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POSITION DETERMINATION WITH
LORAN-C TRIPLETS AND THE HEWLETT-PACKARD
HP-67/97 PROGRAMMABLE CALCULATORS

by

R. H. Shudde

March 1980

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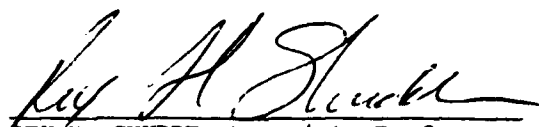
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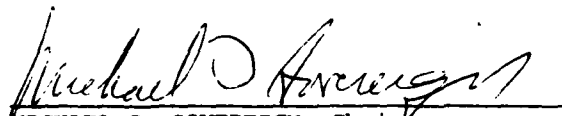
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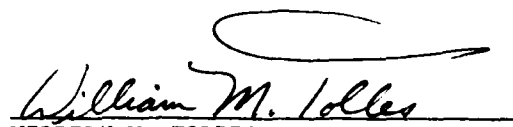
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March 1980

The programs in this report
are for use within the Navy,
and they are presented with-
out representation or warranty
of any kind.

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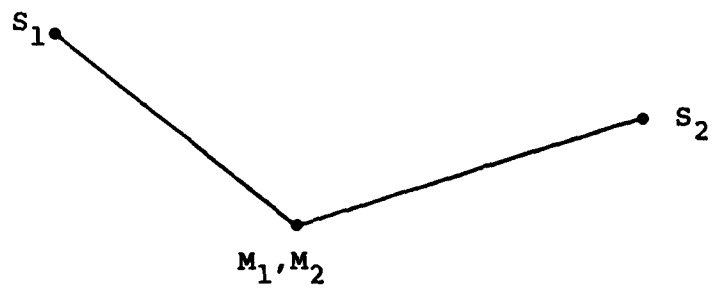
ABSTRACT

This report presents an algorithm and HP-67/97 programs for position determination with Loran-C chains. Operational data cards are prepared in advance for Loran-C triplets. Position determination is performed using a single program card and an appropriate operational data card.

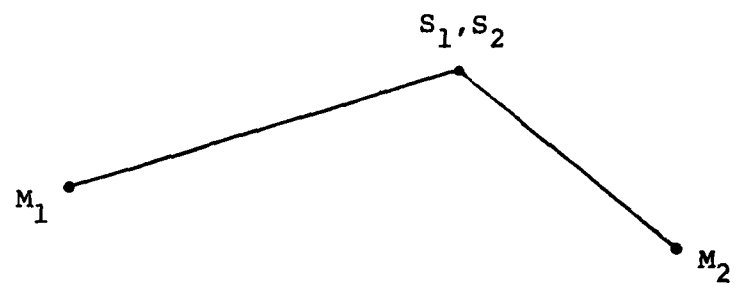
A. Introduction

The Loran system is a radio aid to navigation which utilizes the principle of hyperbolic fixing. The locus of points for which the difference in arrival time of synchronized signals from a pair of transmitters is constant determines a hyperbolic line of positions (LOP). The intersection of two hyperbolic lines of position from two pairs of transmitters determines position or a hyperbolic fix. That two pairs of stations are required for a fix does not necessarily mean that there are four separate stations, for one station of one pair may be colocated with one station of the other pair forming a *Loran triplet* (Figure 1). Triplets may be joined "end-to-end" by station collocation to form a *Loran chain* (Figure 2). Loran chains are common on both the East and West Coasts of the North American continent.

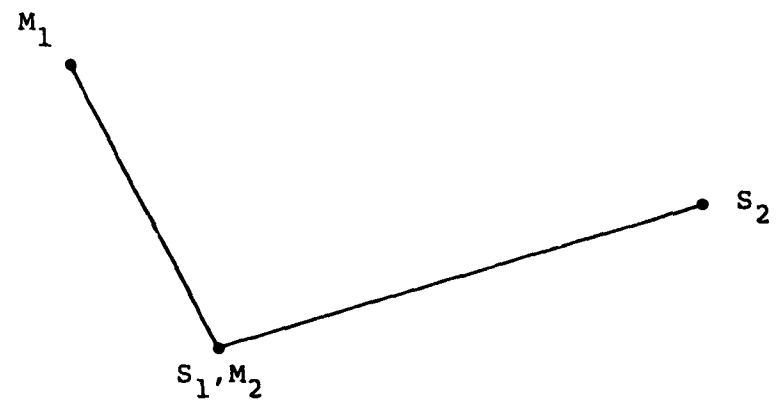
The early "Standard Loran" or Loran-A" operating at a frequency just below 2MHz is still in use in the Pacific area. The present day "Loran-C" operates at 100-kHz and is in use in both the Atlantic and Pacific Areas. The computational algorithm and programs described herein can be used for position determination with Loran-C triplets. Further information on the history, development and operation of the Loran systems may be found in References 1 and 2.



(a) Colocated Master Stations



(b) Colocated Slave Stations



(c) Colocated Master and Slave

Figure 1. Loran Triplets.

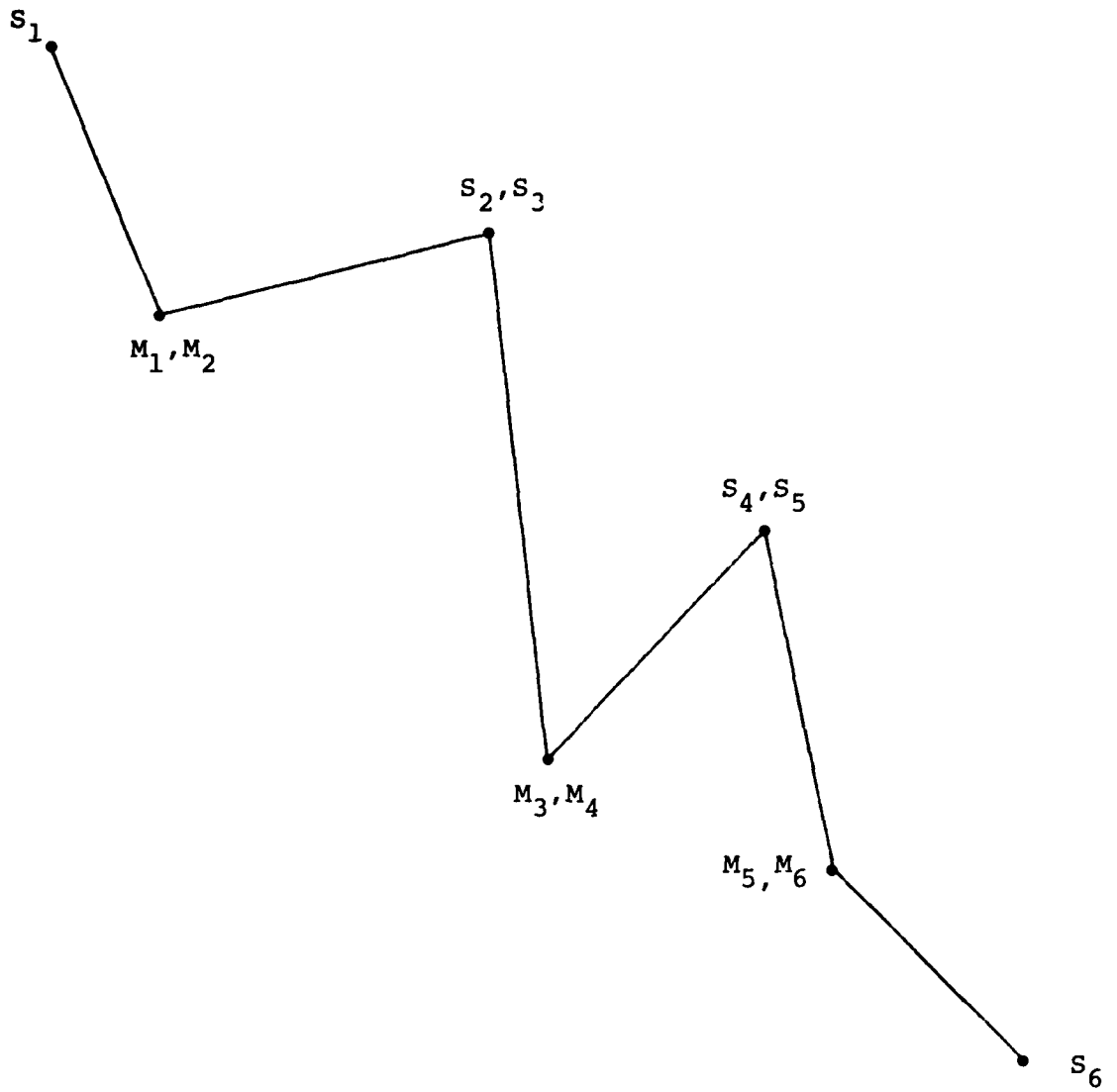


Figure 2. Loran Chain of Five Loran Triplets.

B. Program Description

One program card and one operational data card (described below) are all that is required for on-location position determination from Loran triplet time-difference measurements. Two program cards are required to prepare operational data cards; these operational data cards should be prepared and validated prior to on-location navigational use. Thus although three program cards are described only one program card is required for navigation; two program cards are used to prepare operational data cards during or prior to mission planning. The function of each program card and its intended use follows.

Program Card 1. This program card is used to prepare *master data cards*. A master data card requires the following information for a master(M) station/slave(S) station pair:

1. A M/S pair identification number.
2. The quantity Δt which is the sum of the coding delay plus the one way base line time in microseconds.
3. The latitude and longitude of the master station.
4. The latitude and longitude of the slave station.

Some preprocessing of these data is performed before the master data card is generated. The data generated require only one side of an HP-67/97 magnetic card for each M/S pair, thus a second M/S pair may be placed on side 2 of the card (thus conserving cards) if desired. It is envisaged that a master data card will be prepared in advance for each M/S pair that might be received within an area of operation.

Program Card 2. This program card is used to prepare an *operational data card* for every Loran triplet within an operational area. Each operational data card contains data merged from the master data cards which contain M/S pair information for each pair of the triplet. These merged data are validity checked, colocation of master or slave determined and encoded.

The only inputs required for this program are the two master data cards that comprise the Loran triplet. It is possible to prepare and store operational data cards rather than master data cards. This may be desirable if there is no scarcity of cards and storage space, however the number of possible Loran triplets is considerably larger than the number of M/S pairs.

Program Card 3. This program card is used in conjunction with an operational data card for position determination. Required input is the indicated time difference T for each M/S pair of the triplet. Output is the computed latitude and longitude of the fix. Note: Every Loran fix has two possible solutions. The unwanted solution can almost always be rejected by inspection, however, if the stations of the Loran triplet are nearly aligned then either solution may be valid even though only one solution should be consistent with the flight plan.

C. HP-67/97 Calculator Programs

1. User Instructions

CARD 1

Step	Instructions	Input Data/Units	Keys	Output Data/Units
1.	Read in program card (both sides)			
2.	Input a unique ID number for the Loran pair*	ID	f a	ID
3.	Input the coding delay Δt	Δt	f c	Δt
4a.	Input the master station latitude	ϕ_M	↑	---
b.	and longitude (CHS for West)**	λ_M	A	---
5a.	Input the slave station latitude	ϕ_S	↑	---
b.	and longitude (CHS for West)	λ_S	C	---
6a.	Run	None	E	crd
b.	Pass a blank data card through the card reader.			

* Note: Loran pairs are coded on the navigation maps using designators such as 9930X, 9930Y, 9930Z and 9930W. It is suggested that the ID's for these pairs be coded as 9930.1, 9930.2, 9930.3 and 9930.4, respectively. However, any consistent scheme is acceptable.

** The format for position data input is of the form: +DDD.MMSSFF, where
 DDD denotes degrees
 MMM denotes minutes
 SS denotes seconds
 FF denotes hundredths of a second.

The minus sign (-) denotes Southern latitudes or Western longitudes.

CARD 2

Step	Instructions	Input Data/Units	Keys	Output Data/Units
1.	Read in program card 2			
2a.	Start	---	E	9.00
b.	9.00 will flash in the display. Insert a master data card containing the first pair of a Loran triplet.			
c.	9.00 will flash in the display once more. Insert a master data card containing the second pair of the Loran triplet.			9.00
d.	If the data form a proper triplet, "crd" will appear in the display.			crd
e.	Pass both sides of a blank card thru the card reader to produce the operational data card for the Loran triplet.			
<p>Should "error" appear in the display, then the two master data cards do not compare to form a Loran triplet. Both the latitude and longitude of the colocated stations must be identical on both master data cards in order to successfully produce an operational data card.</p>				
<p>Label the A key position with the identification number of the <u>first</u> Loran pair (the pair inserted in Step 2b) and label the B key position with the identification number of the <u>second</u> Loran pair (from Step 2c).</p>				

CARD 3

Step	Instructions	Input Data/Units	Keys	Output Data/Units
1.	Read in both sides of the program card 3.			
2.	Read both sides of the operational data card for the Loran triplet that you are receiving.			
3a.	Set to compute Solution A.		f a	---
b.	Set to compute Solution B.		f b	---
4.	Input the observed time delay from the first Loran pair.	T	A	---
5.	Input the observed time delay from the second Loran pair.	T	B	---
6.	Compute fix Latitude Longitude		E R/S	Latitude Longitude
7.	Repeat from Step 2 with a new operational data card or from Steps 3 or 4 as required.			

2. Sample Problem

CARD 1

Step	Instructions	Input Data/Units	Keys	Output Data/Units
	In this series of examples we will prepare and use data cards for the Loran-C pairs 9930X and 9930Y.			
1.	Read in program card 1 (both sides)			
2.	Input the ID for 9930X	9930.1	f a	9930.10
3.	Input the coding delay Δt for 9930X	36389.66	f c	36389.66
4a.	Input the master station latitude	34.034604	↑	---
b.	and longitude (CHS for West)	-77.544676	A	---
5a.	Input the slave station latitude	46.463218	↑	---
b.	and longitude (CHS for West)	-53.102816	C	---
6a.	Compute	None	E	crd
b.	Pass a blank data card through the card reader. Label the card 9930X MASTER			---
7.	Input the ID for 9930Y	9930.2	f a	9930.2
8.	Input the coding delay Δt for 9930Y	52541.31	f c	52541.31
9a.	Input the master station latitude	34.034604	↑	---
b.	and longitude (CHS for West)	-77.544676	A	---
10a.	Input the slave station latitude	41.151193	↑	---
b.	and longitude (CHS for West)	-69.583909	C	---
11a.	Compute	None	E	crd
b.	Pass a blank data card (or the second side of the card used in Step 6b) through the card reader. Label the side 9930Y MASTER			
12.	These two cards will be used in the next example.			

CARD 2

Step	Instructions	Input Data/Units	Keys	Output Data/Units
1.	Read in program card 2.			
2a.	Start	---	E	9.00
b.	While 9.00 is flashing in the display, insert the MASTER data card for station 9930X into the card reader.			
c.	When 9.00 starts flashing in the display again, insert the MASTER data card for station 9930Y into the card reader.	---		9.00
d.	"Crd" will appear in the display.	---		crd
e.	Pass both sides of a blank card through the card reader. Label this card 9930X/9930Y OPERATIONAL DATA CARD. Then label the A key position 9990X and the B key position 9930Y. This card will be used in the next example.	---		0.00

CARD 3

Step	Instructions	Input Data/Units	Keys	Output Data/Units
	You are receiving 9930X and 9930Y and wish to obtain a fix.			
1.	Read in program card 3 (both sides)			---
2.	Read in the operational data card for the triplet 9930X/9930Y (both sides)			---
3.	Select Solution A.		f a	
4.	The indicated time delay is 49400 μ s from 9930Y. Input the indicated time delay.	49400	B	0.00
5.	The indicated time delay is 28800 μ s from 9930X. Input the indicated time delay.	28800	A	0.00
6.	Solution A: 42°44'57"N Latitude 41°07'32"W Longitude { Solution B: 27°00'07"S Latitude 102°27'12"E Longitude Since you are navigating over the North Atlantic, Solution A is the desired fix. }		E R/S	42.4457 -41.0732
7.	Repeat from Step 2 with a new operational data card or from Steps 3 or 4 as required.			

3. Program Storage Allocations and Program Listings

Card 1.

Registers:

R0: ID	S0: L	RA:
R1: Δt	S1: T	RB:
R2: $2c$	S2: U	RC: θ_m
R3:	S3: V	RD: $\Delta\theta_m$
R4: θ_M	S4: X	RE: $\Delta\lambda$
R5: λ_M	S5: Y	RI: $\Delta\lambda_m$
R6: ξ_{MS}	S6: δ_{1d}	
R7: θ_S	S7: $\Delta\lambda'_m$	
R8: λ_S	S8: d	
R9: ξ_{SM}	S9: f	

Initial Flag Status and Use:

0: OFF, Unused	2: OFF, Unused
1: OFF, Unused	3: OFF, Unused

Display Status:

DSP 4, FIX, DEG.

User Control Keys:

A: $\phi_M \uparrow \lambda_M$	a: Station ID
B:	b:
C: $\phi_S \uparrow \lambda_S$	c: Δt
D:	d:
E: Prepare data card	e:

Card 2.

Registers:

R0: $\pm ID_1$	S0: $\pm ID_2$	RA:
R1: Δt_1	S1: Δt_2	RB:
R2: $2c_1$	S2: $2c_2$	RC:
R3:	S3:	RD:
R4: θ_{A1}	S4: θ_{A2}	RE: $a_p = 21295.87$
R5: λ_{A1}	S5: λ_{A2}	RI: $f = 1/298.26$
R6: ξ_{A1}	S6: ξ_{A2}	
R7: θ_{B1}	S7: θ_{B2}	
R8: λ_{B1}	S8: λ_{B2}	
R9: ξ_{B1}	S9: ξ_{B2}	

Initial Flag Status and Use:

0: OFF, Vertex determination	2: OFF, Validity checking
1: OFF, Unused	3: OFF, Unused

Display Status:

DSP 2, FIX, DEG

User Control Keys:

A:	a:
B:	b:
C:	c:
D:	d:
E: Run	e:

Card 3.

Registers:

R0: ID_1	S0: ID_2	RA: M
R1: Δt_1	S1: Δt_2	RB: u, N
R2: $(2c)_1$	S2: $(2c)_2$	RC: D, d
R3: A_1, c_2, P	S3: A_2	RD: $\Delta\sigma$
R4: $\theta_1 = \theta_F$	S4: θ_2	RE: $a_p = 21295.87$
R5: $\lambda_1 = \lambda_F$	S5: λ_2	RF: $f = 1/298.26$
R6: ξ_1	S6: ξ_2	
R7: C_1, c_1, H	S7: C_2	
R8: $B_1, S/a = r$	S8: B_2	
R9: α_1	S9:	

Initial Flag Status and Use:

0: OFF, Soln A, Soln B	2: OFF, M/S Vertex Flag
1: OFF, Unused	3: OFF, Unused

Display Status:

DSP 2, FIX, DEG

User Control Keys:

A: T_1	a: Soln A
B: T_2	b: Soln B
C:	c:
D:	d:
E: Run	e:

Address	Instruction	Address	Instruction	Address	Instruction	Address	Instruction	Main Routine: Renewal Solution
001	#LELO	21 16 11	Store longitude	039	#BLE	21 15	Compute and/or store:	$\theta_m = (\theta_1 + \theta_2) / 2$
002	STO0	35 00	and store parametric latitude of the master station.	040	RCL4	36 04		
003	FTN	24		041	RCL7	36 07		
004	#LELO	21 16 17	Store longitude and store parametric latitude of the slave station.	042	+	-55		
005	STO1	35 01		043	2	02		
006	FTN	24		044	÷	-24		
007	#LELA	21 11	Subroutine to convert geographic (geodetic) latitude to parametric latitude.	045	STO0	35 13		
008	HMS+	16 36		046	RCL7	36 07		
009	STO5	35 05		047	RCL4	36 04		
010	GBB9	23 09		048	-	-45		
011	STO4	35 04		049	2	02		
012	FTN	24		050	÷	-24		
013	#LELC	21 12	Store longitude and store parametric latitude of the slave station.	051	STO0	35 14		
014	HMS+	16 36		052	RCL8	36 08		
015	STO6	35 06		053	RCL5	36 05		
016	GBB9	23 09		054	-	-45		
017	STO7	35 07		055	STOE	35 15		
018	FTN	24		056	2	02		
019	#LEL9	21 09		057	÷	-24		
020	XZY	-41		058	STO1	35 4E		
021	HMS+	16 36		059	P+S	16-51		
022	TAN	42		060	RCLD	36 14		
023	1	01		061	COB	42		
024	ENT1	-21		062	XZ	53		
025	2	02		063	RCLC	36 13		
026	9	09		064	SIN	41		
027	6	06		065	XZ	53		
028	.	-62		066	-	-45		
029	2	02		067	RCL1	36 46		
030	6	06		068	SIN	41		
031	1 X	52		069	XZ	53		
032	P+S	16-51		070	XZ	-35		
033	STO9	35 09	Store flattening constant.	071	RCLD	36 14		
034	P+S	16-51		072	SIN	41		
035	-	-45		073	XZ	53		
036	2	-35		074	+	-55		
037	TAN-	16 43		075	STO0	35 00		
038	RTN	24		076	ENT1	-21		

Card 1: Prepare Master Data Card

077	↑	-55		115	RCL2	36 02	
078	↓	01		116	RCL3	36 03	
079	-	-45		117	-	-45	Y = U - V
080	CHS	-21		118	ST05	35 05	
081	CO54	16 42		119	CHS	-22	
082	ST03	35 03		120	RCL4	36 04	
083	D+F	16 45		121	RCL1	36 01	
084	LS7X	16-67		122	>	-35	
085	SIN	41		123	+	-55	
086	÷	-24		124	RCL9	36 09	
087	ST01	35 01		125	^	-35	
088	RCL0	36 12		126	4	04	
089	SIN	41		127	÷	-24	
090	RCL0	36 14		128	ST06	35 06	
091	CO5	42		129	CHS	-22	
092	x	-35		130	RCL1	36 01	
093	x2	57		131	+	-55	
094	ENT↑	-21		132	RCL8	36 08	
095	↑	-55		133	SIN	41	
096	↓	01		134	^	-35	
097	RCL0	36 00		135	F+0	16 46	
098	-	-45		136	F+5	16-51	
099	÷	-24		137	ST02	35 02	
100	ST02	35 02		138	F+5	16-51	
101	RCL0	36 14		139	RCL5	36 05	
102	SIN	41		140	RCL0	36 00	
103	RCL0	36 12		141	ENT↑	-21	
104	CO5	42		142	+	-55	
105	x	-35		143	1	01	
106	x2	57		144	-	-45	
107	ENT↑	-21		145	4	04	
108	↑	-55		146	RCL4	36 04	
109	RCL0	36 02		147	-	-45	
110	÷	-24		148	x	-35	
111	ST03	35 03		149	+	-55	
112	RCL2	36 02		150	RCL9	36 09	
113	↑	-55		151	RCL1	36 01	
114	ST04	35 04		152	x	-35	
							$\delta_1 d = f(TX - Y)/4$
							$2c = S/a_e = (T-\delta_1 d) \sin d$
							$F/2 = [Y - (1-2L)(4-X)]$
							$-2G = fT$
							$d = \cos^{-1}(1-2L)$
							$T = d/\sin d$
							$U = 2 \sin^2 \theta_m \cos^2 \Delta \theta_m / (1-L)$
							$V = 2 \sin^2 \Delta \theta_m \cos^2 \theta_m / L$
							$X = U + V$

Card 1: Continued.

153	^	-35					
154	CHS	-22					
155	RCLC	36 15					
156	TAN	43					
157	x	-35					
158	4	64					
159	=	-24					
160	R+G	16 46					
161	RCLC	36 15					
162	+	-35					
163	2	02					
164	=	-24					
165	STO7	35 07					
166	1	01					
167	+R	77					
168	FCLD	36 14					
169	COS	42					
170	x	-35					
171	X=Y	-41					
172	FCLC	36 13					
173	SIN	41					
174	x	-35					
175	+P	34					
176	CLX	-51					
177	RCL7	36 07					
178	:	01					
179	+F	44					
180	CHS	-22					
181	RCLD	36 14					
182	SIN	41					
183	^	-35					
184	X=Y	-41					
185	RCLC	36 13					
186	COS	42					
187	x	-35					
188	+P	34					
189	R+	-31					
190	CLRG	16-53					
191	P/S	16-51					
192	STO6	35 06					
193	STO5	35 05					
194	R+	-31					
195	ST+6	35-55 06					
196	ST-9	35-45 09					
197	0	00					
198	STO3	35 03					
199	WDTA	16-61					
200	P/S	5:					
	-FG						
	$Q = -(FG \tan \Delta\lambda)/4$						
	$\Delta\lambda'_m = (\Delta\lambda + Q)/2$						
	$\cos \Delta\theta_m \cos \Delta\lambda'_m$						
	$\sin \theta_m \sin \Delta\lambda'_m$						
	t_2 is in the Y-register						
	$-\sin \Delta\theta_m \cos \Delta\lambda'_m$						
	$\cos \theta_m \sin \Delta\lambda'_m$						
	t_1 is in the X-register						
	Store						
	α_{12} in R_6 and						
	α_{21} in R_9 .						

Address	Address	Main Routine	Address	Address	Address	Address
031	041		041	041	041	041
032	042		042	042	042	042
033	043		043	043	043	043
034	044	Clear registers.	044	044	044	044
035	045	Store 9 in R ₁ for merging.	045	045	045	045
036	046	Input two Master Data Cards.	046	046	046	046
037	047		047	047	047	047
038	048		048	048	048	048
039	049		049	049	049	049
040	050		050	050	050	050
041	051		051	051	051	051
042	052	Flag 0 is used for triplet vertex determination.	052	052	052	052
043	053	Flag 2 is used for validity checking.	053	053	053	053
044	054	Check master stations.	054	054	054	054
045	055	Check slave stations.	055	055	055	055
046	056	Check master/slave colocations for pair 1, and pair 2.	056	056	056	056
047	057	Display 'error' if no colocations found.	057	057	057	057
048	058	Rearrange data for collocated slave stations.	058	058	058	058
049	059	Continue preparing data card:	059	059	059	059
050	060	$a_p = \frac{a(1+a_2)}{v_0/n} = 21295.87$	060	060	060	060
051	061		061	061	061	061
052	062		062	062	062	062
053	063		063	063	063	063
054	064		064	064	064	064
055	065		065	065	065	065
056	066		066	066	066	066
057	067		067	067	067	067
058	068		068	068	068	068
059	069		069	069	069	069
060	070		070	070	070	070
061	071		071	071	071	071
062	072		072	072	072	072
063	073		073	073	073	073
064	074		074	074	074	074
065	075		075	075	075	075
066	076		076	076	076	076
067	077		077	077	077	077
068	078		078	078	078	078
069	079		079	079	079	079
070	080		080	080	080	080

Card 2: Prepare Operational Data Card.

001	*1315	21 05	<u>Subroutine</u> Exchange storage of master and slave station data if the slave station is at the vertex of the triplet.
002	F017	35 07	
003	F014	35 04	
004	F007	35 07	
005	F011	-41	
006	F004	35 04	
007	F018	35 03	
008	F015	35 05	
009	F019	35 03	
010	F021	-41	
011	F005	35 05	
012	F019	35 03	
013	F016	35 06	
014	F009	35 03	
015	F017	-41	
016	F006	35 05	
017	F016	35 03	
018	F018	-41	
019	F000	35 03	
100	F013	15-51	Change sign of the ID to signal that the slave station is at the triplet vertex.
101	F010	15-51	
102	F010	31	
103	*1314	21 04	
104	F014	35 04	
105	F013	15-51	
106	F017	35 07	
107	F019	15-52	
108	F016	31	
109	F006	35 03	
110	F018	15-51	
111	F015	35 05	
112	F018	15-51	
113	F016	15-52	
114	F018	31	
115	F005	23 02	
116	F013	15 21 02	
117	F018	31	
			<u>Subroutine</u> Determine if the master station of one pair is co- located with the slave station of the other pair.

Line	Code	Instruction	Address	Fixing Routine
001	STOA	Initialize Solution B	16 21 00	
002	F00		16 21 00	
003	F00		16 21 00	
004	F00		16 21 00	
005	F00		16 21 00	
006	F00		16 21 00	
007	F00		16 21 00	
008	F00		16 21 00	
009	F00		16 21 00	
010	F00		16 21 00	
011	RTN		24	
012	STOA		21 11	
013	RCL8		36 08	
014	X00		16 21 00	
015	SF2		16 21 00	
016	XZY		-41	
017	RCL1		36 01	
018	-		-45	
019	RCL5		36 05	
020	-		-24	
021	P=0		16 46	
022	1		01	
023	-R		44	
024	XZY		-41	
025	F00		16 23 00	
026	CMS		-22	
027	STO7		35 03	
028	CLS		-51	
029	RCL2		36 02	
030	1		01	
031	-R		44	
032	XZ		-41	
033	STO7		35 07	
034	R4		-31	
035	-		-45	
036	STO6		35 06	
037	CLX		-51	
038	RTN		24	
039	F00		16 23 00	
040	F00		16 23 00	
041	F00		16 23 00	
042	F00		16 23 00	
043	F00		16 23 00	
044	X		-35	
045	XZ		-41	
046	RCL3		31 03	
047	X		-35	
048	-		-45	
049	STOA		35 11	
050	RCL8		36 08	
051	RCL5		36 05	
052	RCL7		36 07	
053	F00		16 21 00	
054	RCL8		36 08	
055	X		-25	
056	+P		44	
057	XZY		-41	
058	R4		16 21	
059	RCL7		36 07	
060	X		-35	
061	RCL6		36 06	
062	XZY		-41	
063	+R		44	
064	P4		-31	
065	-		-45	
066	R4		-31	
067	XZY		-41	
068	-		-45	
069	R4		16 31	
070	XZY		-41	
071	+P		34	
072	RCLA		36 11	
073	XZY		-41	
074	=		-24	
075	COS		16 4E	
076	F00		16 23 00	

Card 3: Loran Fixing Program

077	CHS	-22	$\alpha = \gamma \pm \cos^{-1}(\kappa/\rho)$	115		
078	+	-55	Store α	116		
079	STO9	35 09		117		
080	RCL6	36 05		118		
081	-	-45		119		
082	COS	42		120		
083	RCL7	36 07		121		
084	X	-35		122		
085	RCL3	36 02		123		
086	+	-55		124		
087	RCL5	36 06		125		
088	X*Y	-41		126		
089	→P	34		127		
090	R↓	-31		128		
091	STO8	35 09		129		
092	RCL4	36 04		130		
093	COS	42		131		
094	RCL9	36 05		132		
095	SIN	41		133		
096	X	-35		134		
097	STO4	35 11		135		
098	RCL1	36 45		136		
099	X	-35		137		
100	STO7	35 07		138		
101	I	01		139		
102	RCLA	36 11		140		
103	X2	53		141		
104	-	-45		142		
105	4	04		143		
106	=	-24		144		
107	RCL1	36 46		145		
108	X	-35		146		
109	STO3	35 03		147		
110	2	02		148		
111	X	-35		149		
112	CHS	-22		150		
113	RCL7	36 07		151		
114	RCLA	36 11		152		

$$r = \text{qatn} \left[\frac{B_i}{C_i \cos(\alpha - \xi_i) + A_i} \right]$$

$$M = \cos \theta_1 \sin \alpha_{12}$$

$$\text{where } \alpha_{12} = \xi_1$$

$$c_1 = fM$$

$$c_2 = f(1 - M^2)/4$$

$$D = 1 - 2c_2 - c_1M$$

$$P = c_2/D$$

$$d = S/(aD)$$

$$\sigma_1 = \text{qatn}(N, \sin \theta_1)$$

$$u = 2(\sigma_1 - d)$$

$$W = 1 - 2P \cos u$$

$$V = \cos(u + d)$$

153	RCL3	36 03							
154	X	-35							
155	2	02							
156	X	-35							
157	RCLC	36 13							
158	SIN	41							
159	X	-35							
160	R+0	16 46							
161	CHS	-22							
162	RCLC	36 15							
163	+	-55							
164	ST00	35 14							
165	ST07	35-35 07							
166	RCL4	36 04							
167	COS	42							
168	RCL9	36 09							
169	COS	42							
170	X	-35							
171	RCLD	36 14							
172	X*Y	-41							
173	R	44							
174	RCLD	36 14							
175	RCL4	36 04							
176	SIN	41							
177	R	44							
178	R	16-31							
179	+	-55							
180	X*Y	-41							
181	R	16-31							
182	-	-45							
183	X2	53							
184	RCLA	36 11							
185	X2	53							
186	+	-55							
187	JX	54							
188	÷	-24							
189	1	01							
190	RCL1	36 46							
191	-								
192	÷								
193	TAN-								
194	+HMS								
195	PRTX								
196	R/S								
197	RCL9								
198	RCLD								
199	SIN								
200	R								
201	RCL4								
202	SIN								
203	X								
204	CHS								
205	RCL4								
206	COS								
207	RCLD								
208	COS								
209	X								
210	+								
211	R								
212	CLX								
213	RCL7								
214	-								
215	RCL5								
216	+								
217	1								
218	R								
219	R								
220	R								
221	+HMS								
222	PRTX								
223	R/S								
Y = 2PVW sin d									
$\Delta c = d - Y$									
$H = c_1 \Delta c$									
$N = \cos \theta_1 \cos \alpha_{12}$									
$N \cos \Delta c$ and $N \sin \Delta c$									
$\sin \theta_1 \cos \Delta c$ and $\sin \theta_1 \cos \Delta c$									
$\sin \theta_1 \cos \Delta c + N \sin \Delta c$									
$(N \cos \Delta c - \sin \theta_1 \sin \Delta c)^2$									
K									
Display ϕ_2									
$\sin \Delta \sigma \cos \alpha_{12}$									
$\sin \Delta \sigma \sin \alpha_{12}$									
$\sin \theta_1 \sin \Delta \sigma \cos \alpha_{12}$									
$\cos \theta_1 \cos \Delta \sigma$									
$-\sin \theta_1 \sin \Delta \sigma \cos \alpha_{12}$									
$\Delta \eta$									
$\Delta \lambda = \Delta \eta - H$									
$\lambda_2 = \lambda_1 + \Delta \lambda$									
Display λ_2									

D. Loran-C Fixing Algorithms

The development of the Loran fixing algorithms in this report is presented in more detail in a companion report [Ref. 3] and will not be repeated here.

The basic Loran-C equation [Ref. 4] can be written as

$$T = [T_S + p(T_S)] - [T_M + p(T_M)] + [T_B + p(T_B)] + \delta \quad (1)$$

where

T is the "indicated time difference" in microseconds,
 T_M, T_S is the distance, in microseconds, from the master and the slave to the receiver, respectively,
 T_B is the distance, in microseconds, between the master and the slave,
 δ is the assigned coding delay, in microseconds, and
 $p(T)$ is the secondary phase correction, in microseconds, for an all sea water path of length T .

The quantity

$$\Delta t = [T_B + p(T_B)] + \delta$$

is a constant for each master/slave pair. The following World Geodetic System 1972 (WGS 72) values have been adopted for Loran-C navigation [Ref. 4]:

$v_0 = 299792458$ meters/second is the velocity of light
in free space,
 $\eta = 1.000338$ is the index of refraction of the surface
of the earth for standard atmosphere and 100kHz
electromagnetic waves,
 $a_e = 6378135.00$ meters is the equatorial radius of the
earth, and
 $f = 1/298.26$ is the flattening factor ($1 - b/a_e$, where
 b is the polar radius) of the earth.

Accurate formulas for computing the secondary phase
correction $p(T)$ are contained in Reference 4, but for use
with the handheld calculator the following linear approximation
[Ref. 3] will be used:

$$p(T) = a_1 + a_2 T ,$$

where

$$a_1 = -0.321,$$

and

$$a_2 = 0.000635.$$

Using this approximation, it is possible to solve Equation 1
for the quantity $T_S - T_M$. We find

$$T_S - T_M = (T - \Delta t)/(1 + a_2) . \quad (2)$$

On the surface of a sphere a hyperbolic line of position
can be represented by the equation [Ref. 3, page 175]

$$\tan r = \frac{\cos 2a - \cos 2c}{\sin 2c \cos \omega + \zeta \sin 2a} \quad (3)$$

where the origin of the coordinate system is at the prime focus of the spherical hyperbola, $2c$ is the spherical arc joining the foci, $2a$ is a constant for any one LOP, and r and ω are the spherical coordinates of a point on the LOP. If the base line of the coordinate system is the arc joining the foci then ω is the spherical polar angle from the base line to a point P on the LOP and r is the spherical polar distance (or arc) from the prime focus to P . Using the Loran system we take $\zeta = +1$ if the prime focus is at a master station and we take $\zeta = -1$ if the prime focus is at a slave station.

If we take $v = v_0/\eta$ to be the velocity of 100kHz electromagnetic radiation of the earth's surface then

$$2a = v(T_S - T_M)/a_e ,$$

or, using Eq. (2),

$$2a = (T - \Delta t)/a_p , \quad (4)$$

where

$$a_p = \frac{a_e(1 + a_2)}{v_0/\eta} = 21295.87 \text{ } \mu\text{s} .$$

The baseline between master and slave can be obtained from

$$2c = v T_B/a_e . \quad (5)$$

Here $2c$ is computed by program card 1 (preparation of master data cards) using the algorithm in Section E.

Consider a Loran-C triplet with master stations colocated. Let ξ_1 and ξ_2 denote the azimuth angles of slave 1 (S_1) and slave 2 (S_2), respectively, measured from North toward the East from the master stations (M) (see Fig. 3). Further, let α and r denote the azimuth and spherical polar arc (distance) of the receiver (R) from M. For this geometry, Eq. (3) can be written as

$$\tan r_i = \frac{B_i}{C_i \cos(\alpha - \xi_i) + A_i} \quad (6)$$

where

$$A_i = \zeta_i \sin 2a_i$$

$$B_i = \cos 2a_i - \cos 2c_i$$

and

$$C_i = \sin 2c_i$$

for the i^{th} Loran pair, $i = 1, 2$. Since $r = r_1 = r_2$, $\tan r_i$ can be eliminated in Eq. (6). The resulting equation can be rewritten as

$$C \cos \alpha + S \sin \alpha = K, \quad (7)$$

where

$$C = B_1 C_2 \cos \xi_2 - B_2 C_1 \cos \xi_1,$$

$$S = B_1 C_2 \sin \xi_2 - B_2 C_1 \sin \xi_1,$$

$$\text{and } K = B_2 A_1 - B_1 A_2.$$

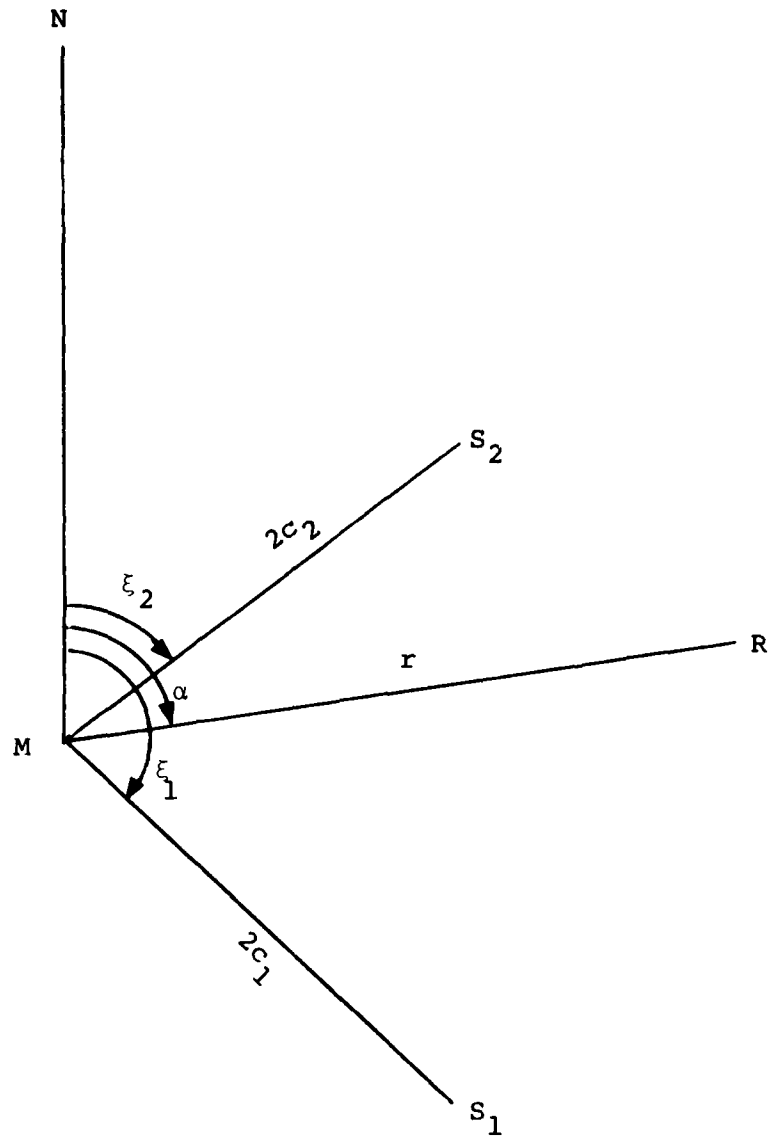


Figure 3. Geometry of a Loran Triplet and a Receiver.

If we define $\rho > 0$ and γ by the equations

$$\begin{aligned} \text{and} \quad & \rho \cos \gamma = C, \\ & \rho \sin \gamma = S, \end{aligned} \tag{8}$$

then

$$\rho = \sqrt{C^2 + S^2},$$

and

$$\gamma = \text{qatn}(S, C).$$

Here the function $\text{qatn}(y, x)$ is the arctangent of y/x adjusted for the proper quadrant according to the signs of x and y . A compact form of this function is

$$\text{qatn}(y, x) = \tan^{-1} \frac{y}{x + 10^{-9} t(x = 0?)} + \pi t(x < 0?)$$

where

$$t(z) = 1 \text{ when } z \text{ is true}$$

and

$$t(z) = 0 \text{ when } z \text{ is false.}$$

When convenient we will use the notation $\text{qatn}(y/x)$ interchangeably with $\text{qatn}(y, x)$. The qatn function is equivalent to the polar angle obtained using the rectangular to polar conversion function on the HP-67/97.

Now substitute Eq. (8) into Eq. (7) and solve for

$$\alpha = \gamma \pm \cos^{-1}(k/\rho) \tag{9}$$

to obtain the azimuth angle α of the two points of intersection of the LOP's. Finally we obtain a value for r by substituting each α into Eq. (5). We find that

$$r = \text{qatn} \left[\frac{B_i}{C_i \cos(\alpha - \xi_i) + A_i} \right] \quad \text{for } i = 1 \text{ or } 2.$$

The distance and azimuth from M or the triplet vertex can be converted into the latitude and longitude of the two possible positions of R .

The fixing algorithm then uses α and r in the *direct* solution algorithm of spheroidal geodesy (Section F).

E. The Reverse (Inverse) Solution Algorithm

This *reverse* solution algorithm is a modification of the first order in flattening (f) algorithm given by Thomas [Ref. 5, pp. 8-10]. Thomas' notation has been followed as closely as possible for ease of comparison of the algorithms. The girth function is defined in Section D. West longitudes (λ) and South latitudes (ϕ) are negative. We are given the points $P_1(\phi_1, \lambda_1)$, $P_2(\phi_2, \lambda_2)$ on the spheroid and are to find the distance S between the points and the forward and back azimuths, α_{12} and α_{21} . Given quantities are $\phi_1, \lambda_1, \phi_2$ and λ_2 . No assumptions about the relative location of P_1 and P_2 are required. The modified *reverse* solution algorithm is:

$$\begin{aligned} \theta_i &= \tan^{-1}[(1-f) \tan \phi_i], \quad i = 1, 2, \\ \theta_m &= (\theta_1 + \theta_2)/2, \quad \Delta\theta_m = (\theta_2 - \theta_1)/2, \quad \Delta\lambda = \lambda_2 - \lambda_1, \\ \Delta\lambda_m &= \Delta\lambda/2, \quad H = \cos^2 \Delta\theta_m - \sin^2 \theta_m = \cos^2 \theta_m - \sin^2 \Delta\theta_m = \cos \theta_1 \cos \theta_2, \\ L &= \sin^2 \Delta\theta_m + H \sin^2 \Delta\lambda_m = \sin^2(d/2), \quad 1 - L = \cos^2(d/2), \\ d &= \cos^{-1}(1 - 2L), \quad U = 2 \sin^2 \theta_m \cos^2 \Delta\theta_m / (1 - L), \\ V &= 2 \sin^2 \Delta\theta_m \cos^2 \theta_m / L, \quad X = U + V, \quad Y = U - V, \\ F &= d \sin d, \quad \alpha_1 d = f(TX - Y)/4, \quad S = a_e(T - \alpha_1 d) \sin d, \\ F &= 2[Y - (1 - 2L)(4 - X)], \quad G = fT/2, \\ \alpha_2 &= (F \tan \alpha_1)/4, \quad \Delta\lambda_m' = (d' + Q)/2 \end{aligned}$$

$$t_1 = \text{qatn}(-\sin \Delta\theta_m \cos \Delta\lambda'_m, \cos \theta_m \sin \Delta\lambda'_m),$$

$$t_2 = \text{qatn}(\cos \Delta\theta_m \cos \Delta\lambda'_m, \sin \theta_m \sin \Delta\lambda'_m),$$

$$\alpha_{12} = t_1 + t_2, \quad \alpha_{21} = t_1 - t_2.$$

This reverse solution algorithm is used by program card 1 (preparation of master data cards) to compute the baseline distance $2c$ and the azimuths ξ_{MS} and ξ_{SM} between the master and slave stations of a Loran pair.

Details of the modifications made to Thomas' algorithm are contained in Reference 3.

F. The Direct Solution Algorithm

This *direct* solution algorithm is a modification of the first order in flattening (f) algorithm given by Thomas [Ref. 5, pp. 7-8]. Thomas' notation has been followed as closely as possible for ease of comparison of the algorithms. The *qatn* function is defined in Section D. West longitudes and South latitudes are negative. We are given the point $P_1(\phi_1, \lambda_1)$ on the spherioid, where ϕ_1, λ_1 are the geodetic latitude and longitude (geographic coordinates); the forward azimuth α_{12} and the distance S to a second point $P_2(\phi_2, \lambda_2)$; and from these we are to find the geographic coordinates ϕ_2, λ_2 and the back azimuth α_{21} . The given quantities are $\phi_1, \lambda_1, \alpha_{12}$ and S . No assumptions about the relative location of P_1 and P_2 are required. The modified *direct* solution algorithm is:

$$\theta_1 = \tan^{-1}[(1-f) \tan \phi_1], \quad M = \cos \theta_1 \sin \alpha_{12}$$

$$N = \cos \theta_1 \cos \alpha_{12}, \quad c_1 = fM, \quad c_2 = f(1 - M^2)/4,$$

$$D = 1 - 2c_2 - c_1M, \quad P = c_2/D, \quad \sigma_1 = \text{qatn}(N, \sin \theta_1)$$

$$d = S/(a_e D), \quad u = 2(\sigma_1 - d), \quad W = 1 - 2P \cos u,$$

$$V = \cos(u + d), \quad Y = 2PVW \sin d, \quad \Delta\sigma = d - Y,$$

$$\alpha_{21} = \text{qatn}[-M, -(N \cos \Delta\sigma - \sin \theta_1 \sin \Delta\sigma)],$$

$$K = (1-f) [M^2 + (N \cos \Delta\sigma - \sin \theta_1 \sin \Delta\sigma)^2]^{1/2},$$

$$\phi_2 = \tan^{-1}[(\sin \theta_1 \cos \Delta\sigma + N \sin \Delta\sigma)/K],$$

$$\Delta\theta = \text{qatn}(\sin \theta_1 \sin \alpha_{12}, \cos \theta_1 \cos \Delta\sigma - \sin \theta_1 \sin \Delta\sigma \cos \alpha_{12}),$$

$$H = \phi_1 + \Delta\theta, \quad \lambda_2 = \lambda_1 + \Delta\lambda.$$

This direct solution algorithm is used by program card 3 (improved fix program) to compute the latitude and longitude of the receiver using the azimuth and range of the receiver from the Loran triplet vertex.

Details of the modifications made to Thomas' algorithm are contained in Reference 3.

G. Discussion and Some Typical Results

The HP-67 program design specifications of COMPATWINGSPAC [Ref. 6] are contained in the following statement.

"There is a need for an HP-67 program that will compute a geographical position from two Loran delay rate readings. Several methodologies are available to compute the desired position but computational complexities increase with the desired accuracy and flexibility. The most desirable accuracy would be an error of less than 4 n.mi. at a range of 500 n.mi. with less error closer to the stations. It is likely that program length considerations will require that the station pairs have a common site (i.e. two slaves or two masters at the same location). This is not an unusual situation as evidenced by strings of station pairs along coast lines. A data card will probably be necessary for the station pairs to be used. However, more than one program card is unacceptable due to the decrease in functional utility when compared to the manual plotting method. As a final requirement, the fix should be obtainable on either side of the baselines connecting the stations, and not limited to a geometric position relative to one side or the other of the stations."

It was further stated that the maximum computation time to obtain a fix be 1.5 minutes.

It is felt that these design goals have been satisfied. Although one program is required to prepare master data cards for all Loran-C pairs and a second card is required to prepare

operational data cards, one each for every triplet, this preparation should be done only once. The data cards should be supplied to users verified and labeled, by the Fleet Mission Program Library. One program card and an appropriate operational data card are all that is required for the fixing algorithm.

The fixing algorithm will display one of the two possible receiver positions in 38 seconds following the entry of the time delay readings. Since there are situations in which *either* of the two solutions could be the valid solution; the decision of which solution to use should be left to the operator, not the program designer.

Testing of the algorithm for all Loran-C triplets and positions relative to those triplets was too extensive a program to be carried out in the available time. Some "typical" scenarios however are presented in Tables I through IV. As can be seen all errors are all well within the design specifications of 4 n.mi at 500 n.mi range from the stations. The time delay values in these Tables were generated using a program discussed in Reference 3. It is recommended that the P-3 community test the algorithm for accuracy in known areas of operation and examine the results for possible regions in which the algorithm may fall outside the design requirements. Such testing should be compatible with the known "unreliable regions" shown on the Loran-C charts.

Table I. Moffett Field South

Position		Indicated Time Delay		Fix		Error n.mi
Lat	Long	9940X	9940Y	Lat (N)	Long (W)	
24°N	122°W	27726.19	40912.76	23°59'55"	122°00'01"	0.08
26	122	27715.97	40998.39	25°59'57"	122°00'01"	0.05
28	122	27702.41	41117.84	27°59'59"	122°00'00"	0.02
30	122	27683.53	41291.85	29°59'59"	122°00'00"	0.02
32	122	27655.47	41555.46	32°00'00"	122°00'00"	0.00
34	122	27609.63	41959.57	34°00'00"	122°00'00"	0.00
36	122	27523.56	42544.11	36°00'00"	121°59'59"	0.01
38	122	27334.61	43248.22	38°00'00"	121°59'58"	0.03

Table II. Moffett Field West

Position		Indicated Time Delay		Fix		Error n.mi
Lat	Long	9940Y	9940W	Lat (N)	Long (W)	
37°N	122°W	42892.86	16257.23	36°59'59"	122°00'01"	0.02
37	125	43056.68	15765.13	37°00'00"	125°00'00"	0.00
37	128	43137.78	15327.12	37°00'00"	128°00'00"	0.00
37	131	43191.10	14970.77	37°00'00"	131°00'00"	0.00
37	134	43232.38	14683.74	37°00'00"	134°00'00"	0.00
37	137	43267.42	14449.40	37°00'00"	137°00'00"	0.00
37	140	43298.80	14254.02	37°00'00"	140°00'01"	0.01
37	143	43327.85	14087.43	37°00'01"	142°59'59"	0.02

Table III. Brunswick Northeast

Position		Indicated Time Delay		Fix		Error n.mi
Lat	Long	7930Z	9930X	Lat (N)	Long (W)	
60°N	30°W	52437.86	28451.72	60°00'03"	29°59'32"	0.24
58	35	51960.93	28391.50	58°00'00"	34°59'46"	0.11
56	40	50992.37	28359.15	55°59'59"	39°59'54"	0.06
54	45	49292.46	28370.85	53°59'59"	44°59'57"	0.03
52	50	47165.60	28490.64	52°00'00"	49°59'59"	0.01
50	55	45236.59	29070.48	50°00'00"	55°00'00"	0.00
48	60	44505.60	30991.94	48°00'00"	60°00'00"	0.00
46	65	44475.70	33697.14	46°00'00"	65°00'00"	0.00
44	70	44588.91	36567.42	43°59'59"	69°59'59"	0.02

Table IV. Jacksonville Southeast

Position		Indicated Time Delay		Fix		Error n.mi
Lat	Long	9930W	9930X	Lat (N)	Long (W)	
9°N	47°W	13058.04	36466.46	8°59'19"	46°59'22"	0.92
12	52	12984.71	37288.35	11°59'34"	51°59'37"	0.57
15	57	12898.73	38267.58	14°59'44"	56°59'47"	0.34
18	62	12793.91	39431.32	17°59'52"	61°59'54"	0.16
21	67	12656.52	40794.36	20°59'56"	66°59'57"	0.08
24	72	12451.30	42330.55	23°59'59"	71°59'59"	0.02
27	77	12097.12	43876.62	27°00'01"	77°00'00"	0.02
30	82	12973.95	44768.53	30°00'01"	82°00'06"	0.09

H. References

1. J. A. Pierce, A. A. McKenzie, and R. H. Woodward, editors, *LORAN*, M.I.T. Radiation Laboratory Series, McGraw-Hill Book Company, Inc., 1948.
2. G. Hefley, *The Development of Loran-C Navigation and Timing*, National Bureau of Standards Monograph 129, U. S. Department of Commerce, U. S. Government Printing Office, Washington, D.C. 20402, October 1972.
3. R. H. Shudde, "An Algorithm for Position Determination Using Loran-C Triplets with a BASIC Program for the Commodore 2001 Microcomputer," Technical Report NPS55-80-009, March 1980, Naval Postgraduate School, Monterey, CA 93940.
4. *LORAN HYPERBOLIC LOP FORMULAS AND GENERAL SPECIFICATIONS FOR LORAN-C* (20 June 1949) were obtained from G. R. Young, Acting Chief, Navigation Department, Defense Mapping Agency, Hydrographic/Topographic Center, Washington, D.C. by private communication, 5 March 1980.
5. Paul D. Thomas, "Spheroidal Geodesics, Reference Systems, and Local Geometry," SP-138, U. S. Naval Oceanographic Office, Washington, D.C., January 1970.
6. Private communication from COMPATWINGSPAC representatives, Moffett Field, CA., October 1979.

APPENDIX. Loran-C Station Parameters

The following list contains the pertinent parameters for each Loran-C station pair. This list was compiled from data in Reference 4. Each column contains the following information:

1. The Loran-C station pair designator
2. Δt , the sum of the coding delay plus one way baseline time, including the secondary phase correction for an all seawater path, in microseconds.
3. The master station latitude.
4. The master station longitude.
5. The slave station latitude.
6. The slave station longitude.

In this list, negative longitudes are West and positive longitudes are East. If desired, this convention may be reversed since the algorithms are independent of such external conventions; if this is done, care should be taken that the signs of all longitudes in the list are reversed. In columns 3 through 6 the latitudes and longitudes appear to be in decimal form, but the actual format is DDD.MMSSFF (which is compatible with the HP-67/97 H.MS input mode) where

DDD designates degrees,
MM designates minutes,
SS designates seconds, and
FF designates hundredths of seconds.

4990X, 15972.23, 16.444395, -169.303120, 20.144916, -155.530970
4990Y, 34253.18, 16.444395, -169.303120, 28.234177, -178.173020
5930X, 13131.88, 46.482720, -067.553771, 41.151193, -069.583909
5930Y, 28755.02, 46.482720, -067.553771, 46.463218, -053.102816
5990X, 13343.60, 51.575878, -122.220224, 55.262085, -131.151965
5990Y, 28927.36, 51.575878, -122.220224, 47.034799, -119.443953
5990Z, 42266.63, 51.575878, -122.220224, 50.362972, -127.212935
7930W, 15068.02, 59.591727, -045.102747, 64.542658, -023.552175
7930X, 27803.77, 59.591727, -045.102747, 62.175968, -007.042671
7930Z, 48212.20, 59.591727, -045.102747, 46.463218, -053.102816
7960X, 13804.45, 63.194281, -142.483190, 57.262021, -152.221122
7960Y, 29651.14, 63.194281, -142.483190, 55.262085, -131.151965
7970W, 30065.64, 62.175968, -007.042671, 54.482980, +008.173633
7970X, 15048.10, 62.175968, -007.042671, 68.380615, +014.274700
7970Y, 48944.53, 62.175968, -007.042671, 64.542658, -023.552175
7970Z, 63216.30, 62.175968, -007.042671, 70.545261, -008.435869
7980W, 12809.54, 30.593874, -085.100930, 30.433302, -090.494360
7980X, 27442.38, 30.593874, -085.100930, 26.315501, -097.500009
7980Y, 45201.88, 30.593874, -085.100930, 27.015849, -080.065352
7980Z, 61542.72, 30.593874, -085.100930, 34.034604, -077.544676
7990X, 12755.97, 38.522061, 016.430596, 35.312088, 012.312996
7990Y, 33273.30, 38.522061, 016.430596, 40.582095, 027.520152
7990Z, 50999.69, 38.522061, 016.430596, 42.033649, 003.121590
8970W, 14355.11, 39.510754, -087.291214, 30.593874, -085.100930
8970X, 31162.06, 39.510754, -087.291214, 42.425060, -076.493386
8970Y, 47752.74, 39.510754, -087.291214, 48.364984, -094.331847
8970Z, 13635.51, 34.034604, -077.544676, 27.015849, -080.065352
9930X, 26289.66, 34.034604, -077.544676, 46.463218, -053.102816
9930Y, 52541.31, 34.034604, -077.544676, 41.151193, -069.583909
9930Z, 69568.72, 34.034604, -077.544676, 39.510754, -087.291214
9940W, 13796.90, 39.330662, -118.495637, 47.034799, -119.443953
9940X, 23894.50, 39.330662, -118.495637, 38.465699, -122.294453
9940Y, 41957.30, 39.330662, -118.495637, 35.191818, -114.481743
9950X, 13797.20, 42.425060, -076.493386, 46.482720, -067.553771
9950Y, 26969.93, 42.425060, -076.493386, 41.151193, -069.583909
9950Z, 42221.65, 42.425060, -076.493386, 34.034604, -077.544676
9960Z, 57102.06, 42.425060, -076.493386, 39.510754, -087.291214
9970W, 15233.94, 24.48041, 141.19290, 24.17077, 153.58515
9970X, 36805.12, 24.48041, 141.19290, 42.443700, 143.430906
9970Y, 59463.12, 24.48041, 141.19290, 26.362499, 128.085621
9970Z, 99746.79, 24.48041, 141.19290, 09.324566, 138.095523
9990Y, 14875.30, 57.090988, -170.145981, 52.494505, +173.105231
9990Z, 30069.09, 57.090988, -170.145981, 65.144012, -166.531447
9990Z, 46590.10, 57.090988, -170.145981, 57.262021, -152.221122

Coverage of Loran-C Systems

<u>Station</u>	<u>Location</u>
4990	Central Pacific
5930	East Coast, Canada
5990	West Coast, Canada
7930	North Atlantic
7960	Gulf of Alaska
7970	Norwegian Sea
7980	Southeast U.S.A.
7990	Mediterranean Sea
8970	Great Lakes
9930	East Coast, U.S.A.
9940	West Coast, U.S.A.
9960	Northeast U.S.A.
9970	Northwest Pacific
9990	North Pacific

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