCL 07		
135 "I----- -----"			184 *		
136 PRA			185 -		
137 1000			186 STO 00		S1
138 ST/ 04			187 RCL 15		
139 1			188 RCL 01		
140 ST+ 04			189 RCL 08		
141 RCL 16			190 *		
142 2			191 +		
143 /			192 RCL 06		
144 RCL 09			193 +		
145 RCL 03			194 STO 09		Bn
146 *			195 RCL 13		
147 -			196 RCL 00		
148 STO 00		S1	197 +		
149 RCL 13			198 RCL 07		
150 2			199 /		
151 /			200 CHS		
			201 X<0?		Dn<0
			202 GTO 04		
			203 STO 01		
			204 RCL 09		

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
205	STO 06				
206	RCL 11			257 0	
207	RCL 01			258 STO 01	
208	RCL 08				
209	*			259♦LBL 02	
210	-			260 RCL 13	
211	ST+ 05	Tm		261 RCL 01	
212	XEQ 97			262 RCL 07	
213	GTO 00			263 *	
				264 +	
214♦LBL 03				265 CHS	
215	XEQ 01			266 STO 00	Si ; Sm
216	RCL 13			267 RCL 11	
217	-2			268 RCL 01	
218	/			269 RCL 08	
219	STO 00			270 *	
220	RCL 11	Si		271 +	
221	2			272 ST+ 05	Ti : Tm
222	/			273 RCL 16	
223	RCL 05			274 RCL 00	
224	-			275 -	
225	STO 05			276 RCL 07	
226	RCL 16			277 /	
227	2	Ti		278 RCL 02	
228	/			279 -	
229	RCL 09			280 STO 01	
230	RCL 03			281 RCL 15	
231	*			282 RCL 01	
232	-			283 RCL 02	
233	STO 10			284 -	
234	RCL 00			285 RCL 08	
235	-			286 *	
236	RCL 07			287 -	
237	/			288 ST+ 06	Bi ; Bm
238	STO 01	D		289 XEQ 97	
239	RCL 08			290 0	
240	*			291 STO 02	
241	CHS			292 GTO 02	
242	RCL 10				
243	RCL 02			293♦LBL 01	
244	*			294 CF 00	
245	RCL 03			295 "DIAG. C	
246	/			H. OF "	
247	+			296 "FINCL."	
248	RCL 06			297 PRA	
249	-			298 RTN	
250	STO 06	B			
251	XEQ 97			299♦LBL 99	
252	GTO 02			300 ACA	
				301 PROMPT	
253♦LBL 04				302 FIX 2	
254	XEQ 01			303 ACX	
255	RCL 01			304 RTN	
256	STO 02				

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

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Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
305♦LBL 98.			51		
306 ACA					
307 " = "					
308 ACA					
309 ACX					
310 FIX 2			55		
311 RTN					
312♦LBL 97					
313 RCL 04					
314 FIX 0			60		
315 ACX					
316 FIX 2					
317 " "					
318 ARCL 05					
319 ACA			65		
320 " "					
321 ARCL 06					
322 ACA					
323 PRBUF					
324 CLA					
325 ARCL 01			70		
326 ACA					
327 " "					
328 ARCL 00					
329 ACA					
330 ADV			75		
331 ISG 04					
332 RTN					
333 RCL 01					
334 RCL 07					
335 *			80		
336 RCL 13					
337 2					
338 /					
339 FC?C 00					
340 +					
341 CHS			85		
342 "SM"					
343 XEQ 98					
344 ADV					
345 GTO "NG"					
346 .END.			90		
45			95		
50			00		

REGISTERS, STATUS, FLAGS

REGISTERBELEGUNG, FLAGS, BETRIEBSARTEN

REGISTRES, INDICATEURS, MODES OPÉATOIRES

REGISTER, INDICATORS, OPERATOR MODES

REGISTRI, MODI OPERATIVI, FLAGS

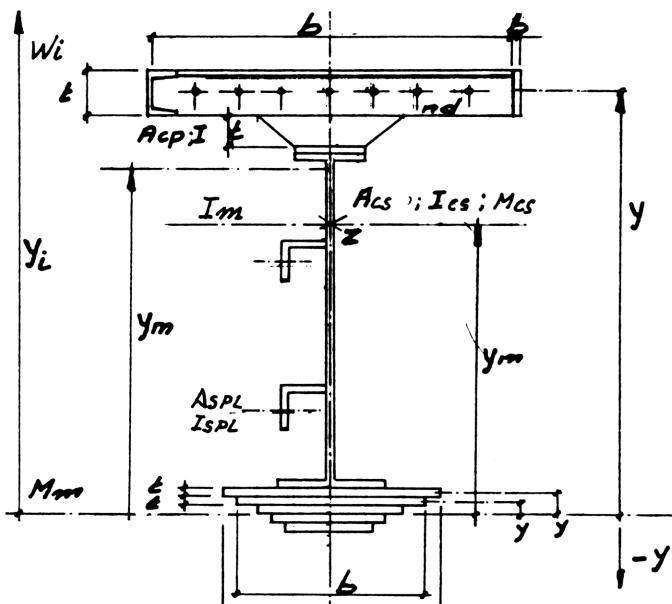
Registers				Status			
Datenspeicher				Betriebsart			
Registres de données				Modes opératoires			
Registri				Modi operativi			
00	X	S		Size <u>17</u>	Total Reg.	<u>95 + 16 = 111</u>	User Mode
L	<u>Q+Q</u> <u>sind</u>	D	X	Eng <input type="checkbox"/>	Fix <input type="checkbox"/>	Sci <input type="checkbox"/>	On <input checked="" type="checkbox"/>
				Deg <input checked="" type="checkbox"/>	Rad <input type="checkbox"/>	Grad <input type="checkbox"/>	Off <input type="checkbox"/>
05	a	A _T A _B	T B	Purpose			
				Bedeutung			
				Signification			
				Scopo			
10	sin γ			00		X	
	cos γ			01			
	q _T	A		02			
	Q _T		X	03			
	P _T	P _T sind		04			
	Q _B			05			
	P _B	P _T cosd		06			
	P _B			07			
15	P _B	P _B sind		08			
	P _B	P _B cos d		09			
				10			
				11	Audio execute		
20				12		X	
				13			
				14			
				15			
				16			
				17			
25				18			
				19			
				20			
				21	Printer Enable		
30				22	Number Input		
				23	Alpha Input		
				24	Range Ignore		
				25	Error Ignore		
				26	Audio Enable		
				27	User Mode		
35				28	Decimal Point		
				29	Digit Grouping		
Assignments							
Tastenbelegung / Assignations / Assegnamenti							
40		Function		Key		Function	
		Funktion		Taste		Funktion	
		Fonction		Touche		Fonction	
		Funzione		Tasto		Funzione	
45							
		Start input and calculation		XEQNG			

CHARACTERISTICS OF COMPOSITE CROSS-SECTIONS**(Requires an additional memory module)**

This program calculates the characteristics of a transformed ($m = E_s/E_c$) composite steel-concrete cross section :

- the area of the cross-section
- the statical moment
- the coordinate of the neutral axis
- the moment of inertia
- the radius of gyration
- the section modulus referred to a given coordinate

After computation of the characteristics the cross-section may be modified by cancelling, substitution or adding members without necessity to recommence the complete input.



$$A_m = \frac{A_c - A_{cs}}{m} + A_{cs} + A_s$$

$$M_m = \frac{M_c + M_{cs}}{c + A_{cs}} + M_{cs} + M_s$$

$$h_m = M_m : A_m$$

$$I_m = h_m^2 A_m - I_{cs} - I_s - \frac{I_c - I_{cs}}{m}$$

$$r_m = (I_m / A_m)^{1/2}$$

$$w_m = I_m / h - h_m < 0 \Rightarrow h_i > h_m$$

indication

Concrete
 CR = Rectangular section
 CT = Triangular section

Steel in concrete
 SCR = Steel reinforcement
 SCP = Steel plates
 CP = Steel profils

Steel
 SPL = Rectangular section
 SPR = Profils

Aerea of cross sections

$$A_c = \sum_{CR} bt + \sum_{CT} bt/2$$

$$A_{cs} = \sum_{SCR} n \pi d^2 / 4 + \sum A_{CP} + \sum_{SCP} bt$$

$$A_s = \sum_{SPL} bt + \sum A_{SPR}$$

Statical moments

$$M_c = \sum_{CR} ybt + \sum_{CT} ybt/2$$

$$M_{cs} = \sum_{SCR} y A_{SCR} + \sum_{SCP} ybt + \sum_{CP} y A_{CP}$$

$$M_s = \sum_{SPL} ybt + \sum_{SPR} y A_{SPR}$$

Moments of inertia

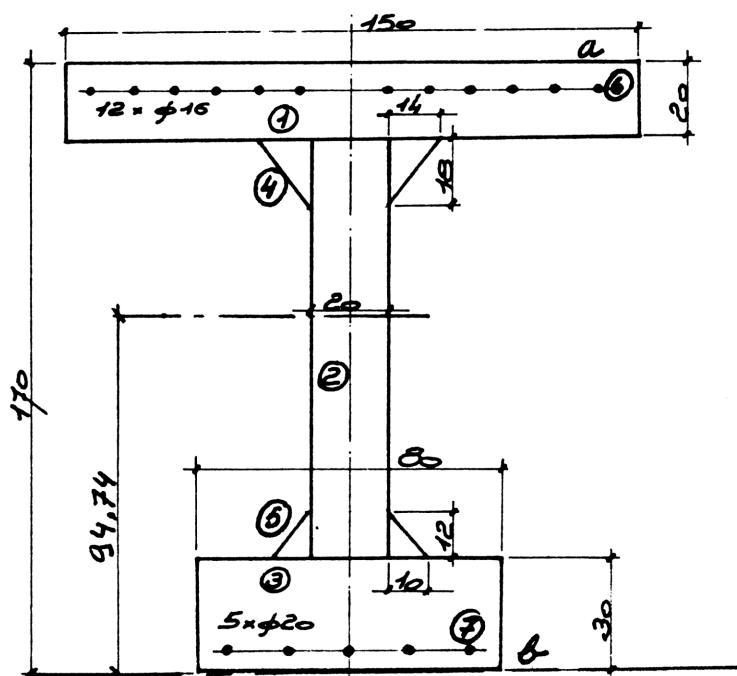
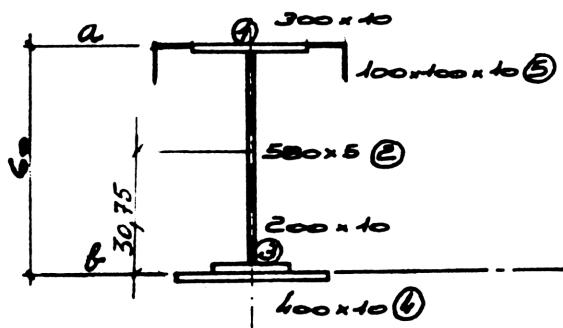
$$I_{cs} = \sum_{SCR} (y^2 \pi d^2 / 4 + \pi d^4 / 64) n + \sum_{CR} (y^2 bt + \frac{bt^3}{12}) +$$

$$\sum_{CP} (h^2 A_{CP} + I_{CP})$$

$$I_s = \sum_{SPL} (y^2 bt + \frac{bt^3}{12}) + \sum_{SPR} (y^2 A_{SP} + I_{SP})$$

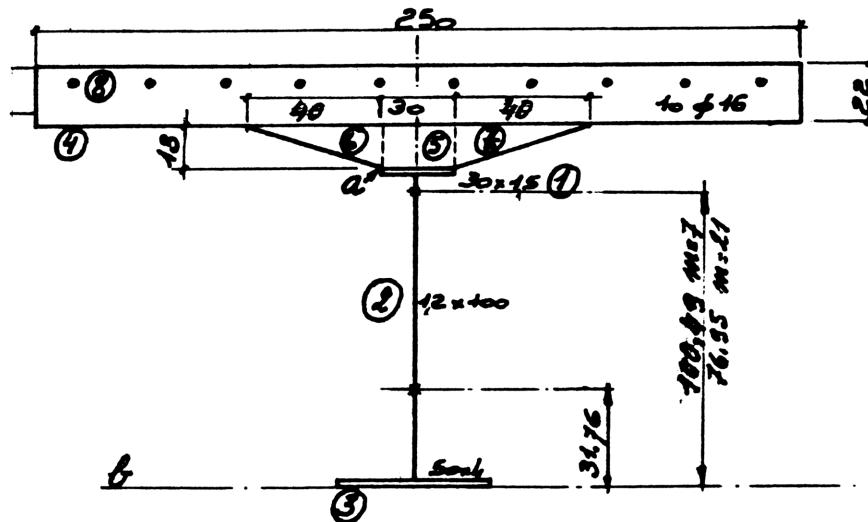
$$I_c = \sum_{CR} (y^2 bt + \frac{bt^3}{12}) + \sum_{CT} (\frac{h^2 bt}{2} + \frac{bt^3}{36})$$

CASE	SPL	CR	SCP	SPR	SCP	CT		SCR
LBL	A	C	F	B	G	D		E



LBL	SECTION	(1)	LBL	SECTION	(2)
J	1	SPL.B ?=30,00 T ?=1,00 Y ?=59,50	J-C	1	CR.B ?=150,00 T ?=20,00 Y ?=160,00
	2	SPL.B ?=0,50 T ?=58,00 Y ?=30,00		2	CR.B ?=20,00 T ?=120,00 Y ?=90,00
	3	SPL.B ?=20,00 T ?=1,00 Y ?=0,50		3	CR.B ?=80,00 T ?=30,00 Y ?=15,00
H		A=79,00 M=2.665,00 Y=33,73 I=50.544,75 R=25,29	D	4	CT.B ?=28,00 T ?=18,00 Y ?=144,00
	a	YX ?=60,00 SX=-1.924,35		5	CT.B ?=20,00 T ?=12,00 Y ?=34,00
	b	YX ?=0,00 SX=1.498,32	E	6	SCR.N ?=12,00 D ?=1,60 Y ?=167,00
A		SPL.B ?=40,00 T ?=1,00 Y ?=-0,50		7	SCR.N ?=5,00 D ?=2,00 Y ?=3,00 MOD. ?=7,00
B	5	SPR.A ?=38,40 Y ?=57,18 I ?=354,00	I		A=1.201,57 M=113.832,35 Y=94,74 I=4.837.100, 26
H		A=157,40 M=4.840,71 Y=30,75 I=117.492,23 R=27,32	a		R=63,45 YX ?=170,00 SX=-64.268,52
	a	YX ?=60,00 SX=-4.017,41	b		YX ?=0,00 SX=51.058,69
	b	YX ?=0,00 SX=3.820,36			

Example 3



LBL	SECTION		LBL	SECTION	
J	1	SPL.B ?=30,00 T ?=1,50 Y ?=104,75 SPL.B ?=1,20 T ?=100,00 Y ?=54,00 SPL.B ?=50,00 T ?=4,00 Y ?=2,00 α =365,00 M =11.593,75 Y =31,76 I =576.500,04 R =39,74 YX ?=105,50 SX ?=-7.818,48 YX ?=0,00 SX =18.149,65 CR.B ?=250,00 T ?=22,00 Y ?=129,50 CR.B ?=30,00 T ?=13,00 Y ?=112,00 CT.B ?=40,00 T ?=13,00 Y ?=114,17 CT.B ?=40,00 T ?=13,00 Y ?=114,17	I		MOD. ?=7,00 α =1.280,71 M =128.064,95 Y =99,99 I =3.015.889,44 R =48,53 YX ?=140,50 SX =-74.457,11 YX ?=105,50 SX =-547.839,66 SCR.N ?=10,00 D ?=1,60 Y ?=137,50 MOD. ?=7,00 α =1.297,95 M =130.434,61 Y =100,49 I =3.039.812,01 R =48,39 YX ?=140,50 SX =-75.981,86 YX ?=105,50 SX =-687.103,42 MOD. ?=21,00 α =689,39 M =53.050,44 Y =76,95 I =2.183.392,49 R =56,28 YX ?=140,50 SX =-34.358,74 YX ?=0,00 SX =28.373,04
H	a		E	8	
c	4		I		
c	5		C		
D	6		a		
	7		I		
			C		
			a		
			I		
			C		
			a		
			I		
			C		
			b		

USER INSTRUCTIONS
PROGRAMMABLELAUF
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE

61

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Données Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
	Properties of composite sections 2 cards	DISPLAY		PRINTER and DISPLAY
1	Enter program		size 14	
2	Printer : used at option		MAN.mode	
3	For beginning the execution or a new data input of another section	push	J or XEQ CS	CLRG
	STEEL SECTIONS			
4	PLATES		<u>A</u>	
5	Input : Width	SPL.B ? b	R/S	SPL.R? = b
6	Input : Thickness	T ? t	R/S	T? = t
7	Input : Y-coordinate of the centroid	Y ? y	R/S	Y? = y
8	For next case Then go to step 5	SPL.B ?		
9	PROFILES		<u>B</u>	
10	Input: area of the cross section	SPR.A ? A _s	R/S	SPR.A? = A _s
11	Input: y-coordinate of the centroid	Y ? y	R/S	Y? = y
12	Input: the moment of inertia	I ? I _s	R/S	I? = I _s
13	For next case SPR Then go to step 10	SPR.A?		
	CONCRETE			
14	RECTANGULAR SECTION		<u>C</u>	
15	Input : Width	CR.B ? b	R/S	CR.B? = b
16	Input : Thickness	T ? t	R/S	T? = t
17	Input: Y-coordinate of the centroid	Y ? y	R/S	Y? = y
18	For next case CR Then go to step 15	CR.B ?		
19	TRIANGULAR SECTION		<u>D</u>	
20	Input: the side of triangular section	CT.B ? b	R/S	CT.B? = b
21	Input: the height	T ? t	R/S	T? = t
22	Input: the Y-coordinate of the centroid	Y ? y	R/S	Y? = y
23	For next case CT Then go to step 20	CT.B ?		
	STEEL IN CONCRETE			
24	STEEL REINFORCEMENT		<u>E</u>	
25	Input: the number of bars	SCR.N ? n	R/S	SCR.N? = n
26	Input: the diameter of the bars	D ? d	R/S	D? = d
27	Input: the coordinate of the centroid	Y ? y	R/S	Y? = y
28	For next case SCR. Then go to step	SCR.N?		
25	STEEL PLATES		<u>F</u>	
26	Input : Width	SCP.B ? b	R/S	SCP.B? = b
27	Input : Thickness	T ? t	R/S	T? = t
28	Input: Y-coordinate of the centroid	Y ? y	R/S	Y? = y
29	For next case SCP. Then go to step 26	SCP.B?		

USER INSTRUCTIONS

**PROGRAMMABLE AUF
INSTRUCTIONS D'EMPLOI
NORME OPERATIVE**

Step Schritt Pas Passo	Instructions Operation Instructions Istruzioni	Variables Dateneingabe Donnees Dati	Function(s) Taste(n) Touche(s) Tasti	Result Resultat Résultat Risultato
30	STEEL PROFILES		G	
31	Input: the cross section	SCP.A ? A	R/S	SCP.A? = A
32	Input: the Y-coordinate of the centroid Y ? y ^c		R/S	Y? = y ^c
33	Input: the moment of inertia I ? I ^c		R/S	I? = I ^c
34	For next case SCP. Then go to step SCP.A ?			
35	RESULTS STEEL SECTION		H	
	Aerea of cross-section			A = A _s
	Statical moment			M = M _s
	Y-coordinate of the neutral axis			Y = y
	Moment of inertia			I = I _s
	Radius of gyration			R = \sqrt{s}
36	Input: y-coordinate YX ? y		R/S	YX? = y
	Output: section modulus of the steel section referred to the given y-coordinate			SX = W _s
37	For a new y-coordinate go to step 36			
38	RESULTS COMPOSITE SECTION		I	
39	Input: modular ratio = E_S/E_C	MOD ? m	R/S	MOD? = m
	Output:			
	Aerea of transformed composite cross section			A = A _{cs}
	Statical moment " " " "			M = M _{cs}
	Y-coordinate of the neutral axis " "			Y = Y _{cs}
	Moment of inertia			I = I _{cs}
	Radius of gyration			R = $\sqrt{I_{cs}}$
40	Input: Y-coordinate YX ? y		R/S	YX? = y
	Output: the section modulus of the transformed composite cross section			SX = W _{cs}
41	For a new y-coordinate go to step 40 YX ?			
42	For cancelling, substitution or adding new sections			
	SPL go to step 4		A	
	SPR " " " 9		B	
	CR " " " 14		C	
	CT " " " 19		D	
	SCR " " " 24		E	
	SCP.B " " " 25		F	
	SCP.A " " " 30		G	
43	For each new case go to step 3		J	CLRG

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

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Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
01+LBL "CS"	XEQ CS OR J		51 2		
02 CLRG	STEEL		52 /		
03+LBL A	A STEEL PLATE		53 ST+ 06		
04 "SPL"	SPL.B? B		54 GTO D		
05 XEQ 07			55+LBL E		STEEL IN CONCRETE
06 RCL 10			56 "SCR.N"		E STEEL REINF.
07 ST+ 01			57 XEQ 02		SCR.N? n
08 RCL 00			58 "D"		D? d
09 ST+ 02			59 XEQ 02		
10 RCL 13			60 X12		
11 ST+ 03			61 STO 10		
12 GTO A			62 *		
13+LBL B	B PROFILES		63 PI		
14 "SPR"	SPR.A? As		64 *		
15 XEQ 08			65 4		
16 RCL 10			66 /		
17 ST+ 01			67 STO 11		
18 RCL 12			68 ST+ 07		
19 ST+ 02			69 "Y"		
20 RCL 11			70 XEQ 02		
21 ST+ 03			71 STO 12		
22 GTO B	CONCRETE		72 *		
23+LBL C	C RECTANGULAR		73 ST+ 08		
24 "CR"	CR.B? B		74 RCL 12		
25 XEQ 07			75 *		
26 RCL 10			76 RCL 11		
27 ST+ 04			77 RCL 10		
28 RCL 00			78 *		
29 ST+ 05			79 16		
30 RCL 13			80 /		
31 ST+ 06			81 +		
32 GTO C			82 ST+ 09		
33+LBL D	D TRIANGULAR		83 GTO E		
34 "CT"	CT.B? B		84+LBL F		F STEEL PLATES
35 XEQ 07			85 "SCP"		SCP.B? B
36 RCL 10			86 XEQ 07		
37 2			87 RCL 10		
38 /			88 ST+ 07		
39 ST+ 04			89 RCL 00		
40 RCL 00			90 ST+ 08		
41 2			91 RCL 13		
42 /			92 ST+ 09		
43 ST+ 05			93 GTO F		
44 RCL 11			94+LBL G		G STEEL PROFILES
45 3			95 "SCP"		SCP.A? AcS
46 /			96 XEQ 08		
47 ST+ 06			97 RCL 10		
48 RCL 13			98 ST+ 07		
49 RCL 11			99 RCL 12		
50 -			100 ST+ 08		
			101 RCL 11		

PROGRAM LISTING

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
102 ST+ 09			152 RCL 04		
103 GTO G			153 RCL 07		
104+LBL 07		...B? = b	154 -		
105 "F.B"			155 RCL 10		
106 XEQ 02			156 /		
107 "T"		T? = t	157 RCL 07		
108 XEQ 02			158 +		
109 STO 11			159 RCL 01		
110 *			160 +		
111 STO 10			161 "A"		A = A COMPOSITE
112 "Y"		y? = y	162 XEQ 00		
113 XEQ 02			163 STO 13		
114 STO 13			164 RCL 05		
115 *			165 RCL 08		
116 STO 00			166 -		
117 RCL 13			167 RCL 10		
118 *			168 /		
119 STO 13			169 RCL 08		
120 RCL 10			170 +		
121 RCL 11			171 RCL 02		
122 X↑2			172 +		
123 *			173 "M"		M = M COMPOSITE
124 12			174 XEQ 00		
125 /			175 X<>Y		
126 STO 11			176 /		
127 ST+ 13			177 "Y"		
128 RTN			178 XEQ 00		
129+LBL 08		...A? = A	179 STO 12		
130 "F.A"			180 X↑2		
131 XEQ 02			181 RCL 13		
132 STO 10			182 *		
133 "Y"			183 RCL 09		
134 XEQ 02			184 -		
135 STO 11			185 RCL 03		
136 *			186 -		
137 STO 12			187 RCL 06		
138 RCL 11			188 RCL 09		
139 *			189 -		
140 "I"		I? = I	190 RCL 10		
141 XEQ 02			191 /		
142 +			192 -		
143 STO 11			193 CHS		
144 RTN			194 "I"		I = I COMPOSITE
145+LBL I		I RES. COMPOSITE	195 XEQ 00		
146 "MOD."		MOD.? = m	196 STO 11		
147 XEQ 02			197 ENTER↑		
148 STO 10			198 ENTER↑		
149+LBL H		H RES. STEEL OR	199 ENTER↑		
150 SF 00			200 RCL 13		
151 SF 12		CONCRETE	201 /		
			202 SQRT		
			203 "R"		R = 2 COMPOSITE
			204 XEQ 00		
			205 CF 12		

PROGRAM LISTING

65

PROGRAMMAUFLISTUNG

LISTAGE DU PROGRAMME

LISTATO DI PROGRAMMA

Line Zeile Ligne Linea	Keystrokes Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti	Line Zeile Ligne Linea	Key pressed Tastenfolge Touches Tasti	Comments Kommentar Commentaires Commenti
~			51		
206♦LBL 03					
207 CLX					
208 RCL 12					
209 "YX ?"		yx ? y	55		
210 PROMPT					
211 XEQ 00					
212 SF 00					
213 -					
214 /					
215 "SX"		SX = S	60		
216 XEQ 00					
217 GTO 03					
218♦LBL 02					
219 CF 00			65		
220 "F ?"					
221 PROMPT					
222♦LBL 00					
223 FIX 2					
224 "F ="			70		
225 ARCL X					
226 AVIEW					
227 FS? 00					
228 PSE					
229 RTN			75		
230 .END.					
30			80		
35			85		
40			90		
45			95		
50			00		

REGISTERS, STATUS, FLAGS
REGISTERBELEGUNG, FLAGS, BETRIEBSARTEN
REGISTRES, INDICATEURS, MODES OPÉRATOIRES
REGISTRI, MODI OPERATIVI, FLAGS

Registers			Status				
Datenspeicher			Betriebsart				
Registres de données			Modes opératoires				
Registri			Modi operativi				
00	tby $\sum tb = A$ $\sum tby = M$ $\sum t^3 b/12 + tby^2$ A_c	ΣA $\Sigma Ay = M$ ΣI	Size 14	Total Reg. 78	User Mode		
05	M_c I_c A_{cs} M_{cs} I_{cs} tb $I : t^3 b/12$ Ay $t^3 b/12 + tby^2 = I_s$	$n\pi d^2/4$ y I_e d^2 t y	Eng <input type="checkbox"/> Fix <input checked="" type="checkbox"/> Sci <input type="checkbox"/>	Deg <input type="checkbox"/> Rad <input type="checkbox"/> Grad <input type="checkbox"/>	On <input checked="" type="checkbox"/> Off <input type="checkbox"/>		
10							
15							
20							
25							
30							
35							
40							
45							
Purpose							
Flags							
SET CLEAR							
00			X	X			
01							
02							
03							
04							
05							
06							
07							
08							
09							
10							
11	Audio execute		X	X			
12							
13							
14							
15							
16							
17							
18							
19							
20							
21	Printer Enable						
22	Number Input						
23	Alpha Input						
24	Range Ignore						
25	Error Ignore						
26	Audio Enable						
27	User Mode						
28	Decimal Point						
29	Digit Grouping						
Assignments							
Tastenbelegung/Assignations/Assegnamenti							
Function			Key	Function	Key		
Funktion			Taste	Funktion	Taste		
Fonction			Touche	Fonction	Touche		
Funzione			Tasto	Funzione	Tasto		
Steel plates			A	Res. steel or			
Profiles			B	beton	H		
Rect. section			C	Res. composite	I		
Triang. section			D	New section =			
Steel reinf.			E	XEQCS	J		
Steel plates			F				
Profiles			G				

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Circuit Analysis	Securities	Navigation
Financial Decisions	Statistics	Real Estate
Mathematics	Stress Analysis	Thermal and Transport Science
	Games	

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Real Estate	Solar Engineering
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Geometry	Cardiac/Pulmonary
High-Level Math	Chemistry
Test Statistics	Games
Antennas	Optometry I (General)
Chemical Engineering	Optometry II (Contact Lens)
Control Systems	Physics
Electrical Engineering	Surveying
Fluid Dynamics and Hydraulics	

* Some books require additional memory modules to accomodate all programs.

STRUCTURAL ANALYSIS

BEAM CALCULATION
CONTINUOUS BEAM
MAXIMUM MAXIMORUM BENDING MOMENT
N-TRUSS GIRDER
CHARACTERISTICS OF COMPOSITE CROSS-SECTIONS

