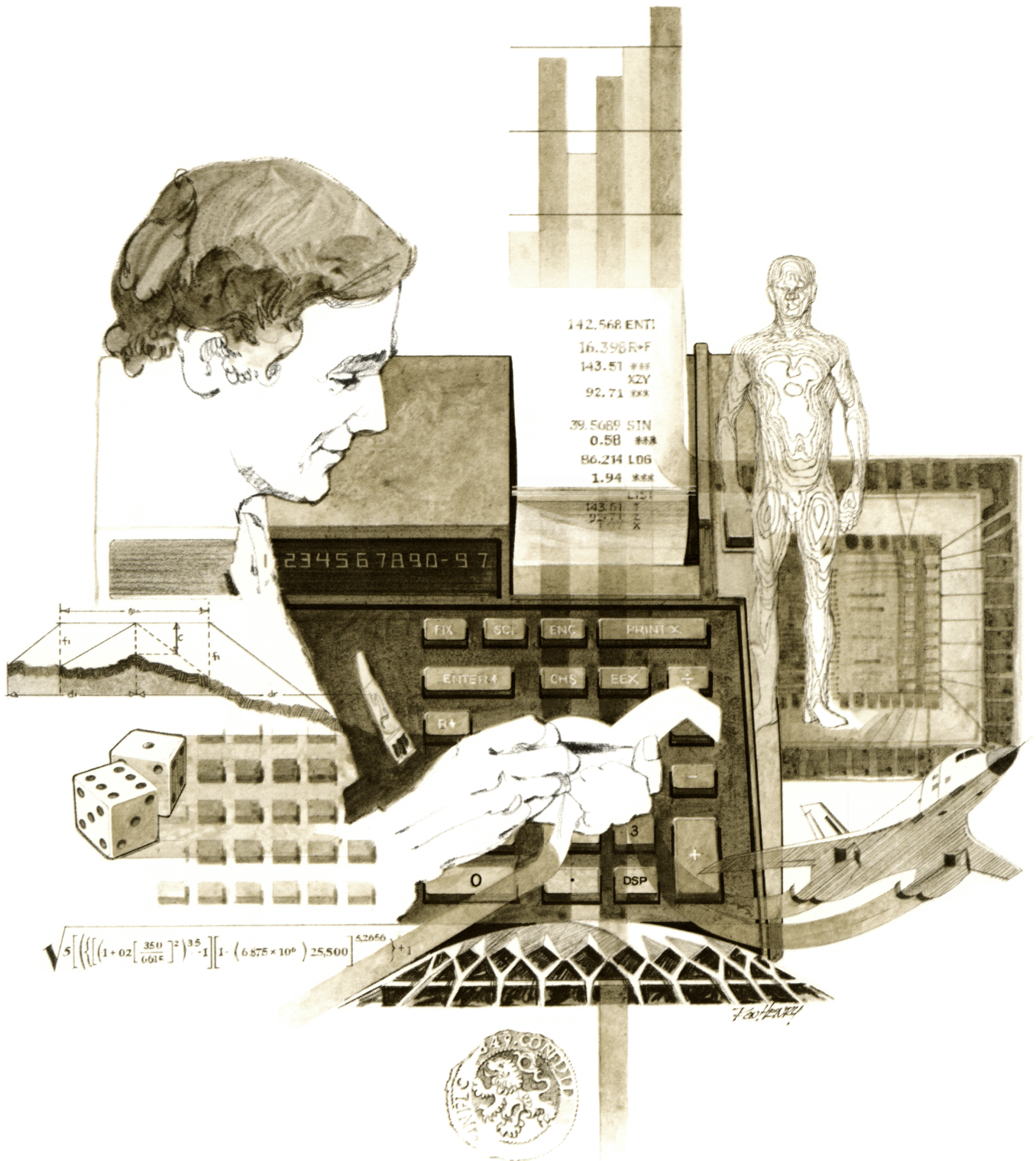


HEWLETT-PACKARD

HP-67/HP-97

Users' Library Solutions

Physics



INTRODUCTION

In an effort to provide continued value to its customers, Hewlett-Packard is introducing a unique service for the HP fully programmable calculator user. This service is designed to save you time and programming effort. As users are aware, Programmable Calculators are capable of delivering tremendous problem solving potential in terms of power and flexibility, but the real genie in the bottle is program solutions. HP's introduction of the first handheld programmable calculator in 1974 immediately led to a request for program **solutions** — hence the beginning of the HP-65 Users' Library. In order to save HP calculator customers time, users wrote their own programs and sent them to the Library for the benefit of other program users. In a short period of time over 5,000 programs were accepted and made available. This overwhelming response indicated the value of the program library and a Users' Library was then established for the HP-67/97 users.

To extend the value of the Users' Library, Hewlett-Packard is introducing a unique service—a service designed to save you time and money. The Users' Library has collected the best programs in the most popular categories from the HP-67/97 and HP-65 Libraries. These programs have been packaged into a series of low-cost books, resulting in substantial savings for our valued HP-67/97 users.

We feel this new software service will extend the capabilities of our programmable calculators and provide a great benefit to our HP-67/97 users.

A WORD ABOUT PROGRAM USAGE

Each program contained herein is reproduced on the standard forms used by the Users' Library. Magnetic cards are not included. The Program Description I page gives a basic description of the program. The Program Description II page provides a sample problem and the keystrokes used to solve it. The User Instructions page contains a description of the keystrokes used to solve problems in general and the options which are available to the user. The Program Listing I and Program Listing II pages list the program steps necessary to operate the calculator. The comments, listed next to the steps, describe the reason for a step or group of steps. Other pertinent information about data register contents, uses of labels and flags and the initial calculator status mode is also found on these pages. Following the directions in your HP-67 or HP-97 **Owners' Handbook and Programming Guide**, "Loading a Program" (page 134, HP-67; page 119, HP-97), key in the program from the Program Listing I and Program Listing II pages. A number at the top of the Program Listing indicates on which calculator the program was written (HP-67 or HP-97). If the calculator indicated differs from the calculator you will be using, consult Appendix E of your **Owner's Handbook** for the corresponding keycodes and keystrokes converting HP-67 to HP-97 keycodes and vice versa. No program conversion is necessary. The HP-67 and HP-97 are totally compatible, but some differences do occur in the keycodes used to represent some of the functions.

A program loaded into the HP-67 or HP-97 is not permanent—once the calculator is turned off, the program will not be retained. You can, however, permanently save any program by recording it on a blank magnetic card, several of which were provided in the Standard Pac that was shipped with your calculator. Consult your **Owner's Handbook** for full instructions. A few points to remember:

The Set Status section indicates the status of flags, angular mode, and display setting. After keying in your program, review the status section and set the conditions as indicated before using or permanently recording the program.

REMEMBER! To save the program permanently, **clip** the corners of the magnetic card once you have recorded the program. This simple step will protect the magnetic card and keep the program from being inadvertently erased.

As a part of HP's continuing effort to provide value to our customers, we hope you will enjoy our newest concept.

TABLE OF CONTENTS

BLACK BODY THERMAL RADIATION	1
Calculates the wavelength of maximum emissive power for a given temperature.	
BLACK HOLE CHARACTERISTICS	9
Computes temperature, Schwarzschild radius, and lifetime of a black hole.	
SPECIAL RELATIVITY CONVERSIONS	13
Provides relativistic conversions between rest mass, velocity, energy, and momentum.	
THREE DIMENSIONAL SPECIAL RELATIVITY.	17
Computes intervals, dilation factors, and Lorentz transformations.	
EINSTEIN'S TWIN PARADOX	22
Calculate real and relative time and age differential based on the Lorentz transform.	
DELTA-V--ORBIT SIMULATOR	27
Computes orbit parameters from initial position and velocity data.	
EQUATIONS OF PARTICLE MOTION	32
Compute two unknown values based on the known values of the variables distance, time, V-final, V-initial, and acceleration.	
BALLISTICS TRAJECTORY COMPUTATIONS	37
Computes range, velocity, energy, time of flight, rise, and drop of a bullet.	
ISOTOPE OVERLAP CORRECTIONS	43
Corrects for spillover between channels in a liquid scintillation spectrometer.	
CRITICAL REACTOR CODE	47
Estimates the parameters of a reactor	
SEMI-EMPIRICAL NUCLEAR MASS FORMULA	54
Calculates approximate binding energies and mass excess for any nucleus.	
CLEBSCH-GORDON COEFFICIENTS AND $3J$ SYMBOLS EVALUATION	59
Uses Racah formula to evaluate coupling two states of angular momentum.	
32-P REMAINING ON MM,DDYYYY GIVEN MCI ON EARLIER MM,DDYYYY.	64
Given millicuries of 32-P on date 1, this program calculates the decays per minute and counts per minute on date 2 as well as the number of days between date 1 and date 2.	

Program Description I

Program Title Black Body Thermal Radiation

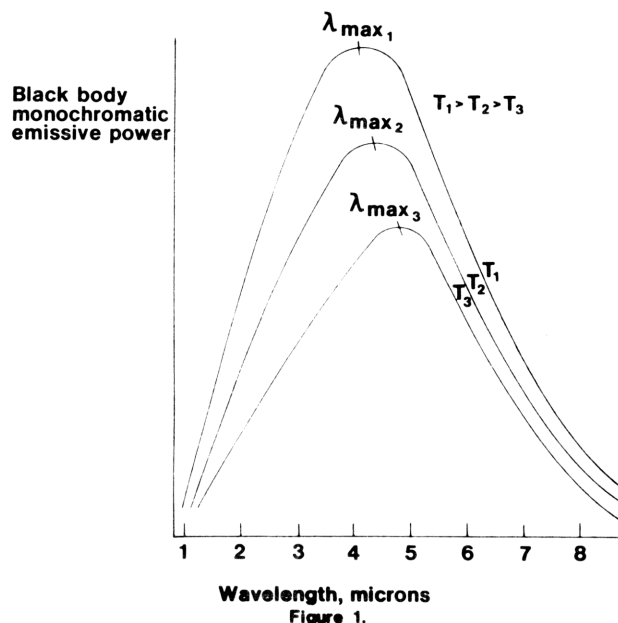
Contributor's Name Hewlett-Packard

Address 1000 N. E. Circle Blvd.

City Corvallis State Oregon Zip Code 97330

Program Description, Equations, Variables

Bodies with finite temperatures emit thermal radiation. The higher the absolute temperature, the more thermal radiation emitted. Bodies which emit the maximum possible amount of energy at every wavelength for a specified temperature are said to be black bodies. While black bodies do not actually exist in nature, many surfaces may be assumed to be black for engineering considerations.



(continued next page)

Operating Limits and Warnings

A minute or more may be required to obtain $E_{b(0-\lambda)}$ or $E_{b(\lambda_1-\lambda_2)}$ since the integration is numerical.

Sources differ on values for constants. This could yield small discrepancies between published tables and program outputs.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Figure 1 is a representation of black body thermal emission as a function of wavelength. Note that as temperature increases, the area under the curves (total emissive power $E_{b(0-\infty)}$) increases. Also note that the wavelength of maximum emissive power λ_{\max} shifts to the left as temperature increases.

This program calculates the wavelength of maximum emissive power for a given temperature, the temperature for which a given wavelength would be the wavelength of maximum emissive power, the total emissive power over all wavelengths, the emissive power at a particular wavelength, the emissive power from zero to a specified wavelength, and the emissive power between specified wavelengths.

Equations:

$$\lambda_{\max} T_{\lambda_{\max}} = c_3$$

$$E_{b(0-\infty)} = \sigma T^4$$

$$E_{b\lambda} = \frac{2\pi c_1}{\lambda^5 (e^{c_2/\lambda T} - 1)}$$

$$E_{b(0-\lambda)} = \int_0^{\lambda} E_{b\lambda} d\lambda$$

$$= 2\pi c_1 \sum_{k=1}^{\infty} \frac{1}{k} e^{-\frac{kc_2}{T\lambda}} \left[\left(\frac{1}{\lambda} \right)^3 + \frac{3T}{\lambda^2 kc_2} + \frac{6}{\lambda} \left(\frac{T}{kc_2} \right)^2 + 6 \left(\frac{T}{kc_2} \right)^3 \right]$$

$$E_{b(\lambda_1 - \lambda_2)} = E_{b(0-\lambda_2)} - E_{b(0-\lambda_1)}$$

where

λ_{\max} is the wavelength of maximum emissivity in microns;

T is the absolute temperature in $^{\circ}\text{R}$ or K;

$E_{b(0-\infty)}$ is the total emissive power in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b\lambda}$ is the emissive power at λ in $\text{Btu/hr-ft}^2\text{-}\mu\text{m}$ or $\text{Watts/cm}^2\text{-}\mu\text{m}$;

$E_{b(0-\lambda)}$ is the emissive power for wavelengths less than λ in Btu/hr-ft^2 or Watts/cm^2 ;

$E_{b(\lambda_1-\lambda_2)}$ is the emissive power for wavelengths between λ_1 and λ_2 in Btu/hr-ft^2 or Watts/cm^2 .

$$\begin{aligned} c_1 &= 1.8887982 \times 10^7 \text{ Btu}\cdot\mu\text{m}^4/\text{hr-ft}^2 \\ &= 5.9544 \times 10^3 \text{ W}\mu\text{m}^4/\text{cm}^2 \end{aligned}$$

$$c_2 = 2.58984 \times 10^4 \mu\text{m}\cdot^{\circ}\text{R} = 1.4388 \times 10^4 \mu\text{m}\cdot\text{K}$$

$$c_3 = 5.216 \times 10^3 \mu\text{m}\cdot^{\circ}\text{R} = 2.8978 \times 10^3 \mu\text{m}\cdot\text{K}$$

$$\sigma = 1.713 \times 10^{-9} \text{ Btu/hr-ft}^2\cdot^{\circ}\text{R}^4 = 5.6693 \times 10^{-12} \text{ W/cm}^2\cdot\text{K}^4$$

$$\sigma_{\text{exp}} = 1.731 \times 10^{-9} \text{ Btu/hr-ft}^2\cdot^{\circ}\text{R}^4 = 5.729 \times 10^{-12} \text{ W/cm}^2\cdot\text{K}^4$$

Program Description II

Sketch(es)

Sample Problem(s) Example 1:

What percentage of the radiant output of a lamp is in the visible range (0.4 to 0.7 microns) if the filament of the lamp is assumed to be a black body at 2400 K? What is the percentage at 2500 K?

Keystrokes:

Outputs:

[f] [B]-----	→	$5.669 \times 10^{-12} \text{ W/cm}^2\text{-K}^4$
2400 [A] .4 [B] .7 [f] [E] [C] [÷] 100 [x]-----	→	2.641%
2500 [A] .7 [f] [E] [C] [÷] 100 [x]-----	→	3.337%

Example 2:

If the human eye was designed to work most efficiently in sunlight and the visible spectrum runs from about 0.4 to 0.7 microns, what is the sun's temperature in degrees Rankine? Assume that the sun is a black body. Using the temperature calculated, find the fraction of the sun's total emissive power which falls in the visible range. Find the percentage of the sun's radiation which has a wavelength less than 0.4 microns.

Keystrokes:

Outputs:

[f] [A]-----	→	$1.713 \times 10^{-9} \text{ Btu/hr-ft}^2\text{-}^\circ\text{R}^4$
Compute mean of visible range.		
.4 [÷] .7 [÷] 2 [÷]-----	→	$550.0 \times 10^{-3} \mu\text{m}$
Compute temperature of sun.		
[B]-----	→	$9.484 \times 10^3 \text{ }^\circ\text{R}$

(continued)

Reference(s)

Robert Siegel and John R. Howell, *Thermal Radiation Heat Transfer*,
Volume 1, National Aeronautics and Space Administration, 1968.

Compute percentage of power in visible range.

[A] .4 [B] .7 ~~[E]~~ [C] [÷] 100 [x]-----→ 33.70 x 10⁰ %

Compute percentage of power under 0.4 microns.

[E] [C] [÷] 100 [x]-----→ **8.433%**

User Instructions

Black Body Thermal Radiation

Eng	SI	Exp	σ	
$T \rightarrow \lambda_{\max}$	$\lambda \rightarrow T(\lambda_{\max})$	$\rightarrow E_b(0-\infty)$	$\rightarrow E_{b\lambda}$	$\lambda' \rightarrow E_b(\lambda-\lambda')$ $E_b(0-\lambda)$

7

REGISTERS

REGISTERS									
0	1	2	3	4	5	6	7	8	9
λ	c_1	c_2	c_3	σ	T	λ, λ'	sum	kc_2/T	
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A		B		C		D		E	
F		G		H		I		J	

97 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	e ^x	33	----- Calculate E _{b(0-λ)} .	169	X ² Y	16-35	----- Calculate E _{b(λ-λ')} .
114	1	01		170	GT01	22 01	
115	-	-45		171	R↓	-31	
116	÷	-24		172	CLX	-51	
117	RTN	24		173	RCL7	36 07	
118	*LBL E	21 15		174	ENT↑	-21	
119	0	00		175	+	-55	
120	ST08	35 08		176	Pi	16-24	
121	ST07	35 07		177	×	-35	
122	*LBL1	21 01		178	RCL1	36 01	
123	R↓	-31	179	×	-35	-----	
124	CLX	-51	180	RTN	24		
125	RCL8	36 08	181	*LBL e	21 16 15		
126	RCL2	36 02	182	ENT↑	-21		
127	RCL5	36 05	183	ENT↑	-21		
128	÷	-24	184	GSBE	23 15		
129	-	-45	185	X ² Y	-41		
130	ST08	35 08	186	RCL6	36 06		
131	3	03	187	ST00	35 00		
132	X ² Y	-41	188	R↓	-31		
133	÷	-24	189	ST06	35 06		
134	RCL6	36 06	190	GSBE	23 15		
135	X ²	53	191	-	-45		
136	÷	-24	192	ABS	16 31		
137	LSTX	16-63	193	RCL0	36 00		
138	1/X	52	194	ST06	35 06		
139	RCL6	36 06	195	R↓	-31		
140	÷	-24	196	RTN	24		
141	-	-45				-----	
142	6	06					
143	RCL6	36 06					
144	÷	-24	200				
145	RCL8	36 08					
146	X ²	53					
147	÷	-24					
148	-	-45					
149	6	06					
150	RCL8	36 08					
151	X ²	53					
152	÷	-24					
153	RCL8	36 08					
154	÷	-24	210				
155	+	-55					
156	RCL8	36 08					
157	RCL6	36 06					
158	÷	-24					
159	e ^x	33					
160	×	-35					
161	RCL8	36 08					
162	÷	-24					
163	ST+7	35-55 07					
164	RCL7	36 07	220				
165	÷	-24					
166	EEY	-23					
167	CHS	-22					
168	5	05					

LABELS					FLAGS	SET STATUS										
A	T→λ _{max}	B	λ→T(λ _{max})	C	E→E _{b(0-∞)}	D	→E _{b-λ}	E	→E _{b(0-λ)}	0		ON OFF		TRIG		DISP
a	Eng	b	SI	c	Exp σ	d		e	λ'→E _{b(λ-λ')}	1		0	<input type="checkbox"/>	DEG	<input checked="" type="checkbox"/>	FIX <input type="checkbox"/>
0		1	E _{b(0-λ)}	2		3		4		2		1	<input type="checkbox"/>	GRAD	<input type="checkbox"/>	SCI <input type="checkbox"/>
5		6		7		8		9		3		2	<input type="checkbox"/>	RAD	<input type="checkbox"/>	ENG <input checked="" type="checkbox"/>
												3	<input type="checkbox"/>			n <u>3</u>

Program Description I

Program Title *Black Hole Characteristics*

Contributor's Name *Geoff Kidd*
 Address *1514 Oxford St #301*
 City *Berkeley*

State *CA*

Zip Code *94709*

Program Description, Equations, Variables

A black hole of mass (M) in grams has a Schwarzschild radius (R_s) in centimeters of:

$$R_s = \frac{2GM}{c^2} = (M) \cdot 1.484986855 \times 10^{-28}$$
 where G is the universal gravitational constant and c is the speed of light.

The lifetime of a black hole (t_L) in seconds is given by:

$$t_L = M^3 \cdot (10^{-28}).$$

The temperature of a black hole (K) in degrees Kelvin is

$$K = 10^{26}/M$$

Operating Limits and Warnings *M must be greater than zero*

Underflow occurs for R_s when $M < 6.734066343 \times 10^{-72}$
 t_L $M < 2.154434653 \times 10^{-24}$

Overflow occurs for K when $M < 1.000000001 \times 10^{-74}$
 t_L $M > 2.154434650 \times 10^{33}$
 M $R_s > 1.484986854 \times 10^{72}$

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s)

- 1.) The sun has a mass 1.99×10^{33} gm. What would be the temperature, Schwarzschild radius, and lifetime of a black hole of that mass?
- 2.) Given a Schwarzschild radius of 6.96×10^{10} cm, what is the mass of the black hole? What is the temperature?

Solution(s) 1.) 1.99 EEX 33 D $\rightarrow 1.9900 \times 10^{33}$
A $\rightarrow 2.9551 \times 10^5$ r_s
B $\rightarrow 5.0251 \times 10^8$ K
C $\rightarrow 7.8806 \times 10^{71}$ t_L

2.) 6.96 EEX 10 A $\rightarrow 6.9600 \times 10^{10}$
D $\rightarrow 4.6869 \times 10^{38}$ M
B $\rightarrow 2.1336 \times 10^{-13}$ K

Reference(s) Harwit, Martin Astrophysical Concepts Wiley, New York

User Instructions

BLACK HOLE CHARACTERISTICS

R_s K t_L M

[illegible]

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	LBL A	31 25 11	Schwarzschild Radius		6	06	
	RF? 3	35 71 03			R X Z y	35 52	$M = \frac{10^{26}}{K}$
	GTO 0	22 00			÷	81	
	1	01		060	STO 3	33 03	
	8	08			RCL 1	34 01	
	4	04	$R_s =$		R RTN	35 22	
	8	08	$M =$		LBL C	31 25 13	Lifetime
	4	04	$1.484986855 \times 10^{-28}$		RF? 3	35 71 03	
	9	09			GTO 0	22 00	
010	8	08			EEX	43	$t_L = M^3 \cdot 10^{-28}$
	6	06			CHS	42	
	8	08			2	02	
	5	05			8	08	
	5	05		070	RCL 3	34 03	
	EEX	43			ENT	41	
	2	02			3	03	
	8	08			R y x	35 63	
	CHS	42			X y	71	
	RCL 3	34 03			STO 2	33 02	
020	X	71			R RTN	35 22	
	STO 0	33 00			LBL 0	31 25 00	if entered value of t_L , compute new mass
	R RTN	35 22			STO 2	33 02	
	LBL 0	31 25 00	if entered value of R_s , compute new mass		EEX	43	
	STO 0	33 00		080	2	02	
	6	06			8	08	
	.	83			X	71	
	7	07			3	03	$M = \sqrt[3]{t_L \cdot 10^{28}}$
	3	03	$M =$		R 1/x	35 62	
	4	04	$R_s \cdot 6.734066344 \times 10^{27}$		R 4 x	35 63	
030	0	00			STO 3	33 03	
	6	06			RCL 2	34 02	
	6	06			R RTN	35 22	
	3	03			LBL D	31 25 14	Mass
	4	04		090	RF? 3	35 71 03	
	4	04			GTO 0	22 00	
	EEX	43			RCL 3	34 03	
	2	02			R RTN	35 22	
	7	07			LBL 0	31 25 00	if new value not entered, display old. Else store value entered.
	X	71			STO 3	33 03	
040	STO 3	33 03			R RTN	35 22	
	RCL 0	34 00			R/S	84	
	R RTN	35 22					
	LBL B	31 25 12	Temperature				
	RF? 3	35 71 03		100			Flags 0-4 off
	GTO 0	22 00	$K = 10^{26}/M$				deg mode
	EEX	43					SCI
	2	02					DSP 4
	6	06					are initial values
	RCL 3	34 03					
050	÷	81					Labels used:
	STO 1	33 01					A, B, C, D, O
	R RTN	35 22					
	LBL 0	31 25 00	if entered value of K , compute new mass	110			
	STO 1	33 01					
	EEX	43					
	2	02					

REGISTERS

0	R _s	1	K	2	t _L	3	M	4		5		6		7		8		9
S0		S1		S2		S3		S4		S5		S6		S7		S8		S9
A		B		C		D		E		F		G		H		I		J

Program Description I

Program Title SPECIAL RELATIVITY CONVERSIONS
Contributor's Name Ctein
Address 298 Vista Grande
City Daly City **State** Ca **Zip Code** 94014

Program Description, Equations, Variables This program provides relativistic conversions between the following quantities: rest mass (m); velocity (v , in units of $c=1$); energy (E), and momentum (P). Given any two it is possible to find the two unknowns by the following equations:

$$\begin{aligned}
 \text{(I)-- } E &= m/\text{SQRT}(1-v^2) \quad // \quad \text{(II)-- } E = \text{SQRT}(P^2 + m^2) \quad // \quad \text{(III)-- } E = P/v \\
 \text{(IV)-- } P &= vE \quad // \quad \text{(V)-- } P = \text{SQRT}(E^2 - m^2) \quad // \quad \text{(VI)-- } v = P/E \quad // \quad \text{(VII) } m = \text{SQRT}(E^2 - P^2)
 \end{aligned}$$

Data may be entered in any order and recalled at any time. The program scans the registers and, after determining if there is enough data to solve for the unknown, selects the appropriate subset of equations. If insufficient data, then the program displays Error. The following selection patterns are used:

TO FIND:	v	m	E	P
GIVEN:	m, E	v, E	v, m	v, E
	use V, VI	use IV, VII	use I	use IV
	m, P	v, P	v, P	v, m
	use II, VI	use III, VII	use III	use I, IV
	E, P	E, P	m, P	m, E
	use VI	use VII	use II	use V

Because of the complexity of this program, a chart is provided on the next page which diagrams the access patterns used by each labeled subsection. Boxes are used to represent direct jumps, and circles represent subroutine calls. The user is advised to review this carefully before modifying this program.

Operating Limits and Warnings

all data must be positive. Velocity must be less than 1. ERROR message will be displayed if a real solution does not exist or the input data is outside these limits.

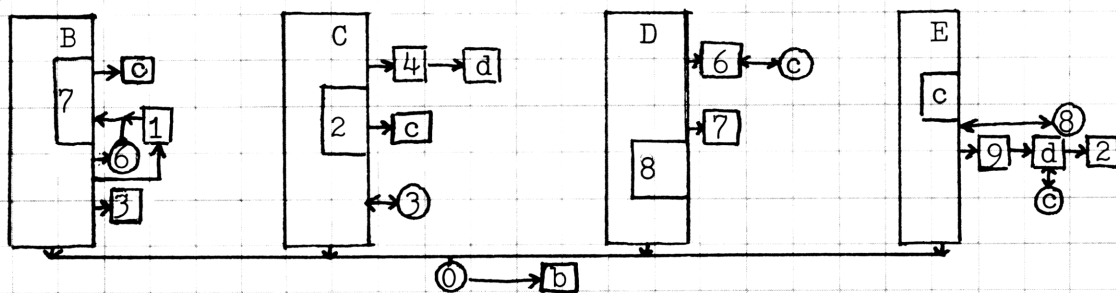
This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Special Relativity

Sketch(es)



Sample Problem(s)

- 1) Find the velocity and momentum of an electron ($m = .511 \text{ MeV}$) with a total energy of 1.0 MeV .
- 2) Given an E of 500 MeV and a P of 498 MeV/c , what is the particle's mass and velocity.
- 3) At $.9c$, an electron has an energy of 1.1723 MeV . Find its rest mass and momentum.
- 4) An electron is traveling at $.3c$. Find its momentum and energy.

Solution(s)

- 1) A , .511, C, 1, D, B, $v = .8596c$; E, $P = .8596 \text{ MeV/c}$.
- 2) A , 500, D, 498, E, B, $v = .996c$; C, $m = 44.6766 \text{ MeV}$
- 3) A , .9, B, 1.1723, D, C, $m = .511 \text{ MeV}$; E, $P = 1.0551 \text{ MeV/c}$
- 4) A , .3, B, .511, C, D, $E = .5357 \text{ MeV}$; E, $P = .1607 \text{ MeV/c}$

Reference(s) HP-65 library program #308 by this author.

15

[illegible]

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS		
001	*LBL A	31 25 11	RESET		*LBL 8	31 25 08	v in X		
	CL REG	31 43			x↔y	35 52			
	CF 3	35 61 03			asin	32 62	SQRT(1-v ²)		
	R/S	84		060	cos	31 63			
	*LBL B	31 25 12	FIND/STORE v		/	81	eq.I gives E		
	1	01			RTN	35 22			
	GSB 0	31 22 00	store new v		*LBL E	31 25 15	FIND/STORE P		
	RCL 2	34 02	m		4	04			
	x=0?	31 51	if m is unknown		GSB 0	31 22 00	store new P		
	GTO 1	22 01	then go to 1		x=0?	31 51	if v is unknown		
010	RCL 3	34 03	E		GTO 9	22 09	then go to 9.		
	x≠0?	31 61	if E,m are known		RCL 2	34 02	if m,v known,		
	GTO 3	22 03	then go to 3		x≠0?	31 61	then eq.I gives		
	GSB 6	31 22 06	eq.II gives E	070	GSB 8	31 22 08	E.		
	ENTER	41			RCL 3	34 03	If R ₃ contains		
	*LBL 7	31 25 07			x=0?	31 51	E(i.e.≠0), then		
	R ↓	35 53			R ↓	35 53	this takes prior-		
	RCL 4	34 04	P		RCL 1	34 01	ity.		
	x↔y	35 52	E		x	71	eq.IV gives P		
020	/	81	eq. VI gives v		*LBL c	32 25 13	-----		
	GTO c	22 31 13	check out P		x=0?	31 51	if variable or		
	*LBL C	31 25 13	FIND/STORE m		/	81	result is not		
	2	02			RTN	35 22	legitimate,end.		
	GSB 0	31 22 00	store new m	080	*LBL 0	31 25 00	check/store 'x'		
	x=0?	31 51	if v is unknown		ST I	35 33	store (i)		
	GTO 4	22 04	then go to 4		F? 3	35 71 03	if data has been		
	RCL 3	34 03	E		GTO b	22 31 12	entered,go to b		
	x	71	eq.IV gives P		RCL(i)	34 24	check contents		
	LST x	35 82	E		x≠0?	31 61	of register 'x'		
030	x≠0?	31 61	if E is known,		R/S	84	and display if		
	GTO 2	22 02	go to 2		RCL 1	34 01	good. Otherwise		
	RCL 4	34 04	P		RTN	35 22	RCL v and return		
	ENTER	41			*LBL b	32 25 12	STORE NEW "x"		
	ENTER	41		090	R ↓	35 53	in register defi-		
	RCL 1	34 01	v		STO(i)	33 24	ned by (i)		
	/	81	eq.III gives E		R/S	84			
	*LBL 2	31 25 02	eq. V or VII		*LBL 1	31 25 01	FIND v;m UNKNOWN		
	ENTER	41			RCL 3	34 03	E		
	R ↓	35 53			ENTER	41	eq.VI gives v		
040	GSB 3	31 22 03	SQRT(x ² -y ²)		GTO 7	22 07	FIND m;v UNKNOWN		
	R ↑	35 54			*LBL 4	31 25 04	P		
	x	71	eq.VII gives m		RCL 4	34 04	go to d		
	GTO c	22 31 13	check for valid		GTO d	22 31 14	EQ. II		
	*LBL 3	31 25 03	results	100	*LBL 6	31 25 06	m		
	/	81	find		RCL 2	34 02	check validity		
	asin	32 62	SQRT(1-y ² /x ²)		GSB c	32 22 13	P		
	cos	31 63			RCL 4	34 04	check validity		
	RTN	35 22			GSB c	32 22 13	E=SQRT(m ² +P ²)		
	*LBL D	31 25 14	FIND/STORE E		R→P	32 72			
050	3	03			RTN	35 22	FIND P:v UNKNOWN		
	GSB 0	31 22 00	store new E		*LBL 9	31 25 09	m		
	x=0?	31 51	if v is unknown		RCL 2	34 02	-----		
	GTO 6	22 06	then go to 6.		*LBL d	32 25 14	check validity		
	RCL 2	34 02	if m is unknown	110	GSB c	32 22 13	E		
	x=0?	31 51	then go to 7.		RCL 3	34 03	eq.V orVII		
	GTO 7	22 07			GTO 2	22 02			
REGISTERS									
0	velocity ² mass		3energy	4momentum	5	6	7	8	9
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A		B	C		D		E	I used	

Program Description I

Program Title Three Dimensional Special Relativity

Contributor's Name William C. Wickes

Address Princeton University, Department of Physics

City Princeton

State N.J.

Zip Code 08540

Program Description, Equations, Variables

- Given the components of any 4-vector, in particular $x'^{\mu} = (x', y', z', ct')$ or $p'^{\mu} = (p'^x, p'^y, p'^z, E')$, calculate the components x^{μ} or p^{μ} in a frame in which the original frame C is moving with velocity $\vec{\beta} = (\beta^x, \beta^y, \beta^z)$.
 \vec{p} = momentum
 E = total energy
 $\vec{\beta} = \vec{v}/c$ \vec{v} = velocity

- For any $\vec{\beta}$, calculate the time-dilation/length contraction factor γ .

- For a 4-vector Δx^{μ} connecting any two space-time events, calculate the invariant interval $c\Delta\tau$.

Formulae:

$$\Delta\vec{x} = \Delta\vec{x}' + \vec{\beta}[(\gamma-1)\frac{\vec{\beta}\cdot\vec{x}'}{\beta^2} + \gamma c\Delta t']$$

$$\Delta t = \gamma(t + \vec{\beta}\cdot\vec{x}/c^2)$$

$$\gamma = [1-\beta^2]^{-1/2}$$

$$\beta = |\vec{\beta}| = [\beta^x^2 + \beta^y^2 + \beta^z^2]^{1/2}$$

$$|\Delta\vec{x}| = [\Delta x^2 + \Delta y^2 + \Delta z^2]^{1/2}$$

$$c^2\Delta\tau^2 = c^2\Delta t^2 - |\Delta\vec{x}|^2$$

The coordinate frames are assumed to be synchronized so that the event (0,0,0,0) has the same coordinates in both frames.

Operating Limits and Warnings

For a spacelike interval, $c^2\Delta\tau^2 < 0$, the calculator will display " - |c\Delta\tau|"

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19

[illegible]

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS			
001	LBL D	31 25 14	Compute $\sum x_i^2$		LST X	35 82	$1/\beta$			
	RCL 6	34 06			STO 1	33 01				
	F? 0	35 71 00			X \div Y	35 52				
	GTO 4	22 04		060	F? 1	35 71 01				
	RCL 4	34 04			GTO 6	22 06				
	R \rightarrow P	32 72			R \uparrow	35 54				
	F? 1	35 71 01			STO 2	33 02				
	GTO 4	22 04			R \rightarrow P	32 72				
	RCL 5	34 05			LBL 6	31 25 06				
010	R \rightarrow P	32 72			STO A	33 11				
	LBL 4	31 25 04	$c^2t^2 - x^2$		COS ⁻¹	32 63	$\sqrt{1-\beta^2}$			
	X ²	32 54			SIN	31 62				
	RCL 7	34 07			1/X	35 62				
	X ²	32 54		070	STO B	33 12		γ		
	-	51			RCL A	34 11			DISPLAY β	
	CHS	42			-X-	31 84				
	X<0	31 71			X \div Y	35 52				
	SFO	35 51 02		SPACE LIKE?	RTN	35 22				
	ABS	35 64		SFO	LBL B	31 25 12				
020	\sqrt{X}	31 54			STO 7	33 07				STO β
	F? 2	35 71 02		R \downarrow	35 53					
	CHS	42	- for SPACE LIKE	STO 6	33 06					
	RTN	35 22		R \downarrow	35 53					
	LBL Q	32 25 11	Calculate β	080	STO 4	33 04				
	STO B	33 12	from γ	R \downarrow	35 53	$X^{1.4} \rightarrow X^{1.4}$ $\beta \cdot X^1$				
	X ²	32 54		STO 5	33 05					
	1/X	35 62		RTN	35 22					
	1	01		LBL C	31 25 13					
	-	51		GSB E	32 22 15					
030	CHS	42		RCL A	34 11					
	\sqrt{X}	31 54		X ²	32 54					
	STO A	33 11		\div	81					
	RTN	35 22		RCL B	34 12					
	LBL E	32 25 15	Compute $\beta \cdot X^1$ $= \sum \beta^i x^i$	090	1		01			
	RCL 6	34 06			-	51				
	RCL 3	34 03			X	71				
	X	71			RCL B	34 12				
	F? 3	35 71 00			RCL 7	34 07				
	RTN	35 22			X	71				
040	RCL 1	34 01			+	61				
	RCL 4	34 04			STO C	33 13				
	X	71			3	03				
	+	61			STO 0	33 00				
	F? 1	35 71 01		100	ST I	35 33	USE R0 AS COUNTER Compute one component each cycle			
	RTN	35 22		LBL 0	31 25 00					
	RCL 2	34 02		RCL 0	34 00					
	RCL 5	34 05		ST I	35 33					
	X	71		RCL C	34 13					
	+	61		RCL (1)	34 24					
050	RTN	35 22		X	71					
	LBL A	31 25 11	Compute γ	RCL I	35 34					
	STO 3	33 03			3	03				
	F? 0	35 71 00			+	61				
	GTO 6	22 06			110	ST I	35 33			
	X \div Y	35 52			CLX	44				
	R \rightarrow P	32 72			RCL (1)	34 24				
REGISTERS										
0 Counter	1 β^4	2 β^2		3 β^3	4 y	5 x	6 z	7 ct	8	9
S0	S1	S2		S3	S4 y'	S5 x'	S6 z'	S7 ct'	S8	S9
A β		B γ		C		D		E		
								I USED		

21

[illegible]

Program Description I

Program Title Einsteins Twin Paradox

Contributor's Name David M. Weingold

Address % Synergy Research P.O. Box 372

City Woodmere

State N.Y.

Zip Code 11598

Program Description, Equations, Variables

The program is arranged to calculate subjective and real time differential between an observer on Earth and the pilot of a vehicle accelerating near the speed of light. If you imagine twins at age 21. One becomes an astronaut and volunteers for the first interstellar flight. He takes off and travels at a ponderous speed of say 2.994444444×10^8 meters per second. In this situation it is accurate enough to call C the speed of light, 3×10^8 . The astronaut travels for what he measures to be a year well past the sun at which time he fires retro and navigational engines, and turns around and heads toward Earth; the journey naturally takes another year. He is now 23 years old but when he steps from the ship his twin is over 37 years old! That over 16 years had passed on Earth. The explanation as to why this happened involves very complicated non Euclidian geometry and relativistic considerations of accelerating frame of reference too complicated for this discussion, it suffices to say that in the event of tremendous accelerations such as the turning around of a space craft traveling near the speed of light that the order of magnitude of energy involved is extremely large and the consideration of it as it interrelates to space as time is conceived as a fourth physical

Operating Limits and Warnings

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description I

Program Title Einsteins Twin Paradox
Contributor's Name David M. Weingold
Address % Synergy Research P.O. Box 372
City Woodmere **State** New York **Zip Code** 11598

Program Description, Equations, Variables

dimension of space, the Universe is then conceived as a giant four dimensional sphere with a three dimensional surface. The space craft in its turning travels relative to the Earth, not as far along that fourth dimension and hence the differential between the twins age. The equations for this case are quite simple and adequate for this case. They consist primarily of the Lorentz transform i.e., $\sqrt{1 - \frac{v^2}{c^2}}$, where v is the velocity of the space craft relative to the Earth, and c is the universal constant, 3×10^8 meters per second, the speed of light. The program inputs consist of speed of space craft in meters per second, time passed on Earth, time passed on board the craft, and the ages of the twins before the flights. With input T_E , time passed on Earth, the equation $T_S = T_E \sqrt{1 - \frac{v^2}{c^2}}$ gives T_S , ["time passed on board"] ship during journey. Input T_S , time passed on board ship, and the equation: $T_E = \frac{T_S}{\sqrt{1 - \frac{v^2}{c^2}}}$ gives you T_E , ["time passed on Earth"] during journey. The label A clears and initiates the program. Lbl B is the input for average velocity of the craft. Lbl C is the input for time passed on earth in years and outputs time passed on board ship by hitting FC Lbl D input time passed on board ship FD give appropriate time passed on earth the E's give ages.

Operating Limits and Warnings

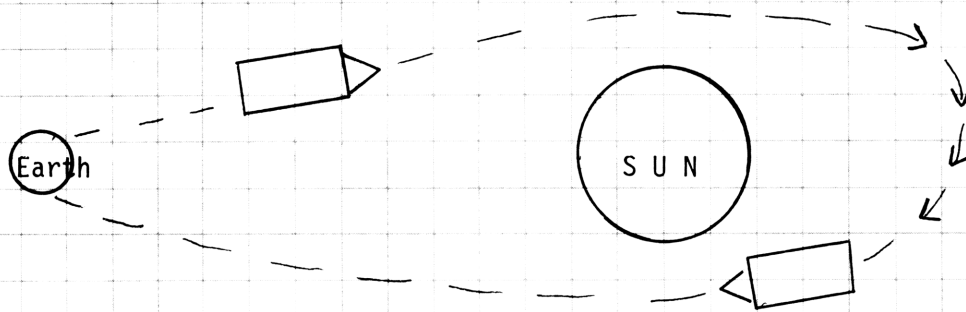
Be certain that you enter the speed of the space craft in meters per second. All time and age entries must be in years. Outputs will be in years. Do not try to make the space travel at the speed of light, $\approx (3.00 \times 10^8 \text{ meters/second})$ as this will only show an error as should be and is implied by the theory of relativity.

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Program Description II

Sketch(es)



Sample Problem(s) Suppose two twins, age thirty, take part in this experiment the velocity of the ship will average 2.999111111×10^8 , if the twin on board travels a total of one year how much time will have passed on Earth? And given that 25 years passes on earth before return of the ship, how much time passed on board? What was the age differential in both cases?

Solution(s) Load side 1 and side 2
 [A] -----> -9.00×10^{16}
 2.999111111 [EEX] 8 [B]
 1 [D] [f] [D] -----> 41.08 years passed on Earth
 30 [E] -----> 71 twin on Earth's age
 Age differential is 40 years (71-31)
 [A]
 2.999111111 [EEX] 8 [B]
 25 [C] [f] [C] -----> .6085 years passed in space

30 [f] [E] -----> 30.6085 twin on board's age
 Age differential is 24.3015 (55-30.6085)

REFERENCE (S) Introduction to Special Relativity by James H. Smith (chp. 6)
 W.A. Benjam Inc., New York, Amsterdam 1965.

25



Always enter time in years, and speed in mtrs. per second, to go to new case i.e., new speed or different amounts of time or ages*. Hit [A], and then continue from step #3 with new values.

A Initiate	B Avg Ship Vel Ent	C 1. passed on Earth Ent	D 1. passed in space Ent	E Earth Twin F. age
a $\sqrt{1 - \frac{v^2}{c^2}}$ routine	b	c Earth T. to ship T.	d Space T. to Earth T.	e Space twin F. age
0	1	2	3	4
5	6	7	8	9

97 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	X	-35	
002	CLRG	16-53		058	RCL1	36 01	Enter Time
003	SCI	-12		059	X	-35	Passed in Space
004	DSP9	-63 09		060	RCL2	36 02	CONVERT from
005	CLX	-51	initiate	061	X	-35	Years To Seconds
006	3	03	store constants	062	STOD	35 14	store in RD
007	6	06	Clear Registers	063	RTN	24	
008	0	00	Find C ² and store	064	*LBLd	21 16 14	
009	0	00	in RA.	065	RCLD	36 14	Calculate
010	STO0	35 00		066	GSO0	23 00	$T_E = \frac{T_s}{\sqrt{1 - \frac{v^2}{c^2}}}$
011	2	02		067	+	-24	
012	4	04		068	RCL0	36 00	Store in R4
013	STO1	35 01		069	+	-24	
014	3	03		070	RCL1	36 01	
015	6	06		071	+	-24	
016	5	05		072	RCL2	36 02	
017	.	-62		073	+	-24	
018	2	02		074	STO4	35 04	
019	5	05		075	PSE	16 51	
020	STO2	35 02		076	SPC	16-11	
021	3	03		077	PRTX	-14	
022	EEX	-23		078	RTN	24	
023	2 ⁸	08		079	*LBL0	21 00	
024	X	53		080	RCLB	36 12	
025	STOA	35 11		081	RCLA	36 11	
026	RTN	24		082	+	-24	
027	*LBLB	21 12	Enter ship Avg. Velocity	083	CHS	-22	
028	X ²	53	Square and Store	084	1	01	
029	STOB	35 12	in RB	085	+	-55	
030	RTN	24		086	VX	54	
031	*LBLC	21 13		087	RTN	24	
032	RCL0	36 00	Enter Time Passed	088	*LBLE	21 15	
033	X	-35	ON Earth in years	089	RCL4	36 04	
034	RCL1	36 01	convert To Seconds	090	+	-55	
035	X	-35	Store in RC	091	PSE	16 51	
036	RCL2	36 02		092	SPC	16-11	
037	X	-35		093	PRTX	-14	
038	STOC	35 13		094	RTN	24	
039	RTN	24		095	*LBLe	21 16 15	
040	*LBLC	21 16 13		096	RCL3	36 03	
041	RCLC	36 13	Calculate	097	+	-55	
042	GSO0	23 00	$T_s = T_E \sqrt{1 - \frac{v^2}{c^2}}$	098	PSE	16 51	
043	X	-35	Store R3	099	SPC	16-11	
044	RCL0	36 00		100	PRTX	-14	
045	+	-24		101	RTN	24	
046	RCL1	36 01	Space and Print		R/S	51	
047	+	-24					
048	RCL2	36 02					
049	+	-24					
050	STO3	35 03					
051	PSE	16 51					
052	SPC	16-11					
053	PRTX	-14					
054	RTN	24					
055	*LBLD	21 14					
056	RCL0	36 00					

REGISTERS

0	3600	1	24	2	365.25	3	T _s	4	T _E	5		6		7		8		9	
S0		S1		S2		S3		S4		S5		S6		S7		S8		S9	
A	C ²	B	V ²	C time passed Earth in sec.				D time passed rocket in sec.				E				I			

Program Description I

Program Title Delta-V - Orbit Simulator

Contributor's Name Harold T. Coderre

Address 414 1915 Hall

City Princeton

State New Jersey

Zip Code 08540

Program Description, Equations, Variables This program calculates orbit parameters from initial position and velocity data both for elliptical and hyperbolic orbits in a plane. It is also possible to move the point of interest to anywhere along the orbit and then recalculate orbit parameters.

Equations Used:

$$\text{Energy: } E = \frac{1}{2} V_i^2 - \frac{GM}{R_i}$$

$$\text{Angular Momentum: } L = V R \sin(\alpha_i - \theta_i)$$

$$\text{Eccentricity: } e = \sqrt{1 + \frac{L^2 E^2}{(GM)^2}}$$

$$R_0 = \frac{L^2}{GM}$$

$$\theta' = \theta_i + \cos^{-1}\left(\frac{R_0}{R_i} - 1\right)$$

$$R_{\min} = R_0 / (1 + e)$$

$$\text{Semimajor Axis: } a = R_0 / (1 - e^2)$$

$$\text{Semiminor Axis: } b = a \sqrt{1 - e^2}$$

$$\text{Period: } T = 2\pi \sqrt{\frac{a^3}{GM}}$$

$$\text{Distance to Asymptote Vertex } S = R_{\min} (1 - \frac{1}{e})$$

$$\text{Angle between Asymptotes and } \theta_a = \cos^{-1}\left(\frac{1}{e}\right)$$

Radius Vector

Given θ_{new} :

$$R_{\text{new}} = R_0 / (1 + e \cos(\theta_{\text{new}} - \theta'))$$

$$V_{\text{new}} = \sqrt{2(E + \frac{GM}{R_{\text{new}}})}$$

$$\alpha_{\text{new}} = \theta_{\text{new}} + \sin^{-1}\left(\frac{L}{V_{\text{new}} R_{\text{new}}}\right)$$

For a change in Velocity

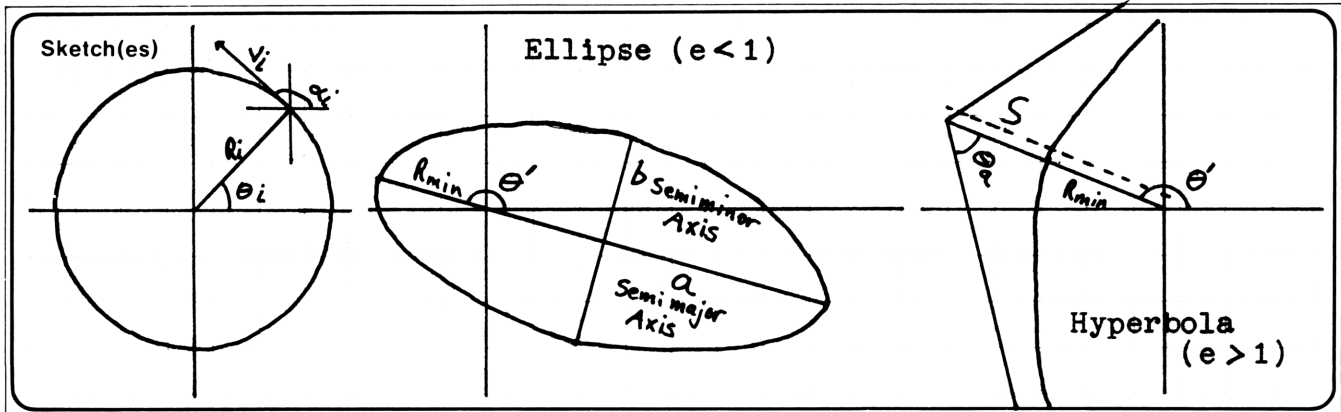
$$\vec{V}_{\text{new}} = \vec{V}_{\text{old}} + \Delta \vec{V}$$

Operating Limits and Warnings All angles should be $0 \leq \theta \leq 360$. If $\hat{\theta}$ (A) gives a negative radius for a hyperbolic orbit ($e > 1$) the orbit does not exist for the inputted θ . This program becomes ill-conditioned and inaccurate near degenerate conics (Circles, Parabolas and Straight lines). For added realism: avoid all orbits where $R_{\min} < \text{radius of the attracting body}$ (6.400×10^6 m for the Earth).

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Program Description II



Sample Problem(s) Execute a transfer from Low Earth Orbit to Geosynchronous

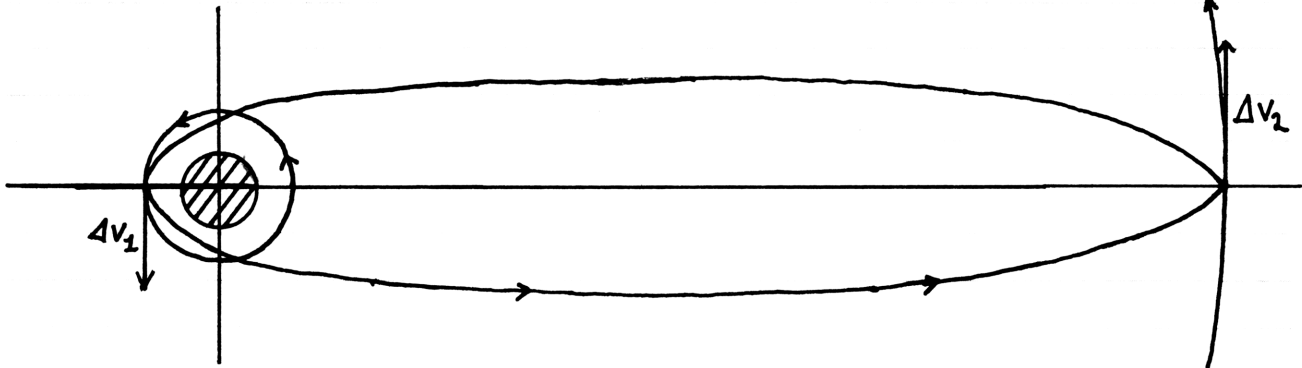
Step 1: Initialize $R_i = 7.1E6$ $\theta_i = 0$ $V_i = 7.4E3$ $\alpha_i = 90$

Step 2: Position Satellite at Perigee

Step 3: Accelerate to Synchronous Transfer

Step 4: Position Satellite at new Apogee

Step 5: Circularize



Solution(s) Keystrokes: (all underlined numbers are machine output)

Step 1: 7.10E6 ENT 0 F A

7.40E3 ENT 90 F B

Step 2: D 180.0 A 6.7462E6

Step 3: 2312 RCL 3 B 270.0

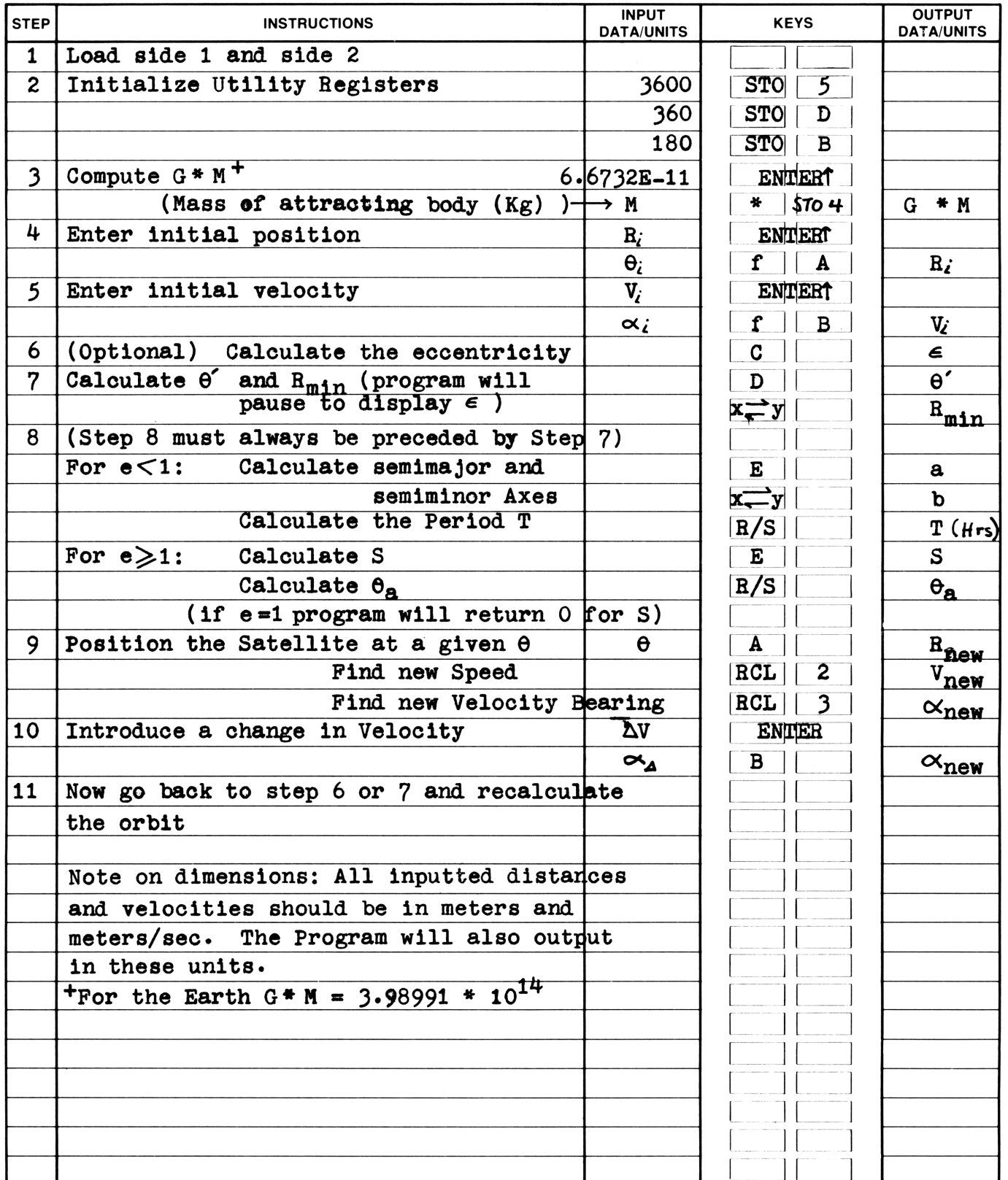
Step 4: D 180.0 180 + A 4.228688E7

Step 5: 1455 RCL 3 B 90.0 C 3.505809E-3 E 4.213916E7

R/S 23.90148 H→H.MS 23.54053 *****

Reference(s) Goldstein: Classical Mechanics Chapt 3

29



Note: All quantities listed below are per kilogram

Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS			
001	LBL a	32 25 11	67		RCL 8	34 08				
	STO 1	33 01			\div	81				
	$x \rightarrow y$	35 52			GSB d	32 22 14				
	STO 0	33 00		060	COS-1	32 63				
	RTN	35 22			RCL 3	34 03				
	LBL b	32 25 12			RCL 1	34 01				
	STO 3	33 03			-	51				
	$x \rightarrow y$	35 52			COS	31 63				
	STO 2	33 02			LST X	35 82				
010	SF 1	35 51 01			SIN	31 62				
	RTN	35 22			*	71				
	LBL C	31 25 13			$x < 0$	31 71				
	RCL 2	34 02			GTO 7	22 07				
	X**2	32 54		070	R↓	35 53				
	2	02			CHS	42				
	\div	81			R↑	35 54				
	RCL 4	34 04			LBL 7	31 25 07				
	RCL 0	34 00			R↓	35 53				
	\div	81			+	61				
020	-	51			GSB e	32 22 15				
	STO 6	33 06	→ ENERGY	STO A	33 11	→ θ'				
	RCL 3	34 03		CLF 1	35 61 01					
	RCL 1	34 01		RCL 8	34 08					
	-	51		RTN	35 22					
	SIN	31 62		080	LBL D	31 25 14				
	RCL 0	34 00		TF 1	35 71 01					
	*	71		GSB C	31 22 13					
	RCL 2	34 02		RCL 8	34 08					
	*	71		Pause	35 72					
030	STO 7	33 07	→ ANGULAR MOMENTUM	1	01					
	X**2	32 54		+	61					
	2	02		1/X	35 62					
	*	71		RCL 9	34 09					
	RCL 6	34 06		090	*	71	→ R _{min}			
	*	71		STO C	33 13					
	RCL 4	34 04		RCL A	34 11					
	X**2	32 54		RTN	35 22					
	\div	81		LBL E	31 25 15					
	1	01		TF 0	35 71 00					
040	+	61		GTO 2	22 02					
	\sqrt{x}	31 54		RCL 9	34 09	ellipse section				
	STO 8	33 08	→ ECCENTRICITY	1	01					
	1	01		RCL 8	34 08					
	CLF 0	35 61 00		100	X**2	32 54				
	$x \leq y$	32 71		-	51					
	STF 0	35 51 00		\div	81					
	RCL 1	34 01		STO E	33 15	→ Semimajor Axis				
	RCL 7	34 07		LST X	35 82					
	X**2	32 54		\sqrt{x}	31 54					
050	RCL 4	34 04		*	71	→ Semiminor Axis				
	\div	81		RCL E	34 15					
	STO 9	33 09	→ R ₀	R/S	84					
	RCL 0	34 00		RCL E	34 15					
	\div	81		110	X**2	32 54				
	1	01		LST X	35 82					
	-	51		*	71					
REGISTERS										
0	Dist	1 BEARING	2 Speed	3 Speed Bearing	4 G * M	5 3600	6 Energy	7 A. M.	8 e	9 R ₀
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9	
A	θ'	B 180	C R _{min}	D 360	E a	I				

67 Program Listing II

31

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS	
	RCL 4	34 04			RCL 1	34 01		
	\div	81						
	\sqrt{x}	31 54						
	2	02						
	*	71						
	π	35 73						
	*	71						
120	RCL 5	34 05						
	\div	81						
	RTN	35 22						
	LBL 2	31 25 02	Hyperbola Section	170	RCL A	34 11		
	RCL C	34 13						
	1	01						
	RCL 8	34 08						
	1/X	35 62						
	-	51		-	51			
	$x \neq 0$	31 61	Output Zero for a Parabola		SIN	31 62		
130	GTO 3	22 03						
	RTN	35 22						
	LBL 3	31 25 03						
	\div	81						
	R/S	84	→ S		*	71		
	RCL 8	34 08			x > 0	31 81		
	1/X	35 62			GTO 4	22 04		
	COS ⁻¹	32 63	→ θ_a		CLX	44		
	RTN	35 22			RCL B	34 12		
	LBL A	31 25 11		180	-	51		
140	STO 1	33 01						
	RCL A	34 11						
	-	51						
	COS	31 63						
	RCL 8	34 08						
	*	71						
	1	01						
	+	61						
	RCL 9	34 09						
	\div	81		CHS	42			
150	1/X	35 62	→ R _{new}		R↑	35 54		
	STO 0	33 00						
	RCL 4	34 04						
	$x \Rightarrow y$	35 52						
	\div	81						
	RCL 6	34 06		LBL 4	31 25 04			
	+	61		$\rightarrow R$	35 53			
	2	02		RCL 1	34 01			
	*	71		+	61			
	\sqrt{x}	31 54		GSB e	32 22 15			
160	STO 2	33 02	→ V _{new}		STO 3	33 03		
	RCL 7	34 07						
	RCL 0	34 00						
	RCL 2	34 02						
	*	71						
	\div	81		RCL 0	34 00			
	GSB d	32 22 14		RTN	35 22			
	SIN ⁻¹	32 62		LBL B	31 25 12			
	RCL 7	34 07		190	$x \Rightarrow y$	35 52		
					→ R	31 72		
					RCL 3	34 03		
					RCL 2	34 02		
					→ R	31 72		
					$x \Rightarrow y$	35 52		
					$\rightarrow R$	35 53		
					+	61		
					R↓	35 53		
					+	61		
				200	R↑	35 54		
					→ P	32 72		
					STO 2	33 02		
					$x \Rightarrow y$	35 52		
					GSB e	32 22 15		
					STO 3	33 03		
					SF 1	35 51 01		
					RTN	35 22		
					LBL e	32 25 15		
					RCL D	34 14		
				210	\div	81		
					FRAC	32 83		
					1	01		
					+	61		
					FRAC	32 83		
					RCL D	34 14		
					*	71		
					RTN	35 22		
					LBL d	32 25 14		
					INT	31 83		
				220	$x \neq 0$	31 61		
					RTN	35 22		
					CLX	44		
					LST X	35 82		
					RTN	35 22		
LABELS				FLAGS		SET STATUS		
A $\hat{\theta}$	B $\Delta \vec{V}$	C \in	D 0, R _{min}	E Graph	0 $e \geq 1$	SET STATUS		
a \vec{R}_1	b \vec{V}_1	c	d Adjust	e Mod 360	1 Find e	FLAGS	TRIG	DISP
0	1	2 -used-	3 -used-	4 -used-	2	ON OFF	DEG <input checked="" type="checkbox"/>	FIX <input type="checkbox"/>
						0 <input type="checkbox"/> <input checked="" type="checkbox"/>	GRAD <input type="checkbox"/>	SCI <input checked="" type="checkbox"/>
						1 <input type="checkbox"/> <input checked="" type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
5	6	7 -used-	8	9	3	2 <input type="checkbox"/> <input checked="" type="checkbox"/>		n <u>6</u>
						3 <input type="checkbox"/> <input checked="" type="checkbox"/>		

Program Description I

Program Title EQUATIONS OF PARTICLE MOTION

Contributor's Name ERIK GOETZE

Address 1613 CAMULOS AVE.

City GLENDALE

State CALIF

Zip Code 91208

Program Description, Equations, Variables HERE ALL VARIABLES ARE IN y, BUT ALL y's COULD BE REPLACED WITH x's.

nr1 $y = \frac{1}{2}(V_{y0} + V_y)t$

nr2 $y = V_{y0}t + \frac{1}{2}a_y t^2$ $V_{y0} = V_y - a_y t$ [nr10]

nr3 $y = \frac{V_y^2 - V_{y0}^2}{2a_y}$ $V_{y0} = \frac{2y}{t} - V_y$ [nr11]

nr4 $t = \frac{V_y - V_{y0}}{a_y}$ $V_{y0} = \frac{y}{t} - \frac{a_y t}{2}$ [nr12]

nr5 $t = \frac{2y}{V_{y0} + V_y}$ $V_{y0} = \sqrt{V_y^2 - 2a_y y}$ [nr13]

nr6 $t = \frac{-V_{y0} \pm \sqrt{V_{y0}^2 + 2a_y y}}{a_y}$

nr7 $V_y = V_{y0} + a_y t$ $a_y = \frac{V_y - V_{y0}}{t}$ [nr14]

nr8 $V_y = \frac{2y}{t} - V_{y0}$ [nr15] $a_y = 2 \left(\frac{y - V_{y0}t}{t^2} \right)$

nr9 $V_y = \sqrt{V_{y0}^2 + 2a_y y}$ [nr16] $a_y = \frac{V_y^2 - V_{y0}^2}{2y}$

y = DISTANCE COVERED BY PARTICLE IN TIME t

t = TIME IN WHICH PARTICLE MOVES

V_y = VELOCITY AT TIME t

V_{y0} = VELOCITY AT TIME 0

a_y = ACCELERATION (AVERAGE OVER TIME t) THAT PARTICLE IS EXPERIENCING IN TIME t

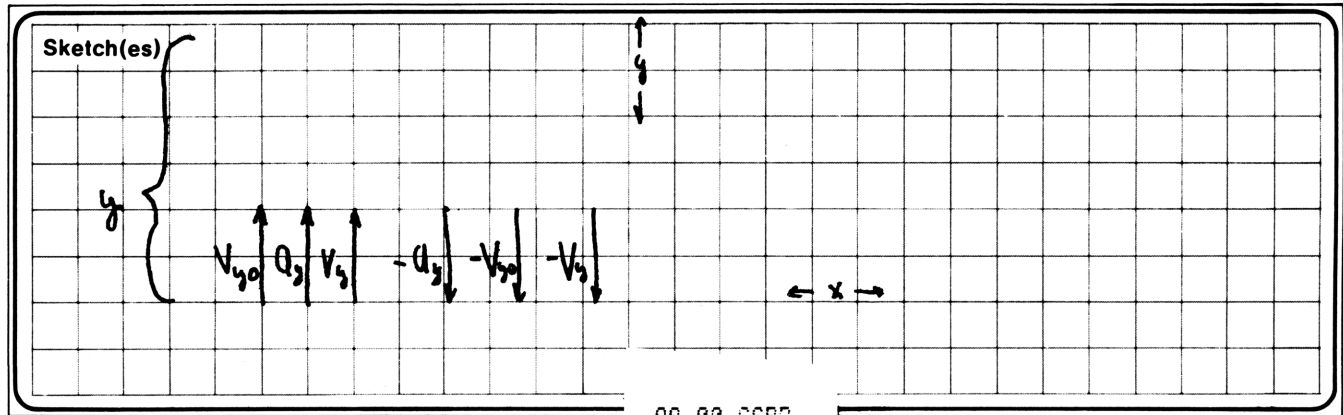
PROGRAM, GIVEN ANY THREE OUT OF THE ABOVE FIVE, WILL SOLVE THE ABOVE EQUATIONS FOR THE OTHER TWO.

Operating Limits and Warnings IF YOU ARE SOLVING FOR V-INITIAL, YOU MUST STORE THE VALUE YOU GET BY PRESSING [D] BEFORE SOLVING FOR THE OTHER UNKNOWN. THIS IS BECAUSE V_{y0} IS IN ALL THE OTHER EQUATIONS. IF THE DISPLAY COMES UP ERROR WHEN YOU ARE SOLVING FOR t , YOU HAVE AN IMAGINARY ROOT. SIMPLY SWITCH TO PROGRAM MODE, PRESS [SST] AND SWITCH BACK TO RUN AND PRESS [R/S]

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II



Sample Problem(s) **TEST**
EACH EQTN. GIVEN
ON PREVIOUS SHEET.

Clear everything

Initial vel. 256.00 GSBD

Final vel. 17.00 GSBC

Time (seconds) 8.60 GSBB

Solve for y 1.00 GSBD

1173.90 ***

GSBe

159.00 GSBD

4.80 GSBB

g down \downarrow -9.80 GSBE

Solve for dist. 1.00 GSBD

650.30 ***

GSBe

12.00 GSBC

19.00 GSBD

-9.80 GSBE

1.00 GSBD

11.07 ***

Solve for time

29.00 GSBD

0.00 GSBC

-32.30 GSBE

2.00 GSBD

0.90 ***

0.00 GSBe

47.00 GSBA

28.00 GSBD

7.00 GSBC

2.00 GSBD

2.69 ***

GSBe

Quad roots
pause \rightarrow

Solve for V_g

Solve for V_{y0}

88.00 GSBD

-32.30 GSBE

12.00 GSBA

2.00 GSBD

5.31 ***

0.14 ***

GSBe

15.00 GSBD

-9.80 GSBE

2.50 GSBE

3.00 GSBD

-9.50 ***

GSBe

7.00 GSBA

1.80 GSBB

12.00 GSBD

3.00 GSBD

-4.22 ***

GSBe

-9.80 GSBE

5.00 GSBA

23.00 GSBD

3.00 GSBD

20.76 ***

GSBe

19.00 GSBC

-9.80 GSBE

.38 GSBE

4.00 GSBD

22.72 ***

GSBe

14.80 GSBA

2.71 GSBB

0.00 GSBC

4.00 GSBD

10.92 ***

GSBe

Solve for a

y down \downarrow

118.00 GSBA

4.965 GSBB

-32.30 GSBE

4.00 GSBD

103.95 ***

GSBe

33.00 GSBC

-32.30 GSBE

15.70 GSBA

4.00 GSBD

45.86 ***

GSBe

24.70 GSBC

44.30 GSBD

2.00 GSBB

5.00 GSBD

-9.80 ***

GSBe

3.00 GSBA

18.00 GSBD

2.50 GSBB

5.00 GSBD

-13.44 ***

GSBe

17.00 GSBC

39.00 GSBD

9.00 GSBA

5.00 GSBD

-68.44 ***

Reference(s) **PHYSICS BY RESNICK AND HALLIDAY CHAP 3 PAGE 49**

97 Program Listing I

35

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	*LBL9	21 09	
002	1	01		058	RCL0	36 00	
003	CF0	16 22 00	NR OF REG DIS IS STORED AT	059	RCL5	36 05	
004	GT00	22 00		060	=	-24	
005	*LBLB	21 12		061	RTN	24	
006	2	02	NR OF REG TIME IS STORED AT	062	*LBL2	21 02	
007	CF1	16 22 01		063	RCL5	36 05	
008	GT00	22 00		064	Pi	16-24	
009	*LBLC	21 13		065	X=Y?	16-33	
010	3	03		066	GT06	22 06	
011	CF2	16 22 02		067	F0?	16 23 00	
012	GT00	22 00		068	GT07	22 07	
013	*LBLD	21 14		069	RCL4	36 04	
014	4	04		070	X ²	53	
015	GT00	22 00		071	RCL5	36 05	
016	*LBLE	21 15		072	RCL1	36 01	
017	5	05		073	2	02	
018	*LBL0	21 00		074	x	-35	
019	ST01	35 46		075	x	-35	
020	R↓	-31		076	+	-55	
021	ST0i	35 45		077	JX	54	
022	RCL3	36 03		078	ST09	35 09	
023	X ²	53		079	RCL4	36 04	
024	RCL4	36 04		080	CHS	-22	
025	X ²	53		081	+	-55	
026	-	-45		082	LSTX	16-63	
027	2	02		083	RCL9	36 09	
028	=	-24		084	-	-45	
029	ST00	35 00		085	RCL5	36 05	
030	CLX	-51		086	=	-24	
031	RTN	24		087	PSE	16 51	
032	*LBL1	21 01		088	LSTX	16-63	
033	F1?	16 23 01		089	X*Y	-41	
034	GT09	22 09		090	R↓	-31	
035	F2?	16 23 02		091	=	-24	
036	GT08	22 08		092	RTN	24	
037	RCL4	36 04		093	*LBL7	21 07	
038	RCL3	36 03		094	RCL3	36 03	
039	+	-55		095	RCL4	36 04	
040	RCL2	36 02		096	-	-45	
041	x	-35		097	RCL5	36 05	
042	2	02		098	=	-24	
043	=	-24		099	RTN	24	
044	RTN	24		100	*LBL6	21 06	
045	*LBL8	21 08		101	RCL1	36 01	
046	RCL4	36 04		102	2	02	
047	RCL2	36 02		103	x	-35	
048	x	-35		104	RCL3	36 03	
049	RCL2	36 02		105	RCL4	36 04	
050	X ²	53		106	+	-55	
051	RCL5	36 05		107	=	-24	
052	x	-35		108	RTN	24	
053	2	02		109	*LBL3	21 03	
054	=	-24		110	F0?	16 23 00	
055	+	-55		111	GT09	22 09	
056	RTN	24		112	F1?	16 23 01	

REGISTERS

0	$V_y^2 - V_{y0}^2$	1	DIST.	2	TIME	3	V_{FINAL}	4	$V_{INITIAL}$	5	ACCELER.	6		7		8		9	$\sqrt{b^2 - 4ac}$
S0	2	S1		S2		S3		S4		S5		S6		S7		S8		S9	
A		B		C		D		E											1 st NR OF LABEL + REG

97Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	GTOa	22 16 11	NO t	169	RCL5	36 05	
114	RCL1	36 01		170	RCL1	36 01	
115	2	02		171	2	02	
116	x	-35		172	x	-35	
117	RCL2	36 02		173	x	-35	
118	=	-24		174	-	-45	
119	RCL4	36 04		175	JX	54	
120	-	-45		176	RTN	24	
121	RTN	24		177	*LBL8	21 08	
122	*LBL9	21 09		178	RCL1	36 01	
123	RCL4	36 04		179	2	02	
124	RCL5	36 05		180	x	-35	
125	RCL2	36 02		181	RCL2	36 02	
126	x	-35		182	=	-24	
127	+	-55		183	RCL3	36 03	
128	RTN	24		184	-	-45	
129	*LBLa	21 16 11		185	RTN	24	
130	RCL4	36 04		186	*LBL5	21 05	
131	X ²	53		187	F0?	16 23 00	
132	RCL1	36 01		188	GTO7	22 07	
133	RCL5	36 05		189	F1?	16 23 01	
134	2	02		190	GTO6	22 06	
135	x	-35		191	RCL1	36 01	
136	x	-35		192	RCL4	36 04	
137	+	-55		193	RCL2	36 02	
138	JX	54		194	x	-35	
139	RTN	24		195	-	-45	
140	*LBL4	21 04		196	RCL2	36 02	
141	F0?	16 23 00		197	X ²	53	
142	GTOb	22 16 12		198	=	-24	
143	F1?	16 23 01		199	2	02	
144	GTOc	22 16 13		200	x	-35	
145	RCL5	36 05		201	RTN	24	
146	Pi	16-24		202	*LBL7	21 07	
147	X=Y?	16-33		203	RCL3	36 03	
148	GTO8	22 08		204	RCL4	36 04	
149	RCL1	36 01		205	-	-45	
150	RCL2	36 02		206	RCL2	36 02	
151	=	-24		207	=	-24	
152	RCL5	36 05		208	RTN	24	
153	RCL2	36 02		209	*LBL6	21 06	
154	x	-35		210	RCL0	36 00	
155	2	02		211	RCL1	36 01	
156	=	-24		212	=	-24	
157	-	-45		213	RTN	24	
158	RTN	24		214	*LBLc	21 16 15	
159	*LBLb	21 16 12		215	SF0	16 21 00	
160	RCL3	36 03		216	SF1	16 21 01	
161	RCL5	36 05		217	SF2	16 21 02	
162	RCL2	36 02		218	Pi	16-24	
163	x	-35		219	ST05	35 05	
164	-	-45		220	0	- 00	
165	RTN	24		221	RTN	24	
166	*LBLc	21 16 13		222	*LBLd	21 16 14	
167	RCL3	36 03		223	ST01	35 46	
168	X ²	53		224	GTOi	22 45	

LABELS

SET STATUS

A	B	C	D	E	F	FLAGS	TRIG	DISP
STORE DIS	STORE TIME	STORE V _F	STORE V _{IN}	STORE A _{CL}	SET IF DIS HASN'T ENTERED	ON OFF		
a USED	USED	USED	d SOLVE	e RESET	1 SET IF TIME HASN'T ENTERED	0 <input checked="" type="checkbox"/> <input type="checkbox"/>	DEG <input checked="" type="checkbox"/>	FIX <input checked="" type="checkbox"/>
0 STORAGE	1 CALC DIS	2 CALL TIME	3 CALL V _F	4 CALL V _{INT}	2 SET IF V _F HASN'T ENTERED	1 <input checked="" type="checkbox"/> <input type="checkbox"/>	GRAD <input checked="" type="checkbox"/>	SCI <input type="checkbox"/>
5 CALL A _{CL}	6 USED	7 USED	8 USED	9 USED	3	2 <input checked="" type="checkbox"/> <input type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
						3 <input type="checkbox"/> <input type="checkbox"/>		n <u>2</u>

Program Description I

Program Title	Ballistics Trajectory Computations		
Contributor's Name	David M. Ivey		
Address	2470 New Clinton Rd.		
City	Macon	State	Ga. Zip Code 31201

Program Description, Equations, Variables The Program computes remaining velocities, energies, flight times, maximum rise and drops of bullets at user specified intervals. Computations technically apply to ICAO conditions which are satisfactory for most shooting conditions. The method uses a Mayevski drag formulation ($\text{drag} = Av^n$) with different constants for different velocity zones. The program automatically selects the correct constants. Program control is by Label A, the various data outputs are done by Labels 2,3,4,5, and 6 so that users may easily arrange output data order. Label 7 computes air resistance. Note that maximum rise gives sight in data.

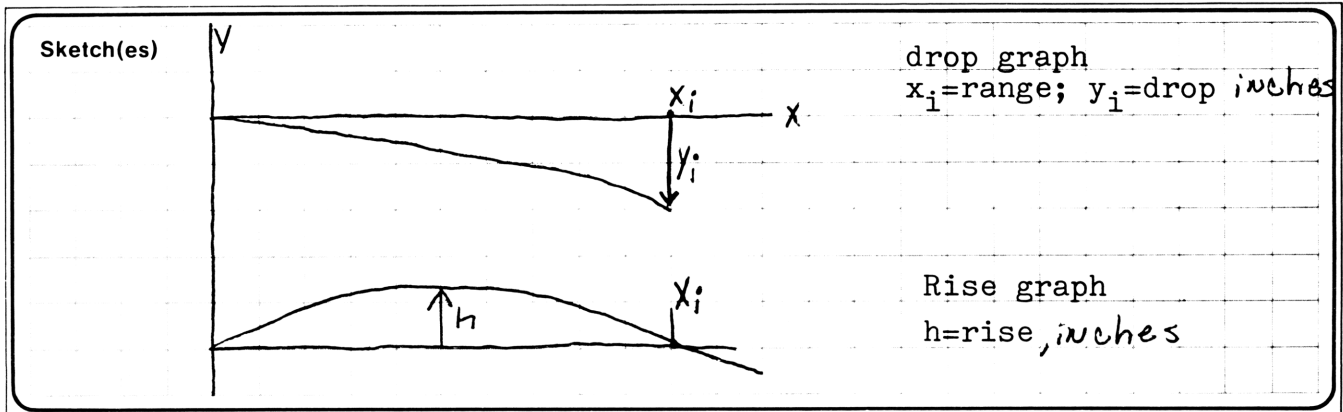
Use English Units Only

Operating Limits and Warnings Be sure to use ballistic coefficients based on Ingall's Tables (most are, usual exceptions are foreign bullets). This system works best when the coefficient (C_b) is greater than .150 and velocities above that of sound. Most importantly however, use range intervals no greater than 100yds, shorter intervals give better accuracy. For typical rifles about 3% error occurs relative to numeric integration techniques at 1000yards.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II



Sample Problem(s) Compute the complete trajectory of a 30/06 cartridge where the bullet weight is 165grain Sierra boat-tail (ballistic coefficient for this bullet=0.470) at a muzzle velocity of 2800ft/sec in 100yd. intervals out to 200yards.

Velocity in Ft/sec
 Energy in ft lbs
 time in seconds
 Rise & drop in inches

Muzzle Vel \rightarrow 2800. ***
 Bullet wt \rightarrow 165. ***
 $C_B \rightarrow$ 0.470 ***

Solution(s) Input keystrokes

$C_b = 0.470$ STO 6
 $\Delta x = 300$ feet STO 7
 $x_m = 200$ yds = 600 ft use 601 to stop.
 601 STO 8
 $w_b = 165$ STO 9
 $V_o = 2800$ STO A
 Set flags Zero and One to
 output energy and rise Press A

Output \Rightarrow

Range yds 100. ***
 Velocity 2585. ***
 Energy 2454. ***
 time 0.1114 sec ***
 Rise 0.50" ***
 drop 2.33" ***
 200. ***
 2385. ***
 2054. ***
 0.2328 ***
 2.50 ***
 9.86 ***

Reference(s) This program represents the first complete ballistic system without extensive numeric integration techniques or long tables. It was specifically developed for microcomputer applications. For more information regarding theoretical development, write the author.

DAVID M. IVEY

2470 NEW CLINTON RD.

MACON, GEORGIA 31201

PH (912) 743-4206

Ballistics Trajectory Computations

A) Equations;

$$V_f = [V_i^2 - Z'D]^{1/2}$$

$$D = AV_i^N$$

$$Z' = \frac{2\Delta X}{c}$$

$$t_f = 2\Delta X \sum \frac{1}{V_i + V_f}$$

$$H = 48.26 t_f^2$$

$$Y_f = \frac{4}{3} H (1 + 2\sqrt{V_f/V_0})$$

$$E_f = \frac{W_8 V_f^2}{450240}$$

(W₈ in grains)

8) Note the constants A and N are stored in registers by the data card.

Mayevski Velocity Zones

Range of V	N	A
3600 to 2600	1.55	4.064882535(10 ⁻³)
2600 to 1800	1.70	1.247951766(10 ⁻³)
1800 to 1370	2.00	1.316(10 ⁻³)
1370 to 1230	3.00	9.569787630(10 ⁻⁸)
1230 to 970	5.00	6.336817507(10 ⁻¹⁴)

Location of Constants

The N, A values occupy secondary storage registers. Zone velocities occupy Registers B to E

Below is a print out of Register Contents:

4.064882535-03	10
1.55	11
1.247951766-03	12
1.7	13
1.316000000-06	14
2.0	15
9.569787630-03	16
3.0	17
6.336817507-14	18
5.0	19
0.0	A
1800.0	B
1370.0	C
1230.0	D
970.0	E
0.0	I

10 Refers to
Address of
storage
Register

User Instructions

Ballistics Trajectory Computations Prgm

1 f0=prints f1=energy and rise

Run

Clears

C_B

2

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS	OUTPUT DATA/UNITS
1	Load Program Card, Both sides		<input type="text"/> <input type="text"/>	
	Load Data Card, Both sides		<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	
2	Store Parameters Ballistic coefficient	C_b	STO 6	C_b
	Range Increment (ft)	Δx	STO 7	Δx
	Maximum Range ft	X_m	STO 8	X_m
	Bullet weight Grains	w_b	STO 9	w_b
	Muzzle Velocity	V_o	STO A	V_o
			<input type="text"/> <input type="text"/>	
3	Set Output status		<input type="text"/> <input type="text"/>	
	Flag Zero set will Print ans, else pause		<input type="text"/> <input type="text"/>	
	Flag One set will compute Energy and rise		<input type="text"/> <input type="text"/>	
	according to Flag Zero's status		<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	
4	Execute program Press LBL A		<input type="text"/> <input type="text"/>	
	Prgm first outputs initial data		<input type="text"/> <input type="text"/>	V_o
			<input type="text"/> <input type="text"/>	w_b
			<input type="text"/> <input type="text"/>	C_b
	Then the computations :		<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	Range
			<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	Velocity
			<input type="text"/> <input type="text"/>	energy
			<input type="text"/> <input type="text"/>	time
			<input type="text"/> <input type="text"/>	rise
			<input type="text"/> <input type="text"/>	drop
5	New Problem go to Step two after clearing		<input type="text"/> <input type="text"/>	
	by LBL C		<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	
6	To Compute a ballistic Coefficient by Ingalls		<input type="text"/> <input type="text"/>	
	A STORE Range between	ΔX	STO 7	ΔX
	Known velocities		<input type="text"/> <input type="text"/>	
	Enter Velocities	V_i	\uparrow <input type="text"/>	V_i
		V_{i+1}	E <input type="text"/>	$-C_B$
			<input type="text"/> <input type="text"/>	
			<input type="text"/> <input type="text"/>	

97 Program Listing I

41

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11	Prgrm Control Initial Settings Initial Data Output	057	CHS	-22	Energy Calculations
002	F0?	16 23 00		058	RCL4	36 04	
003	SFC	16-11		059	X ²	53	
004	GSB2	23 14		060	+	-55	
005	RCL7	36 07		061	JX	54	
006	ST02	35 02		062	GSB1	23 01	
007	1	01		063	RTN	24	
008	0	00		064	*LBL3	21 03	
009	ST01	35 46		065	RCL4	36 04	
010	RCL4	36 11		066	X ² Y	-41	
011	ST04	35 04		067	+	-55	
012	GSB1	23 01		068	LSTX	16-63	
013	RCL5	36 09		069	ST04	35 04	
014	GSB1	23 01		070	X ² Y	-41	
015	RCL6	36 06		071	ST03	35 03	
016	DSP3	-63 03		072	RCL4	36 04	
017	GSB1	23 01		073	X ²	53	
018	DSP0	-63 00		074	RCL9	36 09	
019	F0?	16 23 00	Main Prgrm Control after initialization } data Computations	075	x	-35	Flight Time Calculations
020	SFC	16-11		076	4	04	
021	*LBLB	21 12		077	5	05	
022	F0?	16 23 00		078	0	00	
023	SFC	16-11		079	2	02	
024	GSB2	23 02		080	4	04	
025	F0?	16 23 00		081	0	00	
026	SFC	16-11		082	=	-24	
027	GSB2	23 02		083	F1?	16 23 01	
028	GSB3	23 03		084	GSB1	23 01	
029	GSB4	23 04		085	RTN	24	
030	GSB5	23 05		086	*LBL4	21 04	
031	GSB6	23 06		087	RCL3	36 03	
032	RCL7	36 07		088	1/X	52	
033	ST+2	35-55 02		089	2	02	
034	RCL2	36 02		090	x	-35	
035	RCL8	36 08		091	RCL7	36 07	
036	X ² Y?	16-35		092	x	-35	
037	RTN	24	Range decisions $X_i \leq X_m$ Pause or Print Routine	093	ST+5	35-55 05	Rise (Maximum Ordinate) calculations
038	GT0B	22 12		094	x	-35	
039	*LBL1	21 01		095	RCL5	36 05	
040	F0?	16 23 00		096	DSP4	-63 04	
041	GT0a	22 16 11		097	F1?	16 23 01	
042	PSE	16 51		098	GSB1	23 01	
043	PSE	16 51		099	RTN	24	
044	RTN	24		100	*LBL5	21 05	
045	*LBLa	21 16 11		101	X ²	53	
046	PRTX	-14		102	4	04	
047	RTN	24		103	5	05	
048	*LBL2	21 02		104	.	-62	
049	RCL4	36 04		105	2	02	
050	GSB7	23 07		106	6	06	
051	RCL7	36 07		107	x	-35	
052	x	-35		108	DSP2	-63 02	
053	2	02	Velocity Computations	109	GSB1	23 01	
054	x	-35		110	RTN	24	
055	RCL6	36 06		111	*LBL6	21 06	
056	÷	-24		112	4	04	

REGISTERS

0	1	2	3	4	5	6	7	8	9
		X_i	used	V_i	$\sum \frac{1}{v_i + k}$	C_B	ΔX	X_m	W_B
S0 4.064(10 ³)	S1 1.55	S2 1.24(10 ⁻³)	S3 1.70	S4 1.316(10 ⁻³)	S5 2.00	S6 9.57(10 ⁻³)	S7 3.00	S8 6.34(10 ⁻⁴)	S9 5.00
A V_0	B 1800	C 1370	D 1230	E 970	I USED UNTESTED				

97 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	X	-35	LBL 6 drop Computation	169	GTOb	22 16 12	Clears time Register and Range counter Outputs range in yards Ballistic Coefficient Calculations
114	3	03		170	*LBL e	21 16 15	
115	=	-24		171	1	01	
116	RCL4	36 04		172	4	04	
117	RCL A	36 11		173	STOI	35 46	
118	=	-24		174	GTOb	22 16 12	
119	JX	54		175	*LBL d	21 16 14	
120	2	02		176	1	01	
121	X	-35		177	0	00	
122	1	01		178	STOI	35 46	
123	+	-55	Selection of correct R, N constants for drag calculations determines velocity zones.	179	GTOb	22 16 12	
124	X	-35		180	*LBL D	21 14	
125	GSB1	23 01		181	0	00	
126	RTN	24		182	STO2	35 02	
127	*LBL7	21 07		183	STO5	35 05	
128	2	02		184	RTN	24	
129	6	06		185	*LBL8	21 08	
130	EEA	-23		186	RCL2	36 02	
131	2	02		187	3	03	
132	XZY?	16-35		188	=	-24	
133	GTOb	22 00	Actual Drag Calculations	189	DSP0	-63 00	
134	XZY	-41		190	GSB1	23 01	
135	RCL6	36 12		191	RTN	24	
136	XZY?	16-35		192	*LBL E	21 15	
137	GTOb	22 16 13		193	STO0	35 00	
138	XZY	-41		194	XZY	-41	
139	RCL0	36 13		195	STO1	35 01	
140	XZY?	16-35		196	STO4	35 04	
141	GTOb	22 16 15		197	GSB7	23 07	
142	XZY	-41		198	2	02	
143	RCLD	36 14	Labels 0, C, e and assure correct constant for drag velocity zone	199	X	-35	
144	XZY?	16-35		200	RCL7	36 07	
145	GTOb	22 16 14		201	X	-35	
146	1	01		202	RCL1	36 01	
147	6	06		203	X ²	53	
148	STOI	35 46		204	CHS	-22	
149	*LBL6	21 16 12		205	RCL0	36 00	
150	RCL4	36 04		206	X ²	53	
151	RCL1	36 45		207	+	-55	
152	ISZ1	16 26 46		208	=	-24	
153	RCL1	36 45	Labels 0, C, e and assure correct constant for drag velocity zone	209	GSB1	23 01	
154	XZY	-41		210	RTN	24	
155	R4	-31		211	R/S	51	
156	Y*	31					
157	R1	16-31					
158	X	-35					
159	RTN	24					
160	*LBL0	21 00					
161	1	01					
162	0	00					
163	STOI	35 46					
164	GTOb	22 16 12					
165	*LBL6	21 16 13					
166	1	01					
167	2	02					
168	STOI	35 46					

LABELS

FLAGS

SET STATUS

A Initial Cont	B used	C	D clears	E $V_1, V_{11} \rightarrow C_B$	F Prints	FLAGS	TRIG	DISP
a used	b used	c Zones	d Zones	e Zones	1 Does E+ rise	ON OFF 0 <input checked="" type="checkbox"/> <input type="checkbox"/>	DEG <input checked="" type="checkbox"/>	FIX <input checked="" type="checkbox"/>
0 Zones	1 Print/Pause	2 Velocity	3 Energy	4 time	2	1 <input checked="" type="checkbox"/> <input type="checkbox"/>	GRAD <input type="checkbox"/>	SCI <input type="checkbox"/>
5 rise	6 drop	7 drag	8 Range	9	3	2 <input type="checkbox"/> <input checked="" type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
						3 <input type="checkbox"/> <input checked="" type="checkbox"/>		n 2,4,0

Program Description I

Program Title ISOTOPE OVERLAP CORRECTIONS

Contributor's Name Lawrence I. Grossman

Address 206 Crest Ave.

City Ann Arbor

State MI

Zip Code 48103

Program Description, Equations, Variables Program Corrects for spillover between channels when two radioactive isotopes are being counted in a liquid scintillation spectrometer. Background subtraction for each isotope is also provided. Program may be used with single isotope.

Isotopes x and y are counted in machine channels A and B, respectively.

Let a = fractional spillover of isotope Y from channel B to A.

b = fractional spillover of isotope X from channel A to B.

C_x = corrected counts/min isotope x in channel A = $\frac{C_A - a C_B}{1 - ab}$, where C_A and C_B are the observed counts/min in each channel.

$$C_y = \frac{C_B - b C_A}{1 - ab}$$

Outputs

Total counts/min isotope x = $C_x (1 + b) = T_x$

Total counts/min isotope y = $C_y (1 + a) = T_y$

Operating Limits and Warnings

This program has been verified only with respect to the numerical example given in Program Description II. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s) 2 isotopes. Spillover $A \rightarrow B = 10\%$, $B \rightarrow A = 20\%$, $Bk_A = 10$ cpm, $Bk_B = 50$ cpm

For the following values of cts/min_A and cts/min_B, calculate corrected values and totals.

sample ^A	A	B
1	1000	500
2	2000	1000
3	1400	2200

Solution(s) Keystrokes

[F] [A]	→ 0.00	→ 920 (T _Y)
0.2 ENTER 10 [D]	→ 0.20	→ 3 (next)
0.1 ENTER 50 [E]	→ 0.10	1400 [A] 2200 [B] [C] → 1078 (T _X)
/ [F] [C]	→ 1.00	→ 2462 (T _Y)
1000 [A] 500 [B] [C]	→ 1010 (T _X)	→ 4 (next)
	→ 430 (T _Y)	[F] [B] → 4108 (ΣT _X)
	→ 2 (next sample)	→ 3812 (ΣT _Y)
2000 [A] 1000 [B] [C]	→ 2020 (T _X)	→ 0 (reset)

Reference(s)

45

[illegible]

67 Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBL D	31 25 14			X	71	
	STO 0	33 00	store BKA, a		STO +8	33 61 08	
	R+	35 53			STO 9	33 09	
	STO 1	33 01		060	RCL 7	34 07	output Tx,
	RTN	35 22			-X-	31 84	Ty (if Fo set)
	*LBL C	32 25 13	store first sample no.		RCL 9	34 09	
	ST I	35 33			FO?	35 71 00	
	RTN	35 22			-X-	31 84	
	*LBL E	31 25 15			ISZ	31 34	
010	STO 2	33 02	store BKB, b		RCL	35 34	
	R+	35 53			RTN	35 22	
	STO 3	33 03			*LBL a	32 25 11	sfo for 2 labels
	RTN	35 22			SFO	35 51 00	
	*LBL A	31 25 11	enter counts/min for A	070	RTN	35 22	
	RCL 0	34 00	channel, subtract BKA,		*LBL b	32 25 12	output total x for
	-	51	store.		RCL 6	34 06	all samples, total y
	STO 4	33 04			-X-	31 84	(if Fo set). CFO.
	RTN	35 22			RCL 8	34 08	Clear accumulation
	*LBL B	31 25 12	enter counts/min for B		FO?	35 71 00	registers.
020	RCL 2	34 02	channel, subtract BKB,		-X-	31 84	
	-	51	store		CFO	35 61 00	
	STO 5	33 05			0	00	
	RTN	35 22		080	STO 6	33 06	
	*LBL C	31 25 13	Calculate Cx, Cy,		STO 8	33 08	
	RCL 4	34 04	Tx, Ty		ST I	35 33	
	RCL 1	34 01			RTN	35 22	
	RCL 5	34 05					
	X	71					
	-	51					
030	1	01					
	RCL 1	34 01					
	RCL 3	34 03					
	X	71					
	-	51					
	÷	81					
	1	01					
	RCL 3	34 03					
	+	61					
	X	71					
040	STO +6	33 61 06					
	STO 7	33 07					
	DSP 0	23 00					
	RCL 5	34 05					
	RCL 3	34 03					
	RCL 4	34 04					
	X	71					
	-	51					
	1	01					
	RCL 1	34 01					
050	RCL 3	34 03					
	X	71					
	-	51					
	÷	81					
	1	01					
	RCL 1	34 01					
	+	61					

LABELS				
A counts/min A	B counts/min B	C output Tx,Ty	D a↑ Backgd. A	E b↑ Backgd. B
a 2 labels	b Total cpm	c 1st sample No.	d	e
0	1	2	3	4
5	6	7	8	9

FLAGS				SET STATUS		
0 set for 2 isotopes				FLAGS	TRIG	DISP
				ON OFF		
1				0 <input checked="" type="checkbox"/> <input type="checkbox"/>	DEG <input checked="" type="checkbox"/>	FIX <input checked="" type="checkbox"/>
2				1 <input type="checkbox"/> <input checked="" type="checkbox"/>	GRAD <input type="checkbox"/>	SCI <input type="checkbox"/>
3				2 <input type="checkbox"/> <input checked="" type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
				3 <input type="checkbox"/> <input checked="" type="checkbox"/>		n 0

REGISTERS									
0 Background A	1 a	2 Background B	3 b	4 CA	5 CB	6 ≤ Cx	7 Cx	8 ≤ Cy	9 Cy
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A	B	C	D	E	I	Sample Number			

Program Description I

Program Title Critical Reactor Code

Contributor's Name Richard D. Hyman

Address 23822 80th W.

City Edmonds

State Washington

Zip Code 98020

Program Description, Equations, Variables The program estimates the parameters of a reactor with different fuels, moderator, fuel to moderator ratios, size, and shapes of the reactor. Its most important use is in indicating trends in certain changes of mod. etc.

$$\eta = \frac{\gamma_{235} \Sigma_f(235)}{\Sigma_a(235) + \Sigma_a(238)} = \gamma \frac{\sigma_f}{\sigma_a}$$

$$f = \frac{\Sigma_a F}{\Sigma_a t} = \frac{\Sigma_a m}{\Sigma_a F} \frac{V_m}{V_F} F + E$$

$$F(x) = 1 + \frac{1}{2} \left(\frac{x}{2}\right)^2 - \frac{1}{12} \left(\frac{x}{2}\right)^4 + \frac{1}{48} \left(\frac{x}{2}\right)^6 : x = a/LF$$

$$E(y, z) = 1 + \frac{z^2}{2} \left[-\frac{z^2}{z^2 - y^2} \ln\left(\frac{z}{y}\right) - \frac{3}{4} + \frac{y^2}{4z^2} \right] : \begin{matrix} z = b/LM \\ y = a/LM \end{matrix}$$

$$\rho = \exp - \left[\frac{N_F V_F I}{\Sigma_m \Sigma_{sm} V_m} \right] \quad I = A + C / \sqrt{a\rho}$$

$$B^2 = \left(\frac{\pi}{R}\right)^2 \text{ sphere}$$

$$\epsilon = 1 + .3 \left(\frac{V_F}{V_m}\right) \quad P_L = \frac{1}{1 + B^2 L_T} \quad B^2 = 3 \left(\frac{\pi}{R}\right)^2 \text{ cube}$$

Operating Limits and Warnings This program works best for low enrichment fuel, (-7²-5)% this is much like a power reactor. The accuracy is only to be taken as an estimate. But the trends are good. Note: Radius of reactor is stored in S-6 register to change this you must change [P↔S] [STO 6] [P↔S]

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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New data cards can be made for U^{235} Pu^{239} fuels & H_2O , C, on D_2O moderators. The information needed on these cards can be found in John R. Lamarsh, Introduction to Nuclear Engineering.

P-0 = ρ - Density of Fuel

P-1 = MW - Molecular weight of fuel

P-2 = Atom density of fuel

P-3 = $\Sigma_a F$ - Microscopic cross section of fuel (abs.)(cm⁻¹)

P-4 = Microscopic cross section of mod. (abs.) (cm⁻¹)

P-5 = Const A

P-6 = Const C

P-7 = $\Sigma_m \Sigma_{sm}$

P-8 = Microscopic fission cross section of fuel (in barns)

P-9 = # of neutrons emitted per fission

S-8 = Diffusion length of moderator (cm)

S-9 = Diffusion length of fuel (cm)

A = Enrichment % of fissile fuel

B = Microscopic abs - cross section of fissile fuel (in barns)

C = Microscopic abs cross section of U^{238} (in barns)

D = Radius of fuel pin (cm)

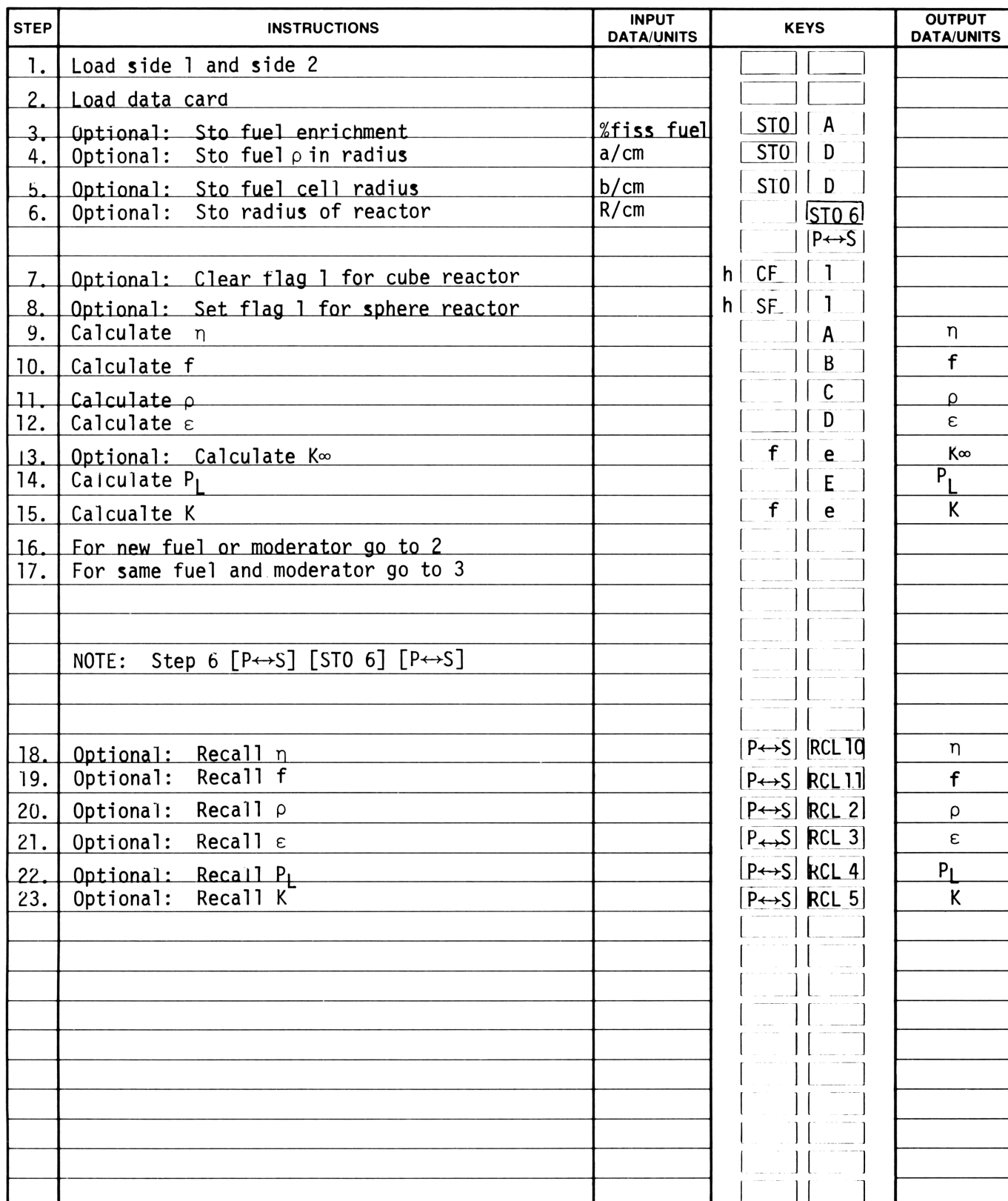
E = Radius of fuel

All these must be set for different fuel + moderators this is why it is best to record this on a card.

Values for Diff. Fuel + Moderators

	U^{235}	Pu^{239}	H_2O	D_2O	C
ρ	19.1	21.45			
MW	238	239			
NF	.04833	.04938			
ΣaF					
Σam			.0222	2.9×10^{-5}	.0002728
A	3.0	3.0			
C	38	38			
$\Sigma m \Sigma sm$			1.46	.178	.0608
σ_f	580	742.5			
γ	2.6	2.98			
Lm			2.85	170	59
L_F	1.55	2.0			
σ_{afiss}	680	1011.3			
σ_{a238}	2.7	2.7			

51



Program Listing I

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	6	06	
002	1	01		058	Y*	31	
003	0	00		059	4	04	
004	0	00		060	8	08	
005	RCLA	36 11		061	1/X	52	
006	-	-45		062	x	-35	
007	RCLA	36 11		063	RCLI	36 46	
008	÷	-24	Calculates η	064	4	04	
009	RCLC	36 13		065	Y*	31	
010	x	-35		066	1	01	
011	RCLB	36 12		067	2	02	
012	+	-55		068	1/X	52	
013	RCL8	36 08		069	x	-35	
014	RCL9	36 09		070	CHS	-22	
015	x	-35		071	+	-55	
016	X*Y	-41		072	RCLI	36 46	
017	÷	-24		073	X ²	53	
018	P*S	16-51		074	.	-62	
019	ST00	35 00		075	5	05	
020	ST05	35 05		076	x	-35	
021	P*S	16-51		077	+	-55	
022	RTN	24		078	1	01	
023	*LBLB	21 12		079	+	-55	
024	RCL0	36 00		080	RCLC	36 15	
025	RCL1	36 01		081	X ²	53	
026	÷	-24		082	STOI	35 46	
027	.	-62		083	RCLD	36 14	
028	6	06	Calculates f	084	X ²	53	
029	0	00		085	-	-45	
030	2	02		086	RCLI	36 46	
031	3	03		087	÷	-24	
032	x	-35		088	x	-35	
033	ST02	35 02		089	P*S	16-51	
034	RCLA	36 11		090	RCL4	36 04	
035	%	55		091	RCL3	36 03	
036	RCLB	36 12		092	÷	-24	
037	x	-35		093	x	-35	
038	1	01		094	P*S	16-51	
039	0	00		095	STOI	35 01	
040	0	00		096	RCLC	36 15	
041	RCLA	36 11		097	RCL8	36 08	
042	-	-45		098	÷	-24	
043	RCL2	36 02		099	STOI	35 46	
044	X*Y	-41		100	RCLD	36 14	
045	%	55		101	RCL8	36 08	
046	RCLC	36 13		102	÷	-24	
047	x	-35		103	÷	-24	
048	+	-55		104	LN	32	
049	ST03	35 03		105	RCLI	36 46	
050	P*S	16-51		106	X ²	53	
051	RCLD	36 14		107	RCLD	36 14	
052	RCL9	36 09		108	RCL8	36 08	
053	÷	-24		109	÷	-24	
054	2	02		110	X ²	53	
055	÷	-24		111	-	-45	
056	STOI	35 46		112	RCLI	36 46	

REGIS

0	1	2	3	4	5	6	7	8	9
ρ	MW fuel	N fuel	ΣaF	Σam	A	C	$\Sigma sm \Sigma sm$	σf_{25}	γ
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
η	f	ρ	ϵ	P_L	K	Radius (cm)		L_M	L_F
A	B	C	D	E	F	G	H	I	J
enrich %	σ_a fiss. fuel	σ_a non fiss fuel	a (cm)	b (cm)	used				

Program Listing II

53

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	X ²	53		169	e ^x	33	
114	X ² Y	-41		170	P ² S	16-51	
115	÷	-24		171	ST02	35 02	
116	x	-35		172	STx5	35-35 05	
117	.	-62		173	P ² S	16-51	End of ρ
118	7	07		174	RTN	24	
119	5	05		175	*LBLD	21 14	
120	-	-45		176	RCLD	36 14	
121	RCLD	36 14		177	X ²	53	
122	RCL8	36 06		178	STOI	35 46	
123	÷	-24		179	RCL5	36 15	
124	4	04		180	X ²	53	Calculates
125	÷	-24		181	RCLI	36 46	ε
126	RCLI	36 46		182	-	-45	
127	÷	-24		183	÷	-24	
128	RCLI	36 46		184	.	-62	
129	÷	-24		185	1	01	
130	+	-55		186	x	-35	
131	RCLI	36 46		187	1	01	
132	X ²	53		188	+	-55	
133	x	-35		189	P ² S	16-51	
134	2	02		190	ST03	35 03	
135	÷	-24		191	STx5	35-35 05	
136	1	01		192	P ² S	16-51	
137	+	-55		193	RTN	24	
138	RCL1	36 01		194	*LBL5	21 15	
139	+	-55		195	P ² S	16-51	
140	1/X	52		196	Pi	16-24	Calculates
141	STOI	35 01	End of f	197	RCL6	36 06	
142	STx5	35-35 05		198	÷	-24	
143	P ² S	16-51		199	X ²	53	
144	RTN	24		200	F1?	16 23 01	
145	*LBLC	21 13		201	GT01	22 01	
146	RCL0	36 00		202	3	03	
147	RCLD	36 14		203	x	-35	
148	x	-35		204	*LBL1	21 01	
149	IX	54		205	STOI	35 46	
150	RCL6	36 06	Calculates	206	RCL8	36 06	
151	X ² Y	-41	ρ	207	GSB9	23 09	
152	÷	-24		208	ST04	35 04	
153	RCL5	36 05		209	STx5	35-35 05	
154	+	-55		210	P ² S	16-51	
155	RCLD	36 14		211	RTN	24	
156	X ²	53		212	*LBL9	21 09	
157	x	-35		213	X ²	53	
158	RCL2	36 02		214	x	-35	
159	x	-35		215	1	01	
160	RCL7	36 07		216	+	-55	
161	÷	-24		217	1/X	52	
162	RCL5	36 15		218	RTN	24	
163	X ²	53		219	*LBL5	21 16 15	
164	RCLD	36 14		220	P ² S	16-51	Recall K
165	X ²	53		221	RCL5	36 05	
166	-	-45		222	P ² S	16-51	
167	÷	-24		223	RTN	24	
168	CHS	-22					

LABELS					FLAGS	SET STATUS		
A	B	C	D	E		FLAGS	TRIG	DISP
η	f	ρ	ε	P _L	0	ON OFF		
a	b	c	d	e	1	0 <input type="checkbox"/> <input checked="" type="checkbox"/>	DEG <input checked="" type="checkbox"/>	FIX <input checked="" type="checkbox"/>
0	1	2	3	4	2	1 <input checked="" type="checkbox"/> <input checked="" type="checkbox"/>	GRAD <input type="checkbox"/>	SCI <input type="checkbox"/>
5	6	7	8	9	3	2 <input type="checkbox"/> <input checked="" type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
				P _L		3 <input checked="" type="checkbox"/> <input type="checkbox"/>		n <u>5</u>

Program Description I

Program Title Semi-Empirical Nuclear mass Formula

Contributor's Name Dan Shapira

Address Physics Division, Oak Ridge National Laboratory, Bldg. 5500 X-10

City Oak Ridge **State** Tennessee **Zip Code** 37830

Program Description, Equations, Variables A Semi Empirical formula is used to calculate approximate binding energies and mass excess for any nucleus with a given nuclear charge $-Z$ and number of neutrons $-N$.

Definitions: Binding energy (B.E.) = $Z * M_p + N * M_n - M(Z,N)$

M_p = proton mass (energy) in MeV, M_n = neutron mass in MeV

$M(N,Z)$ = mass of nucleus having Z protons and N neutrons.

Mass Excess = $M(Z,N) - A * \text{amu}$

$A = Z + N$, $1\text{amu} = M(6,6)/12$ --- 1/12 mass of ^{12}C

Weizsacker's Semi-Empirical mass formula contains seven terms

$$M(Z,N) = Z * M_p + N * M_n + E_v + E_s + E_c + E_{\text{sym}} + E_{\text{pair}}$$

$$E_v = -a_1 * A, \quad E_s = a_2 * A^{2/3}, \quad E_c = a_3 * Z^2/A^{1/3}$$

$$E_{\text{sym}} = a_4 * (Z-N)^2/A$$

$$E_{\text{pair}} = \begin{cases} + \text{ or } - 34/A^{3/4} & \text{depending on whether } Z \text{ and } N \text{ are both odd or both even.} \\ 0 & \text{for odd } A \text{ nuclei} \end{cases}$$

Operating Limits and Warnings The semiempirical formula has been derived from measured masses and binding energies and is expected to work for nuclei reasonably close to the valley of stability. Usually $N \geq Z$ especially for heavier nuclei.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

Sketch(es)

Sample Problem(s) Which one of the mass-25 isobars (Nuclei with same number of protons+neutrons) is stable.

A=25 isobars are nuclei that can have N(#of neutrons) = 10, 11, 12, 13, 14 etc.
and at the same time Z(#of protons) = 15, 14, 13, 12, 11 respectively

The most stable Isobar will be the one that is most strongly bound nucleus.

The experimental observation is that the only stable Isobar of A=25 is the element Mg (Magnesium) which has Z=12 and N=13

One can make use of the semiempirical mass formula in predicting this result

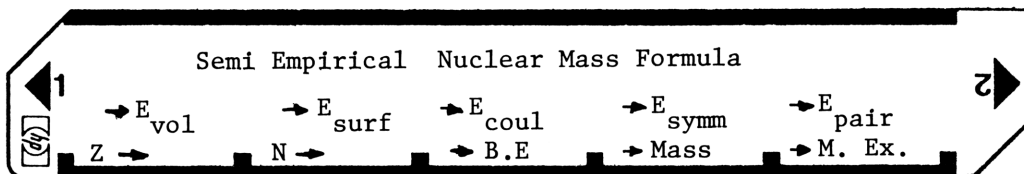
For each Z and N in this group we shall calculate the binding energies (all the binding energies will be negative numbers) the largest number (in this case the most negative one) will belong to the most stable Isobar.

SOLUTION(S)	KEYSROKES	DISPLAY	COMMENTS
	10, A	10	enter Z of Isobar
	15, B	25	N of Isobar(mass displ.)
	C	-180.69	Display Binding energy
	11, A	26	new Z entered
	14, B	25	new N entered
	C	-193.53	Display binding energy
	12, A, 13, B	25	enter new Z and N
	C	-196.88	Display new binding energy
	13, A, 12, B	25	New Z, N
	C	-190.75	Display new binding energy
	14, A, 11, B	25	New Z, N
	C	-175.14	New binding energy

From the results displayed - the Z=12, N=13 combination has the highest value of binding energy.

Reference(s) De Shalit and Feshbach Theoretical Nuclear Physics

User Instructions

[illegible]

57

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	LBL A	31 25 11			+	61	
	STO 1	33 01			RCL Ø	34 00	
	RCL 2	34 02			.	89	
	LBL Ø	31 25 00		060	F	07	
	+	61			S	05	
	STO Ø	33 00			y ^x	35 63	
	CF 1	35 61 01			÷	81	
	F? O	35 71 00			GSR R	31 22 02	
	GSB 9	31 22 09			SF 1	35 51 01	
010	RTN	35 22			RTN	35 22	
	LBL B	31 25 12			LBL 2	31 25 02	
	STO 2	33 02			RCL(2)	34 24	
	RCL 1	34 01			*	71	
	GTO Ø	22 00		070	RCI	35 34	
	LBL 1	31 25 01			g	09	
	F? 1	35 71 01			+	61	
	RTN	35 22			STI	35 33	
	8	08			X = y	35 52	
	ST I	35 33			STO(2)	33 24	
020	RCL Ø	34 00			RCI	35 34	
	GSBR	31 22 02			8	08	
	RCL 1	34 01			-	51	
	GSBR	31 22 02			STI	35 33	
	RCL 2	34 02		080	RTN	35 22	
	GSBR	31 22 02			LBL α	32 25 11	
	RCL Ø	34 00			GSB 1	31 22 01	
	GSBR	31 22 02			RCLA	34 11	
	RCL Ø	34 00			GTO 7	22 07	
	3	03			LBL β	32 25 12	
030	1/x	35 62			GSB 1	31 22 01	
	y ^x	35 63			RCLB	34 12	
	x ²	32 54			GTO 7	22 07	
	GSBR	31 22 02			LBL C	32 25 13	
	RCL 1	34 01		090	GSB 1	31 22 01	
	x ²	32 54			RCLC	34 13	
	RCL Ø	34 00			GTO 7	22 07	
	3	03			LBL d	32 25 14	
	1/x	35 62			GSB 1	31 22 01	
	y ^x	35 63			RCLD	34 14	
040	÷	81			GTO 7	22 07	
	GSBR	31 22 02			LBL e	32 25 15	
	RCL 1	34 01			GSB 1	31 22 01	
	RCL 2	34 02			RCLE	34 15	
	-	51		100	GTO 7	22 07	
	x ²	32 54			LBL C	32 25 13	
	RCL Ø	34 00			GSB 1	31 22 01	
	÷	81			1	01	
	GSBR	31 22 02			g	09	
	1	01			STI	35 33	
050	CHS	42			GSB 4	31 22 04	
	RCL 1	34 01			GTO 7	22 07	
	y ^x	35 63			LBL D	31 25 14	
	1	01			GSB 1	31 22 01	
	CHS	42		110	1	01	
	RCL 2	34 02			f	0f	
	y ^x	35 63			STI	35 33	

REGISTERS

0	A	1	Z	2	N	3		4		5		6		7		8 - a.m.u.	9 Mφ
S0	M(m)	S1	-a₁	S2	a₂	S3	a₃	S4	a₄	S5	-a₅	S6		S7		S8 Z * M _p	S9 N * M _m
A	E _V	B	E _s	C	E _c	D	E _{sym}	E	E _{pair}	I							

67 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
	GSB4	31 22 04			6	06	
	GTO7	22 07		170	GSB8	31 22 08	
	LBL E	31 25 15			1	01	
	GSB1	31 22 01			5	05	
	1	01			.	83	
	6	06			6	06	
	STI	35 33			8	08	
120	GSB4	31 22 04			CHS	42	
	LBL 7	31 25 07			GSB8	31 22 08	
	RIS	84			1	01	
	RCL 0	34 00			8	08	
	÷	81		180	.	83	
	RTN	35 22			5	05	
	LBL 4	31 25 04			6	06	
	0	00			GSB8	31 22 08	
	STO 6	33 06			.	83	
	LBL 5	31 25 05			7	07	
130	ISZ	31 34			1	01	
	RCL I	35 34			7	07	
	2	02			GSB8	31 22 08	
	5	05			2	02	
	-	51		190	8	08	
	X=0	31 51			.	83	
	GTO 6	22 06			1	01	
	RCL (2)	34 24			GSB8	31 22 08	
	STO+6	33 61 06			1	01	
	GTO 5	22 05			7	07	
140	LBL 6	31 25 06			CHS	42	
	RCL 6	34 06			GSB8	31 22 08	
	RTN	35 22			CF 0	35 61 00	
	LBL 9	31 25 09			RCL 0	34 00	
	7	07		200	RTN	35 22	
	STI	35 33			LBL 8	31 25 08	
	9	09			ISZ	31 34	
	3	03			STO (2)	33 24	
	1	01			RTN	35 22	
	.	83					
150	5	05					
	0	00					
	4	04					
	CHS	42					
	GSB8	31 22 08		210			
	9	09					
	3	03					
	8	08					
	.	83					
	7	07					
160	9	09					
	3	03					
	GSB8	31 22 08					
	9	09					
	3	03					
	9	09		220			
	.	83					
	5	05					
	7	07					

LABELS					FLAGS	SET STATUS		
A ENTER	B ENTER	C B.E.	D M(Z,N)	E H. EXCESS	0	FLAGS	TRIG	DISP
Z	N	B.E.	M(Z,N)	H. EXCESS	0	ON OFF		
a → E _v	b → E _s	c → E _c	d → E _{sym}	e → E _{par}	1	0 <input checked="" type="checkbox"/> <input type="checkbox"/>	DEG <input type="checkbox"/>	FIX <input type="checkbox"/>
0	1	2	3	4	2	1 <input checked="" type="checkbox"/> <input type="checkbox"/>	GRAD <input type="checkbox"/>	SCI <input checked="" type="checkbox"/>
5	6	7	8	9	3	2 <input type="checkbox"/> <input type="checkbox"/>	RAD <input type="checkbox"/>	ENG <input type="checkbox"/>
						3 <input type="checkbox"/> <input type="checkbox"/>		n 4

Program Description II

Sketch(es)

Sample Problem(s) ① SUPPOSE THE G.G. COEFFICIENT $\langle j_1 j_2 m_1 m_2 | JM \rangle$ IS NEEDED WITH $j_1 = \frac{3}{2}$, $j_2 = 2$, $J = \frac{5}{2}$; $m_1 = \frac{1}{2}$, $m_2 = 0$, $M = \frac{1}{2}$.

NOTE FOR SOLUTIONS: j_1 is "entered" by pressing "A"

j_2 " " " " B
 J " " " " C
 m_1 " " " " f[A]
 m_2 " " " " f[B]

M is KEYED IN AS $-M$ and
 is "entered" by pressing f[C]

② IF THE 3J SYMOL $\begin{pmatrix} j_1 & j_2 & J \\ m_1 & m_2 & -M \end{pmatrix}$ was desired, IT IS STORED IN REGISTER E.

Solution(s) ① 1.5 [A] 2 [B] 2.5 [C] .5 f[A] 0. f[B] -.5 f[C]
 completes entry of data

[D] starts program $\rightarrow 2.927700221-01$
 (DIMENSIONLESS)

② [RCL] [E] $\rightarrow 1.195228610-01$
 (DIMENSIONLESS)

Reference(s) MESSIAH, ALBERT, QUANTUM MECHANICS, VOLUME II, PP 1054-1058, NORTH-HOLLAND PUBLISHING CO. (AMSTERDAM) AND JOHN WILEY & SONS (NEW YORK), 1958.
 (translated from the French edition)

61

[illegible]

Program Listing I

COMMENTS			STEP	KEY ENTRY	KEY CODE	COMMENTS
001	*LBLA	21 11		057	JX 54	
002	CLRG	16-53		058	ST04 35 04	
003	PzS	16-51		059	1 01	
004	CLRG	16-53		060	1 01	
005	ST01	35 01		061	ST01 35 46	
006	RTN	24		062	RCL1 36 01	
007	*LBLB	21 12		063	RCLi 36 45	
008	ST02	35 02		064	+ -55	
009	RTN	24		065	N! 16 52	
010	*LBLC	21 13		066	RCL1 36 01	
011	ST03	35 03		067	RCLi 36 45	
012	PzS	16-51		068	- -45	
013	RTN	24		069	N! 16 52	
014	*LBLd	21 16 11		070	x -35	
015	ST01	35 01		071	ST05 35 05	
016	RTN	24		072	ISZI 16 26 46	
017	*LBLb	21 16 12		073	RCL2 36 02	
018	ST02	35 02		074	RCLi 36 45	
019	RTN	24		075	+ -55	
020	*LBLc	21 16 13		076	N! 16 52	
021	ST03	35 03		077	RCL2 36 02	
022	PzS	16-51		078	RCLi 36 45	
023	RTN	24		079	- -45	
024	*LBLD	21 14		080	N! 16 52	
025	RCL1	36 01		081	x -35	
026	RCL2	36 02		082	STx5 35-35 05	
027	RCL3	36 03		083	ISZI 16 26 46	
028	-	-45		084	RCL3 36 03	
029	+	-55		085	RCLi 36 45	
030	N!	16 52		086	+ -55	
031	ST04	35 04		087	N! 16 52	
032	RCL2	36 02		088	RCL3 36 03	
033	RCL3	36 03		089	RCLi 36 45	
034	RCL1	36 01		090	- -45	
035	-	-45		091	N! 16 52	
036	+	-55		092	x -35	
037	N!	16 52		093	STx5 35-35 05	
038	STx4	35-35 04		094	RCL5 36 05	
039	RCL3	36 03		095	JX 54	
040	RCL1	36 01		096	ST05 35 05	
041	RCL2	36 02		097	RCL1 36 01	
042	-	-45		098	RCL2 36 02	
043	+	-55		099	RCLi 36 45	
044	N!	16 52		100	+ -55	
045	STx4	35-35 04		101	- -45	
046	1	01		102	1 01	
047	RCL1	36 01		103	CHS -22	
048	RCL2	36 02		104	XZY -41	
049	RCL3	36 03		105	YX 31	
050	+	-55		106	ST06 35 06	
051	+	-55		107	RCL4 36 04	
052	+	-55		108	RCL5 36 05	
053	N!	16 52		109	RCL6 36 06	
054	RCL4	36 04		110	x -35	
055	XZY	-41		111	x -35	
056	÷	-24		112	ST0D 35 14	

CLEAR S
REGISTERS
AND STORES
J₁

STORES J₂

STORES J

STORES m₁

STORES m₂

STORES -M

BEGINS
COMPUTATIONS

$\Delta(j, j_2, J)$

IS COMPUTED

IN STEPS

25-57

STORES
 $\sqrt{\Delta(j, j_2, J)}$
COMPUTES

$\sqrt{(j_1+m)! (j_1-m)! (j_2+m_2)! (j_2-m_2)! (J+M)! (J-M)! (W-M)! (W-J-M)!}$

COMPUTES
 $(-1)^{j_1-j_2+M}$

MULTIPLIES
COMPUTED SQ.
ROOTS TOGETHER;
MULTIPLIES BY
 $(-1)^{j_1-j_2+M}$ STORES^{IN} D

REGISTERS

0	1	2	3	4	5	6	7	8	9
	USED	USED	USED	USED	USED	USED	USED	USED	USED
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
	USED	USED	USED						
A	B	C	D	E	I				
USED	USED	USED	USED	3J VALVE	USED				

97 Program Listing II

63

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	CLX	-51		169	+	-55	
114	SF0	16 21 00	COMPUTES	170	RCL1	36 46	
115	STOI	35 46		171	-	-45	
116	P+S	16-51	SUMMATION	172	X<0?	16-45	
117	RCL1	36 01	IN	173	GT03	22 03	
118	STOA	35 11	RACAH	174	N!	16 52	
119	RCL2	36 02		175	ST08	35 08	
120	STOB	35 12	FORMULA	176	CF0	16 22 00	
121	RCL3	36 03		177	RCL4	36 04	
122	STOC	35 13		178	RCL5	36 05	
123	P+S	16-51	(STEPS	179	RCL6	36 06	
124	*LBL2	21 02	113-198)	180	X	-35	
125	RCL3	36 03		181	X	-35	
126	RCL1	36 46		182	RCL7	36 07	
127	RCLA	36 11		183	RCL8	36 08	
128	+	-55		184	X	-35	
129	+	-55		185	X	-35	
130	RCL2	36 02		186	RCL1	36 46	
131	-	-45		187	N!	16 52	
132	X<0?	16-45		188	X	-35	
133	GT03	22 03		189	1/X	52	
134	N!	16 52		190	1	01	
135	ST04	35 04		191	CHS	-22	
136	RCL3	36 03		192	RCL1	36 46	
137	RCL1	36 46		193	Y*	31	
138	+	-55		194	X	-35	
139	RCL1	36 01		195	ST+9	35-55 09	
140	RCLB	36 12		196	ISZ1	16 26 46	
141	+	-55		197	GT02	22 02	
142	-	-45		198	GT02	22 02	
143	X<0?	16-45		199	*LBL3	21 03	
144	GT03	22 03		200	ISZ1	16 26 46	
145	N!	16 52		201	F0?	16 23 00	
146	ST05	35 05		202	GT02	22 02	
147	RCL1	36 01		203	RCL9	36 09	
148	RCL2	36 02		204	RCLD	36 14	
149	+	-55		205	X	-35	
150	RCL3	36 03		206	STOE	35 15	
151	RCL1	36 46		207	1	01	
152	+	-55		208	CHS	-22	
153	-	-45		209	RCL1	36 01	
154	X<0?	16-45		210	RCLC	36 13	
155	GT03	22 03		211	-	-45	
156	N!	16 52		212	RCL2	36 02	
157	ST06	35 06		213	-	-45	
158	RCL1	36 01		214	Y*	31	
159	RCL1	36 46		215	RCL3	36 03	
160	RCLA	36 11		216	2	02	
161	+	-55		217	X	-35	
162	-	-45		218	1	01	
163	X<0?	16-45		219	+	-55	
164	GT03	22 03		220	JX	54	
165	N!	16 52		221	X	-35	
166	ST07	35 07		222	RCLC	36 15	
167	RCL2	36 02		223	X	-35	
168	RCLB	36 12		224	RTN	24	

CHECKS TO
SEE IF $\frac{E}{F}$ finished;
IF SO, COMPUTES
3J VALUE,
STORES IN
REGISTER E

COMPUTES
CLEBSCH-
GORDON
COEFFICIENT

LABELS				FLAGS	SET STATUS		
A	B	C	D	E	0	1	2
J_1	J_2	J	$\rightarrow C.G$				
m_1	m_2	-M					
0	1	2	3	4	5	6	7
		calc	calc				
5	6	7	8	9			

ON OFF

0 ☒ ☐

1 ☐ ☒

2 ☐ ☒

3 ☐ ☒

DEG ☒

GRAD ☐

RAD ☐

FIX ☐

SCI ☒

ENG ☐

n 9

Program Description I

Program Title 32-P REMAINING ON MM.DDYYYY GIVEN MCI ON
EARLIER MM.DDYYYY
 Contributor's Name GARY G. ALTMAN
 Address 3307 NORTHBROOK DRIVE
 City MIDDLETON State WISCONSIN Zip Code 53562

Program Description, Equations, Variables

1. JULIAN DAY NUMBER IS CALCULATED AS DESCRIBED IN THE HP-67 STANDARD PAC, PAGE 04-01; THE NUMBER OF DAYS BETWEEN DATE 1 AND DATE 2 IS ALSO CALCULATED AS DESCRIBED IN THE HP-67 STANDARD PAC.
2. RADIOACTIVE DECAY: $(\text{INITIAL mCi})(0.5)^n = \text{mCi on DATE 2}$, WHERE $n = 14.3 / \Delta \text{DAYS} = \text{THE NUMBER OF HALF-LIVES OF } ^{32}\text{P WHICH HAVE OCCURRED}$.
3. SUBROUTINE D YIELDS: mCi on DATE 2 ;
 $(\text{mCi on DATE 2})(2.2 \times 10^9 \text{ DPM}) = \text{DPM ON DATE 2}$;
 AND $(0.3)(\text{DPM}) \approx \text{CPM ON DATE 2}$
 [ASSUMES 30% COUNTING EFFICIENCY AND NO QUENCHING]
4. SUBROUTINE F C YIELDS:
 $(0.5)^n (\text{CPM ON DATE 1}) = \text{CPM ON DATE 2}$; AND
 $[(2.2 \times 10^9 \text{ DPM / mCi}) / (\text{CPM / .3})]^{-1} = \text{mCi ON DATE 2}$

Operating Limits and Warnings PROGRAM FAILS IF DATE 1 = DATE 2 OR
IF DATE 1 IS MORE RECENT THAN DATE 2.

This program has been verified only with respect to the numerical example given in *Program Description II*. User accepts and uses this program material AT HIS OWN RISK, in reliance solely upon his own inspection of the program material and without reliance upon any representation or description concerning the program material.

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Program Description II

65

Sketch(es)

Sample Problem(s) 1. HOW MANY DPM (AND CPM) REMAIN OF A 0.135 mCi ^{32}P SAMPLE? GIVEN: DATE OF SPECIFIC RADIOACTIVITY RATING AS FEB 2, 1977; AND TODAY'S DATE APRIL 22, 1977.

2. HOW MANY CPM (AND mCi) REMAIN OF A 3.2×10^6 CPM SAMPLE OF ^{32}P AS MEASURED BY CHERENKOV RADIATION ON AUGUST 11, 1976?

Solution(s) 1. 2.071977 A (DISPLAY: 2443182) 4.221977 B (DISPLAY: 2443256.) C (DISPLAY: 74., THE NUMBER OF DAYS BETWEEN FEB 7 AND APR 22) 0.135 D (DISPLAY: 8.2220×10^6 , 2.466×10^6 - THE DPM AND THE CPM REMAINING)
2. 8.111976 A (2443002.) 4.221977 B (2443256.) C (254. = ΔDAYS) 3.2 EEX 6 F C (ANSWERS: 14., 2.18×10^{-8} - 14 CPM REMAINING, 2.18×10^{-8} mCi REMAINING.)

Reference(s) CALENDAR FUNCTIONS, PAGE 04-01 IN HP-67 STANDARD PAC, AND CHASE, G.D. & J.L. RABINOWITZ, PRINCIPLES OF RADIOISOTOPE METHODOLOGY, BURGESS, MINNEAPOLIS, MN (1962).

[illegible]

6: Program Listing I

67

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
001	F LBL A	31 25 11		57	STO 7	33 07	
2	F FIX	31 23	CALC ΔDAYS	58	RCL A	34 11	CALC
3	DSP 2	23 02	AND PUT CONTROL	59	h X2Y	35 52	DAY OF MONTH
4	RCL 4	34 04	3 IN DISPLAY	060	RCL 6	34 06	
5	RCL C	34 13		61	X	71	
6	-	51		62	F INT	31 83	
7	3	03		63	-	51	
8	GTO 0	22 00		64	STO 6	33 08	
9	F LBL B	31 25 12		65	RCL 7	34 07	BUILD (m'-1).DD
010	RCL 3	34 03	CALCULATE	66	1	01	PART OF DISPLAY
11	RCL C	34 13	ΔDAYS AND PUT	67	RCL 8	34 08	
12	+	61	4 IN DISPLAY	68	F %	31 82	
13	4	04		69	-	51	
14	F LBL 0	31 25 00	STORE CONTROL	070	-	51	
15	h STO i	35 33	CODE	71	RCL 7	34 07	
16	h RV	35 53	STORE	72	1	01	CORRECT m'-1
17	3	03	CONSTANTS	73	4	04	AND Y' TO M
18	6	06		74	÷	81	AND Y.
19	5	05		75	GSB 2	31 22 02	
020	.	83		76	RCL 9	34 09	FINISH BUILDING
21	2	02		77	EEX	43	MM. DDYYYY
22	5	05		78	6	06	RESULT AND DISPLAY
23	STO 5	33 05		79	÷	81	ANSWER.
24	3	03		080	+	61	
25	0	00		81	DSP 6	23 06	
26	.	83		82	h RTN	35 22	
27	6	06		83	F LBL 1	31 25 01	BREAK DATE
28	0	00		84	h RV	35 53	INPUT INTO THE
29	0	00		85	↑	41	INDIVIDUAL
030	1	01		86	F INT	31 83	COMPONENTS OF
31	STO 6	33 06		87	STO 7	33 07	MM, DD, YYYY.
32	h RV	35 53	RETURN ΔDAYS	88	-	51	
33	h RV	35 53	TO DISPLAY	89	EEX	43	
34	h F3?	35 71 03	IF DATA INPUT	090	2	02	
35	GTO 1	22 01	GO TO 1	91	X	71	
36	h ST i	33 24	STORE ΔDAYS	92	↑	41	
37	1	01	ACCORDING TO	93	F INT	31 83	
38	2	02	CONTROL MODE	94	STO 8	33 08	
39	2	02		95	-	51	
040	.	83	CALC Y'.	96	EEX	43	
41	1	01		97	4	04	
42	-	51		98	X	71	
43	RCL 5	34 05		99	STO 9	33 09	
44	÷	81		100	RCL 7	34 07	m+1
45	F INT	31 83		101	1	01	
46	STO 9	33 09	CALC m'.	102	+	61	
47	RCL 5	34 05		103	↑	41	m+1 → m'
48	X	71		104	h 1/X	35 62	
49	F INT	31 83		105	.	83	
050	h RCL i	34 24		106	7	07	y → y'
51	-	51		107	+	61	
52	CHS	42		108	CHS	42	
53	STO A	33 11		109	GSB 2	31 22 02	
54	RCL 6	34 06		110	RCL 6	34 06	COMPUTE
55	÷	81		111	X	71	JULIAN DAY
56	F INT	31 83		112	F INT	31 83	NUMBER

REGISTERS

0	1	2	3 DAY 1	4 DAY 2	5 365.25	6 30.6001	7 MM	8 DD	9 YYYY
S0	S1	S2	S3	S4	S5	S6	S7	S8	S9
A USED	B	C A DAYS	D	E	I CONTROL				

67 Program Listing II

STEP	KEY ENTRY	KEY CODE	COMMENTS	STEP	KEY ENTRY	KEY CODE	COMMENTS
113	RCL 9	34 09		169	RCL 2	34 02	
114	RCL 5	34 05		170	\div	81	
115	X	71		171	$h y^x$	35 63	$(\frac{1}{2})^n$
116	F INT	31 83		172	$h 1/x$	35 62	
117	$+$	61		173	RCL 0	34 00	
118	RCL 8	34 08		174	RCL 1	34 01	
119	$+$	61		175	X	71	
120	h STI	33 24		176	X	71	
121	1	01		177	g SCI	32 23	
122	7	07		178	DSP 4	23 04	
123	2	02		179	f-X-	31 84	DISPLAY DPM
124	ϕ	00		180	\uparrow	41	
125	9	09		181	\cdot	83	
126	8	08		182	3	03	
127	2	02		183	X	71	
128	$+$	61		184	f-X-	31 84	DISPLAY CPM
129	DSP ϕ	23 00		185	h RTN	35 22	
130	h RTN	35 22		186	g LBL C	32 25 13	
131	F LBL 2	31 25 02	IF INPUT TO THIS ROUTINE HAS ABS VALUE OF 1 OR >	187	STO A	33 11	STORE CPM
132	F INT	31 83	$Y = Y \pm 1$	188	RCL C	34 13	
133	STO + 9	33 61 09	$M = M \pm 12$	189	RCL 2	34 02	$\frac{\Delta \text{DAYS}}{14.3} = n$
134	1	01	(+ FOR PLUS INPUT)	190	\div	81	
135	2	02	STORE INPUT	191	\cdot	83	
136	X	71		192	5	05	
137	-	51		193	$h x \rightarrow y$	35 52	
138	h RTN	35 22		194	$h y^x$	35 63	$(\frac{1}{2})^n$
139	F LBL C	31 25 13		195	RCL A	34 11	
140	DSP ϕ	23 00		196	X	71	
141	STO C	33 13		197	f-X-	31 84	DISPLAY CPM
142	h F3	35 71 03	IF INPUT FLAG TRUE, THEN STOP	198	\cdot	83	
143	h RTN	35 22	COMPUTE Δ DAYS AND STOP	199	3	03	
144	RCL 4	34 04		200	\div	81	
145	RCL 3	34 03		201	RCL 1	34 01	
146	-	51		202	\div	81	
147	STO C	33 13		203	h RTN	35 22	DISPLAY mCi
148	h RTN	35 22					
149	h F3	35 71 03					
150	STO 4	22 04					
151	F STO C	31 22 13	COMPUTE Δ DAYS				
152	DSP 1	23 01					
153	F LBL D	31 25 14	STORE CONSTANTS				
154	STO ϕ	33 00					
155	1	01					
156	4	04					
157	\cdot	83					
158	3	03					
159	STO 2	33 02					
160	2	02					
161	\cdot	83					
162	2	02					
163	EEX	43					
164	9	09					
165	STO 1	33 01					
166	F LBL E	31 25 15					
167	2	02	$\frac{\Delta \text{DAYS}}{14.3} = n$				
168	RCL C	34 13					

LABELS

A	DATE 1	B	DATE 2	C	Δ DAYS	D	mCi \rightarrow CPM	E	
a		b		c	CPM \rightarrow mCi	d		e	
0	CALC	1		2		3		4	
5		6		7		8		9	

FLAGS

0		1		2		3	INPUT
---	--	---	--	---	--	---	-------

SET STATUS

FLAGS		TRIG		DISP
0	<input type="checkbox"/> <input checked="" type="checkbox"/>	DEG	<input checked="" type="checkbox"/>	FIX <input type="checkbox"/>
1	<input type="checkbox"/> <input checked="" type="checkbox"/>	GRAD	<input type="checkbox"/>	SCI <input type="checkbox"/>
2	<input type="checkbox"/> <input checked="" type="checkbox"/>	RAD	<input type="checkbox"/>	ENG <input type="checkbox"/>
3	<input type="checkbox"/> <input checked="" type="checkbox"/>			n _____

NOTES

NOTES

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