

PocketProfessional®

EE•Pro™

User's Guide

SPARCOM CORPORATION

Edition 2: April 1994

Software Reorder No. 10211-1A

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In memory of
Amy Lynne Otto

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Contents

Notice	iii
Customer Support	iii
Credits	iv

Contents	v
-----------------------	----------

1	Getting Started.....	1
----------	-----------------------------	----------

Key Features of EE•Pro	2
How to Use This Manual	2
Manual Conventions	3
Differences between HP 48GX and HP 48SX	4
Memory Requirements.....	5
Environmental Limits.....	5
Installing and Removing a Card.....	5
Starting EE•Pro.....	7
Using the Home Screen.....	8
Navigating through EE•Pro	8
Options Menu.....	9
Custom Settings Screen.....	11

Part 1: Analysis

2	Analysis: Navigation Guide	15
	Introduction	15
	Finding Analysis	16
	Analysis Screens	16
	Example: Parallel RLC Circuit.....	20
3	AC Circuits	21
	Impedance Calculations	21
	Voltage Divider	22
	Current Divider	23
	Circuit Performance	24
	Wye \leftrightarrow Δ Conversion	26
4	Polyphase Circuits	28
	Wye \leftrightarrow Δ Conversion	28
	Balanced Wye Load	30
	Balanced Δ Load	31
5	Ladder Network	34
	Using Ladder Network	34
6	Filter Design	41
	Chebyshev Filter	41
	Butterworth Filter	43
	Active Filter.....	45

7	Gain and Frequency	48
	Transfer Function	48
	Bode Plots	50
8	Fourier Transforms.....	52
	FFT.....	52
	Inverse FFT	53
9	Two-Port Networks	54
	Parameter Conversion	54
	Circuit Performance	56
	Interconnected Two-Ports	58
10	Transformer Performance.....	61
	Open Circuit Test	61
	Short Circuit Test	62
	Chain Parameters	64
11	Transmission Lines	66
	Line Characteristics.....	66
	Line Parameters.....	68
	Fault Location Estimate	69
	Stub Impedance Matching.....	70
12	Computer Engineering	72
	Binary Modes Screen	72
	Binary Arithmetic.....	73
	Register Operations	74
	Bit Operations	76
	Binary Conversions.....	77
	Binary Comparisons.....	78
	Karnaugh Map.....	79

13 Algebraic Functions..... 81

 Partial Fraction Expansion81

 Piecewise Functions82

 Polynomial Coefficients.....85

 Polynomial Equation85

 Polynomial Roots86

 Symbolic Simplification.....87

 Taylor Polynomial.....88

14 Error Functions 89

 Using Error Functions89

15 Capital Budgeting..... 90

 Using Capital Budgeting90

16	Equations: Navigation Guide.....	97
	Introduction.....	98
	Finding Equations.....	98
	Equations Screens.....	99
	Solver Screens.....	100
	Plotter Screens.....	106
	Example: Overdamped Parallel RLC Circuit.....	110
17	Resistive Circuits	113
	Variables	113
	Resistance and Conductance	114
	Ohm's Law and Power.....	114
	Temperature Effect	115
	Maximum Power Transfer	115
	V and I Source Equivalence.....	116
18	Capacitance and Electric Fields	117
	Variables	117
	Point Charge.....	118
	Long Charged Line	118
	Charged Disk.....	118
	Parallel Plates	119
	Parallel Wires	119
	Coaxial Cable.....	120
	Sphere	120
19	Inductance and Magnetism	121
	Variables	121
	Long Line.....	122
	Long Strip	122

Parallel Wires	123
Loop	123
Coaxial Cable	124
Skin Effect.....	124

20 Electron Motion 125

Variables	125
Electron Beam Deflection	126
Thermionic Emission	126
Photoemission	126

21 Meters and Bridge Circuits..... 128

Variables	128
Amp, Volt, and Ohmmeter	129
Wheatstone Bridge	130
Wien Bridge	130
Maxwell Bridge.....	131
Owen Bridge	131
Symmetrical Resistive Attenuator	132
Unsymmetrical Resistive Attenuator.....	132

22 RL and RC Circuits..... 134

Variables	134
RL Natural Response.....	135
RC Natural Response	135
RL Step Response	136
RC Step Response	136
RL Series to Parallel.....	137
RC Series to Parallel.....	138

23 RLC Circuits 139

Variables	139
Series Impedance.....	140
Parallel Admittance	141
RLC Natural Response	141
Underdamped Transient.....	142

	Critically-Damped Transient.....	142
	Overdamped Transient.....	143
24	AC Circuits	144
	Variables	144
	RL Series Impedance	145
	RC Series Impedance	146
	Impedance \leftrightarrow Admittance	146
	Two Impedances in Series	147
	Two Impedances in Parallel	148
25	Polyphase Circuits	149
	Variables	149
	Balanced Δ Network	149
	Balanced Wye Network	150
	Power Measurements	150
26	Electrical Resonance.....	151
	Variables	151
	Parallel Resonance I.....	152
	Parallel Resonance II.....	152
	Resonance in Lossy Inductor	153
	Series Resonance.....	154
27	OpAmp Circuits	155
	Variables	155
	Basic Inverter	156
	Non-Inverting Amplifier	157
	Current Amplifier.....	157
	Transconductance Amplifier.....	158
	Level Detector (Inverting).....	158
	Level Detector (Non-Inverting)	159
	Differentiator.....	159
	Differential Amplifier	160

28 Solid State Devices 161

Variables161
Semiconductor Basics165
PN Junctions.....166
PN Junction Currents166
Transistor Currents167
Ebers-Moll Equations.....168
Ideal Currents - pnp.....168
Switching Transients169
MOS Transistor I.....170
MOS Transistor II171
MOS Inverter (Resistive)172
MOS Inverter (Saturated).....172
MOS Inverter (Depletion)173
CMOS Transistor Pair174
Junction FET175

29 Linear Amplifiers 176

Variables176
BJT (Common Base).....177
BJT (Common Emitter).....178
BJT (Common Collector).....178
FET (Common Gate).....179
FET (Common Source)179
FET (Common Drain)180
Darlington (CC-CC)180
Darlington (CC-CE)181
Emitter-Coupled Amplifier181
Differential Amplifier182
Source-Coupled JFET Pair.....182

30 Class A, B, and C Amplifiers 183

Variables183
Class A Amplifier.....184
Power Transistor185
Push-Pull Principle.....186
Class B Amplifier.....186
Class C Amplifier187

31	Transformers	188
	Variables	188
	Ideal Transformer.....	189
	Linear Equivalent Circuit.....	189
32	Motors and Generators	190
	Variables	190
	Energy Conversion.....	192
	DC Generator	192
	Separately-Excited DC Generator	193
	DC Shunt Generator	194
	DC Series Generator	194
	Separately-Excited DC Motor	195
	DC Shunt Motor.....	195
	DC Series Motor	196
	Permanent Magnet Motor	197
	Induction Motor I.....	197
	Induction Motor II.....	198
	Single-Phase Induction Motor.....	199
	Synchronous Machines	199

Part 3: Reference

33	Reference: Navigation Guide	203
	Introduction	203
	Finding Reference	204
	Reference Screens	204
34	Resistor Color Chart	207
35	Standard Component Values	209
36	Semiconductor Properties	211
37	Boolean Expressions	214
38	Boolean Algebra Properties	216
39	Transforms	218
40	Constants.....	220

41 SI Prefixes222

42 Greek Alphabet223

Part 4: Programming & Advanced Use

43 Programmable Commands..... 227

Using Programmable Commands.....	228
Object Syntax.....	228
EE Library Commands.....	229
AC Circuits.....	229
Polyphase Circuits.....	230
Filter Design.....	231
Gain and Frequency	232
Fourier Transforms.....	233
Two-Port Networks.....	233
Transformer Performance	234
Transmission Lines	235
Binary Arithmetic.....	235
Register Operations.....	236
Bit Operations	237
Binary Conversions.....	237
Binary Comparisons.....	237
Binary Modes.....	238
Miscellaneous Binary Operations.....	238
Karnaugh Map.....	239
Algebraic Functions	239
Error Functions.....	240
Capital Budgeting.....	240
Reference.....	240

44 Programmable Screens 242

Using Programmable Screens	242
Analysis Screens	243
Equations Screens	244
Reference Screens	248

45 Tips for Using the Solver249

Creating a Working Directory.....249

How are Multiple Equations Solved?.....250

Using Guesses to Improve Solving250

Solver Icons.....251

46 Tips for Using the Plotter253

Appendixes and Index

A	Service and Warranty.....	257
	Technical Support	257
	Shipping Instructions.....	258
	Service Charge for Out-of-Warranty Cards	258
	Limited 90-Day Warranty	259
B	Key and Screen Summary	260
	Screen Summary	261
	Key Summary.....	262
C	User Flags.....	268
	Flag 4: Carry Flag	268
	Flag 5: Range Flag	268
	Flags 13 and 14: Binary Sign Mode.....	269
	Flag 57: Font Size	269
	Flag 58: Help Text.....	270
	Flag 61: Units	270
	User Flag Summary.....	271
D	Questions and Answers	272
	General Questions	272
	Analysis Questions	274
	Equations Questions	275
	Reference Questions.....	277
	Index.....	278

Chapter 1

Getting Started

PocketProfessional® software is the first of its kind, developed to provide speed, efficiency and portability to students and professionals in technical fields. When you slide a PocketProfessional plug-in card into your HP 48GX or HP 48SX, your calculator is instantly transformed into an electronic “textbook,” ready to efficiently solve your technical problems.

PocketProfessional EE•Pro™ is state-of-the-art electrical engineering software for the HP 48GX and HP 48SX calculators. Sparcom Corporation thanks all the current owners of our PocketProfessional software for their many helpful suggestions and comments.

This chapter covers:

- ☐ Key Features of EE•Pro 2
- ☐ How to Use This Manual 2
- ☐ Manual Conventions 3
- ☐ Differences between HP 48GX and HP 48SX 4
- ☐ Memory Requirements..... 5
- ☐ Environmental Limits..... 5
- ☐ Installing and Removing a Card..... 5
- ☐ Starting EE•Pro 7
- ☐ Using the Home Screen..... 8
- ☐ Navigating through EE•Pro 8
- ☐ Options Menu..... 9
- ☐ Custom Settings Screen..... 11

NOTE



Please retain the software license agreement printed on the envelope your EE•Pro card came in. It contains important information regarding your rights.

Key Features of EE•Pro

- ❑ *Highest speed and performance of any HP 48 software sold today*
- ❑ *Easy-to-use, menu-based interface*
- ❑ *Context-sensitive help text for every screen*
- ❑ *Advanced electrical engineering analysis routines, equations, and reference tables*
- ❑ *Integrated access to the HP 48 stack for calculations*
- ❑ *Comprehensive documentation for quick reference*
- ❑ *Learn one Pro product and you can use them all!*

How to Use This Manual

This manual is designed as a learning and reference tool to be used with your PocketProfessional EE•Pro software. This section explains the layout of the manual.

Manual Organization

The manual is divided into four parts: Analysis, Equations, Reference, and Programming & Advanced Use. These sections mirror the divisions within EE•Pro, with the addition of an advanced section for experienced users.

Part 1: Analysis includes analysis routines to perform calculations, such as AC circuit analysis, two-port networks, and computer engineering. Easy-to-use, intuitive analysis screens are available for each routine.

Part 2: Equations includes an equation library of over five hundred solvable equations organized in related groups. Full descriptions of each variable, a variety of user-selectable units, and appropriate diagrams are included.

Part 3: Reference includes reference tables based on information in standard reference books, such as Laplace transform tables, semiconductor properties, and donor and acceptor levels in silicon.

Part 4: Programming & Advanced Use includes detailed syntax for each programmable command included in EE•Pro and other tips for experienced users.

What to Read Next...

To get the most information from this manual, read the following sections:

1. Read all of this chapter, “Getting Started.” You will learn how to install EE•Pro, and you will be introduced to the menus and screens of EE•Pro, which provide easy-to-use access to all the features.
2. Read the Navigation Guides for Analysis, Equations and Reference (Chapters 2, 16, and 33). You will learn how to use each major section of EE•Pro through step-by-step instructions and context-sensitive help.
3. Use the table of contents and index to locate further topics of interest.
4. Refer to Appendix D, “Questions and Answers,” to answer the most commonly asked questions about EE•Pro.

Manual Conventions





There are a few simple conventions used throughout this manual:










- The heading of each chapter and its modules displays a “map” of the path taken to get to that particular section. For example, the Impedance Calculations analysis section is in the chapter on AC Circuits, in the Analysis section. The heading shows this path. Keep in mind that there may be several sections within the AC Circuits chapter. The heading only shows the current one.


Impedance Calculations

Analysis
AC Circuits
<i>Impedance Calculations</i>
Equations
Reference

- Keys on the HP 48 keyboard are shown in a boxed typeface, such as **ENTER**.
- Boxed typeface is also used to indicate the green and purple key labels (HP 48GX) or the blue and orange key labels (HP 48SX) located above the keys. For instance, on the HP 48 GX, the I/O command is a green label located above the **1** key, and is accessed by pressing the green shift key then the **1** key. In this manual, these keystrokes are represented in the following manner: **I/O**.













Similarly, with the HP 48SX, the I/O command is an orange label located above the  key, and is accessed by pressing the orange shift key then the  key. In this manual, these keystrokes are represented in the following manner:  .

- Keys which should be pressed at the same time are indicated with a hyphen between them: -. **Do not press the minus key.**
- Menu keys are located at the bottom of the HP 48 screen and correspond directly to the top row of keys on the HP 48 keyboard. They are shown in inverse typeface, such as .
- Programmable commands are shown in uppercase letters, such as SIN. Uppercase is also used to show field names, like RESULT, which are displayed on the HP 48 screen.
- Steps to be followed in a particular order are numbered: 1, 2, 3, etc.
- HP 48 variables/directories are listed in single quotes, such as 'SPARCOM'.
- Equation variables are shown in boldface to separate them from the text, as in: “The source current and impedance are **Is** and **Zs**, respectively.”
- All examples assume that pressing   locks the Alpha entry mode. If you have set the HP 48 system flag -60, press  instead of   to lock Alpha entry mode.
- In each example, there is a box listing the mode settings for that example. To change the modes, press the  key at any EE•Pro screen. Most examples are in the following modes:

MODES (Press )	∠:	Degrees	Result:	Symbolic
	Coord:	Rectangular	Units:	On or Off
	Format:	Standard	Help:	On
	Digits:	N/A	Font:	Small

Differences between HP 48GX and HP 48SX

This manual was written using the HP 48GX as the standard, with notations made for the HP 48SX where necessary. The following keys are different between the HP 48GX and HP 48SX, but they perform the same function:

HP 48GX	HP 48SX	Description
 	 	Displays all libraries.
 - 	 - 	Performs a screen dump.
 	 	Displays an item if it is too wide for the screen.

Memory Requirements

A minimum of 5 Kbytes of free memory is needed for using *EE•Pro*, although complicated operations may require more memory. If *EE•Pro* seems to be functioning incorrectly, low memory may be the cause. For more information about free memory, see your HP 48 User's Guide. If you are using *EE•Pro* in Card Slot 2 of an HP 48GX and you receive the error message, "Insufficient Memory," you should reinstall *EE•Pro* in Card Slot 1, which requires less memory overhead. See "Installing and Removing a Card" below for more information about how to switch *EE•Pro* from Card Slot 2 to Card Slot 1.

Environmental Limits

The reliability of a PocketProfessional plug-in card depends upon the following temperature and humidity limits:

- **Operating Temperature:** 0 to 45° C (32 to 113° F).
- **Storage Temperature:** -20 to 60° C (-4 to 140° F).
- **Operating and Storage Humidity:** 90% relative humidity at 40° C (104° F) maximum.

Installing and Removing a Card


The HP 48GX and HP 48SX have two ports for installing PocketProfessional plug-in cards. A card can be installed in either port. Due to the manner in which the HP 48GX manages memory, *EE•Pro* will perform better in Card Slot 1 of an HP 48GX. *EE•Pro* will perform equally well in either card slot on the HP 48SX.

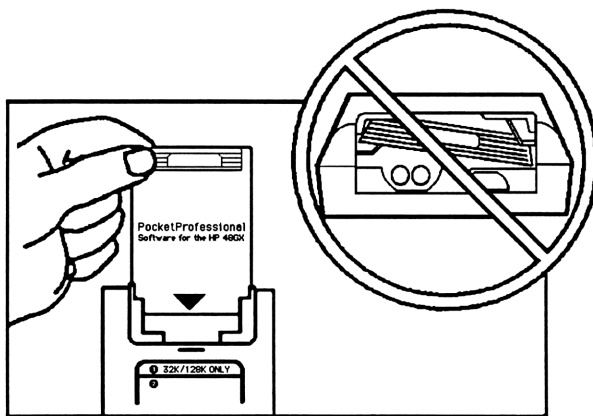
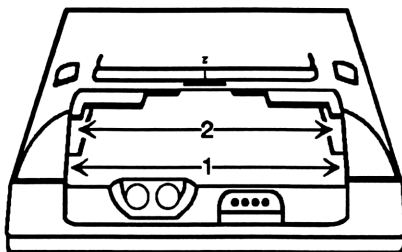
WARNING


Turn off the HP 48 *before* installing or removing a card!
Otherwise, user memory may be erased.

Installing a Card

To install a card, follow these steps:




1. Press  **OFF** to turn the HP 48 off. Do not turn it back on until you have completed the installation procedure.
2. Remove the port cover.
Press against the grip lines and push forward.
Lift the cover to expose the two plug-in ports, as shown to the right:
3. Select either empty port for the card, and position the card just outside the slot. (HP 48GX users will find that placing the card in Port 1 gives optimal performance.) Point the triangular arrow on the card toward the HP 48 port opening, as shown below:

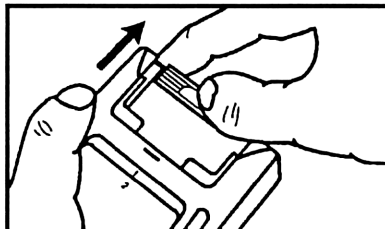


4. Slide the card firmly into the slot. After you first feel resistance, push the card further (about 5-6 mm or about 1/4 inch), until it is fully seated.
5. Replace the port cover. Press  **ON** to turn the HP 48 on.

Removing a Card










To remove a card, follow these steps:

1. Press   to turn the HP 48 off. Do not turn it back on until you have removed the card.
2. Remove the port cover. Press against the grip lines and push forward. Lift the cover to expose the two plug-in ports, as shown in “Installing a Card.”
3. Press against the card’s grip and slide the card out of the port, as shown.
4. Replace the port cover. Press  to turn the HP 48 on.



Starting EE•Pro











To start EE•Pro, follow these steps:

1. Install the card as described above and press  to turn the HP 48 on.
2. HP 48GX: Press   to display the available libraries.
HP 48SX: Press   to display the available libraries.
3. Press  to display the EE•Pro library menu.
4. Press   to start EE•Pro, or press  to display product information and the current version of EE•Pro. The other menu keys in the EE•Pro library menu are covered in Chapter 43, “Programmable Commands.”







NOTE



At any point, you can exit EE•Pro and return to the HP 48 stacks by pressing . You can return to EE•Pro at exactly the same point you left it, by pressing   (GX) or   (SX)  , or by typing   EE .

Using the Home Screen



The home screen appears when you start *EE•Pro* for the first time. It can also be reached by pressing  **HOME** from any *EE•Pro* screen.

The home screen lists the three major sections of *EE•Pro*: Analysis, Equations, and Reference. To select a section, move the highlight bar up or down ( or ) to the desired section and press **ENTER** or .



NOTE





To move back to a previous screen at any time, press  or **UP**. To return to the home screen at any time, press  **HOME** or **HOME**.


- ABOUT** Displays product information and current version of *EE•Pro*.
- VIEW** Displays the highlighted item on the screen by itself, in the large font (text view). This is useful if the item scrolls off the right side of the screen with an ellipsis (“...”) displayed.
- FIND** Searches for the specified character or string. To perform a search, enter a letter or string of letters of the desired word or sequence and press **ENTER**. **FIND** only searches the current screen for a match.
- OPTS** Displays the options menu. See “Options Menu,” page 9.
- PATH** Displays screens chosen to reach the current screen. After pressing this key, you will see the path listing in the title bar of the screen. Press **→STK** to place this path list on the stack. This can then be used to create a quick link to that specific screen. See chapter 44 “Programmable Screens” for more details.
- QUIT** Quits *EE•Pro* and returns to the HP 48 stack.


At screens other than the home screen, two new menu keys may appear:

- HOME** Goes to the home screen.
- UP** Goes to the previous screen.

Navigating through *EE•Pro*


The HP 48 arrow keys are your navigation tools for accessing every part of *EE•Pro*. The right arrow  takes you to the next screen. The left arrow  takes you to the previous screen. When you have gone as far as you can go in one path, for instance:


Analysis 


AC Circuits 

Impedance Calculations 

To return to the previous screens, press:

 Impedance Calculations

 AC Circuits

 Analysis

or press  **HOME** to return to the home screen.

The up arrow  and down arrow  allow you to move the highlight bar from one line to another, selecting a new topic or a new field.

Options Menu

The options menu helps you customize settings for EE•Pro and is available throughout the software. These settings apply to EE•Pro only, not to the HP 48 stack.

To access the options menu, press **OPTS** or  **CST**. This will display the following menu keys:

SPD: ▮ Changes the scrolling speed of the highlight bar. The bar inside the key (**SPD: ▮**), shows the current level of speed: a tall bar indicates fast scrolling speed, while a short bar indicates slow scrolling speed. To change the speed, press the **SPD: ▮** button to step through the choices.

UNITS Toggles units on or off. When the block inside the key appears (**UNIT ▮**), units are turned on.

HELP Toggles display of help text on the bottom of the screen. When the block inside the key appears (**HELP ▮**), help is turned on.

FONT Toggles font size between large and small. The default setting is the small font, which displays information in condensed, uppercase letters only. The large font displays information in a larger, case-sensitive font.

EXIT Leaves the options menu. Returns to the regular menu.



For more options, press **[NXT]** to display the following additional menu keys (you can also display these menu keys by pressing **[CST]**):

→STK Copies one or all of the items shown to the HP 48 stack. Pressing this key prompts you for **[ONE]** or **[ALL]**. If you decide not to copy the item to the stack, press **[ON]** to cancel.



[VIEW] Displays the highlighted item in a text view. This is useful if the item scrolls off the right side of the screen with “...” (an ellipsis) displayed.

If the highlighted item is an equation, pressing **[→]** or **[←]** **[VIEW]** displays the equation in graphics view.

[FIND] Searches for a specified character or string. To perform a search, enter a letter or string of letters of the desired word or sequence and press **[ENTER]**. **[FIND]** only searches the current screen for a match. See detailed explanation below, “Using the Find Option.”

[PRINT] Prints one or all of the items shown to an HP 48 printer.

[PATH] Displays screens chosen to reach the current screen. After pressing this key, you will see the path listing in the title bar of the screen. Press **→STK** to place this path list on the stack. This can then be used to create a quick link to that specific screen. See chapter 44 “Programmable Screens” for more details.

[EXIT] Leaves the options menu. Returns to the regular menu.

Press **[←]** **[PREV]** or **[NXT]** to go to the previous “page” of menu keys.

Using the Find Option

To initiate a search, press **[FIND]** to display the following screen:

The HP 48 is now ready to search for the information entered at the command line. The calculator is automatically locked in alpha entry mode, which activates the capital letters printed in white to the lower right of selected keys.



To perform a search, enter a letter or string of letters of the desired word or sequence and press **[ENTER]**. The find function is not case-sensitive. **[FIND]** then searches the current screen for a match. To abort the search, press **[ON]** (Cancel). To repeat the search, press the **[FIND]** key again and the last search string will be displayed. Press the **[ENTER]** key to renew the search.

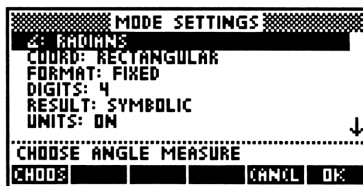
The menu keys on the Find screen are the standard HP 48 editing keys and are described below. To use these keys, turn the Alpha lock off by pressing α . To turn Alpha lock back on, press α α .

- ←SKIP** Moves the cursor to the beginning of the current word.
- SKIP→** Moves the cursor to the beginning of the next word.
- ←DEL** Deletes the characters from the beginning of the word to the cursor.
- DEL→** Deletes the characters from the cursor to the end of the word.
- INS•** Switches the entry mode between *Insert* mode (← cursor) and *Replace* mode (█ cursor). A █ in the menu key indicates Insert mode is active.
- ↑STK** Allows you to copy an item from the HP 48 stack:
 1. Press α to cancel the alpha-entry mode, then press **↑STK** to go to the HP 48 stack.
 2. Use the arrow keys to select the stack level with the desired item.
 3. Press **ECHO** then **ENTER** to copy the item into the 'Find' string.

Custom Settings Screen

The custom settings screen is displayed by pressing **CST**. This screen sets the default settings for the HP 48 and *EE•Pro*. Once you leave the *EE•Pro* program, these settings will still remain in effect. The custom settings screen is available throughout *EE•Pro*.

To change any of these settings, move the highlight bar to the desired item and press **CHOOS** or α . Then press **OK** to implement the changes, or to exit the screen without changing the settings, press **CANCL** or **ON**.



- ∠:** (*Angle measure*) Press **CHOOS** or **ENTER** to select degrees, radians, or grads. Determines how angular functions interpret angular inputs and what angle measure is used to display angular outputs.
- Coord:** (*Coordinate system*) Press **CHOOS** or **ENTER** to select rectangular, polar or spherical. Determines whether complex numbers are displayed as (x,y) or (r,∠θ).
- Format:** (*Number format*) Press **CHOOS** or **ENTER** to select Standard, Fixed, Scientific or Engineering.
- Digits:** (*# of decimal places displayed*) Type in the desired number of decimal places. (This field disappears when Standard number format has been selected.)

Result: (*Result mode*) Press **CHOOS** or **ENTER** to select symbolic or numeric. Determines whether some functions return symbolic or numeric results.

Units: (*Units*) Press **CHOOS** or **ENTER** to select on or off. Determines whether units are on or off for Equations and Reference. In the Analysis sections units are disregarded completely, so the units setting makes no difference.

Help: (*Help text*) Press **CHOOS** or **ENTER** to select on or off. Determines whether context-sensitive help text is displayed on the screen.

Font: (*Font size*) Press **CHOOS** or **ENTER** to select on or off. Determines whether items are displayed in large or small font.

Analysis

Chapter 2

Analysis: Navigation Guide

Analysis
Equations
Reference

This chapter is designed as a navigation guide to introduce you to the Analysis section, show you the keys available at each screen, and describe the types of input fields you will encounter. At the end of the chapter is a detailed Analysis example.

Introduction.....	15
Finding Analysis.....	15
Analysis Screens.....	16
Using Analysis Routines.....	17
Analysis Menu Keys.....	18
Example: Parallel RLC Circuit.....	20

Introduction









EE•Pro is divided into three major sections: Analysis, Equations, and Reference. This chapter addresses the Analysis section, which includes analysis routines covering AC circuits, polyphase circuits, ladder networks, filter design, gain and frequency, Fourier transforms, two-port networks, transformer performance, transmission lines, computer engineering, algebraic functions, error functions, and capital budgeting.





The Analysis routines are indispensable tools for performing quick calculations. You can design filters, evaluate performance of two-port networks, calculate transmission line properties, design transformers or minimize logic networks, draw the classic Bode plot, and determine capital budget constraints—all with context-sensitive help.

Finding Analysis



The Analysis section is found at the home screen of EE•Pro.

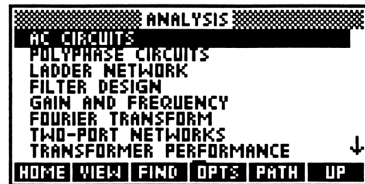
1. Start EE•Pro:



- HP 48GX: Press    .
- HP 48SX: Press    .
- Press   to show the home screen.

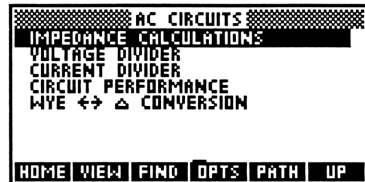
EE•Pro is structured with a hierarchy of screens for choosing a specific topic or item. This is the home screen. To return here at any time, press   or  .



2. Select Analysis by moving the highlight bar to Analysis and pressing  or . The screen now displays Analysis as its title and a list of Analysis sections from which to choose.



3. Choose an Analysis section by moving the highlight bar to the desired item and pressing  or . This will display a list of topics for the selected section. For the purposes of this navigation guide, select AC Circuits, then Impedance Calculations.

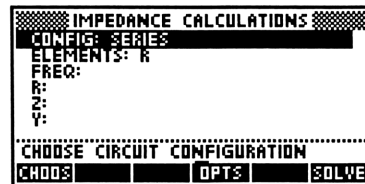


Pressing  (if available) or  returns you to the previous screen.

Pressing  (if available) or   returns you to the home screen.

Analysis Screens

An Analysis screen displays a list of fields for entering and displaying data. The screen to the right is the Impedance Calculations screen. To get to this screen, select Analysis, then AC Circuits, then Impedance Calculations (as described above). The main part of the screen contains input fields for data entry and




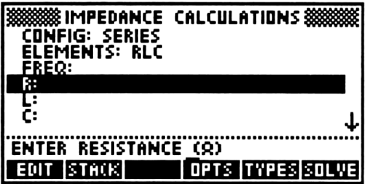
result fields for displaying calculated results. The help text at the bottom of the screen describes the action required for the highlighted field or the type of result to be displayed. In screens with numerous fields, you may want to turn the help text off to view more of the fields at one time. See “Options Menu,” page 9 for more information.

Analysis modules which contain more than two or three result fields will display those results in a separate output screen. To view the output screen, input values for the necessary fields and press **SOLVE**.

Using Analysis Routines

The instructions below are general instructions for using Analysis routines. For a detailed example using Impedance Calculations, see page 20. In addition, each section in each Analysis chapter contains at least one example.

1. Choose parameters (if available). In the screen for Impedance Calculations to the right, the **Config** and **Elements** fields are *choose* fields and contain a list of items for selection. Press **CHOOS** to access this list, or press  to step through the choices.



NOTE






Some choose fields affect the appearance of the remaining fields. For instance, choosing RLC in the **Elements** field here displays all the remaining input fields: **Freq**, **R**, **L**, and **C**. However, if **R** is chosen in the **Elements** field, only the relevant fields **Freq** and **R** appear.

2. Enter values into the *edit* fields. In this screen, the **Freq**, **R**, **L**, and **C** are edit fields. The values are to be entered as real numbers, but they will be interpreted as being in the units specified in the help text at the bottom of the screen. In this screen, the resistance entered in field **R** will be assumed to be a quantity of ohms.

NOTE



If an edit field requires a delimiter, it will automatically be inserted. Typical delimiters are: { } for a list, [] for an array, ' ' for a symbolic expression, and # for a binary number.

3. Press **SOLVE** to calculate the result of the analysis.
4. The result appears in the *result* field(s) – in this case, **Impedance** and **Admittance**.
Some Analysis modules have too many result fields to display on the input screen. In that case, a separate output screen is displayed with all the result fields.
5. When finished press  to return to the AC Circuits screen or press 
 to return to the home screen.



Analysis Menu Keys

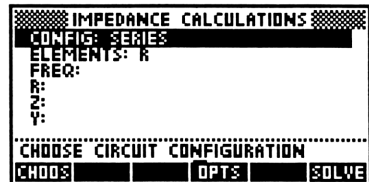
The menu keys in Analysis screens change depending on the type of field that is highlighted. Analysis screens use three basic types of fields: choose fields, edit fields and result fields. These fields and their associated menu keys are outlined below. The **OPTS** and **SOLVE** menu keys are always present, regardless of the field type.

Input Screens

Input screens contain fields for entering data and, in some cases, for displaying the results of the calculations. The screen below is the Impedance Calculations input screen.

Choose Fields: These fields only accept values from a pre-defined list that is accessed by pressing **CHOOS**. In this example, both **Config** and **Elements** are choose fields.



CHOOS Displays the possible choices for a choose field. In the list of choices, highlight the desired item and press  or , or press **CANCL** to abort the selection.



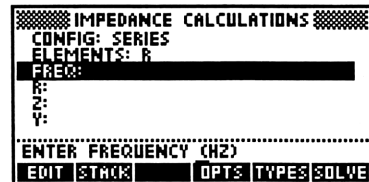
OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

SOLVE Performs a calculation using the inputs that have been entered. The result is displayed in the result field(s).

Edit Fields: These fields accept values entered from the keyboard. In this example, **Freq**, **R**, **L**, and **C** are edit fields.

EDIT Edits the highlighted item. The menu keys then change to the standard HP 48 editing keys. Press  to save edit changes or  to cancel editing.

STACK Copies the highlighted item to



the HP 48 stack and temporarily goes to the HP 48 stack environment. While at the stack, you can use all the normal built-in functions of your HP 48 to manipulate or change the copied item. When you have finished editing the item, press **OK** to leave the stack and insert the edited item into the current edit field, or press **CANCEL** to leave the stack without changing the value of the current edit field.

OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

TYPES Displays the allowed object types, such as real number, list, array, algebraic, etc. Move the highlight bar to the desired input type and press **OK** or **ENTER** to start a new item of that type, with the appropriate delimiters, on the command line. Or press **CANCEL** to return to the Analysis screen.

SOLVE Performs a calculation using the entered values. The result is displayed in the result field(s).

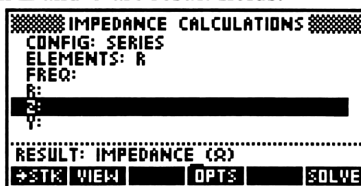
Result Field: These fields display the result of a calculation. In the Impedance Calculations screen, both **Z** and **Y** are result fields.

→STK Copies one or all of the items shown to the HP 48 stack. For more information, see “Options Menu,” page 9.

VIEW Displays the highlighted item in a text view. For more information, see “Options Menu,” page 9.

OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

SOLVE Performs a calculation using the entered values. The result is displayed in the result field(s).



Output Screens

Output screens contain *only* result fields, so the menu keys are the same as those above, with the addition of an **EXIT** key. The screen below is the output screen from the Circuit Performance example in the AC Circuits chapter, see page 24.

→STK Copies one or all of the items shown to the HP 48 stack. For more information, see “Options Menu,” page 9.

VIEW Displays the highlighted item in a text view. For more information, see “Options Menu,” page 9.



OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

EXIT Returns to the input screen.

NOTE



Pressing **HOME** will not work at an output screen. To return to the home screen, first press **EXIT** to return to the input screen, *then* press **HOME** or **◀**.

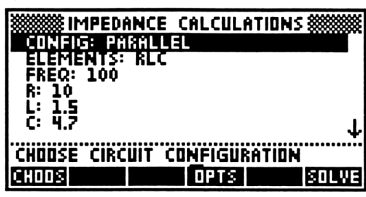
Example: Parallel RLC Circuit

MODES (Press CST)	∠: Degrees Coord: Polar Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Compute the impedance of a parallel RLC circuit with a 10 ohm resistor, a 1.5 Henry inductor and a 4.7 farad capacitor at a frequency of 100 hertz.

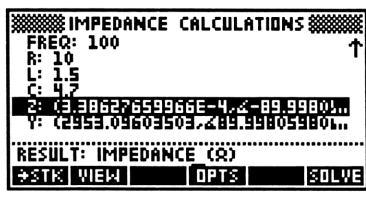
- Go to the Impedance Calculations screen:
 - Press **HOME** to go to the home screen.
 - Choose Analysis.
 - Choose AC Circuits.
 - Choose Impedance Calculations.

- Move the highlight bar to the **Config** field and press **CHOOS** to display the two choices for this field. Move the highlight bar down to Parallel and press **OK** or **ENTER**. The circuit configuration is now set and the highlight bar will automatically move down to the next field.



- At the **Elements** field press **CHOOS** and select RLC.
- Enter 100 for **Freq**, 10 for **R**, 1.5 for **L**, and 4.7 for **C**. If you make a mistake while entering these values, move the highlight bar back up to the field with the incorrect value and type in the correct value.

- Press **SOLVE** to calculate the impedance **Z** and admittance **Y**. Because the result for the impedance is too wide for the screen, move the highlight bar to the **Z** field and press **VIEW** to display the full value in text view, if desired.



- When finished press **◀** to return to the AC Circuits screen or press **HOME** to return to the home screen.

Chapter 3

AC Circuits

Analysis <i>AC Circuits</i> Equations Reference
--

This chapter covers the basic properties of simple AC circuits:

- ☐ Impedance Calculations
- ☐ Voltage Divider
- ☐ Current Divider
- ☐ Circuit Performance
- ☐ Wye \leftrightarrow Δ Conversion

Impedance Calculations

Analysis <i>AC Circuits</i> <i>Impedance Calculations</i> Equations Reference

The Impedance Calculations section computes the conductance of a resistor, the impedance and admittance of an isolated inductor or a capacitor, and the impedance and admittance of a series or parallel combination of a resistor, inductor and/or capacitor.

Field Descriptions

Config: (*Circuit Configuration*) Press **CHOOS** to select Series or Parallel.

Elements: (*Element Combination*) Press **CHOOS** to select R, L, C, RL, RC, LC, or RLC. Determines which of the remaining fields are visible:

Freq, R, L and/or **C**.

Freq: (*Frequency in Hz*) Enter a real number, global name, or algebraic.

R: (*Resistance in Ω - only appears if R, RL, RC or RLC is chosen in Elements field*) Enter a real number, global name, or algebraic.

L: (*Inductance in H - only appears if L, RL, LC or RLC is chosen in Elements field*) Enter a real number, global name, or algebraic.

C: (*Capacitance in F - only appears if C, LC, RC or RLC is chosen in Elements field*) Enter a real number, global name, or algebraic.

Z: (*Impedance in Ω*) Returns a real or complex number, global name, or algebraic.

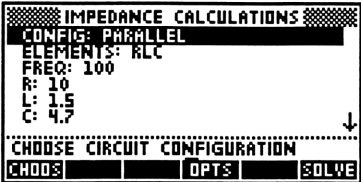
Y: (*Admittance in S*) Returns a real or complex number, global name, or algebraic.

Example

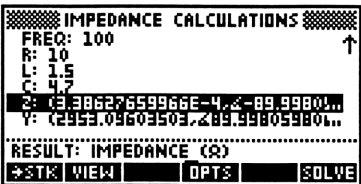
MODES (Press CST)	∠: Degrees Coord: Polar Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Compute the impedance of a parallel RLC circuit consisting of a 10 ohm resistor, a 1.5 Henry inductor and a 4.7 farad capacitor at a frequency of 100 hertz.

1. Choose Parallel for **Config** and RLC for **Elements**.
2. Enter 100 for **Freq**.
3. Enter 10 for **R**, 1.5 for **L**, and 4.7 for **C**.
4. Press **SOLVE** to calculate **Z** and **Y**.



Input Screen



Output Screen

Voltage Divider

This section computes the voltage drop across a load connected to an ideal voltage or current source. The load chain consists of impedances in series or admittances in series. The module computes the voltage across each impedance/admittance and the current through the load.

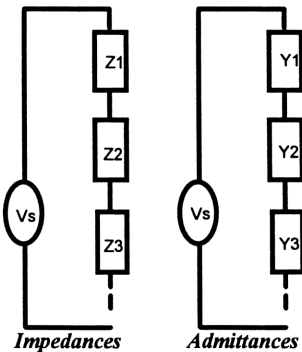
Analysis
AC Circuits
<i>Voltage Divider</i>
Equations
Reference

Field Descriptions

Load Type: (*Type of Load*) Press **CHOOSE** to select Impedance (Z) or Admittance (Y). Determines whether the third field is Z (impedance chain) or Y (admittance chain).

Vs: (*Source Voltage in V*) Enter a real or complex number, global name, or algebraic.

Z: (*Impedances*) Enter a list of real or complex numbers, global names, or algebraics.



Y: (*Admittances*) Enter a list of real or complex numbers, global names, or algebraics.

IL: (*Output Current in A*) Returns a real or complex number, global name or algebraic.

V: (*Element Voltages in V*) Returns a list of real or complex numbers, global names, or algebraics.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

An ideal voltage source with a (100,20) AC voltage is connected to three impedances (50,0), (100,-30) and (50,-50) connected in series. Compute the load current and the voltage drop across each impedance.

1. Choose Impedances for **Load Type**.
2. Enter (100,20) for **Vs**.
3. Enter {(50,0) (100,-30) (50,-50)} for **Z**.
4. Press **SOLVE** to calculate **IL** and **V**.

```

VOLTAGE DIVIDER
LOAD TYPE: IMPEDANCE
VS: (100,20)
Z: { (50,0) (100,-30) (50,-50) }
IL:
V:

CHOOSE IMPEDANCE OR ADMITTANCE
CHOOSE OPTS SOLVE
  
```

Input Screen

```

VOLTAGE DIVIDER
LOAD TYPE: IMPEDANCE
VS: (100,20)
Z: { (50,0) (100,-30) (50,-50) }
IL: (0.06551724138, -0.03068965517)
V: { (3.275862069, 12.93103448)

RESULT: OUTPUT CURRENT (A)
VIEW OPTS SOLVE
  
```

Output Screen

Current Divider

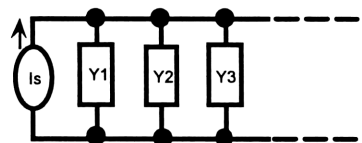
This section computes the individual branch currents in a load defined as a set of impedances or admittances connected in parallel. The section also computes the voltage across the load.

Analysis
AC Circuits
Current Divider
Equations
Reference

Field Descriptions

Load Type: (*Type of Load*) Press **CHOOSE** to select Impedance (Z) or Admittance (Y). This sets the third field to be Z (Impedances) or Y (Admittances).

Is: (*Source Current in A*) Enter a real or complex number, global name, or algebraic.



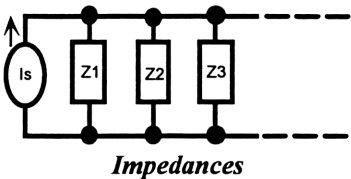
Admittances

Z: (*Impedances*) Enter a list of real or complex numbers, global names or algebraics.

Y: (*Admittances*) Enter a list of real or complex numbers, global names or algebraics.

VL: (*Load Voltage in V*) Returns a real or complex number, global name or algebraic.

I: (*Currents in A*) Returns a list of real or complex numbers, global names or algebraics.



Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

An AC current source of (15, 20) amps has a load consisting of three admittances: (0.05, 0), (0.001, -0.03) and (0.025, -0.015) mhos, connected in parallel. Compute the current in each element and the voltage drop across the load.

1. Choose Admittance for **Load Type**.
2. Enter (15,20) for **Is**.
3. Enter {(0.05,0) (0.001,-0.03) (0.025,-0.015)} for **Y**.
4. Press **SOLVE** to calculate **VL** and **I**.

```
CURRENT DIVIDER
LOAD TYPE: ADMITTANCE
IS: (15,20)
Y: { (0.05,0) (0.001,-0.03) (0.025,-0.015) }
VL:
I:

CHOOSE IMPEDANCE OR ADMITTANCE
CHOOSE: [ ] [ ] [ ] DPTS: [ ] SOLVE
```

Input Screen

```
CURRENT DIVIDER
LOAD TYPE: ADMITTANCE
IS: (15,20)
Y: { (0.05,0) (0.001,-0.03) (0.025,-0.015) }
VL: (30.7652865017,281.37418223)
I: { (1.53826432509,14.06870913) ... }

RESULT: OUTPUT VOLTAGE (V)
STK: [ ] VIEW: [ ] DPTS: [ ] SOLVE
```

Output Screen

Circuit Performance

This section computes the circuit performance of a simple load connected to a voltage or a current source. Performance parameters computed include load voltage and current, complex power delivered, power factor, maximum power available to the load, and the load impedance required to deliver maximum power.

Analysis
AC Circuits
<i>Circuit Performance</i>
Equations
Reference

Field Descriptions - Input Screen

Load Type: (*Type of Load*) Press **CHOOS** to select load impedance (Z) or admittance (Y). Determines whether remaining fields are **Vs**, **Zs**, and **ZL** or **Is**, **Ys**, and **YL**, respectively.

Vs: (*RMS Source Voltage in V*) Enter a real or complex number, global name, or algebraic.

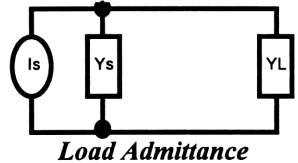
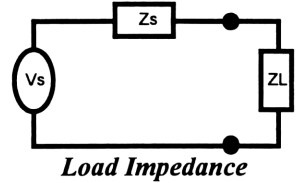
Zs: (*Source Impedance in Ω*) Enter a real or complex number, global name, or algebraic.

ZL: (*Load Impedance in Ω*) Enter a real or complex number, global name, or algebraic.

Is: (*RMS Source Current in A*) Enter a real or complex number, global name, or algebraic.

Ys: (*Source Admittance in S*) Enter a real or complex number, global name, or algebraic.

YL: (*Load Admittance in S*) Enter a real or complex number, global name, or algebraic.



Field Descriptions - Output Screen

VL: (*Load Voltage in V*) Returns a real or complex number, global name, or algebraic.

IL: (*Load Current in A*) Returns a real or complex number, global name, or algebraic.

P: (*Real Power in W*) Returns a complex number, global name, or algebraic.

Q: (*Reactive Power in W*) Returns a complex number, global name, or algebraic.

VI: (*Apparent Power in W*) Returns a complex number, global name, or algebraic.

θ : (*PF Angle in \angle*) Returns a real number, global name or algebraic.

PF: (*Load Power Factor*) Returns a real number, global name, or algebraic.

Pmax: (*Maximum Power Available in W*) Returns a real number, global name, or algebraic.

YLopt: (*Load Admittance for Maximum Power in S - if Admittance was chosen for Load Type at input screen*) Returns a real or complex number, global name, or algebraic.

ZLopt: (*Load Impedance for Maximum Power in Ω - if Impedance was chosen for **Load Type** at input screen*) Returns a real or complex number, global name, or algebraic.

Example

MODES (Press CST)	\angle: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Calculate the circuit performance parameters for a (125,-100) ohm load connected to an AC voltage source with a voltage of (10, 0) and a source impedance of (50, 25) ohms.

1. Choose Impedance for **Load Type**.
2. Enter (10, 0) for **Vs**, (50, 25) for **Zs**, and (125, -100) for **ZL**.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

CIRCUIT PERFORMANCE		
LOAD TYPE: IMPEDANCE		
VS: (10,0)		
ZS: (50,25)		
ZL: (125,-100)		
.....		
CHOOSE IMPEDANCE OR ADMITTANCE		
CHOOSE		OPTS SOLVE

Input Screen

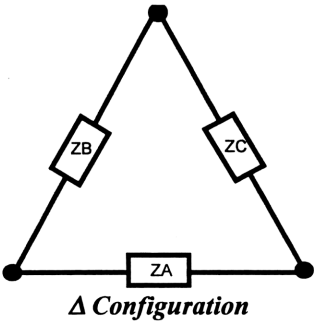
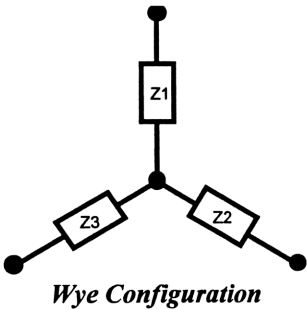
RESULTS: CIRCUIT PERFORMANCE		
WL: 0.10444882565	P: 0.2418991104	
IL: 0.048275862069	P: 0.344827586207	
Q: -2.75862068965		
VI: 4.41594774995		
Q: -38.659808254		
.....LOAD VOLTAGE (V).....		
STK	VIEW	OPTS
EXIT		

Output Screen

Wye \leftrightarrow Δ Conversion

This section converts the three impedances Z1, Z2 and Z3 connected in a Y configuration to its equivalent Δ values of ZA, ZB and ZC or vice versa, as shown in the diagrams below. This section uses the clockwise notation.

Analysis
AC Circuits
Wye \leftrightarrow Δ Conversion
Equations
Reference



Field Descriptions

Input Type: (*Circuit Configuration*) Press **CHOOS** to select $\Delta \rightarrow Y$ or $Y \rightarrow \Delta$.
Determines whether next 3 fields (input fields) accept Δ Impedances or Z Impedances.

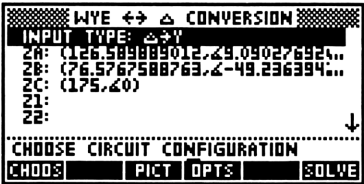
- ZA:** (Δ Impedance in Ω) Real or complex number, global name, or algebraic.
- ZB:** (Δ Impedance in Ω) Real or complex number, global name, or algebraic.
- ZC:** (Δ Impedance in Ω) Real or complex number, global name, or algebraic.
- Z1:** (Y Impedance in Ω) Real or complex number, global name, or algebraic.
- Z2:** (Y Impedance in Ω) Real or complex number, global name, or algebraic.
- Z3:** (Y Impedance in Ω) Real or complex number, global name, or algebraic.

Example

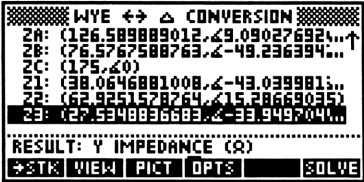
MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Polar	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Convert a Δ network with impedances (125,20), (50,-58) and (175,0) to its equivalent Y values.

1. Choose $\Delta \rightarrow Y$ for **Input Type**.
2. Enter (125,20) for **ZA**, (50,-58) for **ZB**, and (175,0) for **ZC**.
3. Press **SOLVE** to calculate **Z1**, **Z2** and **Z3**.



Input Screen



Output Screen

Chapter 4

Polyphase
Circuits

Analysis
<i>Polyphase Circuits</i>
Equations
Reference

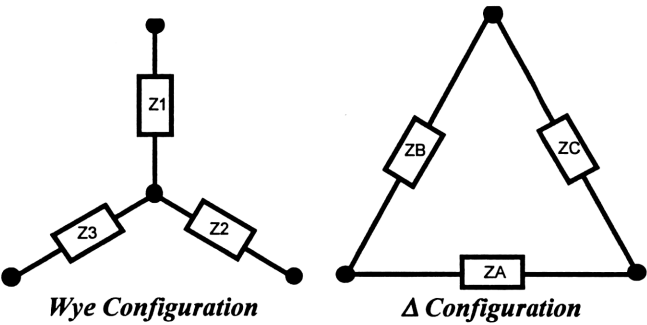
This chapter covers the basic principles of polyphase (3 phase) circuits:

- ☐ Wye ↔ Δ Conversion
- ☐ Balanced Wye Load
- ☐ Balanced Δ Load

Wye ↔ Δ Conversion

Analysis
Polyphase Circuits
<i>Wye ↔ Δ Conversion</i>
Equations
Reference

This section converts the three impedances Z1, Z2 and Z3 connected to form a Wye connection to their equivalent Δ values of ZA, ZB and ZC or vice versa, as shown in the diagram below. Clockwise notation is used for the conversion.



Field Descriptions

Input Type: (*Circuit Configuration*) Press **CHOOS** to select Δ→Y or Y→Δ. Determines whether next 3 fields (input fields) accept Δ Impedances or Wye Impedances.

ZA: (*Δ Impedance*) Real or complex number, global name, or algebraic.

ZB: (*Δ Impedance*) Real or complex number, global name, or algebraic.

- ZC:** (Δ Impedance) Real or complex number, global name, or algebraic.
Z1: (Y Impedance) Real or complex number, global name, or algebraic.
Z2: (Y Impedance) Real or complex number, global name, or algebraic.
Z3: (Y Impedance) Real or complex number, global name, or algebraic.

Example 1

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Convert a Δ network with impedances (10,0), (20,-60) and (0,-20) to its equivalent Wye values.

- Choose $\Delta \rightarrow Y$ for **Input Type**.
- Enter (10,0) for **ZA**, (20,-60) for **ZB**, and (0,-20) for **ZC**.
- Press **SOLVE** to calculate **Z1**, **Z2** and **Z3**.

WYE ↔ Δ CONVERSION

INPUT TYPE: Δ→Y

ZA: (10,0)
 ZB: (20,-60)
 ZC: (0,-20)
 Z1:
 Z2:
 Z3:

CHOOSE CIRCUIT CONFIGURATION

CHOOSE PICT OPTS SOLVE

Input Screen

WYE ↔ Δ CONVERSION

ZA: (10,0)
 ZB: (20,-60)
 ZC: (0,-20)
 Z1: (-947945205479,-14.79945205...
 Z2: (2.19128082182,-831912808...
 Z3: (7.99726027997,-279972602...

RESULT: Y IMPEDANCE (Ω)

→STK VIEW PICT OPTS SOLVE

Output Screen

Example 2

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Convert a Wye network with impedances 15, 10 and 6 to its equivalent Δ values.

- Choose $Y \rightarrow \Delta$ for **Input Type**.
- Enter 15 for **Z1**, 10 for **Z2**, and 6 for **Z3**.
- Press **SOLVE** to calculate **ZA**, **ZB** and **ZC**.

WYE ↔ Δ CONVERSION

INPUT TYPE: Y→Δ

Z1: 15
 Z2: 10
 Z3: 6
 ZA:
 ZB:
 ZC:

CHOOSE CIRCUIT CONFIGURATION

CHOOSE PICT OPTS SOLVE

Input Screen

WYE ↔ Δ CONVERSION

Z1: 15
 Z2: 10
 Z3: 6
 ZA: 20
 ZB: 30
 ZC: 50

RESULT: Δ IMPEDANCE (Ω)

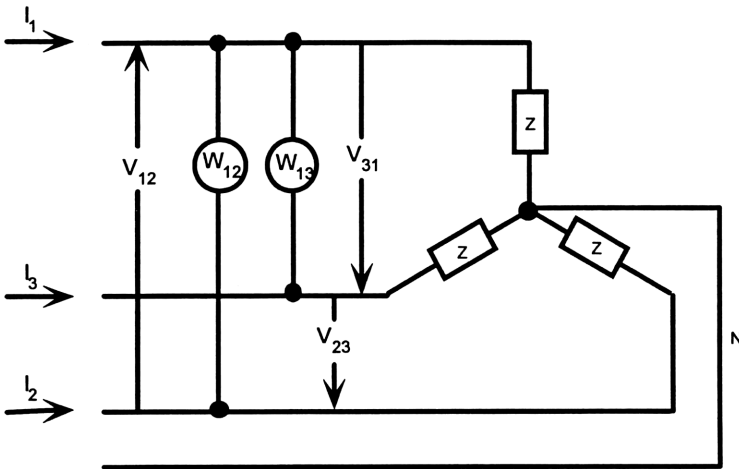
→STK VIEW PICT OPTS SOLVE

Output Screen

Balanced Wye Load

Analysis
Polyphase Circuits
Balanced Wye Load
Equations
Reference

In this section, three identical impedances Z are connected in the Wye configuration. The voltage V_{12} represents the line voltage from line 1 to line 2 which is the reference voltage applied to this Wye network. The voltages across lines 2 and 3, and 3 and 1 have the same magnitude as V_{12} , but are out of phase by -120° and 120° respectively. This section calculates the currents I_1 , I_2 , and I_3 in each leg of the Wye network, line to neutral voltage in each phase V_{1N} , V_{2N} , and V_{3N} , power dissipated in each phase P , wattmeter readings W_{12} and W_{13} connected as shown in the figure below.



Field Descriptions - Input Screen

V12: (Reference Voltage in V across lines 1 and 2) Enter a real or complex number, global name, or algebraic.

Z: (Phase Impedance in Ω) Enter a real or complex number, global name, or algebraic.

Field Descriptions - Output Screen

V23: (Voltage in V across lines 2 and 3) Returns a real or complex number, global name or algebraic.

V31: (Voltage in V across lines 3 and 1) Returns a real or complex number, global name or algebraic.

- V1N:** (Voltage in V across 1N) Returns a real or complex number, global name or algebraic.
- V2N:** (Voltage in V across 2N) Returns a real or complex number, global name or algebraic.
- V3N:** (Voltage in V across 3N) Returns a real or complex number, global name or algebraic.
- I1:** (Line Current 1 in A) Returns a real or complex number, global name or algebraic.
- I2:** (Line Current 2 in A) Returns a real or complex number, global name or algebraic.
- I3:** (Line Current 3 in A) Returns a real or complex number, global name or algebraic.
- P:** (Phase Power in W) Returns a real number, global name or algebraic.
- W12:** (Wattmeter reading in W across lines 1 and 2) Returns a real number.
- W13:** (Wattmeter reading in W across lines 1 and 3) Returns a real number.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Polar	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

A Wye network consists of three impedances of $(5, \angle 36.87)$ ohms each and is supplied by a reference voltage of $(110, 0)$ volts. Compute the line currents and the power dissipated in each leg of the network.

1. Enter $(110, 0)$ for **V12**.
2. Enter the value $(5, \angle 36.87)$ for **Z**.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

BALANCED WYE LOAD	
V12: $(110, \angle 0)$	
Z: $(5, \angle 36.87)$	
ENTER REF. VOLTAGE ACROSS 12 (V)	
EDIT	STACK PICT OPTS TYPES SOLVE

Input Screen

RESULTS: BALANCED WYE LOAD	
V23: $(110, \angle -120)$	
V31: $(110, \angle 120)$	
V1N: $(63.5085296109, \angle -30.000000...)$	
V2N: $(63.5085296109, \angle -150)$	
V3N: $(63.5085296109, \angle 90)$	
I1: $(12.7017059222, \angle -66.87000000...)$	↓
VOLTAGE ACROSS 23 (V)	
→ STK	VIEW PICT OPTS EXIT

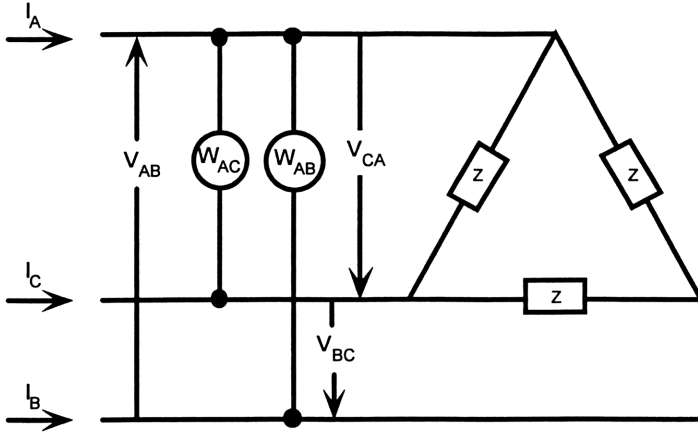
Output Screen

Balanced Δ Load

In this section, three identical impedances **Z** are connected in a Δ configuration. The voltage **VAB** represents the line voltage from line A to line B which is the reference voltage applied to this Δ network. The voltages across lines B and

Analysis
Polyphase Circuits
Balanced Δ Load
Equations
Reference

C, and C and A have the same magnitude as V_{AB} , but are out of phase by -120° and 120° respectively. This section calculates the currents I_A , I_B , and I_C in each leg of the Δ network, power dissipated in each phase P , and the readings in a two-wattmeter system of power measurement W_{AB} and W_{AC} .



Field Descriptions - Input Screen

VAB: (Reference Voltage in V across lines 1 and 2) Enter a real or complex number, global name, or algebraic.

Z: (Phase Impedance in Ω) Enter a real or complex number, global name, or algebraic.

Field Descriptions - Output Screen

VBC: (Voltage in V across lines B and C) Returns a real or complex number, global name or algebraic.

VCA: (Voltage in V across lines C and A) Returns a real or complex number, global name or algebraic.

IA: (Line Current A in A) Returns a real or complex number, global name or algebraic.

IB: (Line Current B in A) Returns a real or complex number, global name or algebraic.

IC: (Line Current C in A) Returns a real or complex number, global name or algebraic.

P: (Phase Power in W) Returns a real number, global name or algebraic.

WAB: (Wattmeter reading in W across lines A and B) Returns a real number.

WAC: (Wattmeter reading in W across lines A and C) Returns a real number.

Example

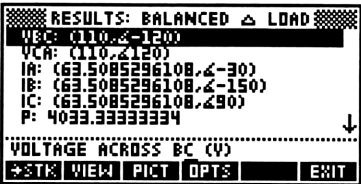
MODES (Press CST)	∠: Degrees Coord: Polar Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

A Δ network consists of three impedances of 3 ohms each and is supplied by a reference voltage of (110, 0) volts. Compute the line currents and the power dissipated in each leg of the network.

- 2. Enter (110, 0) for **VAB**.
- 1. Enter 3 for **Z**.
- 3. Press **SOLVE** to calculate the final results as shown in the output screen.



Input Screen



Output Screen

Chapter 5

Ladder Network

Analysis
<i>Ladder Network</i>
Equations
Reference

This chapter covers ladder network analysis:
a circuit reduction method by which branches of the circuit are treated as rungs (series connection) or sides (parallel or shunt connection) of a ladder.

Using Ladder Network

NOTE



In a ladder network, the order in which you enter the elements is significant.

In the examples that follow, the left end of the ladder is the input end and the right end of the ladder is the output end, where the load is connected. The elements of the ladder (from 1 to N) are entered from right to left, as you go from output to input. The input impedance Z_{in} is calculated as if you were “looking in” to the left end of the ladder.

Field Descriptions - Input Screen

Frequency: (*Frequency*) Enter a real number, global name, or algebraic.

Load: (*Initial Load*) Enter a real or complex number, global name, or algebraic.

1: (*Element 1 - closest to the load*)

...

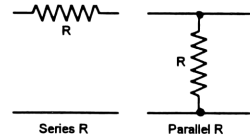
N: (*Element N - furthest from the load*)

Field Descriptions - Element Screen

Press **ADD** from the input screen to add one of the sixteen different element types.

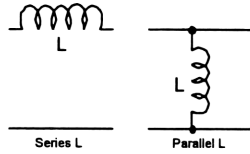
Resistor

Can be added as a rung or side. Choose Series or Parallel for **Config** and enter a value for **R**.



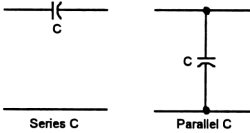
Inductor

(ideal inductor) Can be added as a rung or side. Choose Series or Parallel for **Config** and enter a value for **L**.



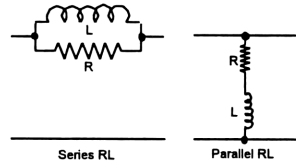
Capacitor

(ideal capacitor) Can be added as a rung or side. Choose Series or Parallel for **Config** and enter a value for **C**.



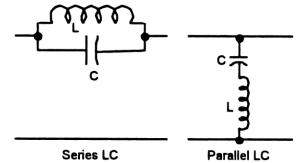
RL

RL series circuit can be added as a rung.
RL parallel circuit can be added as a side.
Choose Series or Parallel for **Config** and enter a value for **R** and **L**.



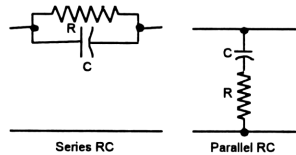
LC

LC series circuit can be added as a rung.
LC parallel circuit can be added as a side.
Choose Series or Parallel for **Config** and enter a value for **L** and **C**.



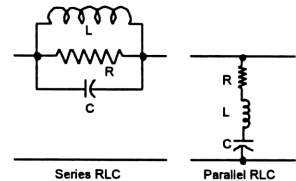
RC

RC series circuit can be added as a rung.
RC parallel circuit can be added as a side.
Choose Series or Parallel for **Config** and enter a value for **R** and **C**.



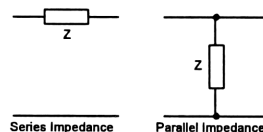
RLC

RLC series circuit can be added as a rung.
RLC parallel circuit can be added as a side.
Choose Series or Parallel for **Config** and enter a value for **R**, **L**, and **C**.



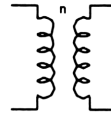
General Impedance

Can be added as a rung or side. Choose Series or Parallel for **Config** and enter a value for **Z**.



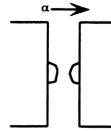
Transformer

(ideal transformer) Can be added only in cascade connection. Specify turns ratio, by entering a value for **N**.



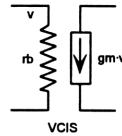
Gyrator

(synthetic inductance filer) Can be added only in cascade connection. Specify gyrator parameter by entering a value for α .



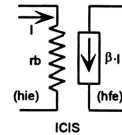
Voltage-Controlled I

Can be added only in cascade connection. Specify base resistance and transconductance by entering values for **rb** and **gm**.



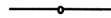
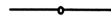
Current-Controlled I

Can be added only in cascade connection. Specify base resistance and common base current gain by entering values for **rb** and β .



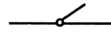
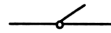
Transmission Line

Can be added only in cascade connection. Specify characteristic impedance and electrical length by entering values for **Z0** and θ .



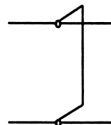
Open Circuited Stub

Can be added only in cascade connection. Specify characteristic impedance and electrical length by entering values for **Z0** and θ .



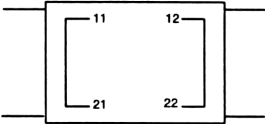
Short Circuited Stub

Can be added only in cascade connection. Specify characteristic impedance and electrical length by entering values for **Z0** and θ .



Two-Port Network

Can be added only in cascade connection.
Choose z, y, g, h, a, or b for Input
Parameters, and enter values for **..11**, **..12**,
..21, and **..22**.



Field Descriptions - Output Screen

Zin: (*Input Impedance*) Returns a real or complex number, global name or algebraic.

I2/V1: (*Forward Transfer Admittance*) Returns a real or complex number, global name or algebraic.

I2/I1: (*Current Transfer Ratio*) Returns a real or complex number, global name or algebraic.

Pout/Pin: (*Real Power Gain*) Returns a real or complex number, global name or algebraic.

V2/V1: (*Forward Voltage Transfer Ratio*) Returns a real or complex number, global name or algebraic.

V2/I1: (*Forward Transfer Impedance*) Returns a real or complex number, global name or algebraic.

To use Ladder Network:

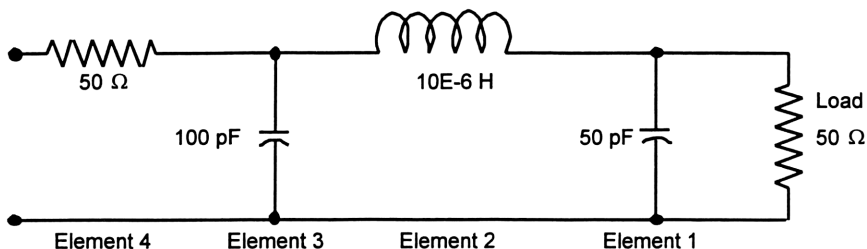
These are general instructions for entering the elements and computing the parameters of a ladder network.

1. Enter **Frequency** and **Load**.
2. Build the ladder by adding elements to it. Press **ADD** to insert an element on the line below the highlight bar.
3. Choose an element type and press **ENTER** or **OK**.
4. Enter the appropriate values.
5. Press **OK** to return to the Ladder Network screen.
6. Repeat steps 2-5 as needed to add more elements.
7. If you decide to delete an element, move the highlight bar to that element and press **DEL**.
8. Press **SOLVE** to compute the overall ladder network parameters.

Example 1

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Scientific Digits: 3	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

What is the input impedance of the circuit shown below at 1 MHz and 10 MHz?



1. Enter 1E6 for **Frequency**.
2. Enter 50 for **Load**.
3. Press **ADD** to enter the first element.

```

LADDER NETWORK
FREQUENCY: 1.000E6
LOAD: 5.000E1

-----
ENTER FREQUENCY (HZ)
EDIT  ADD  STACK  OPTS  TYPES  SOLVE
  
```

Input Screen

4. In the Select Element screen, move the highlight bar to **Capacitor** and press **ENTER** or **OK** to enter the Edit Capacitor screen.

```

SELECT AN ELEMENT TYPE
RESISTOR
INDUCTOR
CAPACITOR
RL
RC
LC
RLC
GENERAL IMPEDANCE
                                ↓
                                [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ]
                                CANCEL OK
  
```

Select Element Screen

5. In the Edit Capacitor screen, choose Parallel for **Config**.
6. Enter 50E-12 for **C**.
7. Press **OK** to return to the Ladder Network screen.
8. Move the highlight bar to **1: Capacitor** and press **ADD** to enter the second element.

```

EDIT CAPACITOR
CONFIG: PARALLEL
C: 5.000E-11

-----
CHOOSE CIRCUIT CONFIGURATION
CHOOSE [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ] OPTS CANCEL OK
  
```

Edit Capacitor Screen

NOTE



The **ADD** key adds a new element on the line *below* the highlight bar, so make sure the highlight bar is on the last element entered (in this case, **1: Capacitor**) before adding the second element.

9. Move the highlight bar to **Inductor** and press **ENTER** or **OK** to enter the Edit Inductor screen.
10. Choose Series for **Config**
11. Enter 10E-6 for **L**.

12. Press **OK** to return to the original screen.
13. Enter the remaining two elements in the same manner as the first two: a 100pF (100E-12) capacitor in parallel and a 50 ohm resistor in series.

```

LADDER NETWORK
FREQUENCY: 1.000E6
LOAD: 5.000E1
1: CAPACITOR
2: INDUCTOR
3: CAPACITOR
4: RESISTOR
LADDER ELEMENT
EXIT ADD DEL OPTS SOLVE
  
```

Input Screen (completed)

13. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

```

RESULTS: LADDER NETWORK
ZIN: (1.041E-3-2.385E-1)
I2/I1: (-7.103E-3-4.769E-3)
I2/I1: (-1.039E0-5.029E-2)
POUT/PIN: 5.195E-1
V2/V1: (3.551E-1-2.385E-1)
V2/I1: (5.193E1-2.514E0)
INPUT IMPEDANCE (Z)
*STK VIEW OPTS EXIT
  
```

Output Screen (1 MHz)

To find the ladder network parameters at a second frequency of 10 MHz:

1. Press **◀** to return to the input screen.
2. In the **Frequency** field, type 10E6.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

```

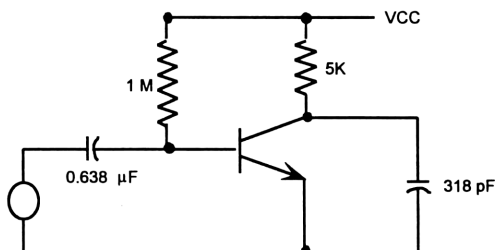
RESULTS: LADDER NETWORK
ZIN: (5.574E1-2.134E2)
I2/I1: (4.625E-4-1.465E-3)
I2/I1: (3.384E-1-1.709E-2)
POUT/PIN: 1.030E-1
V2/V1: (-2.313E-2-7.323E-2)
V2/I1: (-1.692E1-8.545E-1)
INPUT IMPEDANCE (Z)
*STK VIEW OPTS EXIT
  
```

Output Screen (10 MHz)

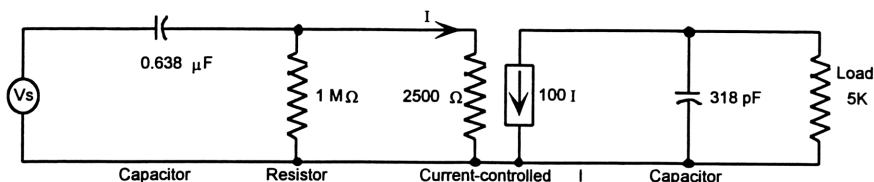
Example 2

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Scientific	Help: On
	Digits: 3	Font: Small

A transistor amplifier is shown in the figure below. The transistor is characterized by a base resistance of 2500 ohms, a current gain of 100 and is operating at a frequency of 10,000 Hertz.



This schematic can be reduced to the ladder network that appears on the next page.



1. Enter the frequency and load values:

Frequency: 10,000 Hz

Load: 5000 ohms

2. Enter the ladder elements in the following order:

1: Capacitor: Parallel, 318E-12

2: Current-Controlled I: Enter 2500 for RB and 100 for β

3: Resistor: Parallel, 1E6

4: Capacitor: Series, 0.638E-6

3. Press **SOLVE** to compute the results, which will be displayed in the output screen.

LADDER NETWORK	
FREQUENCY:	1.000E4
LOAD:	5.000E3
1:	CAPACITOR
2:	CURRENT CONTROLLED I
3:	RESISTOR
4:	CAPACITOR
LADDER ELEMENT	
EDIT	ADD DEL OPTS SOLVE

Input Screen

RESULTS: LADDER NETWORK	
ZIN:	(-4.000E-6, -2.495E1)
I2/V1:	(-3.965E-3, -3.969E-2)
I2/I1:	(-9.901E-1, 9.892E-2)
POUT/PIN:	-1.238E9
V2/V1:	(1.983E1, 1.985E2)
V2/I1:	(4.951E3, -4.946E2)
INPUT IMPEDANCE (Ω)	
→STK VIEW	OPTS EXIT

Output Screen

Chapter 6

Filter Design

This chapter covers the basic design principles for three commonly-used filters:

- ☐ Chebyshev Filter
- ☐ Butterworth Filter
- ☐ Active Filter

Analysis
<i>Filter Design</i>
Equations
Reference

Chebyshev Filter

This section computes component values for Chebyshev filters between equal terminations.

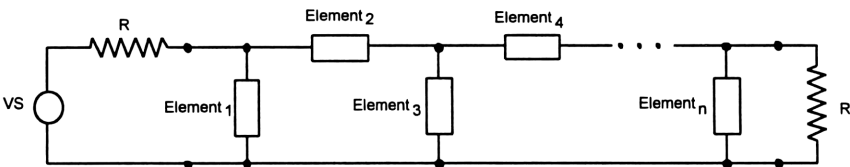
Inputs are termination resistance, pass band characteristics, attenuation at some out-of-band frequency, and allowable passband ripple. The Chebyshev circuit elements are assumed to be ideal, and are illustrated below.

Analysis
Filter Design
<i>Chebyshev Filter</i>
Equations
Reference

NOTE



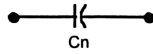
The order of the Chebyshev filter module is reported only in odd numbers. If the result is computed to be an even number, it will be incremented to the next higher odd number.



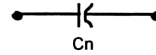
Odd Elements

Even Elements

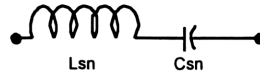
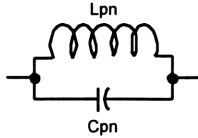
Low Pass



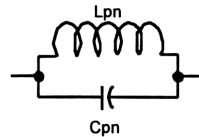
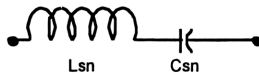
High Pass



Band Pass



Band Elimination



Field Descriptions - Input Screen

Char: (*Bandpass Characteristic*) Press **CHOOS** to select Low Pass, High Pass, Band Pass, or Band Elimination.

R: (*Termination Resistance in Ohms*) Enter a real number, global name or algebraic.

f0: (*Cutoff Frequency in Hz - for Low Pass and High Pass*) Enter a real number.

(*Center Frequency in Hz - for Band Pass and Band Elimination*) Enter a real number.

f1: (*Attenuation Frequency in Hz*) Enter a real number.

ΔdB: (*Attenuation in dB*) Enter a real number.

Bandwidth: (*Bandwidth in Hz - only appears for Band Pass or Band Elimination*) Enter a real number.

Ripple: (*Pass Band Ripple in dB*) Enter a real number.

Field Descriptions - Output Screen

Element1: (*First element in parallel*) Returns a real number.

Element2: (*Second element in series*) Returns a real number.

Element3: (*Third element in parallel*) Returns a real number.

Element4: (*Fourth element in series*) Returns a real number.

ElementN: (*nth element in series because N is always odd*) Returns a real number.

Example

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Design a low-pass Chebyshev filter with a cutoff at 500 Hz, a termination resistance of 50 ohm, 3 dB pass band ripple, and a 30 dB attenuation at 600 Hz.

1. Enter 50 for **R**, 500 for **f0**, and 600 for **f1**.
2. Enter 30 for **ΔdB** and 3 for **Ripple**.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

CHEBYSHEV FILTER		
CHHP: LOW PASS		
R: 50		
F0: 500		
F1: 600		
ΔDB: 30		
RIPPLE: 3		
CHOOSE BANDPASS CHARACTERISTIC		
CHODS	DPTS	SOLVE

Input Screen

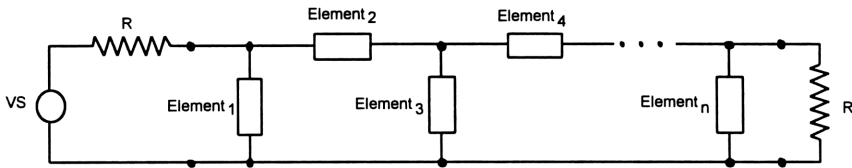
RESULTS: CHEBYSHEV FILTER		
C1: 2.23996221898E-5		
C2: 1.228899455527E-2		
C3: 2.95326564625E-2		
C4: 1.27930266688E-2		
C5: 2.95326564626E-2		
C6: .0122889945553		
C7: 2.23996221899E-5		
→STK	VIEW	DPTS
		EXIT

Output Screen

Butterworth Filter

This section computes the component values for Butterworth filters between equal terminations. Inputs are termination resistance, pass band characteristics, and attenuation at some out-of-band frequency. The basic form of the filter is shown in the figures below:

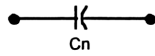
Analysis
Filter Design
Butterworth Filter
Equations
Reference



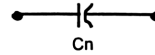
Odd Elements

Even Elements

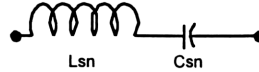
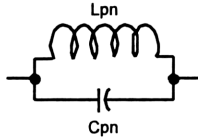
Low Pass



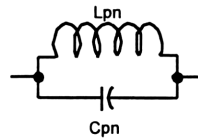
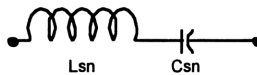
High Pass



Band Pass



Band Elimination



Field Descriptions - Input Screen

Char: (*Bandpass Characteristic*) Press **CHOOS** to select Low Pass, High Pass, Band Pass, or Band Elimination.

R: (*Termination Resistance in Ohms*) Enter a real number.

f0: (*Cutoff Frequency in Hz - for Low Pass and High Pass*) Enter a real number.

(*Center Frequency in Hz - for Band Pass and Band Elimination*) Enter a real number.

f1: (*Attenuation Frequency in Hz*) Enter a real number.

ΔdB: (*Attenuation in DB*) Enter a real number.

Bandwidth: (*Bandwidth in Hz - for Band Pass or Band Elimination*) Enter a real number.

Field Descriptions - Output Screen

Element1: (*First element in parallel*) Returns a real number.


Element2: (*Second element in series*) Returns a real number.

Element3: (*Third element in parallel*) Returns a real number.

Element4: (*Fourth element in series*) Returns a real number.

ElementN: (*nth element in series (if n is odd) or parallel (if n is even)*) Returns a real number.

Example

MODES (Press )	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
--	---	---

Design a 100 Hz wide Butterworth band pass filter centered at 800 Hz with a 30 dB attenuation at 900 Hz. The termination resistance is 50 ohms. The source resistance is also 50 ohms.

1. Choose Band Pass for **Char**.
2. Enter 50 for **R** and 800 for **f0**, and 900 for **f1**.
3. Enter 30 for **ΔdB** and 100 for **Bandwidth**.
4. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

BUTTERWORTH FILTER			
CHAR: BAND PASS			
R:	50		
F0:	800		
F1:	900		
ΔDB:	30		
BANDWIDTH:	100		
CHOOSE BANDPASS CHARACTERISTIC			
CHOOSE		OPTS	SOLVE

Input Screen

RESULTS: BUTTERWORTH FILTER			
C1:	1.41651226322E-5		
L1:	2.72388888889E-3		
C2:	9.9821488334E-5		
C3:	9.9885110845E-5		
C4:	3.73574595596E-5		
L3:	6.9003382758E-4		
L4:	1.5915494309E-7		
C4:	2.48673598581E-7		
→	VIEW	OPTS	EXIT

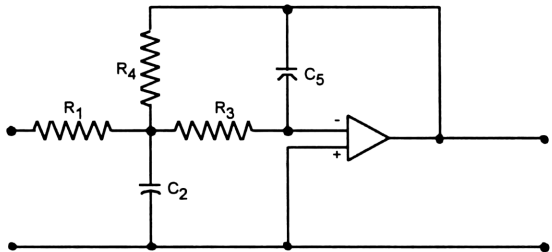
Output Screen

Active Filter

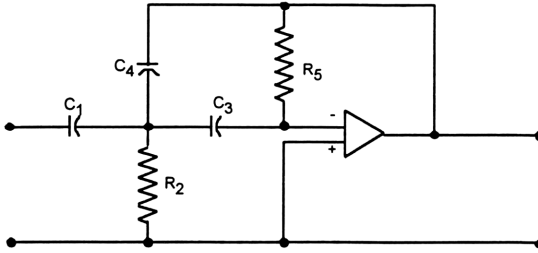
This section computes element values for the standard active filter circuits shown below. In each case, five different elements are calculated.

Analysis
Filter Design
Active Filter
Equations
Reference

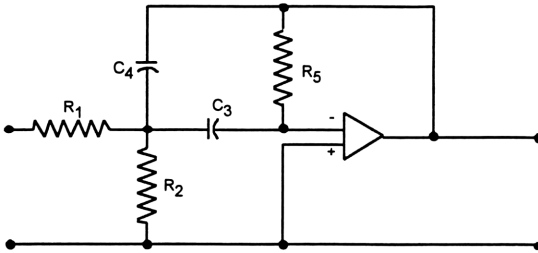
Low Pass Filter



High Pass Filter



Band Pass Filter



Field Descriptions - Input Screen

Type: (*Filter Type*) Press **CHOOS** to select Low Pass, High Pass, or Band Pass.

f0: (*Band Cutoff in Hz*) Enter a real number, global name, or algebraic.

A: (*Midband Gain in dB*) Enter a real number, global name, or algebraic.

Q: (*Quality Factor: $Q = \frac{1}{\alpha} = \frac{1}{2\zeta}$ where α is peaking factor and ζ is damping factor*) Enter a real number, global name, or algebraic.

C: (*Capacitor in F*) Enter a real number, global name, or algebraic.

Field Descriptions - Output Screen

Element1: (*First element*) Returns a real number.

Element2: (*Second element*) Returns a real number.

Element3: (*Third element*) Returns a real number.

Element4: (*Fourth element*) Returns a real number.

Element5: (*Fifth element*) Returns a real number.

Example

MODES	\angle : Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Design a High Pass active filter with a cutoff at 10 Hz, a midband gain of 10, a quality factor of 1 and a capacitor of 1 μF .

1. Choose High Pass for **Type**.
2. Enter 10 for **f0** and 10 for **A**.
3. Enter 1 for **Q** and 1E-6 for **C**.
4. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

```

ACTIVE FILTER
TYPE: HIGH PASS
F0: 10
A: 10
Q: 1
C: .000001

CHOOSE FILTER TYPE
CHOOSE [ ] OPTS [ ] SOLVE
  
```

Input Screen

```

RESULTS: ACTIVE FILTER
C1: .000001
R2: 7578.80681388
C3: .000001
C4: .000001
R5: 334225.380493

EXIT VIEW [ ] OPTS [ ] EXIT
  
```

Output Screen

Chapter 7

Gain and Frequency

Analysis <i>Gain and Frequency</i> Equations Reference

This chapter covers the basic principles of circuit analysis involving a transfer function model and plots the resulting equations using the classic graphical representation referred to as Bode plots for gain or phase:

- ☐ Transfer Function
- ☐ Bode Plots

Transfer Function

Analysis Gain and Frequency <i>Transfer Function</i> Equations Reference
--

A transfer function is defined as the ratio of an output to its input signal and is generally modified by the network between the two. In the classic sense, the transfer function is dependent upon the output and input definitions and is represented by a ratio of two polynomials of s . The roots of the numerator and denominator polynomials are referred to as *zeros* and *poles*, respectively. Transfer functions can be defined by the poles and zeros or by the coefficients of the numerator and denominator polynomials. The results computed include symbolic expressions for the transfer function and its partial fraction expansion.

Field Descriptions

- Inputs:** (*Type of Input*) Press **CHOOS** to select Roots or Coefficients. Determines whether the third and fourth fields are **Zeros** and **Poles** or **Numer** and **Denom**.
- Constant:** (*Constant Multiplier*) Enter a real number. Default is 1.
- Zeros:** (*Numerator Roots - if Roots chosen for input type*) Enter an array or list of real or complex numbers. The number of zeros must be less than the number of poles.

Poles: (*Denominator Roots - if Roots chosen for input type*) Enter an array or list of real or complex numbers. The number of poles must be greater than the number of zeros.

Numer: (*Numerator Coefficients - if Coefficients chosen for input type*) Enter an array or list of real or complex numbers. The number of numerator coefficients must be less than the number of denominator coefficients.

Denom: (*Denominator Coefficients - if Coefficients chosen for input type*) Enter an array or list of real or complex numbers. The number of denominator coefficients must be greater than the number of numerator coefficients.

H(s): (*Transfer Function*) Returns a symbolic expression of the form

$$\frac{K \cdot (1 - s/z_1)(1 - s/z_2) \dots}{(1 - s/p_1)(1 - s/p_2) \dots}$$

PFE: (*Partial Fraction Expansion*) Returns a symbolic expression of the form

$$\frac{K_1}{1 - s/p_1} + \frac{K_2}{1 - s/p_2} + \dots$$

Example

MODES	∠: Degrees	Result: Symbolic
(Press [CST])	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Find the transfer function and its partial fraction expansion for a circuit with a zero located at -10 r/s and three poles located at -100 r/s, -1000 r/s and -5000 r/s. Assume that the multiplier constant is 100000.

1. Choose Roots for **Inputs**.
2. Enter 100000 for **Constant**, [-10] for **Zeros**, and [-100 -1000 -5000] for **Poles**.
3. Press **[SOLVE]** to calculate **H(s)** and **PFE**.
4. To use this transfer function in the next example, “Bode Gain and Phase Plot,” move the highlight bar to the **H(s)** field and press **[→STK]**. This will place the transfer function on the first level of the stack so that you can use it in the next example. At the message screen “Copy to Stack...”, press **[ONE]**.

```

TRANSFER FUNCTION
INPUTS: ROOTS
CONSTANT: 100000
ZEROS: [ -10 ]
POLES: [ -100 -1000 -5000 ]
H(S):
PFE:
-----
CHOOSE INPUT TYPES
[CHOOSE] [ ] [OPTS] [SOLVE]

```


Input Screen

```

TRANSFER FUNCTION
INPUTS: ROOTS
CONSTANT: 100000
ZEROS: [ -10 ]
POLES: [ -100 -1000 -5000 ]
H(S): 100000*(s+10)/(s+100)(s+1000)(s+5000)
PFE: -(2.04081633/(s+100))+27.5m
-----
RESULT: TRANSFER FUNCTION
[→STK] [VIEW] [ ] [OPTS] [SOLVE]

```

Output Screen

5. Now you are ready to go on to the next example. Press  to return to the Gain and Frequency screen and choose Bode Plots. The next example is on page 51.

Bode Plots

Analysis
Gain and Frequency
Bode Plots
Equations
Reference

The behavior of the transfer function, as the frequency of a sinusoidal source varies, is of great interest to engineers. A very effective way to grasp the relationship between transfer function and frequency is to plot the magnitude and argument of the transfer function on two separate graphs. These plots are often called Bode gain and phase plots. A gain plot shows the magnitude of the transfer function expressed in decibels (dB) as $20 \cdot \text{LOG}(\text{Magnitude of Transfer Function})$ as a function of the logarithm of the radian frequency on the horizontal scale. The phase plot shows the argument of the transfer function expressed as the phase angle (i.e., $\text{ARG}(\text{Transfer Function})$) plotted as a function of the logarithm of the radian frequency on the horizontal scale.

Field Descriptions

Xfer: (*Transfer Function*) Enter a symbolic expression.

Indep: (*Independent Variable*) Enter a global name. Default is 's'.

Plot Type: (*Bode Gain or Bode Phase*) Press **CHOOS** to select Gain or Phase. Determines whether the y axis range fields appear as **A-Min** and **A-Max** (for Gain) or **θ-Min** and **θ-Max** (for Phase).

ω-Min: (*Minimum Frequency in r/s - X axis*) Enter a real number.

ω-Max: (*Maximum Frequency in r/s - X axis*) Enter a real number.

Autoscale: (*Scales the plot - hides A-min and A-max fields*) Press **✓CHK** to select.

A-Min: (*Minimum amplitude in dB (Y axis) - if Gain is chosen for Plot Type*) Enter a real number.

A-Max: (*Maximum amplitude in dB (Y axis) - if Gain is chosen for Plot Type*) Enter a real number.

θ-Min: (*Minimum amplitude in dB (Y axis) - if Phase is chosen for Plot Type*) Enter a real number, which will be interpreted as degrees or radians, depending on the current setting in the Custom Settings screen.

θ-Max: (*Maximum amplitude in dB (Y axis) - if Phase is chosen for Plot Type*) Enter a real number, which will be interpreted as degrees or radians, depending on the current setting in the Custom Settings screen.

Label Plot: (*Labels X and Y axes*) Press **✓CHK** to label the plot.

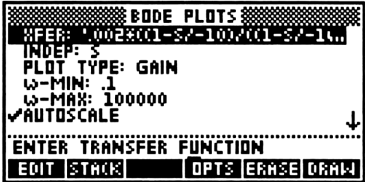
Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Plot the gain and phase plots for the transfer function example on page 49.

Plot the Bode gain plot

1. Complete the entire example for the transfer function on page 49.
2. In the Bode Plots screen, move the highlight bar to the **Xfer** field and press **STACK**. The **H(s)** field result from the transfer function example will be on the first level of the stack. Press **OK** to copy it into the Bode Plots screen in the **Xfer** field.
3. Choose **s** for **Indep**. (The default is **s** and should rarely be changed, because the Transfer Functions screen always generates transfer functions as functions of lowercase **s**.)
4. Choose **Gain** for **Plot Type**.
5. Enter 0.1 for **ω-Min** as the start of the radian frequency plot.
6. Enter 100000 for **ω-Max** as the endpoint of the radian frequency plot.
7. Put a checkmark in the **Autoscale** field. Press **✓CHK** if necessary.
8. Put a checkmark in the **Label Plot** field. Press **✓CHK** if necessary.
9. Press **ERASE** to clear previous plots.
10. Press **DRAW** to plot the function.



Input Screen



Output Screen - Bode gain plot

Plot the Bode phase plot

1. Press **ON** to return to the input screen.
2. Choose **Phase** for **Plot Type**.
3. Press **ERASE** to erase previous plot.
4. Press **DRAW** to plot the function.



Output Screen - Bode phase plot

NOTE



This example is shown in degrees. If your HP 48 is set to radians, it will scale the vertical axis in radians.

Chapter 8

Fourier
Transforms

Analysis
<i>Fourier Transforms</i>
Equations
Reference

This chapter covers discrete “Fast” Fourier transforms:

- ☐ FFT
- ☐ Inverse FFT

FFT

Analysis
Fourier Transforms
FFT
Equations
Reference

A physical process can be monitored in two significantly different ways. First, the process can be monitored in time domain in analog or digital form. Second, the data can be collected in the frequency domain in analog or digital form. In a variety of measurement and digital storage devices, data is gathered at regular, discrete time intervals. This data can be converted to its equivalent set in the frequency domain by the use of the so-called FFT algorithm. This algorithm maps a data array of N items to the corresponding array in the frequency domain using the following equation.

$$H_k = \sum_{n=0}^{N-1} h_n \cdot e^{-2\pi j k \cdot n / N}$$

where h_n is the nth element in the time domain and H_k is the kth element in the frequency domain. The FFT algorithm treats the data block provided as though it is one of a periodic sequence. If the underlying data is not periodic, the resulting FFT-created wave is subject to substantial harmonic distortion. This section does not pad the input array with 0’s when the number of data points is not a power of 2.

Field Descriptions

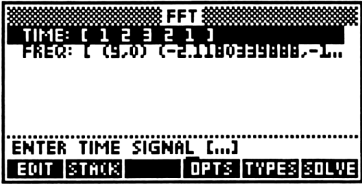
- Time:** (*Time Signal*) Enter an array or list of real or complex numbers.
- Freq:** (*Frequency Spectrum*) Returns spectral coefficients.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Find spectral coefficients for the periodic time signal [1 2 3 2 1].

- 1. Enter [1 2 3 2 1] for **Time**.
- 2. Press **SOLVE** to calculate **Freq**.



Output Screen

Inverse FFT

Analysis
Fourier Transforms
<i>Inverse FFT</i>
Equations
Reference

This section focuses on transforming data

from the frequency domain to the time domain. The inverse transform algorithm uses the relationship displayed here, where H_k is the k th element in the frequency domain and h_n is the n th element in the time domain.

$$h_n = \frac{1}{N} \sum_{k=0}^{N-1} H_k \cdot e^{2\pi j k \cdot n / N}$$

Field Descriptions

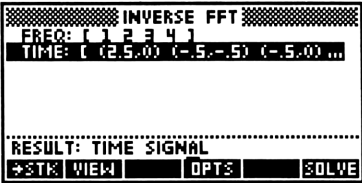
- Freq:** (*Frequency Spectrum*) Enter an array or list of real or complex numbers.
- Time:** (*Time Signal*) Returns time signal.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Given [1 2 3 4] as coefficients, find the original time signal.

- 1. Enter [1 2 3 4] for **Freq**.
- 2. Press **SOLVE** to calculate **Time**.



Output Screen

Chapter 9

Two-Port Networks

Analysis
<i>Two-Port Networks</i>
Equations
Reference

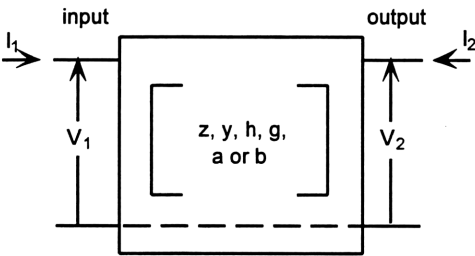
This chapter covers the basic principles of two-port network analysis:

- ❑ Parameter Conversion
- ❑ Circuit Performance
- ❑ Interconnected Two-Ports

Parameter Conversion

Analysis
Two-Port Networks
<i>Parameter Conversion</i>
Equations
Reference

Many electrical or electronic circuits are modelled as two-port networks with four variables, namely input voltage V_1 , input current I_1 , output voltage V_2 , and output current I_2 . In broad terms, a two-port network is a black-box approach



to solving simple to sophisticated problems of electrical and electronic circuits. The figure below shows a schematic representation of a two-port network where all four variables are identified.

For instance, a two-port characterized by z parameters is defined by the following pair of equations:

$$\begin{aligned} V_1 &= I_1 \cdot Z_{11} + I_2 \cdot Z_{12} \\ V_2 &= I_1 \cdot Z_{21} + I_2 \cdot Z_{22} \end{aligned}$$

The four components of z parameters are defined as follows:

$$Z_{11} = V_1/I_1 \quad \text{with} \quad I_2 = 0$$

$$Z_{21} = V_2/I_1 \quad \text{with} \quad I_2 = 0$$

$$Z_{12} = V_1/I_2 \quad \text{with} \quad I_1 = 0$$

$$Z_{22} = V_2/I_2 \quad \text{with} \quad I_1 = 0$$

The table below lists the choices for the independent variables for two-port circuits, followed by the dependent variables and parameters associated with each set of independent variables. This section allows you to convert two-port parameters from one type to another.

Independent Variables	Dependent Variables	Two-Port Parameter Type
I_1, I_2	V_1, V_2	z
V_1, V_2	I_1, I_2	y
I_1, V_2	V_1, I_2	h
I_2, V_1	I_1, V_2	g
V_2, I_2	V_1, I_1	b
V_1, I_1	V_2, I_2	a

Field Descriptions - Input Screen

Input Type: Press **CHOOS** to select z , y , h , g , a , or b .

..11: Enter a real or complex number, global name, or algebraic.

..12: Enter a real or complex number, global name, or algebraic.

..21: Enter a real or complex number, global name, or algebraic.

..22: Enter a real or complex number, global name, or algebraic.

Output Type: Press **CHOOS** to select z , y , h , g , a , or b .

Note: The help text (e.g., “Enter P1 Impedance V_1/I_1 ($I_2=0$)”) shows whether the ratio is an impedance, admittance or dimensionless ratio; which port is being described; and whether it is the current or the voltage that is open.

Field Descriptions - Output Screen

..11: Returns a real or complex number, global name, or algebraic.

..12: Returns a real or complex number, global name, or algebraic.

..21: Returns a real or complex number, global name, or algebraic.

..22: Returns a real or complex number, global name, or algebraic.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Convert a resistive two-port network with $z_{11} = 10$, $z_{12} = 7.5$, $z_{21} = 7.5$, $z_{22} = 9.375$ into its equivalent y values.

1. Choose z for **Input Type**.
2. Enter 10 for z_{11} , 7.5 for z_{12} , 7.5 for z_{21} , and 9.375 for z_{22} .
3. Choose y for **Output Type**.
4. Press **SOLVE** to calculate the results which will be displayed in the output screen.

```

PARAMETER CONVERSION
INPUT TYPE: Z
Z11: 10
Z12: 7.5
Z21: 7.5
Z22: 9.375
OUTPUT TYPE: Y
-----
CHOOSE INPUT PARAMETER TYPE
CHOOS [ ] [ ] OPTS [ ] SOLVE
  
```

Input Screen

```

RESULTS: PARAMETER CONVERSION
Y11: .25
Y12: -.2
Y21: -.2
Y22: .2666666666667
-----
P1 ADMITTANCE I1/V1 (V2=0)
+STK VIEW [ ] OPTS [ ] EXIT
  
```

Output Screen

Circuit Performance

This section computes the circuit performance of a two-port network. For example, given a voltage source of a finite impedance with a finite load, this section will compute the input and output impedances, current and voltage gain, voltage gain to source, current gain to source, power gain, power available at the load, maximum power available at the load, and load impedance for maximum power deliverable to the load.

Analysis
Two-Port Networks
Circuit Performance
Equations
Reference

Field Descriptions - Input Screen

Parameter Type: Press **CHOOS** to select z , y , h , g , a , or b .

..11: Enter a real or complex number, global name, or algebraic.

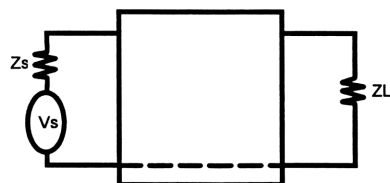
..12: Enter a real or complex number, global name, or algebraic.

..21: Enter a real or complex number, global name, or algebraic.

..22: Enter a real or complex number, global name, or algebraic.

Note: The help text (e.g., “Enter P1 Impedance $V1/I1$ ($I2=0$)”) shows whether the ratio is an impedance, admittance or dimensionless ratio; which port is being described; and whether it is the current or the voltage that is open.

Vs: (*Source Voltage in V*) Enter a real or complex number, global name, or algebraic.



- Zs:** (*Source Impedance in Ω*) Enter a real or complex number, global name, or algebraic.
- ZL:** (*Load Impedance in Ω*) Enter a real or complex number, global name, or algebraic.

Field Descriptions - Output Screen

- Zin:** (*Input Impedance*) Returns a real or complex number, global name, or algebraic.
- Iout:** (*Output Current*) Returns a real or complex number, global name, or algebraic.
- Vout:** (*Thevenin Voltage*) Returns a real or complex number, global name, or algebraic.
- Zout:** (*Thevenin Impedance*) Returns a real or complex number, global name, or algebraic.
- I2/I1:** (*Current Gain*) Returns a real or complex number, global name, or algebraic.
- V2/V1:** (*Voltage Gain*) Returns a real or complex number, global name, or algebraic.
- V2/Vs:** (*Absolute Voltage Gain*) Returns a real or complex number, global name, or algebraic.
- GP:** (*Power Gain*) Returns a real or complex number, global name, or algebraic.
- Pav:** (*Average Power*) Returns a real or complex number, global name, or algebraic.
- Pmax:** (*Maximum Power at ZLopt*) Returns a real or complex number, global name, or algebraic.
- ZLopt:** (*Optimum Load Impedance*) Returns a real or complex number, global name, or algebraic.

Example

MODES	\angle: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Find the circuit performance for a transistor amplifier given the following conditions: $h_{11} = 125$, $h_{12} = .001$, $h_{21} = 100$, $h_{22} = .0025$, source voltage $V_s = 0.50$, source impedance $Z_s = 50$, and load impedance $Z_L = 1500$.

1. Choose **h** for **Parameter**.

CIRCUIT PERFORMANCE		
PARAMETER TYPE: H		
H11:	125	
H12:	.001	
H21:	100	
H22:	.0025	
VS:	.5	
CHOOSE PARAMETER TYPE		
CHOOSE	OPTS	SOLVE

Input Screen

2. Enter 125 for **h11**, .001 for **h12**, 100 for **h21**, and .0025 for **h22**.
3. Enter 0.5 for **Vs**, 50 for **Zs** and 1500 for **ZL**.
4. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

RESULTS: CIRCUIT PERFORMANCE	
ZIN:	99.4210526316
IOUT:	7.3394954128E-2
VOUT:	-148.148148148
ZOUT:	518.518518519
I2/V1:	21.0526315789
V2/V1:	-338.028169014

INPUT IMPEDANCE (Z)	
→	EXIT
VIEW	OPTS
EXIT	

Output Screen

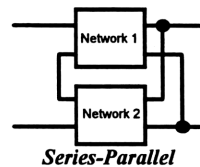
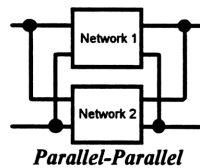
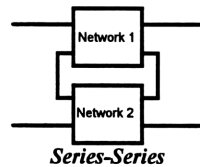
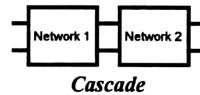
Interconnected Two-Ports

Two-port networks constitute basic building blocks of linear electrical/electronic systems.

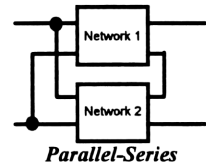
In the design of large, complex systems, it is easier to synthesize the system by first designing subsections. Usually, a large and complex system can be built using simpler two-port building blocks. The two-port subsections can be interconnected in five ways:

- **Cascade:** The output of network 1 is connected directly to the input of network 2.
- **Series-Series:** The inputs and outputs of the two networks are both connected in series.
- **Parallel-Parallel:** The inputs and outputs of the two networks are both connected in parallel.
- **Series-Parallel:** The inputs of the two networks are connected in series, while the outputs are connected in parallel.

Analysis
Two-Port Networks
<i>Interconnected Two-Ports</i>
Equations
Reference



- **Parallel-Series:** The inputs of the two networks are connected in parallel, while the outputs are connected in series.



NOTE



When using this section, the user needs to pay particular attention to the two-ports being interconnected in non-cascaded modes. Natural laws can be violated when the two-port network contains dependent voltage or current sources and the so-called Brune's test has to be satisfied. EE•Pro does *not* check for Brune's test.

This section accepts parameters for either network as **z**, **y**, **h**, **g**, **a**, or **b** and yields the output in any form based on the choice made.

Field Descriptions - Input Screen

Connection: (*Type of Connection*) Press **CHOOS** to select Cascade, Series Series, Parallel Parallel, Series Parallel, or Parallel Series.

First Input Type: Press **CHOOS** to select **z**, **y**, **h**, **g**, **a**, or **b**.

..111: Enter a real or complex number, global name, or algebraic.

..112: Enter a real or complex number, global name, or algebraic.

..121: Enter a real or complex number, global name, or algebraic.

..122: Enter a real or complex number, global name, or algebraic.

Second Input Type: Press **CHOOS** to select **z**, **y**, **h**, **g**, **a**, or **b**.

..211: Enter a real or complex number, global name, or algebraic.

..212: Enter a real or complex number, global name, or algebraic.

..221: Enter a real or complex number, global name, or algebraic.

..222: Enter a real or complex number, global name, or algebraic.

Output Type: Press **CHOOS** to select **z**, **y**, **h**, **g**, **a**, or **b**.

Note: The help text (e.g., “Enter P1 Impedance V1/I1 (I2=0)”) shows whether the ratio is an impedance, admittance or dimensionless ratio; which port is being described; and whether it is the current or the voltage that is open.

Field Descriptions - Output Screen


..11: Returns a real or complex number, global name, or algebraic.

..12: Returns a real or complex number, global name, or algebraic.

..21: Returns a real or complex number, global name, or algebraic.

..22: Returns a real or complex number, global name, or algebraic.

Example

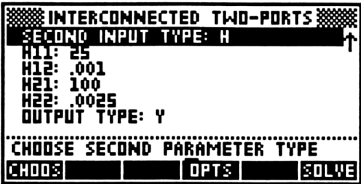
MODES (Press )	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
--	---	---

The 2 two-port networks in the two previous examples (“Parameter Conversion,” page 55, and “Circuit Performance,” page 57) were described in terms of their **z** and **h** parameters. If the two-ports are connected in a cascade configuration, compute the **y** parameters for the resulting equivalent two-port.

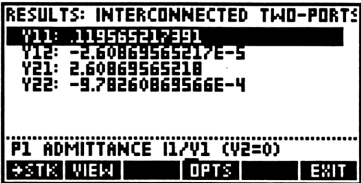
1. Choose Cascade for **Connection**.
2. Choose **z** for **First Input Type**.
3. Enter 10 for **z11**, 7.5 for **z12**, 7.5 for **z21**, and 9.375 for **z22**.
4. Choose **h** for **Second Input Type**.
5. Enter 25 for **h11**, .001 for **h12**, 100 for **h21**, and .0025 for **h22**.
6. Choose **y** for **Output Type**.
7. Press **SOLVE** to calculate the results, which will be displayed in the output screen..



Input Screen - Z



Input Screen - H



Output Screen

Chapter 10

Transformer Performance

Analysis
<i>Transformer Performance</i>
Equations
Reference

This chapter covers important power transformer principles: The open and short circuit tests, and chain parameters, which form the basis of a two-port network approach to evaluating transformer performance:

- ☐ Open Circuit Test
- ☐ Short Circuit Test
- ☐ Chain Parameters

Open Circuit Test

Analysis
Transformer Performance
<i>Open Circuit Test</i>
Equations
Reference

The open circuit test described in this section is performed at rated values of primary or secondary windings. It is assumed that the voltage is applied to the primary windings. The primary voltage, current, and power determine the core parameters of the transformer.

Field Descriptions - Input Screen

- V1:** (*Primary RMS Voltage in V*) Enter a real number, global name, or algebraic.
- V2:** (*Secondary RMS Voltage in V*) Enter a real number, global name, or algebraic.
- I1:** (*Primary RMS Current in A*) Enter a real number, global name, or algebraic.
- P1:** (*Primary Real Power in W*) Enter a real number, global name, or algebraic.

Field Descriptions - Output Screen

- n:** (*Primary to secondary turns ratio*) Returns a real number, global name, or algebraic.
- Q1:** (*Reactive power in W*) Returns a real number, global name, or algebraic.

- Gc:** (Primary core conductance in *S*) Returns a real number, global name, or algebraic.
- Bc:** (Primary core susceptance in *S*) Returns a real number, global name, or algebraic.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Perform an open circuit test on the primary side of a transformer using the following data: The input to primary is 125 volts, with an open circuit current of 1 ampere and a power input of 45 watts. The secondary open circuit voltage is 440 volts. Find the circuit parameters of the transformer.

1. Enter the values 125 for **V1** and 440 for **V2**.
2. Enter 1 for **I1** and 45 for **P1**.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

OPEN CIRCUIT TEST
V1: 125
V2: 440
I1: 1
P1: 45
.....
ENTER PRIMARY RMS VOLTAGE (V)
EDIT STACK OPTS TYPES SOLVE

Input Screen

RESULTS: OPEN CIRCUIT TEST
N: 284000000001
Q1: 116.618037897
GC: .00288
BC: -7.46361842541E-3
.....
PRIM. TO SEC. TURNS RATIO
STK VIEW OPTS EXIT

Output Screen

Short Circuit Test

Short circuit tests are often used to determine winding impedances of a transformer and are conducted at rated values. The test consists of placing a short circuit on the secondary windings and measuring primary and secondary currents, and power supplied to the transformer. The calculated circuit parameters (i.e., resistance and reactance of primary and secondary coils) are based on the assumption that the heat dissipation in the primary and secondary windings are equal.

Analysis
Transformer Performance
<i>Short Circuit Test</i>
Equations
Reference

Field Descriptions - Input Screen

- V1:** (Primary RMS Voltage in *V*) Enter a real number, global name, or algebraic.

- I2:** (*Secondary RMS Current in A*) Enter a real number, global name, or algebraic.
- P1:** (*Primary Real Power in W*) Enter a real number, global name, or algebraic.
- kVA:** (*kVA rating in kVA*) Enter a real number, global name, or algebraic.
- V1R:** (*Primary Voltage Rating in V*) Enter a real number, global name, or algebraic.

Field Descriptions - Output Screen

- n:** (*Primary to secondary turns ratio*) Returns a real number, global name, or algebraic.
- Q1:** (*Primary Reactive Power in W*) Returns a real number, global name, or algebraic.
- R1:** (*Primary Resistance in Ω*) Returns a real number, global name, or algebraic.
- R2:** (*Secondary Resistance in Ω*) Returns a real number, global name, or algebraic.
- X1:** (*Primary Reactance in Ω*) Returns a real number, global name, or algebraic.
- X2:** (*Secondary Reactance in Ω*) Returns a real number, global name, or algebraic.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

A transformer rated at 20 kVA and 400 volts is subjected to a short circuit test. The measured current in the secondary is 85 amperes. A primary voltage of 65 volts and a power of 150 watts are applied to obtain this current in the secondary. Find the transformer parameter.

SHORT CIRCUIT TEST	
V1: 65	
I2: 85	
P1: 150	
KVA: 20	
V1R: 400	
ENTER PRIMARY RMS VOLTAGE (V)	
EDIT STACK	OPTS TYPE3 SOLVE

Input Screen

1. Enter the values 65 for **V1**, 85 for **I2**, and 150 for **P1**.
2. Enter 20 for **kVA** and 400 for **V1R**.
3. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

RESULTS: SHORT CIRCUIT TEST	
N: 1.7	
Q1: 3246.53661615	
R1: .03	
R2: 1.03806228374E-2	
X1: .64930732323	
X2: .224673814266	
PRIM. TO SEC. TURNS RATIO	
→STK VIEW	OPTS EXIT

Output Screen

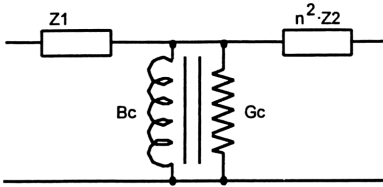
Chain Parameters

Analysis
Transformer Performance
Chain Parameters
Equations
Reference

Chain parameters (or the so-called ABCD parameters) are convenient problem-solving tools used in solving transmission and distribution problems. The parameters are expressed essentially as two-port type parameters by the use of the following pair of linear equations:

$$V_{in} = A \cdot V_{out} - B \cdot I_{out}$$

$$I_{in} = C \cdot V_{out} - D \cdot I_{out}$$



where V_{in} and I_{in} are input voltage and current, and V_{out} and I_{out} are output voltage and current. (All quantities in the diagram refer to the primary winding.) This approach is useful as cascaded transformers follow two-port rules.

Field Descriptions - Input Screen

Z1: (Primary impedance in Ω) Enter a real or complex number, global name, or algebraic.

Z2: (Secondary impedance in Ω) Enter a real or complex number, global name, or algebraic.

n: (Primary to secondary turns ratio) Returns a real number, global name, or algebraic.

Gc: (Primary core conductance in S) Enter a real number, global name, or algebraic.

Bc: (Primary core susceptance in S) Enter a real number, global name, or algebraic.

Field Descriptions - Output Screen

A: (A Parameter) Returns a real or complex number, global name, or algebraic.

B: (B Parameter) Returns a real or complex number, global name, or algebraic.

C: (C Parameter) Returns a real or complex number, global name, or algebraic.

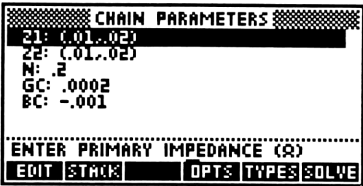
D: (D Parameter) Returns a real or complex number, global name, or algebraic.

Example

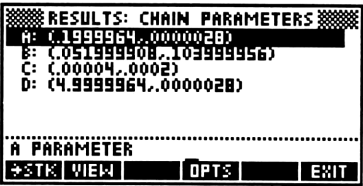
MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

A transformer has an input impedance of (0.01, 0.02) and a core admittance of (0.0002, -0.001). Find the ABCD parameter if the turns ratio is 0.2.

1. Enter (0.01, 0.02) for **Z1** and (0.01, 0.02) for **Z2**.
2. Enter 0.2 for **N**, 0.0002 for **Gc**, and -0.001 for **Bc**.
3. Press solve to calculate the results, which will be displayed in the output screen.



Input Screen



Output Screen

Chapter 11

Transmission Lines

Analysis
<i>Transmission Lines</i>
Equations
Reference

This chapter covers the basic principles of transmission line analysis:

- ☐ Line Characteristics
- ☐ Line Parameters
- ☐ Fault Location Estimate
- ☐ Stub Impedance Matching

Line Characteristics

Analysis
Transmission Lines
<i>Line Characteristics</i>
Equations
Reference

This section computes the basic characteristics of a transmission line from the given parameters.

Field Descriptions - Input Screen

- L:** (*Series Inductance in H/Unit Length*) Enter a real number, global name or algebraic.
- R:** (*Series Resistance in Ω /Unit Length*) Enter a real number, global name or algebraic.
- G:** (*Shunt Conductance in S/Unit Length*) Enter a real number, global name or algebraic.
- C:** (*Shunt Capacitance in F/Unit Length*) Enter a real number, global name or algebraic.
- ZL:** (*Load Impedance in Ω*) Enter a real or complex number, global name or algebraic.
- d:** (*Distance to Load - unit length*) Enter a real number, global name or algebraic.
- f:** (*Frequency in Hz*) Enter a real number, global name or algebraic.

Field Descriptions - Output Screen

- Z0:** (*Characteristic Impedance in Ω*) Returns a real or complex number, global name, or algebraic.
- Y0:** (*Characteristic Admittance in S*) Returns a real or complex number, global name, or algebraic.
- α :** (*Neper Constant in 1/unit length*) Returns a real number, global name, or algebraic.
- β :** (*Phase Constant in \angle /unit length*) Returns a real number, global name, or algebraic.
- λ :** (*Wavelength in unit lengths*) Returns a real number, global name, or algebraic.
- vp:** (*Phase Velocity in unit length/s*) Returns a real number, global name, or algebraic.
- Zoc:** (*Open Circuit Impedance in Ω*) Returns a real or complex number, global name, or algebraic.
- Zsc:** (*Short Circuit Impedance in Ω*) Returns a real or complex number, global name, or algebraic.
- p:** (*Reflection Coefficient*) Returns a real or complex number, global name, or algebraic.
- SWR:** (*Standing Wave Ratio*) Returns a real number, global name, or algebraic.

Example

MODES	\angle: Radian	Result: Symbolic
(Press CST)	Coord: Polar	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

A transmission line has a series inductance of 1 mH/mile, a line resistance of 85.8 ohm/mile, a conductance of 1.5×10^{-6} mhos/mile, and a shunt capacitance of 62×10^{-9} F/mile. With a load impedance of 75 ohms at 3 miles from the load, compute the line characteristics at a frequency of 1000 Hz.

Note: For this example, the unit length is the mile, so all values will be entered with respect to miles.

- Enter the values 0.001, 85.8, and $1.5E-6$ for **L**, **R**, and **G**, respectively.
- Enter the values $62E-9$, 75, and 3 for **C**, **ZL**, and **d**, respectively.

LINE CHARACTERISTICS	
L: 0.001	
R: 85.8	
G: .0000015	
C: .000000062	
ZL: 75	
d: 3	
ENTER SERIES INDUCTANCE (H/LEN)	
EDIT	STAY
OPTS	TYPE3 SOLVE

Input Screen

RESULTS: LINE CHARACTERISTICS	
Z0: 469.934088658	\angle : 246922851
Y0: 2.12785788269E-3	\angle : 2.746922851
α : .124888593544	
β : .1338520544	
λ : 46.941269115	
VP: 46941.269115	
CHARACTERISTIC IMPEDANCE (Ω)	
*STK	VIEW
OPTS	EXIT

Output Screen

3. Enter 1000 for **f**.
4. Press **SOLVE** to calculate the results and display them as shown to the right.

Line Parameters

This section computes the parameters of a transmission line from measured data describing the line.

Analysis
Transmission Lines
Line Parameters
Equations
Reference

NOTE



The algorithm used in this section solves for γ in the following equation, where $\gamma = 2 + j\beta$:

$$\text{TANH}(\gamma \cdot d) = \sqrt{Z_{sc}/Z_{oc}}$$

In general γ , Z_{sc} , and Z_{oc} have complex values. In solving for γ , there is a principal value and a set of equivalent values because of the cyclical nature of the equation. Recognizing the fact that physical parameters such as **R**, **L**, **G**, **C**, and **vp** are all real and positive numbers, extreme caution should be exercised when entering input data. In particular, **d** should be less than one wavelength.

Field Descriptions - Input Screen

Zoc: (*Open Circuit Impedance in Ω*) Enter a real number.

Zsc: (*Short Circuit Impedance in Ω*) Enter a real number.

d: (*Distance to Load Location*) Enter a real number.

f: (*Frequency in Hertz*) Enter a real number.

Field Descriptions - Output Screen

R: (*Series Resistance in Ω /unit length*) Returns a real number.

L: (*Series Inductance in H/unit length*) Returns a real number.

G: (*Shunt Conductance in S/unit length*) Returns a real number.

C: (*Shunt Capacitance in F/unit length*) Returns a real number.

Z0: (*Characteristic Impedance in Ω*) Returns a real number.

Y0: (*Characteristic Admittance in Ω*) Returns a real number.

α : (*Neper Constant in 1/unit length*) Returns a real number.

β : (*Phase Constant in $^\circ$ /unit length*) Returns a real number.

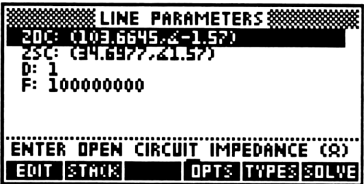
vp: (*Phase Velocity in unit length/s*) Returns a real number.

Example

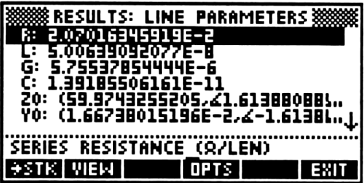
MODES (Press CST)	∠: Radian Coord: Polar Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	--	---

A transmission line is measured to have an open circuit impedance of (103.6645, ∠-1.57) and a short circuit of (34.6977, ∠1.57) at a distance 1 unit length from the load location. All measurements are carried out at 100 MHz. Compute all the parameters.

1. Enter (103.6645, ∠-1.57) for **Zoc**.
2. Enter (34.6977, ∠1.57) for **Zsc**.
3. Enter 1 and 100E6 for **d** and **f**, respectively.
4. Press **SOLVE** to calculate the results and display them as shown to the right.



Input Screen



Output Screen

Fault Location Estimate

This section makes a best estimate of the closest possible location of a fault in a lossless transmission line.

Analysis
Transmission Lines
Fault Location Estimate
Equations
Reference

Field Descriptions

Xin: (*Input Reactance in Ω*) Enter a real number, global name, or algebraic.

R0: (*Characteristic Resistance in Ω*) Enter a real number, global name, or algebraic.

β: (*Phase Constant - ∠/unit length*) Enter a real number, global name, or algebraic.

docmin: (*Minimum distance to an open circuit fault in unit lengths*) Returns a real number, global name, or algebraic.

dscmin: (*Minimum distance to short circuit fault in unit lengths*) Returns a real number, global name, or algebraic.

Example

MODES (Press CST)	∠: Radians Coord: Polar Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

A transmission line measures a capacitive reactive impedance of 275 ohms. The characteristic line impedance is 75 ohms, with a phase constant of 0.025 r/length. Estimate the fault location.

1. Enter the values 275, 75, and 0.025 for **Xin**, **R0**, and **β**, respectively.
2. Press **SOLVE** to calculate the results as shown in the screen to the right.

FAULT LOCATION ESTIMATE			
XIN: 275			
R0: 75			
β: 0.025			
DOCMIN:			
DSCMIN:			
RESULT: MIN. D TO OPEN (LENG)			
←STK	VIEW	DPTS	SOLVE

Input Screen

FAULT LOCATION ESTIMATE			
XIN: 275			
R0: 75			
β: 0.025			
DOCMIN: 115.013624178			
DSCMIN: 52.1817711056			
RESULT: MIN. D TO OPEN (LENG)			
←STK	VIEW	DPTS	SOLVE

Output Screen

Stub Impedance Matching

This section calculates the parameters of a single-stub impedance-matching device. From the input data, the location and electrical length of an open- and short-circuit stub is computed. Because the solution is circular in nature, there are two possible stub-locations d1 and d2.

Analysis
Transmission Lines
<i>Stub Impedance Matching</i>
Equations
Reference

Field Descriptions - Input Screen

- ZL:** (*Load Impedance in Ω*) Enter a real or complex number, global name, or algebraic.
- R0:** (*Characteristic Resistance in Ω*) Enter a real, global name, or algebraic.

Field Descriptions - Output Screen

- β*d1:** (*Electrical length from a stub at location d1 to the load in ∠*) Returns a real, global name, or algebraic.
- β*d1-sc:** (*Electrical length of a short-circuited shunt stub at distance d1 from load in ∠*) Returns a real, global name, or algebraic.
- β*d1-oc:** (*Electrical length of an open-circuited shunt stub at distance d1 from load in ∠*) Returns a real, global name, or algebraic.

$\beta \cdot d2$: (Electrical length from a stub at location $d2$ to the load in \angle) Returns a real, global name, or algebraic.

$\beta \cdot d2\text{-sc}$: (Electrical length of a short-circuited shunt stub at distance $d2$ from load in \angle) Returns a real, global name, or algebraic.

$\beta \cdot d2\text{-oc}$: (Electrical length of an open-circuited shunt stub at distance $d2$ from load in \angle) Returns a real, global name, or algebraic.

Example

MODES	\angle : Radians	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

A transmission line has a terminating impedance of (75,25) ohms and a characteristic impedance of 50 ohms. Eliminate standing waves in the transmission line using a short or open shunt stub. Determine the electrical length of the stub and its distance from the load.

1. Enter (75,25) for **ZL** and 50 for **R0**.
2. Press **SOLVE** to calculate the results, which will be displayed in the output screen.

```

STUB IMPEDANCE MATCHING
ZL: (75,25)
R0: 50

.....
ENTER LOAD IMPEDANCE (Z)
[EXIT] [STUB] [OPTS] [TYPES] [SOLVE]
  
```

Input Screen

```

RESULTS: STUB IMPEDANCE MATCHING
SXD1: 1.31991691592
SXDI-SC: 1.0471975512
SXDI-OC: 2.61799387799
SXDI: 2.50967834122
SXDI-SC: 2.09439510239
SXDI-OC: .523598775598

.....
FIRST STUB (DIST. D1 FROM LOAD)
[STK] [VIEW] [OPTS] [EXIT]
  
```

Output Screen

Chapter 12

Computer Engineering

Analysis
Computer Engineering
Equations
Reference

This chapter covers functions of interest in the design of logic systems commonly used by students and professionals in computer engineering. The modules include binary arithmetic, bit operations, comparisons and a form of logic minimization using the Quine-McCluskey algorithm:

- ☐ Binary Modes Screen
- ☐ Binary Arithmetic
- ☐ Register Operations
- ☐ Bit Operations
- ☐ Binary Conversions
- ☐ Binary Comparisons
- ☐ Karnaugh Map

Binary Modes Screen

The binary modes screen, available in all Computer Engineering screens except Karnaugh Map, is displayed by pressing **MODE**. The first three settings will remain in effect until the user resets them again from the binary modes screen. The Carry and Range flags may be set or cleared by various functions in the Computer Engineering module. The binary modes screen simply gives the user a way to set or clear them by hand.

To change any of these settings, move the highlight bar to the desired item and press **CHOOS** or **+/-**. Then press **OK** to implement the changes, or to exit the screen without changing the settings, press **CANCEL** or **ON**.



Base: (*Binary Base*) Press **CHOOS** to select Binary, Octal, Decimal or Hexadecimal.

Wordsize: (*Size of Binary Number*) Enter a number from 0 to 64 to set word size.

Sign: (*Sign Convention*) Press **CHOOS** to select Unsigned, One's Complement, or Two's Complement.

Carry: (*Carry Flag - User Flag 4*) Press **CHOOS** to select Set or Clear.

Range: (*Range Flag - User Flag 5*) Press **CHOOS** to select Set or Clear.

Range and Carry Flags

Whenever a binary addition results in a carry beyond the most significant bit, the carry flag will be set. If an addition does not result in a carry, the flag will be cleared. This is true for all complement modes.

Whenever binary arithmetic results cannot be represented in the current word size and complement mode, the range flag will be set.

Binary Arithmetic

Analysis Computer Engineering <i>Binary Arithmetic</i> Equations Reference
--

This section allows you to add, subtract, multiply, and divide binary numbers, as well as negate or find the absolute value of a binary number.

Field Descriptions

Binary: (*Input Field*) Enter a binary integer.

Binary: (*Input Field*) Enter a binary integer.

Operator: (*Binary Operation*) Press **CHOOS** to select:

ADD16C Add two binary or real numbers. Affects range and carry flags.

SUB16C Subtract one binary or real number from another. Affects range and carry flags.

MULT16C Multiply two binary or real numbers. Affects range and carry flags.

DIV16C Divide two binary or real numbers and return quotient. Affects carry flag only.

RMD16C Divide two binary or real numbers and return remainder. Does not affect range or carry flags.

NEG16C Negate a binary or real number. Affects range flag only.

ABS16C Find the absolute value of a binary or real number. Affects range flag only.

Result: (*Binary Function Value*) Returns a binary integer or real number.



Flags: (*State of Carry and Range Flags*) Returns Carry if carry flag is set.
Returns Range if range flag is set.

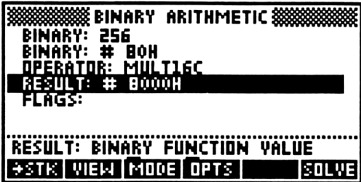
Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Binary Modes Press MODE	Base: Hexadecimal Wordsize: 32 Sign: Unsigned	Carry: Clear Range: Clear
--	--	--

Multiply a real number 256 and a binary number #128d.

- 1. In the first **Binary** field, press **TYPES** to select Real Number.
- 2. Enter 256 in the first **Binary** field.
- 3. Enter 128d (128   D) in the second **Binary** field.
- 4. Choose MULT16C for **Operator**.
- 5. Press **SOLVE** to calculate **Result**.



Output Screen

Register Operations

Analysis
Computer Engineering
Register Operations
Equations
Reference

This section allows you to perform operations on any bit of a binary integer. Such operations include shifting bits to the left or right, rotating bits to the left or right, and shifting or rotating through the carry flag.

Field Descriptions

- Binary:** (*Input Field*) Enter a binary integer.
- N:** (*Number of places for shifting or rotating - appears only when SRN16C, RLN16C, RLN16C, RRN16C, RLCN16C, or RRCN16C are selected*) Enter a real number.
- Operator:** (*Binary Operation*) Press **CHOOS** to select:
- Note:** All register operations set the carry flag if a 1 is rotated or shifted off the end, otherwise they clear the carry flag.
- SL16C Shifts the input to the left by one bit and shifts a 0 into the rightmost position.
- SR16C Shifts the input to the right by one bit and shifts a 0 into the leftmost position.

- RL16C** Rotates the input to the left by one bit. The leftmost bit wraps around to the rightmost position.
- RR16C** Rotates the input to the right by one bit. The rightmost bit wraps around to the leftmost position.
- RLC16C** Rotates bits left by one bit through carry. Loads the leftmost bit into the carry and moves the carry bit into the rightmost position.
- RRC16C** Rotates bits right by one bit through carry. Loads the rightmost bit into the carry and moves the carry bit into the leftmost position.
- ASR16C** Arithmetic shift right: For One's Complement and Two's Complement, shifts bits to the right, but keeps the leftmost bit (the sign bit) the same. For Unsigned mode, which has no sign bit, a 0 is shifted into the leftmost position.
- SLN16C** Shifts left by N bits.
- SRN16C** Shifts right by N bits.
- RLN16C** Rotate left by N bits.
- RRN16C** Rotate right by N bits.
- RLCN16C** Rotate left by N bits through the carry.
- RRCN16C** Rotate right by N bits through the carry.

Result: (*Binary Function Value*) Returns a binary integer.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Binary Modes Press MODE	Base: Hexadecimal Wordsize: 32 Sign: Unsigned	Carry: Clear Range: Clear
--	--	--

Rotate the binary number 1256 to the right by 4 bits.

1. Enter 1256 in the **Binary** field.
2. Choose RRN16C for **Operator**.
3. Enter 4 for **N**.
4. Press **SOLVE** to calculate **Result**.

REGISTER OPERATIONS	
BINARY: # 1256H	
N: 4	
OPERATOR: RRN16C	
RESULT: # 60000125H	
FLAGS:	
RESULT: BINARY FUNCTION VALUE	
→STK VIEW MODE OPTS	SOLVE

Output Screen

Bit Operations

Analysis
Computer Engineering
<i>Bit Operations</i>
Equations
Reference

This section allows you to perform bit-specific operations. You can set a bit, clear a bit, test a bit or find the total number of bits set.

Field Descriptions

- Binary:** (*Input Field*) Enter a binary integer.
- Bit #:** (*Bit Position - not active if ΣB is selected*) Enter a binary integer or real number.
- Operator:** (*Binary Operation*) Press **CHOO**S to select
- Note:** All bit operations affect the carry flag only.
- SB Sets the bit in the specified position.
 - CB Clears the bit in the specified position.
 - B? Tests the bit in the specified position.
 - ΣB Returns the number of bits set.
- Result:** (*Binary Function Value*) Returns a binary integer.

Example

MODES (Press CST)	\angle: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Binary Modes Press MODE	Base: Binary Wordsize: 32 Sign: Unsigned	Carry: Clear Range: Clear
--	---	--

Test the fifth bit of the binary number #1256d in its binary form.

- Enter 1256d (1256 **[α]** **[\leftarrow]** D) for **Binary**.
- Enter 5 for **Bit #**.
- Choose B? for **Operator**.
- Press **SOLVE** to calculate **Result**. A “1” means the bit is set.

BIT OPERATIONS			
BINARY: # 10011101000E			
BIT #: 5			
OPERATOR: B?			
RESULT: 1			

CHOOSE AN OPERATION			
CHOO	MODE	OPTS	SOLVE

Output Screen

Binary Conversions

Analysis
Computer Engineering
Binary Conversions
Equations
Reference

This section allows you convert real numbers to binary numbers and vice versa. It also allows you to convert real numbers to IEEE format and vice versa.

Field Descriptions

Binary: (*Input Field for B→R16C and IEEE→*) Enter a binary integer.

Real: (*Input Field for R→B16C and →IEEE*) Enter a real number.

Function: (*Binary Function*) Press **CHOOS** to select:

R→B16C Converts a real number to a binary number (decimal, binary, hexadecimal or octal). Affects the range flag only.

B→R16C Converts a binary number (decimal, binary, hexadecimal or octal) to a real number.

→IEEE Converts a real number to the IEEE 32 bit format. The word size is automatically set to 32 bits. Affects the range flag only.

IEEE→ Converts a IEEE number to a real number. The word size is automatically set to 32 bits. Affects the carry and range flags.

Result: (*Binary Function Value*) Returns a binary integer.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Binary Modes	Base: Binary	Carry: Clear
Press MODE	Wordsize: 32	Range: Clear
	Sign: Unsigned	

Convert the real number 451236 to a binary number.

1. Enter 451236 for **Real**.
2. Choose R→B16C for **Function**.
3. Press **SOLVE** to calculate **Result**.

BINARY CONVERSIONS			
REAL:	451236		
FUNCTION:	R→B16C		
RESULT:	# 11011100010101001008		
CHOOSE A FUNCTION			
CHOOS	MODE	OPTS	SOLVE

Output Screen

Binary Comparisons

Analysis
Computer Engineering
Binary Comparisons
Equations
Reference

This section allows you to compare two binary numbers to determine if they are the same value, unequal, greater than, less than, etc.

Field Descriptions

Binary: (*Input Field*) Enter a binary integer or real number.

Binary: (*Input Field*) Enter a binary integer or real number.

Operator: (*Binary Operation*) Press **CHOOS** to select:

Note: All binary comparison commands affect the carry flag only.

=16C Compares two binary or real numbers. The result field shows a 1 if they are equal, otherwise 0.

≠16C Compares two binary or real numbers. The result field shows a 1 if they are NOT equal, otherwise 0.

<16C Compares two binary or real numbers. If the number in the first field is less than the number in the second field, then the result field displays a 1, otherwise 0.

>16C Compares two binary or real numbers. If the number in the first field is greater than the number in the second field, then the result field displays a 1, otherwise 0.

≤16C Compares two binary or real numbers. If the number in the first field is less than or equal to the number in the second field, then the result field displays a 1, otherwise 0.

≥16C Compares two binary or real numbers. If the number in the first field is greater than or equal to the number in the second field, then the result field displays a 1, otherwise 0.





Result: (*Binary Function Value*) Returns 1 (True) or 0 (False).

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Binary Modes Press MODE	Base: Binary Wordsize: 32 Sign: Unsigned	Carry: Clear Range: Clear
--	---	--

Compare two binary numbers #45312h and #16725o and determine if they are equal.

1. Enter 45312h (45312   H) in the first **Binary** field.
2. Enter 16725o (  O) in the second **Binary** field.
3. Choose ==16C for **Operator**.
4. Press **SOLVE** to calculate **Result**.
5. The result is 0, meaning false, so the two numbers are not equal.

BINARY COMPARISONS	
BINARY: #	1000101001100010010B
BINARY: #	1110111010101B
OPERATOR: ==	16C
RESULT:	0
RESULT: BINARY FUNCTION VALUE	
STK	VIEW MODE OPTS SOLVE

Output Screen

Karnaugh Map

In this section, the user is provided with a powerful tool to design efficient combinatorial logic networks. The program provides a convenient symbolic representation of the minimization method in a “sum of products form.” The variable naming convention is restricted to 1 character per variable and is case-sensitive. The algorithm used in developing the logic uses the defined form of minimization developed by W.V. Quine and E.J. McCluskey. The resulting output is an algebraic expression for the prime implicants. In this representation, a logic variable (e.g., A) represents its true value, while A' is used to represent its negation.

Analysis
Computer Engineering
Karnaugh Map
Equations
Reference

NOTE



The sum of products form displayed here may not be the most optimum solution.

Field Descriptions

Minterms: (*List of Minterms*) Enter a list of real or binary numbers. Real and binary numbers can be combined in the same list.

Don't Care: (*List of Don't Care Terms*) Enter a list of real or binary numbers. Real and binary numbers can be combined in the same list.

Variables: (*List of Variables*) Enter a string or global name, with no spaces between variables.

Expr: (*Prime Implicant Expression*) Returns an algebraic expression.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Minimize a five input function with minterms at 0, 2, 4, 6, 8, 10, 11, 12, 13, 14, 16, 19, 29, 30. The input variables are V, W, X, Y and Z. Find the prime implicant expression.

1. Enter {0, 2, 4, 6, 8, 10, 11, 12, 13, 14, 16, 19, 29, 30} for **Minterms**.
2. Enter {1} for **Don't Care**.
3. Enter VWXYZ for **Vars**.
4. Press **SOLVE** to calculate **Expr**.
5. Move the highlight bar to the **Expr** field and view the entire result by pressing **VIEW**.

KARNAUGH MAP

MINTERMS: 0 2 4 6 8 10 11 ...

DON'T CARE: 1 1 }

VARs: VWXYZ

EXPR:

ENTER LIST OF MINTERMS

EDIT STACK OPTS TYPES SOLVE

Input Screen

KARNAUGH MAP

MINTERMS: 0 2 4 6 8 10 11 ...

DON'T CARE: 1 1 }

VARs: VWXYZ

EXPR: VWXYZ + V'W'X'Y' + W'X'Y'Z' + V'WX'Y + V'WXY' + WXY'Z + WXYZ

RESULT: PRIME IMPICANT EXPR.

→STK VIEW OPTS SOLVE

Output Screen

KARNAUGH MAP

VW'X'YZ + V'W'X'Y' + W'X'Y'Z' + V'WX'Y + V'WXY' + WXY'Z + WXYZ

EXPR

Chapter 13

Algebraic Functions

Analysis <i>Algebraic Functions</i> Equations Reference
--

This chapter covers commonly-used algebraic functions:

- ☐ Partial Fraction Expansion
- ☐ Piecewise Functions
- ☐ Polynomial Coefficients
- ☐ Polynomial Equation
- ☐ Polynomial Roots
- ☐ Symbolic Simplification
- ☐ Taylor Polynomial

Partial Fraction Expansion

Analysis Algebraic Functions <i>Partial Fraction Expansion</i> Equations Reference
--

The partial fraction expansion function separates a rational function of the form

$f(x)/g(x)$ by splitting it into a sum of fractions with simpler denominators.

Field Descriptions

Inputs: (*Form of numerator and denominator*) Press **CHOOS** to select Coefficients or Roots. Determines whether inputs for **Numer** and **Denom** are interpreted as coefficients or roots.

Constant: (*Constant*) Enter a real number. (Default is 1.)

Numer: (*Numerator coefficients or roots*) Enter an array or list of real or complex numbers.

Denom: (*Denominator coefficients or roots*) Enter an array or list of real or complex numbers.

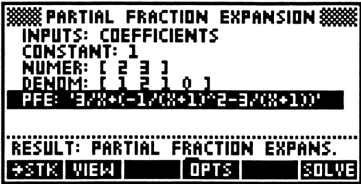
PFE: (*Partial fraction expansion*) Returns an algebraic expression.

Example: Coefficients Format

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

What is the partial fraction expansion of the rational function $\frac{2x+3}{x^3+2x^2+x}$?

- 1. Choose Coefficients for **Inputs**.
- 2. Enter 1 for **Constant**.
- 3. Enter [2 3] for **Numer** and [1 2 1 0] for **Denom**.
- 4. Press **SOLVE** to calculate **PFE**.

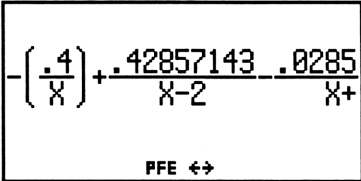
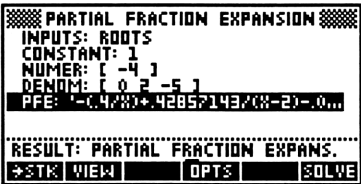


Example: Roots Format

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

What is the partial fraction expansion of the rational function $\frac{x+4}{x(x-2)(x+5)}$?

- 1. Choose Roots for **Inputs**.
- 2. Enter 1 for **Constant**.
- 3. Enter [-4] for **Numer** and [0 2 -5] for **Denom**.
- 4. Press **SOLVE** to calculate **PFE**.
- 5. To display **PFE** in graphics view, press **VIEW**.
- 6. Press **←** and **→** to scroll the equation.



Piecewise Functions

Piecewise functions take on different functional forms (expressions) over different regions of the independent variable:

$$f(x) = \begin{cases} \text{expression}_1 & \text{region}_1 \\ \text{expression}_2 & \text{region}_2 \end{cases}$$

Analysis
Algebraic Functions
<i>Piecewise Functions</i>
Equations
Reference

The HP 48 can manipulate and plot piecewise functions if they are entered in the IFTE (If-Then-Else) format:

$$f(x) = \text{IFTE}(\text{region}_1, \text{expression}_1, \text{expression}_2)$$

This section enables you to easily enter a piecewise function as one or more *terms*, where each term is specified by two fields: one for the expression (EXPR) and the other for the corresponding region (REGION). Then the appropriate IFTE representation of the piecewise function is generated.

Entry Rules

- Use == in place of =. The HP 48 uses the = operator only for assigning variables, while the == command is used to check for equality. Therefore, the region $X=0$ should be entered as 'X==0'. The most common operators used in regions are found in the TEST menu: ==, ≠, <, >, <=, and >=.
- To make a section of a piecewise function undefined, enter Undefined as the expression for the term, along with the corresponding region. An Undefined term will automatically be appended to complete all one-term piecewise functions. (Note: Undefined is simply a global name that presumably does not exist in user memory and will therefore remain unevaluated when plotting.)
- Always specify terms in the function in order of increasing regions. For example, specify the term for the region $X < -3$ before the term for the region $X < 3$. This is because the HP 48 will not properly evaluate expressions like ' $-3 < X < 3$ ', so this region must be entered as ' $X < 3$ '. However, this would incorrectly imply that the corresponding expression should be used for all values of $X < 3$, so you must have first entered a term for the region $X \leq -3$.
- For regions like $X = 2, 3$ the entry must be split into two separate terms because the HP 48 will not recognize an expression like ' $X == 2, 3$ '. Therefore, enter the same expression twice, for two different regions: ' $X == 2$ ' and ' $X == 3$ '.

Field Descriptions

Expr: (*Expression*) Enter a real number, complex number, global name, algebraic or unit.

Region: (*Region of validity*) Enter a real number, global name or algebraic.

Pwise: (*Piecewise function*) Returns an algebraic expression.

Example 1

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Define the piecewise function

$$f(x) = \begin{cases} \sin(x)/x & x \neq 0 \\ 1 & x = 0 \end{cases}$$

This will require two terms.

1. Enter $\sin(X)/X$ for **Expr**.
2. Enter $X \neq 0$ for **Region** (key sequence: **CX** **X** **PRG** **TEST** **≠** **0** **ENTER**).
3. Press **ADD** to create new **Expr** and **Region** fields for the second term.
4. Enter 1 for the second **Expr** field and $X=0$ for the **Region** field.
5. Press **SOLVE** to calculate **Pwise**.

PIECEWISE FUNCTIONS	
EXPR: 'SIN(X)/X'	
REGION: 'X≠0'	
EXPR: 1	
REGION: 'X=0'	
PWISE: 'IFTECH≠0.SIN(X)/X.IFTECH=...	
RESULT: PIECEWISE FUNCTION	
STK VIEW ADD OPTS	SOLVE

Example 2

MODES (Press CST)	∠: Degrees	Result: Symbolic
	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Define the piecewise function: $f(x) = \begin{cases} 3x+2 & x < -3 \\ 2x+7 & -3 \leq x \leq 2 \\ 7x-2 & x > 2 \end{cases}$

This will require three terms.

1. Enter $3*X+2$ for **Expr** and $X < -3$ for **Region**.
2. Press **ADD** to create new **Expr** and **Region** fields.
3. Enter $2*X+7$ for the second **Expr** field and $X \leq 2$ for **Region**.
4. Press **ADD**.
5. Enter $7*X-2$ for the third **Expr** field and $X > 2$ for **Region**.
6. Press **SOLVE** to calculate **Pwise**.

PIECEWISE FUNCTIONS	
REGION: 'X<-3'	
EXPR: '2X+7'	
REGION: 'X≤2'	
EXPR: '7X-2'	
REGION: 'X>2'	
PWISE: 'IFTECH<-3.3X+2.IFTECH≤...	
RESULT: PIECEWISE FUNCTION	
STK VIEW ADD OPTS	SOLVE

Polynomial Coefficients

Analysis
Algebraic Functions
Polynomial Coefficients
Equations
Reference


This section takes the roots (real or complex) of a polynomial and returns the coefficients (real or complex) of the polynomial.

Field Descriptions

Roots: (*Polynomial roots*) Enter an array or list of real or complex numbers.

Coefs: (*Polynomial coefficients*) Returns a real or complex array.

Example

MODES (Press )	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
--	---	---

What are the coefficients of the polynomial that has the roots 4, 5, and 6? (What equation results when (x-4), (x-5), and (x-6) are multiplied?)

1. Enter [4 5 6] for **Roots**.
2. Press **SOLVE** to calculate **Coefs**. The result is [1 -15 74 -120], which means the polynomial is $x^3 - 15x^2 + 74x - 120$.

POLYNOMIAL COEFFICIENTS
ROOTS: [4 5 6]
COEFS: [1 -15 74 -120]
RESULT: COEFFICIENTS [AN ... A0]
*STK VIEW OPTS SOLVE

NOTE



Round-off error limits the accuracy of coefficients returned by the polynomial coefficients function, so the coefficients are automatically rounded to 8 digit accuracy.

Polynomial Equation

Analysis
Algebraic Functions
Polynomial Equation
Equations
Reference

This section takes the coefficients (real or complex) of a polynomial and returns the polynomial as an algebraic expression. The coefficients must be entered in descending order, as in: [AN ... A2 A1 A0], which represents the equation $A_n \cdot x^n + \dots + A_2 \cdot x^2 + A_1 \cdot x + A_0$.

Field Descriptions

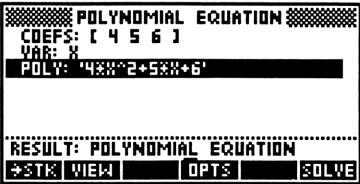
- Coefs:** (*Polynomial coefficients*) Enter an array or list of real or complex numbers.
- Var:** (*Variable*) Enter global name.
- Poly:** (*Polynomial equation*) Returns an algebraic expression.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

The coefficients (in descending order) of an equation are 4, 5, and 6.

1. Enter [4 5 6] for **Coefs**.
2. Press **SOLVE** to calculate **Poly**.



Polynomial Roots

This section takes the coefficients (real or complex) of a polynomial and returns the roots of that polynomial.

Analysis
Algebraic Functions
<i>Polynomial Roots</i>
Equations
Reference

Field Descriptions

- Coefs:** (*Polynomial coefficients*) Enter an array or list of real or complex numbers.
- Roots:** (*Polynomial roots*) Returns a real or complex array.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

What are the roots of the polynomial

$$x^2 - 9 = 0?$$

1. Enter [1 0 -9] for **Coefs**.
2. Press **SOLVE**, to calculate **Roots**.

The result is [-3 3], which means the polynomial has the two roots 3 and -3.



NOTE



Round-off error limits the accuracy of roots returned by the polynomial roots function, so the roots are automatically rounded to 8 digit accuracy. To improve the accuracy of a particular root, use the built-in HP 48 solver to solve the original polynomial equation for 'X', using the value of the desired root returned by the polynomial roots function as a guess.

The polynomial roots function is based on a routine developed by Wayne Scott, using the Bairstow algorithm for finding quadratic factors.

Symbolic Simplification

This section returns the simplified form of an expression.

Analysis
Algebraic Functions
Symbolic Simplification
Equations
Reference

Field Descriptions

Expr: (*Expression*) Enter a real number, complex number, global name or algebraic.

Simpl: (*Simplified expression*) Returns a real number, complex number, global name, or algebraic.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Simplify the expression $(x+1)^2 + (x-5)^3$.

1. Enter (X+1)^2+(X-5)^3 for **Expr**.
2. Press **SOLVE**, to calculate **Simpl**.

The result is $x^3 - 14x^2 + 77x - 124$.



Taylor Polynomial

Analysis
Algebraic Functions
<i>Taylor Polynomial</i>
Equations
Reference

This section computes the Taylor Polynomial of a function to the specified order about a given point.

Field Descriptions

- Expr:** (*Expression*) Enter a global name or algebraic.
Var: (*Variable*) Enter a global name.
Order: (*Order of Taylor polynomial*) Enter a real number.
Point: (*Expansion point*) Enter a real or complex number, or global name.
Taylor: (*Taylor polynomial*) Returns an algebraic expression.

Example

MODES	∠: Radians	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

What is the 2nd-order Taylor polynomial of 'SIN(X)' about the point X=2?

1. Enter SIN(X) for **Expr** and X for **Var**.
2. Enter 2 for **Order** and 2 for **Point**.
3. Press **SOLVE** to calculate **Taylor**.

TAYLOR POLYNOMIAL
EXPR: 'SIN(X)'
VAR: X
ORDER: 2
POINT: 2
TAYLOR: '.909297426826-.4161466..
RESULT: TAYLOR POLY. ABOUT POINT
STK VIEW OPTS SOLVE

Chapter 14

Error Functions

Analysis
<i>Error Functions</i>
Equations
Reference

This chapter covers the error function and the complementary error function:

❑ Error Functions

Using Error Functions

This section computes the numerical values for the error function and complementary error function of one real argument. The definitions of the error function and complementary error function are:

$$erf(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-t^2} dt \qquad erfc(x) \equiv 1 - erf(x) = \frac{2}{\sqrt{\pi}} \int_x^\infty e^{-t^2} dt$$

Field Descriptions

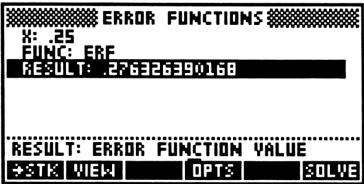
- X:** (*Value*) Enter a real number, global name, or algebraic.
Func: (*Error function type*) Press **CHOOS** to select ERF or ERFC.
Result: (*Error function value*) Returns a real number or algebraic.

Example

MODES	∠: Degrees	Result: Symbolic
(Press CST)	Coord: Rectangular	Units: On or Off
	Format: Standard	Help: On
	Digits: N/A	Font: Small

What is the value of ERF(.25)?

1. Enter .25 for **X**.
2. Choose ERF in **Func**.
3. Press **SOLVE** to calculate **Result**.



Chapter 15

Capital Budgeting

Analysis <i>Capital Budgeting</i> Equations Reference
--

This chapter covers the four basic measures of capital budgeting:

- ☐ Payback Period
- ☐ Net Present Value
- ☐ Internal Rate of Return
- ☐ Profitability Index

Using Capital Budgeting

This section allow you to analyze the capital expenditure of a project and compare projects against one another. Four measures of capital budgeting are included in this section: Payback period (Payback), Net Present Value (NPV), Internal Rate of Return (IRR), and Profitability Index (PI). This module provides the capability of entering, storing and editing capital expenditures for nine different projects. The following definitions are important:

CF_t: Cash Flow at time t.

Payback: The number of time periods (usually years) it takes a firm to recover its original investment.

NPV: The present values of all future cash flows, discounted at the selected rate, minus the cost of the investment.

$$NPV = \sum_{t=1}^n \frac{CF_t}{(1+k)^t} - CF_{t=0}$$

IRR: The discount rate that equates the present value of expected cash flows to the initial cost of the project.

$$\sum_{t=1}^n \frac{CF_t}{(1+IRR)^t} - CF_{t=0} = 0$$

PI: The present value of the future cash flows, discounted at the selected rate, over the initial cash outlay.

$$PI = \frac{\sum_{t=1}^n \frac{CF_t}{(1+k)^t}}{CF_{t=0}}$$

Field Descriptions - Input Screen

Project: (*Project*) Press **CHOOS** to select one of nine unique projects or edit the current project by pressing **CASH**.

k: (*Discount Rate per Period in %*) Enter a real number.

Payback: (*Payback Period*) Returns a real number.

NPV: (*Net Present Value*) Returns a real number.

IRR: (*Internal Rate of Return*) Returns a real number (%).

PI: (*Profitability Index*) Returns a real number.

Field Descriptions - Project Edit Screen

Name: (*Project Name*) Enter name of the project.

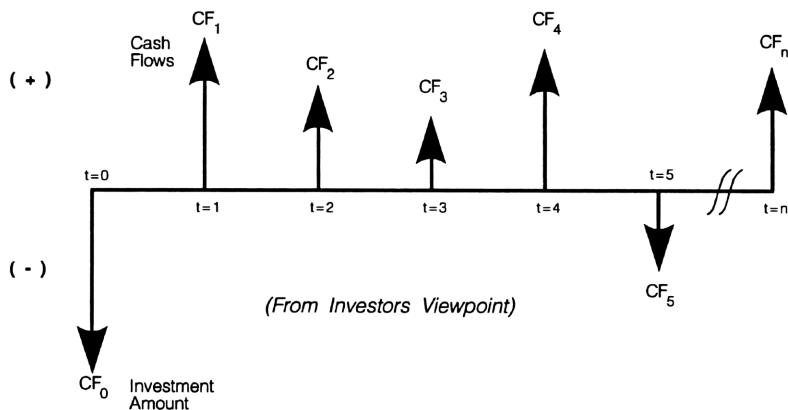
t0: (*Investment at t=0*) Enter a real number. Must be a negative number.

t1: (*Cash flow at t=1*) Enter a real number. Can be positive or negative.

....

tn: (*Cash flow at t=n*) Enter a real number. Can be positive or negative.

Cash Flow Diagram



Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

The following projects have been proposed by your company. What is the payback period, Net Present Value, Internal Rate of Return, and Profitability Index of each project? Which is the more viable project?

Name of Project:	Plant 1		Plant 2	
Investment Outlay:	\$75,000 (at t=0)		\$75,000 (at t=0)	
Cost of Capital:	12%		12%	
	Year	Net Cash Flow (\$)	Year	Net Cash Flow (\$)
	0	-75,000	0	-75,000
	1	40,000	1	10,000
	2	30,000	2	20,000
	3	20,000	3	30,000
	4	10,000	4	40,000

1. With the highlight bar on the **Project** field, press **CHOOS** to select a project to edit. Select a project that has not been used (this example uses projects 1 and 2). Press **OK** to return to the Capital Budgeting screen.
2. Press **CASH** to enter the Project Edit screen and edit the cash flows.
3. Enter Plant 1 for **Name**.
4. Press **ADD** 5 times to add 5 time points and enter the cash flows at each time point from the table above. When finished, your screen should look like the Project Edit screen to the right. Be sure to enter 75,000 as a negative number. Press **OK** to save your changes and return to the Capital Budgeting screen.
5. Enter 12 for **K**.
6. Press **SOLVE** to calculate **Payback**, **NPV**, **IRR**, and **PI**.

CAPITAL BUDGETING	
PROJECT: PROJECT 1	
K: 0	
PAYBACK:	
NPV:	
IRR:	
PI:	
.....	
CHOOSE OR EDIT PROJECT	
CHOOSE	CASH OPTS PLOT SOLVE

Input Screen

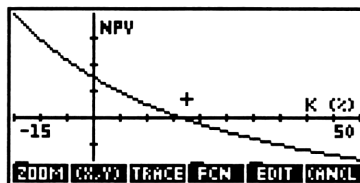
EDIT PROJECT 1	
NAME: PLANT 1	
T0: -75000	
T1: 40000	
T2: 30000	
T3: 20000	
T4: 10000	
.....	
ENTER PROJECT NAME	
EDIT	ADD STACK CANCEL OK

Project Edit Screen

CAPITAL BUDGETING	
PROJECT: PLANT 1	
K: 12	
PAYBACK: 2.25	
NPV: 5220.88778115	
IRR: 16.0946133455	
PI: 1.06961183708	
.....	
RESULT: PAYBACK PERIOD	
→	STK VIEW CASH OPTS PLOT SOLVE

Output Screen

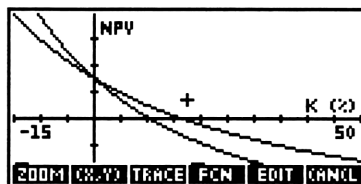
7. Press **PLOT** to show the curvilinear relationship between the Net Present Value and the Discount Rate. You will see a message screen asking if you wish to clear the previous plot. Press **YES**.



Plot Screen

The curve indicates that where $K=0$, the Net Present Value is simply cash inflows minus cash outflows. The IRR % is shown at the point where $NPV=0$. Using the built-in graphing capabilities of the HP 48, you can trace the graph to find the values for these two points. The HP 48GX will give you the exact coordinates of any point, the HP 48SX will only give you a close approximation. Press **CANCEL** to return to the Capital Budgeting screen.

8. Repeat steps 1 through 7 for the second project. Name the project Plant 2 and input the values in the table on page 92. When you plot the second project, press **NO** when you are prompted to clear the previous plot. This will overlay the second project on the first for a quick comparison of the two projects. The most viable project in terms of discounted cash flows, in this example, is the one with the highest curve: Plant 1.



Plot Screen II

Bibliography

Campsey, B.J., and Eugene F. Brigham, *Introduction to Financial Management*, Dryden Press, 1985, pp. 392-400.

Van Horne, James C., *Financial Management and Policy*, Eighth Edition, Prentice Hall, 1989, pp. 126-132.

Equations

Chapter 16

Equations: Navigation Guide

Analysis <i>Equations</i> Reference

This chapter is designed as a navigation guide to introduce you to the Equations section, show you the keys available at each screen, and describe the types of input fields and symbols you will encounter. At the end of the chapter is a detailed Equations example.

Introduction.....	98
Finding Equations.....	98
Equations Screens.....	99
Viewing Equations.....	99
Displaying a Picture.....	99
Selecting Equations.....	100
Equations Menu Keys.....	100
Solver Screens.....	100
Solving an Equation.....	101
Using the Stack.....	102
Resetting Variables.....	102
Converting a Value.....	102
Units On/Units Off.....	102
Font Size.....	103
Solver Icons.....	103
Solver Menu Keys.....	105
Plotter Screens.....	106
Plotting an Equation.....	106
Plotter Field Descriptions.....	108
Plotter Menu Keys.....	109
Example: Overdamped Parallel RLC Circuit.....	110
Solve the Equation.....	110
Plot the Equation.....	111











Introduction





EE•Pro is divided into three major sections: Analysis, Equations, and Reference. This chapter addresses the Equations section, which includes equations covering resistive circuits, capacitance and electric fields, inductance and magnetism, electron motion, RLC circuits, AC circuits, motors and generators, OpAmp circuits, transformers, linear circuits, and solid state devices.



The Equations section enables you to select a specific equation or a set of equations, solve for specific variables, and plot the equations with the EE•Pro plotting functions. The three equation-related features of selecting, solving, and plotting, each have their own screen. The Equations screen displays a group of related equations, which can be selected for solving or plotting. The Solver screen allows you to enter and convert values, then solve for unknowns. The Plotter screen allows you to plot the selected equation. A diagram is often available to illustrate the variable relationships in the selected equation set and can be accessed from any of these three screens. In some cases, extra diagrams in the manual help illustrate the nature of the problems being solved.

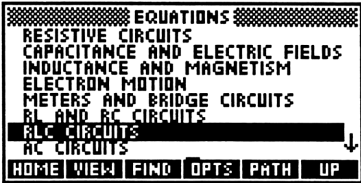
Finding Equations

The Equations section is found at the home screen of EE•Pro.

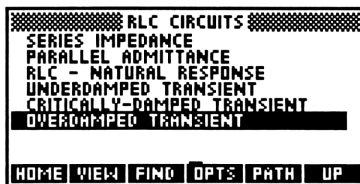
1. Start EE•Pro:
 - HP 48GX: Press    .
 - HP 48SX: Press    .
 - Press   to show the home screen.

EE•Pro is structured with a hierarchy of screens for choosing a specific topic or item. This is the home screen. To return here at any time, press   or  .

2. Select Equations by moving the highlight bar to Equations and pressing  or . The screen now displays Equations as its title and a list of Equations sections from which to choose.



- Choose an Equations section by moving the highlight bar to the desired item and pressing **ENTER** or **▶**. This will display a list of topics for the selected section. For the purposes of this navigation guide, select RLC Circuits then Overdamped Transient.



Pressing **UP** (if available) or **◀** returns you to the previous screen.

Pressing **HOME** (if available) or **▶ HOME** returns you to the home screen.

Equations Screens

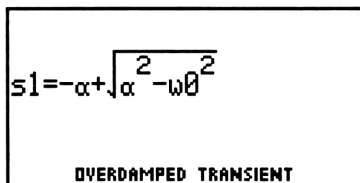
An Equations screen displays a list of related equations which can be displayed in a graphics view or selected for solving. The screen to the right is the Overdamped Transients screen.



The Equations screen is accessible from the Plotter screen or the Solver screen by pressing **EQNS**.

Viewing Equations

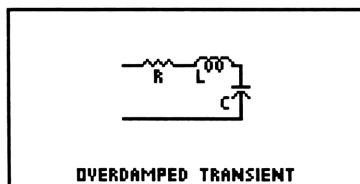
To display an equation in a graphics view using the HP 48 EquationWriter, move the highlight bar to the desired equation and press **EQWR**. Press any key to return to the Equations screen.



Displaying a Picture

To display a diagram for the current equation set, press **PICT**. If available, this menu key will also appear in the Plotter screen and the Solver screen.

(Note: Variable names in pictures are always uppercase, regardless of which case they appear when encountered in the equations themselves.) Press any key to return to the previous screen.



Selecting Equations

When solving a problem, one or more of the equations from the Equations screen can be selected for use at the Solver screen. Generally, you will want to solve all of the equations together, but sometimes it may be the case that you can quickly select a single equation or a subset of the entire equation set to speed up the solving computations. (Solving one or two equations is usually faster than solving many equations.)

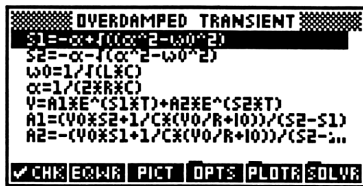
To select an equation, move the highlight bar to the desired equation and press **✓CHK** or **✓/-**. Once selected, an equation can be unselected in the same fashion.



Equations Menu Keys

These are descriptions of the menu keys available at Equations screens:

✓CHK Checks or unchecks the highlighted equation. Only checked equations will be solved, but if none of the equations are checked, all of them will be solved.



EQWR Displays the highlighted equation in a graphics view.

PICT Displays a picture for the equation set.

OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

PLOTR Goes to the Plotter screen. For more information, see “Plotter Screens,” page 106.

SOLVR Goes to the Solver screen. Solves only the checked equations (unless none are checked, in which case all are solved). For more information, see “Solver Screens” below.

Solver Screens

A Solver screen allows you to enter values for each variable in the selected equation(s). Variables can also be edited, copied to the stack, or converted to different units. After all the known variables have been entered, you can press **SOLVE** to compute the values of the unknown variables.

NOTE

The Solver cannot handle complex numbers. To solve a problem which requires complex inputs, use the appropriate Analysis routine.

The Solver screen is accessible from the Equations screen or the Plotter screen by pressing **SOLVR**.

Solving an Equation

Below are general instructions for using Solver screens. For a detailed example using Overdamped Transient, see page 110.

1. *Optional:* Select equation(s) to solve. (If no equations are selected, the Solver will solve all the equations in the set.)
 - a. Go to the Equations screen by pressing **NXT** **EQNS**.
 - b. Move the highlight bar to the desired equation(s) and press **✓CHK**.
(Note: The following screens assume that none of the equations have been selected, and therefore all will be solved.)
2. Go to the Solver screen by pressing **SOLVR** from the Equations screen or the Plotter screen. The screen to the right is the Solver screen for Overdamped Transient.
3. Enter the known values.
 - a. Move the highlight bar to the desired variable.
 - b. Type in the appropriate value for the variable and press **ENTER** or a unit menu key to complete the entry.



If you make a mistake or want to change the value of a variable:

- a. Move the highlight bar to the variable and press **EDIT** to place it on the command line.
- b. Edit the value.
- c. After you have finished editing the value, press **ENTER** to change the value or **ON** to abort the change.

Alternatively, to *replace* the existing value of a variable:

- a. Move the highlight bar to the variable.
- b. Type in the new value.
- c. Press **ENTER** or a unit menu key to complete the entry.




Any time you edit or change a value, that variable will be marked as “known” with a solid circle (●). See “Solver Icons,” page 103.

4. Press **SOLVE** to solve for the remaining variables. Shaded circles (●) will appear next to variables for which exact solutions have been found. See “Solver Icons,” page 103.
5. *Optional:* Press  to return to the RLC Circuits screen or press  **HOME** to return to the home screen.

Using the HP 48 Stack



There are two stack-related commands:

→STK Copies one or all of the variables currently on the screen to the HP 48 stack for later use, without leaving the Solver screen.


1. To access this command, press **OPTS**  or  **CST** then **→STK**.
2. You will be asked if you want to copy one or all items to the stack.
3. Choose **ONE** or **ALL**, or press  to abort the copy.

STACK Copies the value of the highlighted variable to the HP 48 stack for immediate use and temporarily goes to the HP 48 stack environment. For more information, see “Solver Menu Keys,” page 105.


Resetting Variables

To reset the values of variables, press  or  **RESET** and select **ONE** or **ALL**. This will clear the values of the selected variables at the Solver screen and will also purge the selected variables from user memory, where they are created by the solver each time you enter a value or press **SOLVE**.

Converting a Value

Once a variable value has been entered, it can easily be converted to different units. To do this, highlight the desired variable and press **CONV**. The available units for the highlighted variable will be displayed as menu keys (press  for more menu keys, if appropriate). When you have finished converting a value, either move the highlight bar to another variable value to convert it, or press **EXIT** to leave the convert menu and return to the standard menu.

Units On/Units Off

You can choose to display variable values with units (units on) or without units (units off). With units on, variable values will be displayed in the units you specify when you enter the value or when you convert the value to a different unit. If you simply enter a number and press , the

default unit will be the SI unit for the variable. The default SI unit is typically displayed as the first menu key when entering a value.

With units off, variable values will be displayed as SI values without units. The units you specified will be remembered if you later turn units on again, but all values will temporarily be converted and displayed in the default SI units. SI units are used to ensure that the values sent to the solver are consistent with each other.

To access the units setting:

1. Press **OPTS** or **← CST** and then **UNITS** to turn units on or off. When the block inside the key appears (**UNIT**), units are turned on. Press **EXIT** to leave the Options menu and return to the standard Solver menu keys.

OR

2. Press **← UNITS** or **→ UNITS** to turn units on or off. When units appear next to the values, units are turned on.

Font Size

The small font shows variables only in uppercase, which makes it difficult to distinguish between an **a** and an **A**. However, it does allow more data to be displayed on the screen, making it easier to see your results.

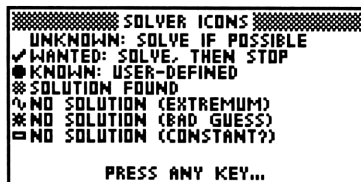


To change the font size:

1. Press **OPTS** **FONT** to switch to the larger font, which is case-sensitive. Also, pressing **HELP** to turn help text off provides more room on the screen so that more of the variables can be displayed at once.
2. Press **EXIT** to leave the options menu and return to the standard menu.

Solver Icons

There are several different symbols or icons used to identify different kinds of variables. To see a list of these icons, press **NXT** **ICONS** to display the Solver Icons screen. See Chapter 33, “Advanced Use of the Solver.”




✓ Wanted Variables

A check mark (✓) indicates that a variable is wanted. It is not necessary to mark the desired variable(s) as wanted in order to calculate their values,

because the solver will calculate the values of *all* unknown variables (those with no icons) if none are marked as wanted. The reason you may want to mark one or more variables as wanted is if you want the solver to *stop* after it has found the values of those wanted variables and not continue to calculate the values of all remaining unknown variables. If you are solving multiple equations with many variables and you only want the value of a specific variable, it is a good idea to mark that variable as wanted by selecting it with the highlight bar and pressing **WANT**. To remove a wanted icon from a variable, move the highlight bar to the variable and press **WANT** again.

The solver may still calculate the values of other unknown variables in addition to those specifically marked as wanted, most likely because it is impossible to calculate the value of the wanted variable(s) without first calculating the values of other variables.

● Known Variables

A solid circle (●) indicates that a variable is known. The values of known variables are never changed by the solver, because those variables are considered user-defined. Every time you enter a value for a variable, the variable is automatically marked as known. To remove the known icon from a variable, move the highlight bar to the variable and press **KNOW** or , and the solid circle will disappear, which means the variable is unknown.

NOTE



Every time you want to solve equations, you must pick some variables to be known and enter values for them, so the solver can use the known variables to calculate values for any unknown variables.

● Solution Found

A shaded circle (●) indicates that an exact solution was found for a variable by the Solver.

No Solution Found

When the solver cannot find a solution, one of three messages will be displayed:

~ No Solution (Extremum)

This message is displayed when the solver finds a point where the value of the equation approximates a local minimum or maximum, or when the solver had to stop searching because it encountered the largest (MAXR) or smallest (–MAXR) possible number.

✱ No Solution (Bad Guess)

This message is displayed when one or more of the initial guesses are outside the domain of the equation, or when complex numbers are encountered by the Solver.

☐ No Solution (Constant).

This message is displayed when the equation has the same value at every point sampled.

For more information, see Chapter 33, “Advanced Use of the Solver.”

Solver Menu Keys

These are descriptions of the menu keys available at Solver screens:

EDIT Edits the highlighted variable.

Press **ENTER** to save edit changes
or **ON** to cancel editing.

STACK Copies the highlighted variable to the HP 48 stack and temporarily goes to the HP 48 stack environment. While at the stack, you can use all the normal built-in functions of your HP 48 to manipulate or change the copied value. When you have finished editing the value, press **OK** to leave the stack and insert the edited value into the current variable, or press **CANCEL** to leave the stack without changing the value of the current variable.

PICT Displays a picture, if available.

OPTS Displays the options menu. For more information, see “Options Menu,” page 9.

CONV Displays the convert menu for the highlighted variable. For more information, see “Converting a Value,” page 102.

SOLVE Solves the equation(s) using the known values. For more information, see “Solving an Equation,” page 101.

Press **NXT** for the following menu keys:

KNOW Marks or unmarks the highlighted variable as known. See “Known Variables,” page 104.

WANT Marks or unmarks the highlighted variable as wanted. See “Wanted Variables,” page 103.

RESET Resets one or all of the variables. See “Resetting Variables,” page 102.



ICONS Displays the Solver Icons screen. See Chapter 33, “Advanced Use of the Solver.”

PLOTR Goes to the Plotter screen. See “Plotter Screens,” page 106.

EQNS Goes to the Equations screen. See “Equations Screens,” page 99.

Plotter Screens

A Plotter screen enables you to plot any of the equations from the Equations screen. A variety of plot parameters can be specified. The HP 48 graphics environment is used to display the plots.

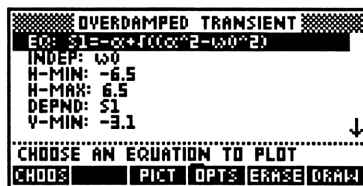
Below are general instructions for using Plotter screens. For a detailed example using Overdamped Transient, see page 110.

Plotting an Equation

1. Go to the Plotter screen by pressing **PLOTR** from the Equations screen or Solver screen.

2. Select an equation to plot.

- a. Move the highlight bar to the **EQ** field, which displays the equation to be plotted.
- b. To choose another equation, press **CHOOS** and select the desired equation from the list that appears.

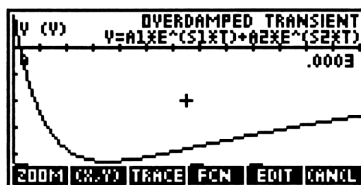


Selecting an equation automatically sets default values for the independent and dependent variables and units.

3. Set the values of any extra variables. (Only the independent and dependent variables will vary as the equation is plotted, so all other variables must have constant values.)
 - a. Press **NXT SOLVR** to go to the Solver screen.
 - b. Move the highlight bar to each of the remaining variables in turn and type in values for them.
 - c. Press **NXT PLOTR** to return to the Plotter screen.
4. Selecting the independent variable.
 - a. Move the highlight bar to the **INDEP** field.
 - b. Press **CHOOS** or **1/□** to select the independent variable.
 - c. If units are turned on, choose the desired units for the independent variable in the **H-UNITS** field by moving the highlight bar to that field

and pressing **CHOOS**. Once you have selected the desired units, press **OK** to return to the Plotter screen.

5. Set the horizontal range.
 - a. Move the highlight bar to the **H-MIN** and **H-MAX** fields and enter values for the range of the horizontal axis in the plot.
6. Select the dependent variable.
 - a. Move the highlight bar to the **DEPND** field.
 - b. Press **CHOOS** or **$\frac{+}{-}$** to select the dependent variable.
 - c. If units are turned on, choose the desired units for the dependent variable in the **V-UNITS** field by scrolling down to that field and pressing **CHOOS**. Once you have selected the desired units, press **OK** to return to the Plotter screen.
7. Set the vertical range *OR* autoscale.
 - To set the vertical range: Move the highlight bar to the **V-MIN** and **V-MAX** fields and enter values for the range of the vertical axis in the plot.
 - To autoscale the plot: Move the highlight bar to the **Autoscale** field and press **✓CHK**.
8. Draw the plot.
 - a. *Optional:* Press **ERASE** to erase any previous plots. As with the built-in plotting routines of the HP 48, you can overlay multiple plots by pressing **DRAW** more than once with different parameters without pressing **ERASE** between plots.
 - b. Press **DRAW** to plot the equation. (The plot shown above is from the example on page 110.)
 - c. Press **ON** to return to the Plotter screen.
9. *Optional:* Press **◀** to return to the RLC Circuits screen or press **➡ HOME** to return to the home screen.



Plotter Field Descriptions

These are descriptions of each of the fields which appear in a Plotter screen.

EQ: (*Equation to plot*) Press **CHOOS** to select an equation the current Equations screen.

INDEP: (*Independent variable*) This variable varies across the horizontal axis of the plot.

Changing the independent variable automatically resets the independent variable units to the default SI unit. Press **CHOOS** to select from the variables in current equation.

H-UNITS: (*Horizontal axis units*) This field contains the independent variable units. To select the units for the horizontal axis, press **CHOOS**. This field is only present if units are on. To turn units on or off, press **UNITS**.

H-MIN: (*Horizontal axis minimum*) This is the minimum value of the independent variable, which is plotted along the horizontal axis.

H-MAX: (*Horizontal axis maximum*) This is the maximum value of the independent variable.

DEPND: (*Dependent variable*) This variable varies along the vertical axis of the plot. Changing the dependent variable automatically resets the dependent variable units to the default SI unit. Press **CHOOS** to select from the variables in current equation. (The dependent variable should be different from the independent variable.)

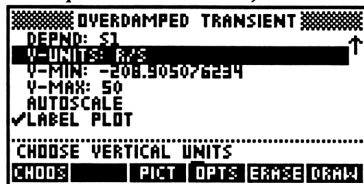
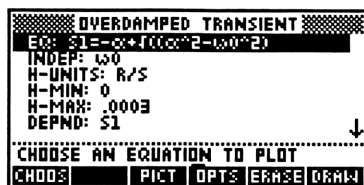
V-UNITS: (*Vertical axis units*) This field contains the dependent variable units. To select the units for the vertical axis, press **CHOOS**. This field is only present if units are on. To turn units on or off, press **UNITS**.

V-MIN: (*Vertical axis minimum*) This is the minimum value of the dependent variable, which is plotted along the vertical axis. This field is disregarded if autoscale is on.

V-MAX: (*Vertical axis maximum*) This is the maximum value of the dependent variable. This field is disregarded if autoscale is on.

Autoscale: (*Autoscale vertical axis*) Press **✓CHK** to autoscale the plot. If autoscale is checked (✓), the values for **V-MIN** and **V-MAX** are disregarded.

Label Plot: (*Label plot*) Press **✓CHK** to control whether plot is labeled (checked) or not labeled (unchecked).



Plotter Menu Keys

The menu keys in Plotter screens change depending on the type of field that is highlighted. Plotter screens use three basic types of fields: **Edit** fields, **Choose** fields and **Check** fields. These fields and their associated menu keys are outlined below. The **LOPTS**, **ERASE** and **DRAW** menu keys are always present regardless of the field type.

Choose Fields: These fields only accept values from a pre-defined list that is accessed by pressing **CHOOS**. **EQ**, **INDEP**, **H-UNITS**, **DEPND**, and **V-UNITS** are **Choose** fields.

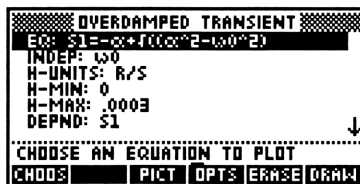
CHOOS Displays the possible choices for a choose field. Highlight the desired value and press **ENTER** or **OK**, or press **CANCL** to abort the selection.

PICT Displays a picture.

LOPTS Displays the options menu. For more information, see “Options Menu,” page 9.

ERASE Erases any previous plots.

DRAW Plots the current equation. As with the built-in plotting routines of the HP 48, you can overlay multiple plots by pressing **DRAW** more than once with different parameters without pressing **ERASE** between plots.



Edit Fields: These fields accept values entered from the keyboard. **H-MIN**, **H-MAX**, **V-MIN** and **V-MAX** are **Edit** fields.

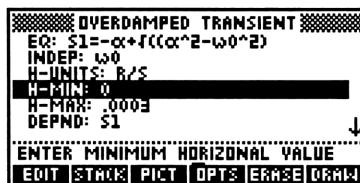
EDIT Edits the highlighted item. The menu keys then change to the standard HP 48 editing keys. Press **ENTER** to save edit changes or **ON** to cancel editing.

STACK Copies the highlighted item to the HP 48 stack and temporarily goes to the HP 48 stack environment. While at the stack, you can use all the normal built-in functions of your HP 48 to manipulate or change the copied item. When you have finished editing the item, press **OK** to leave the stack and insert the edited item into the current **Edit** field, or press **CANCL** to leave the stack without changing the value of the current **Edit** field.

PICT Displays a picture (if available).

LOPTS Displays the options menu. For more information, see “Options Menu,” page 9.

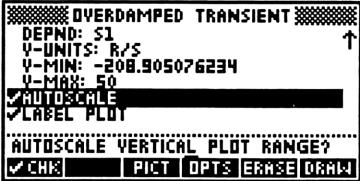
ERASE Erases any previous plots.



DRAW Plots the current equation.

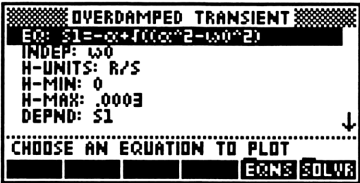
Check Fields: These fields are toggle fields. A ✓ in front of the field turns that specific control on. **Autoscale** and **Label Plot** are **Check** fields.

- ✓CHK** Toggles a check mark.
- PICT** Displays a picture (if available).
- OPTS** Displays the options menu.
- ERASE** Erases any previous plots.
- DRAW** Plots the current equation.



In all fields, press **NXT** for these two menu keys:

- EONS** Goes to the Equations screen. See “Equations Screens.”
- SOLVR** Goes to the Solver screen. See “Solver Screens,” page 100.



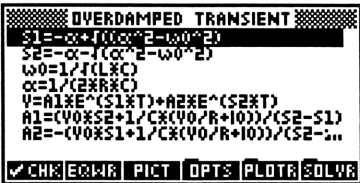
Example: Overdamped Parallel RLC Circuit

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

An overdamped parallel RLC circuit is characterized by a 100 ohm resistor, a 40 mH inductor and a 0.25 μ F capacitor. The initial inductor current is 2 A, and the capacitor has an initial charge of 50 V. Find the voltage transient response across the parallel circuit. Plot the voltage across the capacitor during the first 300 μ s.

Solve Multiple Equations

- Enter the Overdamped Transient screen:
 - Press **→** **HOME** to go to the home screen.
 - Choose Equations.
 - Choose RLC Circuits.
 - Choose Overdamped Transient.
- At the Equations screen, make sure no equations are checked and press



Equations Screen

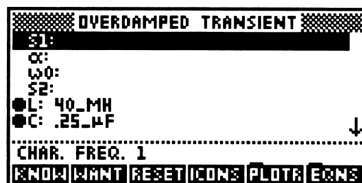
SOLVR to go to the Solver screen.

- Reset all the variable values by pressing **DEL**, then **ALL**.
- Enter the following values in the appropriate fields. Select the units by pressing the indicated menu key:

L: 40 (**MH**)
C: 0.25 (**MF**)
R: 100 (**Ω**)
V0: 50 (**V**)
I0: 2 (**A**)

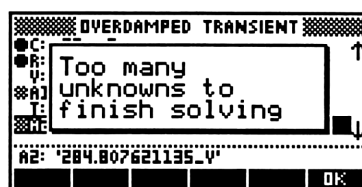
A solid circle will appear beside the entered variables, marking them as

known. If necessary, press **UNIT** to turn units on.



Solver Screen

- Press **SOLVE**. The solver will solve for the unknown variables, one by one. With the information entered, it will not be able to find values for v or t, so you will get the message shown to the right. Press **OK** to continue.



Solver Message

The found variables are those for which values were calculated and are marked by shaded circles. You have just computed the values of the variables **A1**, **s1**, **A2**, and **s2** in the equation $v = A1 \cdot e^{s1 \cdot t} + A2 \cdot e^{s2 \cdot t}$ which determines the capacitor voltage as a function of time.

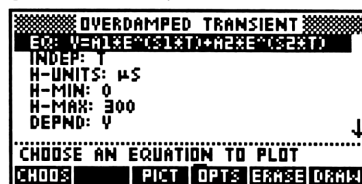


Solver: Answers

Plot one Equation

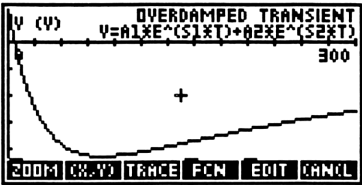
To plot the voltage across the capacitor during the first 300 μ s:

- Press **NXT** **PLOTR** to go to the Plotter screen.
- In the **EQ** field, press **ENTER** and choose the equation pictured to the right.
- Choose **t** for **INDEP**.
- Choose μ s for **H-UNITS**.
- Enter 0 for **H-MIN** and .0003 for **H-MAX**.
- Choose **v** for **DEPND**.



Plotter Entry Screen

7. Scroll down to the **Autoscale** field and press **✓CHK** to turn autoscale on.
8. Scroll down to the **Label Plot** field and press **✓CHK** to turn label the plot.
9. Press **ERASE** to erase any previous plots.
10. Press **DRAW** to draw the plot.
11. *Optional:* Press **◀** to return to the RLC Circuits screen or press **▶ HOME** to return to the home screen.



Plot of Capacitor Voltage

Chapter 17

Resistive Circuits

Analysis
Equations
<i>Resistive Circuits</i>
Reference

This chapter covers the equations relevant for dealing with simple resistive circuits.

- ☐ Resistance and Conductance
- ☐ Ohm’s Law and Power
- ☐ Temperature Effects
- ☐ Maximum Power Theorem
- ☐ V and I Source Equivalence

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

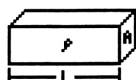
Variable	Description	Unit
α	Temperature coefficient	1/K
A	Area	m ²
G	Conductance	S
I	Current	A
I _L	Load current	A
I _S	Current source	A
l _{en}	Length	m
P	Power	W
P _{max}	Maximum power in load	W
ρ	Resistivity	$\Omega \cdot m$
R	Resistance	Ω
R ₁	Resistance, T1	Ω
R ₂	Resistance, T2	Ω
R _L	Load resistance	Ω
R _{lm}	Match load resistance	Ω
R _s	Source resistance	Ω
σ	Conductivity	S/m
T ₁	Temperature 1	K

T2	Temperature 2	K
V	Voltage	V
Vl	Load voltage	V
Vs	Source voltage	V

Resistance and Conductance

Analysis
Equations
Resistive Circuits
Resistance & Conductance
Reference

The four equations in this section represent the basic relationships between resistance and conductance. The first equation describes the resistance R of a bar with a length len and a uniform cross-sectional area A with a resistivity ρ . The second equation defines the conductance G of the same bar in terms of conductivity σ and len and A . The third equation shows the reciprocity



between conductance G and resistance R , while the fourth equation shows the corresponding reciprocity between resistivity ρ and conductivity σ .

$$R = \frac{\rho \cdot len}{A}$$

$$G = \frac{\sigma \cdot A}{len}$$

$$G = \frac{1}{R}$$

$$\sigma = \frac{1}{\rho}$$

Ohm's Law and Power

Analysis
Equations
Resistive Circuits
Ohm's Law and Power
Reference

These equations represent the fundamental relationships between voltage, current and power. The first equation expresses the relationship between current I and voltage V in terms of the resistance R , the classic Ohm's law. The next four equations connect power dissipation P , voltage V , current I , resistance R and conductance G . The final equation represents the reciprocity between resistance R and conductance G .

$$V = I \cdot R$$

$$P = V \cdot I$$

$$P = I^2 \cdot R$$

$$P = \frac{V^2}{R}$$

$$P = V^2 \cdot G$$

$$R = \frac{1}{G}$$

Temperature Effect

Analysis
Equations
Resistive Circuits
Temperature Effect
Reference

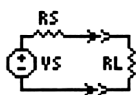
This equation shows the effect of temperature on resistance. Resistance changes from **R1** to **R2** when the temperature **T1** to a temperature **T2** is modulated by the temperature coefficient resistance **α** .

$$R_2 = R_1 \cdot (1 + \alpha \cdot (T_2 - T_1))$$

Maximum Power Transfer

Analysis
Equations
Resistive Circuits
Maximum Power Transfer
Reference

These five equations are organized to compute load voltage **V_L**, load current **I_L**, power dissipation in the load **P**, maximum power available in the load **P_{max}**, and load impedance **R_{Lm}** needed for maximum power deliverable to the load. The first equation computes the load voltage **V_L** of a circuit with a simple voltage source **V_s**, source resistance **R_s**, and a load resistance **R_L**. The second equation defines the load current **I_L** in terms of **V_s**, **R_s** and **R_L**. The power dissipation in the load resistance is defined by the third equation linking **P** with **I_L** and **V_L**. The fourth equation refers to maximum power available to the load from the voltage source **V_s** with its internal resistance **R_s**. The last equation represents load resistance value needed for a maximum power to be transferred from the source.



$$V_L = \frac{V_s \cdot R_L}{R_s + R_L}$$

$$I_L = \frac{V_s}{R_s + R_L}$$

$$P = I_L \cdot V_L$$

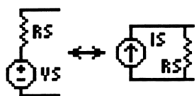
$$P_{\max} = \frac{V_s^2}{4 \cdot R_s}$$

$$R_{Lm} = R_s$$

V and I Source Equivalence

Analysis
Equations
Resistive Circuits
V and I Source Equivalence
Reference

The two equations in this section represent the equivalence between a voltage source and a current source. A voltage source V_s with an internal series resistance of R_s is equivalent in all its functionality to a current source I_s with a resistance R_s connected across it.



$$I_s = \frac{V_s}{R_s}$$

$$V_s = I_s \cdot R_s$$

Bibliography

Edminister, Joseph A., *Electric Circuits, 2nd Edition, Schaum's Outline Series in Engineering*, McGraw-Hill Book Company, New York, N.Y. 1983.

Nilsson, James W., *Electric Circuits, 2nd Edition*, Addison-Wesley Publishing Company, Reading, MA 1987.

Chapter 18

Capacitance and Electric Fields

Analysis
Equations
<i>Capacitance & Electric Fields</i>
Reference

This chapter covers the equations describing a variety of configurations where capacitive properties are calculated.

- ☐ Point Charge
- ☐ Long Charged Line
- ☐ Charged Disk
- ☐ Parallel Plates
- ☐ Parallel Wires
- ☐ Coaxial Cable
- ☐ Sphere

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
a	Radius	m
A	Area	m ²
b	Outer radius	m
C	Capacitance	F
c	Capacitance per unit length	F/m
d	Separation	m
E	Electric field	V/m
ϵ_r	Relative permittivity	unitless
E_r	Radial electric field	V/m
E_z	Electric field along z axis	V/m
F	Force on plate	N
Q	Charge	C
r	Radial distance	m
ρ_l	Line charge	C/m

ρ_s	Charge density	C/m^2
V	Potential	V
V_z	Potential along z axis	V
W	Energy stored	J
z	z axis distance from disk	m

Point Charge

Analysis
Equations
Capacitance & Electric Fields
Point Charge
Reference

The two equations in this module represent the radial electric field E_r and the potential V at a location r away from a point charge Q . It is evident that the electric field is inversely proportional to the square of the distance r , while the potential is inversely proportional to r . The equations have been generalized to include ϵ_r , the relative permittivity of the medium.

$$E_r = \frac{Q}{4 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r \cdot r^2} \quad V = \frac{Q}{4 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r \cdot r}$$

Long Charged Line

Analysis
Equations
Capacitance & Electric Fields
Long Charged Line
Reference

An infinite line charge with a strength of ρ_l Coulombs per unit length exerts a radial electric field a distance r away from the line. The electric field E_r is radial and can be easily seen to decay inversely as r .

$$E_r = \frac{\rho_l}{2 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r \cdot r}$$

Charged Disk

Analysis
Equations
Capacitance & Electric Fields
Charged Disk
Reference

There are two equations listed here describing the electric field and potential along the vertical axis through the center of a uniformly charged disk. The first

equation defines the electric field along the z-axis of the disk with a radius **a** and charge density of **ps**, a distance **z** from the plane of the disk. The second equation yields the electrostatic potential **Vz** at an arbitrary point along the z-axis.

$$E_z = \frac{ps}{2 \cdot \epsilon_0 \cdot \epsilon_r} \cdot \left(1 - \frac{ABS(z)}{\sqrt{a^2 + z^2}} \right) \quad V_z = \frac{ps}{2 \cdot \epsilon_0 \cdot \epsilon_r} \cdot \left(\sqrt{a^2 + z^2} - ABS(z) \right)$$

Parallel Plates

Analysis
Equations
Capacitance & Electric Fields
Parallel Plates
Reference

The five equations listed in this section describe the electrical and mechanical properties of a parallel plate capacitor. It is assumed that plate separation **d** is small compared to the lateral dimensions so that fringing field effects can be ignored. The first equation yields the electric field **E** at the plate for a potential difference **V** between the plates. The second equation computes the capacitance **C** of the system given the relative permittivity **εr** and area **A**. The third equation shows the charge on each parallel plate. The last two equations show the mechanical force **F** on the plates and energy stored **W** in the capacitor.



$$E = \frac{V}{d} \quad C = \frac{\epsilon_0 \cdot \epsilon_r \cdot A}{d} \quad Q = C \cdot V$$

$$F = \frac{\frac{1}{2} \cdot V^2 \cdot C}{d} \quad W = \frac{1}{2} \cdot V^2 \cdot C$$

Parallel Wires

Analysis
Equations
Capacitance & Electric Fields
Parallel Wires
Reference

The equation listed here represents the calculation of capacitance per unit length **c** of a pair of transmission lines of radius **a** and center to center spacing **d** in a dielectric medium with a relative permittivity of **εr**.

$$C = \frac{\pi \cdot \epsilon_0 \cdot \epsilon_r}{\text{ACOSH}\left(\frac{d}{2 \cdot a}\right)}$$

Coaxial Cable

Analysis
Equations
Capacitance & Electric Fields
Coaxial Cable
Reference

These three equations describe properties of a coaxial cable. The first two equations show the voltage between the outer and inner conductors carrying a charge of ρl per unit length, relative permittivity ϵ_r , and conductor diameters a and b . The last equation computes the radial electric field E_r between the conductors while the last equation calculates the capacitance per unit length.



$$V = \frac{\rho l}{2 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r} \cdot \text{LN}\left(\frac{b}{a}\right)$$

$$E_r = \frac{V}{r \cdot \text{LN}\left(\frac{b}{a}\right)}$$

$$C = \frac{2 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r}{\text{LN}\left(\frac{b}{a}\right)}$$

Sphere

Analysis
Equations
Capacitance & Electric Fields
Sphere
Reference

The three equations in this module compute the potential between two concentric spheres of radius a and b , with a charge Q , and separated by a medium with a relative permittivity of ϵ_r . The second equation computes the electric field outside a sphere at a distance r from the center of the sphere. The last equation computes the capacitance between the spheres.

$$V = \frac{Q}{4 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r} \cdot \left(\frac{1}{a} - \frac{1}{b}\right)$$

$$E_r = \frac{Q}{4 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r \cdot r^2}$$

$$C = \frac{4 \cdot \pi \cdot \epsilon_0 \cdot \epsilon_r \cdot a \cdot b}{b - a}$$

Chapter 19

Inductance and Magnetism

Analysis
Equations
<i>Inductance and Magnetism</i>
Reference

This chapter covers the equations describing inductance and magnetic properties of typical electrical configurations.

- ☐ Long Line
- ☐ Long Strip
- ☐ Parallel Wires
- ☐ Loop
- ☐ Coaxial Cable
- ☐ Skin Effect

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
a	Loop radius or side	m
b	Side b of loop	m
B	Magnetic field	T
B _x	Magnetic field, x axis	T
B _y	Magnetic field, y axis	T
δ	Skin depth	m
d	Strip width	m
D	Center-center wire spacing	m
f	Frequency	Hz
F	Force between wires	N/m
I	Current	A
I ₁	Current in line 1	A
I ₂	Current in line 2	A
I _s	Current in strip	A/m
L	Inductance per unit length	H/m
L ₁₂	Mutual inductance	H
L _s	Loop self-inductance	H
μ _r	Relative permeability	unitless

r	Radial distance	m
r0	Loop wire radius	m
ρ	Resistivity	$\Omega \cdot m$
η	Angle	r
R _{eff}	Effective resistance	Ω
T12	Torque	N*m
x	x axis distance	m
y	y axis distance	m
z	Distance to loop z axis	m

Long Line

The magnetic field **B** due to a current **I** from an infinite wire in an infinitely long line is computed here at a distance **r** from the line.

Analysis
Equations
Inductance and Magnetism
Long Line
Reference

$$B = \frac{\mu_0 \cdot I}{2 \cdot \pi \cdot r}$$

Long Strip

A thin conducting ribbon strip of width **d** is infinitely long and carrying a current **I_s** amperes per meter. The x and y component of the magnetic field **B_x** and **B_y** are dependent upon the location described by (x, y) coordinates.

Analysis
Equations
Inductance and Magnetism
Long Strip
Reference

$$B_x = \frac{-\mu_0 \cdot I_s}{2 \cdot \pi} \cdot \left(\text{ATAN} \left(\frac{\left(x + \frac{d}{2} \right)}{y} \right) - \text{ATAN} \left(\frac{\left(x - \frac{d}{2} \right)}{y} \right) \right)$$

$$B_y = \frac{\mu_0 \cdot I_s}{4 \cdot \pi} \cdot \text{LN} \left(\frac{\left(y^2 + \left(x + \frac{d}{2} \right)^2 \right)}{y^2 + \left(x - \frac{d}{2} \right)^2} \right)$$

Parallel Wires

Analysis
Equations
Inductance and Magnetism
Parallel Wires
Reference

Two thin infinite wires carrying currents **I1** and **I2** separated by a distance **D** exert a force of **F** newtons/m between them and generate a tangential magnetic field **B** at the center of one wire due to the field from the other wire. The third equation shows the expression for the tangential magnetic field **B** between the two parallel wires. The distance **x** is measured from the line carrying current **I1**, while the distance of the same point from the second line carrying a current **I2**. The last equation in this set computes the inductance from the two wires of diameter **a** with a spacing of **D**, carrying equal and opposite currents.

$$B = \frac{\mu_0 \cdot I}{2 \cdot \pi \cdot D}$$

$$F = \frac{\mu_0 \cdot I_1 \cdot I_2}{2 \cdot \pi \cdot D}$$

$$B_x = \frac{\mu_0 \cdot I}{2 \cdot \pi} \cdot \left(\frac{1}{x} + \frac{1}{D-x} \right)$$

$$L = \frac{\mu_0}{4 \cdot \pi} + \frac{\mu_0}{\pi} \cdot \text{ACOSH} \left(\frac{D}{2 \cdot a} \right)$$

Loop

Analysis
Equations
Inductance and Magnetism
Loop
Reference

The first two equations consider a thin wire bent into a circular loop and carrying a current **I**. The loop radius is **a** and is in the **xy** plane. The equation for the magnetic field **B** is computed along the **z**-axis through the center of the loop. The



second equation shows the self-inductance of the loop. The last two equations represent the inductance **L12** and torque **T12** of a rectangular loop of sides **a** and **b**, and carrying a current **I2** in the vicinity of a wire carrying a current of **I1** and located at distance **D** as shown in the diagram to the left here.

$$B = \frac{\mu_0 \cdot I \cdot a^2}{2 \cdot \sqrt{a^2 + z^2}^3}$$

$$L_s = \mu_0 \cdot a \cdot \left[\text{LN} \left(\frac{8 \cdot a}{r_0} \right) - 2 \right]$$

$$L_{12} = \frac{-\mu_0 \cdot a \cdot \cos(\theta)}{2 \cdot \pi} \cdot \text{LN} \left(\frac{(b+d)}{d} \right)$$

$$T_{12} = \frac{\mu_0 \cdot a \cdot \sin(\theta)}{2 \cdot \pi} \cdot I_1 \cdot I_2 \cdot \ln\left(\frac{(b+d)}{d}\right)$$

Coaxial Cable

Analysis
Equations
Inductance and Magnetism
Coaxial Cable
Reference

A coaxial transmission line with an outer



radius of inner conductor of a and inner radius of the outer conductor of b is characterized by the inductance L .

$$L = \frac{\mu_0}{8 \cdot \pi} + \frac{\mu_0}{2 \cdot \pi} \cdot \ln\left(\frac{b}{a}\right)$$

Skin Effect

Analysis
Equations
Inductance and Magnetism
Skin Effect
Reference

These two equations represent the effect of high frequency on the resistance of a conductor. The first equation connects the skin depth δ with the frequency f and the resistivity ρ . The skin depth represents the RF signal penetration from the surface of a conductor. The second equation shows the relationship between the effective resistance and f and ρ . The effective resistance R_{eff} is specified in terms of ohms/length/width or often specified as ohms/square.

$$\delta = \frac{1}{\sqrt{\pi \cdot f \cdot \mu_0 \cdot \mu_r \cdot \rho}} \quad R_{eff} = \sqrt{\pi \cdot f \cdot \mu_0 \cdot \mu_r \cdot \rho}$$

Bibliography

Plonsey, Robert and Robert E. Collin, *Principles and Applications of Electromagnetic Fields*, McGraw-Hill Book Company, Inc. 1961.

Chapter 20

Electron Motion

Analysis
Equations
<i>Electron Motion</i>
Reference

This chapter covers equations describing the properties of electrons as they are subjected to electric and magnetic fields.

- ☐ Electron Beam Deflection
- ☐ Thermionic Emission
- ☐ Photoemission

Variables

The table below lists all the variables used in this chapter.

Variable	Description	Unit
A0	Richardson's constant	$A/(m^2 \cdot K^2)$
B	Magnetic field	T
d	Deflection tube diameter	m
f	Frequency	Hz
f0	Critical frequency	Hz
I	Thermionic current	A
L	Deflecting plate length	m
Ls	Beam length to destination	m
ϕ	Work function voltage	V
r	Radius of circular path	m
S	Surface area	m^2
T	Temperature	K
u	Velocity	m/s
u0	Electron velocity	m/s
v	Vertical velocity	m/s
Va	Accelerating voltage	V
Vd	Deflecting voltage	V
y	Vertical deflection	m
yd	Beam deflection on screen	m
z	Distance along beam axis	m

Electron Beam Deflection

Analysis
Equations
Electron Motion
<i>Electron Beam Deflection</i>
Reference

A beam of electrons subject to accelerating voltage V_a achieves a velocity v as described by the first equation. The second equation computes the radius of curvature r when an electron beam with an electron velocity u_0 is passing through a magnetic field B . The last two equations show the y -deflection y_d at distance L_s from the center of deflection plates separated by a distance d and subject to a deflecting voltage V_d .

$$v = \sqrt{2 \cdot \left(\frac{q}{m_e}\right) \cdot V_a} \qquad r = \frac{m_e \cdot u_0}{q \cdot B} \qquad y_d = \frac{L \cdot L_s}{2 \cdot d \cdot V_a} \cdot V_d \qquad y = \frac{q \cdot V_d}{2 \cdot m_e \cdot d \cdot u^2} \cdot z^2$$

Thermionic Emission

Analysis
Equations
Electron Motion
<i>Thermionic Emission</i>
Reference

When a material is heated to a high temperature T the free electrons gain enough thermal energy, forcing a finite fraction to escape the work function barrier ϕ and contribute to the external current I . The current also depends directly on the surface area S and the so-called Richardson's constant A_0 .

$$I = A_0 \cdot S \cdot T^2 \cdot e^{\frac{-q \cdot \phi}{k \cdot T}}$$

Photoemission

Analysis
Equations
Electron Motion
<i>Photoemission</i>
Reference

These two equations represent the behavior of electrons when excited by photon energy. A light beam with a frequency f generates an RMS velocity v for electrons that have to overcome a work function ϕ . The second equation shows the threshold frequency for the light beam to extract electrons from the surface of a solid.

$$h \cdot f = q \cdot \phi + \frac{1}{2} m_e \cdot v^2$$

$$f \phi = \frac{q \cdot \phi}{h}$$

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Chapter 21

Meters and Bridge Circuits

Analysis
Equations
<i>Meters and Bridge Circuits</i>
Reference

This chapter covers the equations describing commonly-used meters, bridges, and attenuator circuits.

- ☐ Amp, Volt, and Ohmmeter
- ☐ Wheatstone Bridge
- ☐ Wien Bridge
- ☐ Maxwell Bridge
- ☐ Owen Bridge
- ☐ Symmetrical Resistive Attenuator
- ☐ Unsymmetrical Resistive Attenuator

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

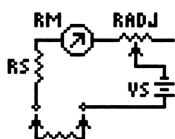
Variable	Description	Unit
C2	Capacitance, arm 2	F
C4	Capacitance, arm 4	F
Cs	Series capacitor	F
Cx	Unknown capacitor	F
DB	Attenuator loss	unitless
f	Frequency	Hz
Ig	Galvanometer current	A
Imax	Maximum current	A
Isen	Current sensitivity	A
Lx	Unknown inductance	H
Q	Quality factor	unitless
R1	Resistance, arm 1	Ω
R2	Resistance, arm 2	Ω
R3	Resistance, arm 3	Ω

R4	Resistance, arm 4	Ω
Ra	Resistance, leg a	Ω
Radj	Adjustable resistor	Ω
Rb	Resistance, leg b	Ω
Rc	Resistance, leg c	Ω
Rg	Galvanometer resistance	Ω
Rj	Resistance in L pad	Ω
Rk	Resistance in L pad	Ω
Rl	Resistance from left	Ω
Rm	Meter resistance	Ω
Ro	Terminating resistance	Ω
Rr	Resistance from right	Ω
Rs	Series resistance	Ω
Rse	Series resistance	Ω
Rsh	Shunt resistance	A
Rx	Unknown resistance	Ω
Vm	Voltage across meter	V
Vmax	Maximum voltage	V
Vs	Source voltage	V
Vsen	Voltage sensitivity	V
ω	Radian frequency	r/s

Amp, Volt, and Ohmmeter

Analysis
Equations
Meters and Bridge Circuits
Amp, Volt, and Ohmmeter
Reference

The three equations in this section highlight the use of resistors in extending the range of ammeters, voltmeters and ohmmeters. The first equation illustrates the use of a shunt resistor **Rsh** to increase the range of an ammeter with a current sensitivity **I_{sen}** and a maximum range **I_{max}**. The second equation shows the use of a series resistance **Rse** to extend the range of a voltmeter. The third equation extends the range of a series ohmmeter with an internal resistance **Rm** and internal voltage **Vs**, with an adjustable resistor **Radj**. In a practical setup, **Radj** is usually set at its midpoint to compensate for variations in the component values, resulting in a systematic error in the measured result. The



third equation is also applicable to a measurement system wherein an unknown resistance is placed in parallel to a shunt ohmmeter. In such a configuration, the meter deflection is designed to show full deflection for an infinite unknown impedance and zero deflection for a short circuit.

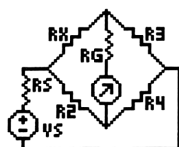
$$R_{sh} = \frac{R_m \cdot I_{sen}}{I_{max} - I_{sen}}$$

$$R_{se} = \frac{(V_{max} - V_{sen})}{I_{sen}}$$

$$I_{sen} = \frac{V_s}{R_s + R_m + \frac{R_{adj}}{2}}$$

Wheatstone Bridge

These three equations represent the classic relationship in a Wheatstone bridge network with four resistor elements **R_x**, **R₂**, **R₃** and **R₄**. When the bridge is balanced, there is no current in the galvanometer circuit. The first equation defines the requirement for a balanced bridge. The second and third equations compute the voltage **V_m** across the bridge and the galvanometer current **I_g**. The special function **GALV** calculates the voltage across the bridge, and is a complex function of **V_s**, **R_x**, **R₂**, **R₃**, **R₄**, **R_g** and **R_s**.



Analysis
Equations
Meters and Bridge Circuits
Wheatstone Bridge
Reference

$$\frac{R_x}{R_2} = \frac{R_3}{R_4}$$

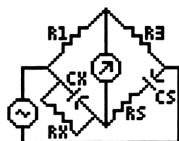
$$V_m = \text{GALV}(R_x, R_2, R_3, R_4, R_g, R_s, V_s)$$

$$I_g = \frac{V_m}{R_g}$$

Wien Bridge

A Wien bridge circuit is designed to measure an unknown capacitance **C_x**. The first two

equations focus on two methods of measuring **C_x** in terms of the branch resistances **R₁** and **R₃**, series resistance **R_s**, and parallel resistance **R_x**. The bridge can also be used to measure frequency **f** with the third equation after setting **C_x=C_s**, **R_x=R_s**, and **R₃=2*R₁**.



Analysis
Equations
Meters and Bridge Circuits
Wien Bridge
Reference

$$\frac{C_x}{C_s} = \frac{R_3}{R_1} \cdot \frac{R_s}{R_x}$$

$$C_s \cdot C_x = \frac{1}{\omega^2 \cdot R_s \cdot R_x}$$

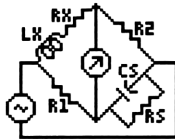
$$f = \frac{1}{2 \cdot \pi \cdot C_s \cdot R_s}$$

$$\omega = 2 \cdot \pi \cdot f$$

Maxwell Bridge

Analysis
Equations
Meters and Bridge Circuits
Maxwell Bridge
Reference

A Maxwell bridge is designed to measure the inductance L_x and its series resistance R_x in a bridge circuit. The input stimulus to the bridge circuit is typically an AC source with variable frequency and an AC meter detecting a null. The first two equations measure the unknown inductance L_x and its resistance R_x is by



varying the capacitance C_s and its parallel resistance R_s . The third and fourth equations measure the quality factor Q by using either measured L_x and R_x or known C_s and R_s . The final equation links the radian frequency ω to the frequency f .

$$L_x = R_2 \cdot R_3 \cdot C_s$$

$$R_x = \frac{R_2 \cdot R_3}{R_s}$$

$$Q = \omega \cdot \left(\frac{L_x}{R_x} \right)$$

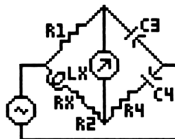
$$Q = \omega \cdot C_s \cdot R_s$$

$$\omega = 2 \cdot \pi \cdot f$$

Owen Bridge

Analysis
Equations
Meters and Bridge Circuits
Owen Bridge
Reference

The Owen bridge circuit is an alternative AC bridge circuit used to measure an inductance and its series resistance. The input stimulus to the bridge circuit is typically an AC source with variable frequency and an AC meter detecting a null. The inductance L_x is measured in terms of the capacitor C_3 , and the branch resistance R_1 and R_4 . The series resistance R_x is measured by a ratio of the capacitors C_3 and C_4 tempered by R_2 , the variable resistance in the L_x arm of the bridge.



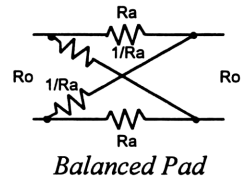
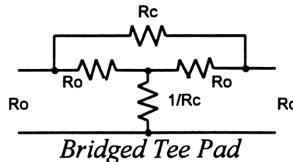
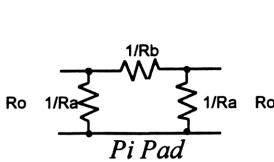
$$L_x = C_3 \cdot R_1 \cdot R_4$$

$$R_x = \frac{C_3 \cdot R_1}{C_4} - R_2$$

Symmetrical Resistive Attenuator

Analysis
Equations
Meters and Bridge Circuits
Sym. Resistive Attenuator
Reference

Balanced resistive networks are commonly used as attenuators in transmission line circuits. These three equations form the basis of design of an attenuator in a Tee pad, a Pi pad, a bridged Tee pad or a balanced pad configuration. These design equations compute the resistance values in the circuit given an attenuation loss **DB**, which is defined in decibels. The first equation defines the value of **Ra** for a Tee pad, Pi pad, a bridged Tee pad or a balanced pad configuration. The resistance **Rb** is defined by the second equation for a Tee pad or a Pi pad. The third equation defines **Rc** for a bridged Tee pad or a balanced pad configuration.



$$R_a = \frac{R_o \cdot \left(10^{\frac{DB}{20}} - 1 \right)}{10^{\frac{DB}{20}} + 1}$$

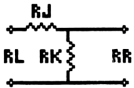
$$R_b = \frac{R_o \cdot 2 \cdot 10^{\frac{DB}{20}}}{10^{\frac{DB}{10}} - 1}$$

$$R_c = R_o \cdot \left(10^{\frac{DB}{20}} - 1 \right)$$

Unsymmetrical Resistive Attenuator

Analysis
Equations
Meters and Bridge Circuits
Unsym. Res. Attenuator
Reference

Unsymmetrical resistive attenuator design equations are given in this section. These equations compute the resistance values for a minimum loss **L** pad of an unsymmetrical network with an impedance **Rl** to the left of the L-network and an impedance **Rr** to the right of the network. The first two equations calculate **Rj** and **Rk**, the resistor values of the L network. The third equation determines the minimum loss of signal strength **DB**.



$$R_j = R_l - \frac{R_k \cdot R_r}{R_k + R_r}$$

$$R_k = \sqrt{\frac{R_l \cdot R_r^2}{R_l - R_r}}$$

$$DB = 20 \cdot \text{LOG} \left(\sqrt{\frac{(R_l - R_r)}{R_r}} + \sqrt{\frac{R_l}{R_r}} \right)$$

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Chapter 22

RL and RC Circuits

Analysis
Equations
<i>RL and RC Circuits</i>
Reference

This chapter covers equations for on RL and RC Circuits.

- ☐ RL Natural Response
- ☐ RC Natural Response
- ☐ RL Step Response
- ☐ RC Step Response
- ☐ RL Series to Parallel
- ☐ RC Series to Parallel

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
C	Capacitor	F
Cs	Series capacitance	F
Cp	Parallel capacitance	F
f	Frequency	Hz
iC	Capacitor current	A
iL	Inductor current	A
I0	Initial inductor current	A
L	Inductance	H
Lp	Parallel inductance	H
Ls	Series inductance	H
Qp	Q, parallel circuit	unitless
Qs	Q, series circuit	unitless
R	Resistance	Ω
Rp	Parallel resistance	Ω
Rs	Series resistance	Ω
τ	Time constant	s

t	Time	s
vC	Capacitor voltage	V
vL	Inductor voltage	V
V0	Initial capacitor voltage	V
Vs	Voltage stimulus	V
ω	Radian frequency	r/s
W	Energy dissipated	J

RL Natural Response

Analysis

Equations

RL and RC Circuits

RL Natural Response

Reference

These four equations define all the key properties for the natural response of an RL circuit with no energy sources. The first equation shows the characteristic time constant τ in terms of the resistance R and the inductance L . The second equation computes the decay of the voltage v_L across the inductor with an initial current I_0 . The third equation displays the decay of the inductor current i_L . The final equation shows the energy dissipation properties of the circuit.



$$\tau = \frac{L}{R}$$

$$v_L = I_0 \cdot R \cdot e^{\frac{-t}{\tau}}$$

$$i_L = I_0 \cdot e^{\frac{-t}{\tau}}$$

$$W = \frac{1}{2} \cdot L \cdot I_0^2 \cdot \left(1 - e^{\frac{-2 \cdot t}{\tau}} \right)$$

RC Natural Response

Analysis

Equations

RL and RC Circuits

RC Natural Response

Reference

These four equations define all the natural response characteristics of an RC circuit with no energy sources. The first equation specifies the characteristic time constant τ in terms of the resistance R and the capacitance C . The second equation computes the decay of the voltage v_C across the capacitor with an initial voltage of V_0 . The third equation shows the decay of the capacitor current i_C . The final equation computes the energy dissipation properties.



$$\tau = R \cdot C$$

$$v_C = V_0 \cdot e^{\frac{-t}{\tau}}$$

$$i_C = \frac{V_0}{R} \cdot e^{\frac{-t}{\tau}}$$

$$W = \frac{1}{2} \cdot C \cdot V_0^2 \cdot \left(1 - e^{\frac{-2 \cdot t}{\tau}} \right)$$

RL Step Response

Analysis
Equations
RL and RC Circuits
RL Step Response
Reference

These three equations describe the response of an inductive circuit to a voltage step stimulus.

The first equation calculates the time constant τ in terms of the inductance L and the resistance R . The last two equations compute the inductor voltage v_L and current i_L in terms of the step stimulus V_s , initial condition I_0 , time t , and time constant τ .



$$\tau = \frac{L}{R}$$

$$v_L = (V_s - I_0 \cdot R) \cdot e^{\frac{-t}{\tau}}$$

$$i_L = \frac{V_s}{R} + \left(I_0 - \frac{V_s}{R} \right) \cdot e^{\frac{-t}{\tau}}$$

RC Step Response

Analysis
Equations
RL and RC Circuits
RC Step Response
Reference

These three equations show the step response properties of an RC circuit. The first equation

defines the characteristic time constant τ in terms of the resistance R and the capacitance C . The last two equations compute the capacitor voltage v_C and current i_C in terms of the step stimulus voltage V_s , initial capacitor voltage V_0 , time t and time constant τ .



$$\tau = R \cdot C$$

$$v_C = V_s + (V_0 - V_s) \cdot e^{\frac{-t}{\tau}}$$

$$i_C = \frac{(V_s - V_0)}{R} \cdot e^{\frac{-t}{\tau}}$$

RL Series to Parallel

Analysis
Equations
RL and RC Circuits
RL Series to Parallel
Reference

The ten equations in this section show the equivalence between a series RL circuit with values **Rs** and **Ls** and its parallel equivalent circuit with values **Rp**, **Lp**. The first equation defines the relationship between the radian frequency ω and the frequency **f**. The second equation specifies the quality factor **Qs** for the series circuit values **Rs** and **Ls**. The next two equations define the values of **Rp** and **Lp** in terms of **Rs**, **Ls** and the radian frequency ω . The fifth and sixth equations compute **Rp** and **Lp** in terms of **Rs**, **Ls** and **Qs**. The remaining five equations show the inverse relationships, where the series equivalent values



Rs and **Ls** are expressed in terms of the parallel RL circuit values **Rp**, **Lp**, ω and the quality factor for the parallel RL circuit **Qp**.

$$\omega = 2 \cdot \pi \cdot f$$

$$Q_s = \frac{\omega \cdot L_s}{R_s}$$

$$R_p = \frac{(R_s^2 + \omega^2 \cdot L_s^2)}{R_s}$$

$$L_p = \frac{(R_s^2 + \omega^2 \cdot L_s^2)}{\omega^2 \cdot L_s}$$

$$R_p = R_s \cdot (1 + Q_s^2)$$

$$L_p = L_s \cdot \left(1 + \frac{1}{Q_s^2}\right)$$

$$Q_p = \frac{R_p}{\omega \cdot L_p}$$

$$R_s = \frac{\omega^2 \cdot L_p^2 \cdot R_p}{R_p^2 + \omega^2 \cdot L_p^2}$$

$$L_s = \frac{R_p^2 \cdot L_p}{R_p^2 + \omega^2 \cdot L_p^2}$$

$$R_s = \frac{R_p}{1 + Q_p^2}$$

$$L_s = \frac{Q_p^2 \cdot L_p}{1 + Q_p^2}$$

RC Series to Parallel

Analysis

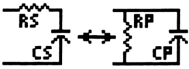
Equations

RL and RC Circuits

RC Series to Parallel

Reference

The ten equations in this section show the equivalence between a series RC circuit with values R_s and C_s and its parallel equivalent circuit with values R_p and C_p . The first equation defines the radian frequency ω in terms of f . The second equation computes the quality factor Q_s in terms of ω and the series resistance R_s and capacitance C_s . The next two equations compute the parallel equivalent values as a function of R_s and ω . The fifth equation computes R_p as a function of R_s , C_s and Q_s . The remaining five equations show the inverse set of relationships where the series equivalent values R_s and C_s are expressed in terms of the parallel RC circuit values R_p , C_p , ω and the quality factor for the parallel RC circuit Q_p .



$$\omega = 2\pi \cdot f$$

$$Q_s = \frac{1}{\omega \cdot R_s \cdot C_s}$$

$$R_p = R_s \cdot \left(1 + \frac{1}{\omega^2 \cdot R_s^2 \cdot C_s^2} \right)$$

$$C_p = \frac{C_s}{1 + \omega^2 \cdot C_s^2 \cdot R_s^2}$$

$$R_p = R_s \cdot (1 + Q_s^2)$$

$$Q_p = \omega \cdot R_p \cdot C_p$$

$$R_s = \frac{R_p}{1 + \omega^2 \cdot R_p^2 \cdot C_p^2}$$

$$C_s = \frac{(1 + \omega^2 \cdot R_p^2 \cdot C_p^2)}{\omega^2 \cdot R_p^2 \cdot C_p}$$

$$R_s = \frac{R_p}{1 + Q_p^2}$$

$$C_s = \frac{C_p \cdot (1 + Q_p^2)}{Q_p^2}$$

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Chapter 23

RLC Circuits

Analysis
Equations
<i>RLC Circuits</i>
Reference

This chapter covers all the essential equations for computing impedance and admittance, natural response, and transient behavior of RLC circuits.

- ☐ Series Impedance
- ☐ Parallel Admittance
- ☐ RLC Natural Response
- ☐ Underdamped Transient
- ☐ Critically-Damped Transient
- ☐ Overdamped Transient

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
α	Neper's frequency	r/s
A1	Constant	V
A2	Constant	V
B	Susceptance	S
B1	Constant	V
B2	Constant	V
BC	Capacitive susceptance	S
BL	Inductive susceptance	S
C	Capacitance	F
D1	Constant	V/s
D2	Constant	V
f	Frequency	Hz
G	Conductance	S
I0	Initial inductor current	A
L	Inductance	H
θ	Phase angle	r

R	Resistance	Ω
s1	Characteristic frequency 1	r/s
s2	Characteristic frequency 2	r/s
s1i	Characteristic frequency 1 (imag.)	unitless
s1r	Characteristic frequency 1 (real)	unitless
s2i	Characteristic frequency 2 (imag.)	unitless
s2r	Characteristic frequency 2 (real)	unitless
t	Time	s
v	Capacitor voltage	V
V0	Initial capacitor voltage	V
ω	Radian frequency	r/s
ωd	Damped resonant frequency	r/s
$\omega 0$	Classical resonant frequency	r/s
X	Reactance	Ω
XC	Capacitive reactance	Ω
XL	Inductive reactance	Ω
Ym	Admittance magnitude	S
Zm	Impedance magnitude	Ω

Series Impedance

Analysis
Equations
RLC Circuits
<i>Series Impedance</i>
Reference

These six equations compute the series impedance of an RLC circuit. The first two equations focus on calculating the magnitude and phase angle of the impedance in terms of resistance the **R** and reactance **X**. The third equation computes the reactance **X** as the sum of the inductive and capacitive parts **XL** and **XC**, respectively. In the fourth and fifth equations, **XL** is computed in terms of the radian frequency ω and inductance **L**, while **XC** is computed in terms of ω and **C**. In the last equation, ω is defined in terms of the frequency **f**.

$ABS(Z_m)^2 = R^2 + X^2$	$\theta = ATAN\left(\frac{X}{R}\right)$	$X = XL + XC$
$XL = \omega \cdot L$	$XC = \frac{-1}{\omega \cdot C}$	$\omega = 2 \cdot \pi \cdot f$

Parallel Admittance

Analysis
Equations
RLC Circuits
Parallel Admittance
Reference

These seven equations compute the admittance of an RLC parallel circuit. The first two equations calculate the magnitude of the admittance Y_m and its phase angle θ in terms of the conductance G and susceptance B . The third equation calculates the conductance G in terms of the resistance R . The next three equations compute the susceptance B as a sum of its inductive and capacitive components B_L and B_C , respectively. The final equation links the radian frequency ω and frequency f .

$$ABS(Y_m)^2 = G^2 + B^2$$

$$\theta = ATAN\left(\frac{G}{B}\right)$$

$$G = \frac{1}{R}$$

$$B = B_L + B_C$$

$$B_L = \frac{-1}{\omega \cdot L}$$

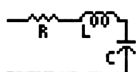
$$B_C = \omega \cdot C$$

$$\omega = 2 \cdot \pi \cdot f$$

RLC Natural Response

Analysis
Equations
RLC Circuits
RLC Natural Response
Reference

These six equations compute the generalized complex frequencies for an RLC circuit. In general there are two complex conjugate frequencies s_1 and s_2 with real and imaginary parts s_{1r} , s_{1i} , s_{2r} , and s_{2i} , respectively. They are computed in terms of the classical resonant frequency ω_0 , and Neper's frequency α , which are defined by the final two equations.



$$s_{1r} = RE\left(-\alpha + \sqrt{\alpha^2 - \omega_0^2}\right) \quad s_{1i} = IM\left(-\alpha + \sqrt{\alpha^2 - \omega_0^2}\right)$$

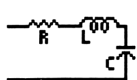
$$s_{2r} = RE\left(-\alpha - \sqrt{\alpha^2 - \omega_0^2}\right) \quad s_{2i} = IM\left(-\alpha - \sqrt{\alpha^2 - \omega_0^2}\right) \quad \omega_0 = \sqrt{\frac{1}{L \cdot C}}$$

$$\alpha = \frac{1}{2 \cdot R \cdot C}$$

Underdamped Transient

Analysis
Equations
RLC Circuits
Underdamped Transient
Reference

The six equations in this section represent the transient response of an underdamped RLC circuit. *The condition for an underdamped system is that $\omega_0 > \alpha$.* The first equation shows the classical radian frequency ω_0 , which is determined by the inductance and capacitance L and C . The Neper's frequency α is calculated in the second equation. The damped resonant frequency ω_d is computed from ω_0 and α in the third equation. The fourth equation shows the voltage across the capacitor v , while the last two equations show the relationship of the constants $B1$ and $B2$ to the initial capacitor voltage V_0 , initial inductor current



I_0 , the capacitor C and resistor R , and frequencies ω_d and α . The voltage across the capacitor shows an oscillatory behavior with respect to the characteristic frequency ω_d .

$$\omega_0 = \sqrt{\frac{1}{L \cdot C}}$$

$$\alpha = \frac{1}{2 \cdot R \cdot C}$$

$$\omega_d = \sqrt{\omega_0^2 - \alpha^2}$$

$$v = B1 \cdot e^{-\alpha \cdot t} \cdot \cos(\omega_d \cdot t) + B2 \cdot e^{-\alpha \cdot t} \cdot \sin(\omega_d \cdot t)$$

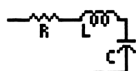
$$B1 = V_0$$

$$B2 = \frac{-\alpha}{\omega_d} \cdot V_0 - \frac{1}{\omega_d \cdot C} \cdot \left(\frac{V_0}{R} + I_0 \right)$$

Critically-Damped Transient

Analysis
Equations
RLC Circuits
Critically-Damped Transient
Reference

The five equations in this section represent the RLC transient response of a critically-damped circuit. *The condition for an critically-damped system is that $\omega_0 = \alpha$.* The first two equations define the Neper's frequency α and the classical resonant frequency ω_0 . The third equation represents the transient response to a step function stimulus of the voltage across the capacitor v , as expressed in terms of the constants $D1$ and $D2$, Neper's frequency, and time t .



The last two equations compute the constants $D1$ and $D2$ in terms of the capacitor voltage V_0 and the initial inductor current I_0 .

$$\alpha = \frac{1}{2 \cdot R \cdot C}$$

$$\omega_0 = \sqrt{\frac{1}{L \cdot C}}$$

$$v = D1 \cdot t \cdot e^{\alpha \cdot t} + D2 \cdot e^{\alpha \cdot t}$$

$$D1 = -\alpha \cdot (V_0 + 2 \cdot I_0 \cdot R)$$

$$D2 = V_0$$

Overdamped Transient

Analysis

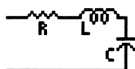
Equations

RLC Circuits

Overdamped Transient

Reference

The seven equations in this section show the transient performance of an overdamped RLC circuit.. *The condition for an overdamped system is that $\alpha > \omega_0$.* The first two equations define the characteristic frequencies $s1$ and $s2$ in terms of the Neper's frequency α and the classical resonant frequency ω_0 , which are calculated in the third and fourth equations. The fifth equation represents the transient response to a step function stimulus of the voltage across the capacitor v . This response is determined by the constants $A1$ and $A2$, the characteristic frequencies $s1$ and $s2$, and the time t . The last two equations compute the constants $A1$ and $A2$ from the initial capacitor voltage V_0 , the initial inductor current I_0 , and the characteristic frequencies $s1$ and $s2$.



$$s1 = -\alpha + \sqrt{\alpha^2 - \omega_0^2}$$

$$s2 = -\alpha - \sqrt{\alpha^2 - \omega_0^2}$$

$$\omega_0 = \frac{1}{\sqrt{L \cdot C}}$$

$$\alpha = \frac{1}{2 \cdot R \cdot C}$$

$$v = A1 \cdot e^{s1 \cdot t} + A2 \cdot e^{s2 \cdot t}$$

$$A1 = \frac{\left(V_0 \cdot s2 + \frac{1}{C} \cdot \left(\frac{V_0}{R} + I_0 \right) \right)}{s2 - s1}$$

$$A2 = \frac{-\left(V_0 \cdot s1 + \frac{1}{C} \cdot \left(\frac{V_0}{R} + I_0 \right) \right)}{s2 - s1}$$

Bibliography

Nilsson, James W., *Electric Circuits, 2nd Edition, Chapter 8*, Addison-Wesley Publishing Company, Reading, MA 1987.

Chapter 24

AC Circuits

Analysis
Equations
<i>AC Circuits</i>
Reference

This chapter covers equations describing the properties of AC circuits.

- ☐ RL Series Impedance
- ☐ RC Series Impedance
- ☐ Impedance ↔ Admittance
- ☐ Two Impedances in Series
- ☐ Two Impedances in Parallel

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
B	Susceptance	S
C	Capacitance	F
f	Frequency	Hz
G	Conductance	S
I	Instantaneous current	A
Im	Current amplitude	A
L	Inductance	H
θ	Impedance phase angle	r
θ1	Phase angle 1	r
θ2	Phase angle 2	r
θy	Admittance phase angle	r
θz	Impedance phase angle	r
R	Resistance	Ω
R1	Resistance 1	Ω
R2	Resistance 2	Ω
t	Time	s
V	Total voltage	V
VC	Voltage across capacitor	V

VL	Voltage across inductor	V
Vm	Maximum voltage	V
VR	Voltage across resistor	V
ω	Radian frequency	r/s
X	Reactance	Ω
X1	Reactance 1	Ω
X2	Reactance 2	Ω
Ym	Admittance magnitude	S
Z1m	Impedance 1 magnitude	Ω
Z2m	Impedance 2 magnitude	Ω
Zm	Impedance magnitude	Ω

RL Series Impedance

Analysis
Equations
AC Circuits
RL Series Impedance
Reference

The eight equations in this section describe the relationships of an RL series circuit. The first equation shows a sinusoidal current **I** defined in terms of an amplitude **Im**, radian frequency ω , and time **t**. The second equation defines the magnitude of the impedance **Zm** in terms of the resistance **R**, and the inductance **L** and ω . The third and fourth equations show the voltage drops **VR** and **VL** across the resistor and inductor, respectively. The fifth equation shows the instantaneous voltage across the RL circuit, the next two equations



show the amplitude **VM** and phase θ of the voltage across the circuit. The final equation shows the relation between ω and frequency **f**.

$$I = I_m \cdot \sin(\omega \cdot t) \quad \text{ABS}(Z_m)^2 = R^2 + \omega^2 \cdot L^2$$

$$V_R = Z_m \cdot I_m \cdot \sin(\omega \cdot t) \cdot \cos(\theta) \quad V_L = Z_m \cdot I_m \cdot \cos(\omega \cdot t) \cdot \sin(\theta)$$

$$V = V_R + V_L \quad V_m = I_m \cdot Z_m \quad \theta = \text{ATAN}\left(\frac{\omega \cdot L}{R}\right)$$

$$\omega = 2 \cdot \pi \cdot f$$

RC Series Impedance

Analysis
Equations
AC Circuits
RC Series Impedance
Reference

The eight equations in this section describe the relationships of an RC series circuit. The first equation shows a sinusoidal current **I** defined in terms of an amplitude **Im**, radian frequency **ω**, and time **t**. The second equation defines the magnitude **Zm** of the AC impedance of the circuit in terms of the resistance **R**, capacitance **C**, and radian frequency **ω**. The third and fourth equations express the voltage **VR** across the resistor and the voltage **VC** across the capacitor. The sum of **VR** and **VC** represents the total voltage **V** across the RC series circuit. The next two equations show the amplitude **Vm** and phase **θ** of the voltage across the circuit. The final equation connects **ω** with the frequency **f**.



$$I = I_m \cdot \sin(\omega \cdot t) \quad \text{ABS}(Z_m)^2 = R^2 + \frac{1}{(\omega \cdot C)^2}$$

$$V_R = Z_m \cdot I_m \cdot \sin(\omega \cdot t) \cdot \cos(\theta) \quad V_C = Z_m \cdot I_m \cdot \cos(\omega \cdot t) \cdot \sin(\theta)$$

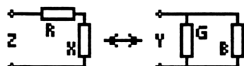
$$V = V_R + V_C \quad V_m = I_m \cdot Z_m \quad \theta = \text{ATAN}\left(\frac{-1}{\omega \cdot C \cdot R}\right)$$

$$\omega = 2 \cdot \pi \cdot f$$

Impedance ↔ Admittance

Analysis
Equations
AC Circuits
Impedance ↔ Admittance
Reference

These ten equations describe the relationship between impedance and admittance. The first four equations focus on the impedance: its magnitude **Zm**, its real and imaginary parts **R** and **X**, and its phase angle **θz**. The fifth and sixth equations link the phase and magnitude of the impedance and admittance. The last five equations focus on the admittance: its magnitude **Ym**, its real and imaginary parts **G** and **B**, and its phase angle **θy**.



$$\text{ABS}(Z_m)^2 = R^2 + X^2$$

$$\theta_z = \text{ATAN}\left(\frac{X}{R}\right)$$

$$R = Z_m \cdot \cos(\theta_z)$$

$$X = Z_m \cdot \sin(\theta_z)$$

$$\theta_y = -\theta_z$$

$$Y_m = \frac{1}{Z_m}$$

$$G = Y_m \cdot \cos(\theta_y)$$

$$B = Y_m \cdot \sin(\theta_y)$$

$$\text{ABS}(Y_m)^2 = G^2 + B^2$$

$$\theta_y = \text{ATAN}\left(\frac{B}{G}\right)$$

Two Impedances in Series

Analysis

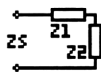
Equations

AC Circuits

Two Impedances in Series

Reference

These eight equations characterize the manner of combining two impedances **Z1** and **Z2** in series with real and imaginary parts **R1** and **X1**, **R2** and **X2**, respectively. The impedances **Z1** and **Z2** can be expressed in terms of their magnitudes **Z1m** and **Z2m**, and phase angles **θ1** and **θ2** as shown by the last four equations. The resulting impedance has a magnitude **Zm** and a phase angle **θ**, as shown by the first two equations. **R** and **X** represent the real and imaginary parts of the resulting impedance, and are defined by the third and fourth equations.



$$\text{ABS}(Z_m)^2 = R^2 + X^2$$

$$\theta = \text{ATAN}\left(\frac{X}{R}\right)$$

$$R = R1 + R2$$

$$X = X1 + X2$$

$$\text{ABS}(Z1_m)^2 = R1^2 + X1^2$$

$$\text{ABS}(Z2_m)^2 = R2^2 + X2^2$$

$$\theta1 = \text{ATAN}\left(\frac{X1}{R1}\right)$$

$$\theta2 = \text{ATAN}\left(\frac{X2}{R2}\right)$$

Two Impedances in Parallel

Analysis
Equations
AC Circuits
<i>Two Impedances in Parallel</i>
Reference

These eight equations describe the properties of combining two impedances **Z1** and **Z2** in parallel. **Z1** is expressed in terms of real and imaginary parts **R1** and **X1**, or of magnitude **Z1m** and phase **θ1**. Similarly, **Z2** can be defined by real and imaginary parts **R2** and **X2** or magnitude and phase **Z2m** and **θ2**. **Zm** and **θ** are computed from known values of **R1**, **X1**, **R2** and **X2**.



$$ABS(Z_m)^2 = \frac{\left[(R1 \cdot R2 - X1 \cdot X2)^2 + (R1 \cdot X2 + R2 \cdot X1)^2 \right]}{(R1 + R2)^2 + (X1 + X2)^2}$$

$$\theta = ATAN\left(\frac{X1 \cdot R2 + R1 \cdot X2}{R1 \cdot R2 - X1 \cdot X2}\right) - ATAN\left(\frac{X1 + X2}{R1 + R2}\right)$$

$$R = Z_m \cdot \cos(\theta) \qquad X = Z_m \cdot \sin(\theta) \qquad ABS(Z1_m)^2 = R1^2 + X1^2$$

$$ABS(Z2_m)^2 = R2^2 + X2^2 \qquad \theta1 = ATAN\left(\frac{X1}{R1}\right) \qquad \theta2 = ATAN\left(\frac{X2}{R2}\right)$$

Chapter 25

Polyphase
Circuits

Analysis
Equations
<i>Polyphase Circuits</i>
Reference

This chapter covers equations describing polyphase circuits.

- ☐ Balanced Δ Network
- ☐ Balanced Wye Network
- ☐ Power Measurements

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
IL	Line current	A
Ip	Phase current	A
P	Power per phase	W
PT	Total power	W
θ	Impedance angle	r
VL	Line voltage	V
Vp	Phase voltage	V
W1	Wattmeter 1	W
W2	Wattmeter 2	W

Balanced Δ Network

Analysis
Equations
Polyphase Circuits
<i>Balanced Δ Network</i>
Reference

These five equations cover the essential relationships for a balanced Δ network. The first equation defines the line voltage **VL** in terms of the phase voltage **Vp**. The second equation defines the line current **IL** in terms of the phase current **Ip**. The third equation shows the power in each phase in terms of **Vp**, **Ip** and

the phase delay θ between voltage and current. The last two equations represent the total power **PT** delivered to the system in terms of line voltage and current or the phase voltage and current.

$V_L = V_P$	$I_L = \sqrt{3} \cdot I_P$	$P = V_P \cdot I_P \cdot \cos(\theta)$
$PT = 3 \cdot V_P \cdot I_P \cdot \cos(\theta) \quad PT = \sqrt{3} \cdot V_L \cdot I_L \cdot \cos(\theta)$		

Balanced Wye Network

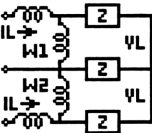
These five equations cover the essential relationships for a balanced star network. The first equation defines the line voltage **VL** in terms of the phase voltage **Vp**. The second equation defines the line current **IL** in terms of the phase current **Ip**. The third equation shows the power in each phase in terms of **Vp**, **Ip** and phase delay θ . The last two equations represent total power **PT** delivered to the system in terms of line voltage and current or phase voltage and current.

Analysis
 Equations
 Polyphase Circuits
Balanced Wye Network
 Reference

$V_L = \sqrt{3} \cdot V_P$	$I_L = I_P$	$P = V_P \cdot I_P \cdot \cos(\theta)$
$PT = 3 \cdot V_P \cdot I_P \cdot \cos(\theta) \quad PT = \sqrt{3} \cdot V_L \cdot I_L \cdot \cos(\theta)$		

Power Measurements

These three equations for a two-wattmeter connection are used to measure the total



power of a balanced network. The wattmeter readings **W1** and **W2** are expressed in terms of the line current **IL**, line voltage **VL**, and phase delay θ between voltage and current. The final equation represents the total power delivered to the three-phase load.

Analysis
 Equations
 Polyphase Circuits
Power Measurements
 Reference

$W1 = V_L \cdot I_L \cdot \cos\left(\theta + \frac{\pi}{6}\right) \quad W2 = V_L \cdot I_L \cdot \cos\left(\theta - \frac{\pi}{6}\right) \quad PT = \sqrt{3} \cdot V_L \cdot I_L \cdot \cos(\theta)$		
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Chapter 26

Electrical Resonance

Analysis
Equations
<i>Electrical Resonance</i>
Reference

This chapter covers equations describing the electrical properties of resonance in circuits made of ideal circuit elements.

- ☐ Parallel Resonance I
- ☐ Parallel Resonance II
- ☐ Resonance in Lossy Inductor
- ☐ Series Resonance

Variables

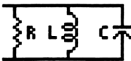
The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
α	Damping coefficient	r/s
β	Bandwidth	r/s
C	Capacitance	F
I_m	Current	A
L	Inductance	H
η	Phase angle	r
Q	Quality factor	unitless
R	Resistance	Ω
R_g	Generator resistance	Ω
V_m	Maximum voltage	V
ω	Radian frequency	r/s
ω_0	Resonant frequency	r/s
ω_1	Lower cutoff frequency	r/s
ω_2	Upper cutoff frequency	r/s
ω_d	Damped resonant frequency	r/s
ω_m	Frequency for max amplitude	r/s
Y_{res}	Admittance at resonance	S
Z	Impedance	Ω
Z_{res}	Impedance at resonance	Ω

Parallel Resonance I

Analysis
Equations
Electrical Resonance
<i>Parallel Resonance I</i>
Reference

These nine equations describe the properties of a parallel resonant circuit. The first equation expresses **V_m**, the voltage across the circuit, in terms of **I_m**, the magnitude of the current supplied and the equivalent impedance of the parallel circuit consisting of an inductor **L**, a capacitor **C** and a resistor **R** at the radian frequency **ω**. The second equation shows the phase angle relationship between **V_m** and **I_m**. The third equation connects the resonant frequency **ω₀** and reactive parameters **L** and **C**. The equations for **ω₁** and **ω₂** represent the upper and lower cutoff frequencies beyond resonance, where the impedance is half the impedance at resonance. The bandwidth **β** is expressed in terms of **ω**



1 and **ω₂**. The last three equations calculate the quality factor **Q** in terms of **R**, **C**, **L** and **ω₀**.

$$V_m = \frac{I_m}{\sqrt{\frac{1}{R^2} + \left(\omega C - \frac{1}{\omega L}\right)^2}} \quad \tan(\theta) = \left(\omega C - \frac{1}{\omega L}\right) \cdot R \quad \omega \theta = \frac{1}{\sqrt{L \cdot C}}$$

$$\omega_1 = \frac{-1}{2 \cdot R \cdot C} + \sqrt{\frac{1}{(2 \cdot R \cdot C)^2} + \frac{1}{L \cdot C}} \quad \omega_2 = \frac{1}{2 \cdot R \cdot C} + \sqrt{\frac{1}{(2 \cdot R \cdot C)^2} + \frac{1}{L \cdot C}} \quad \beta = \omega_2 - \omega_1$$

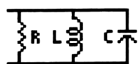
$$Q = \frac{\omega \theta}{\beta} \quad Q = R \cdot \sqrt{\frac{C}{L}} \quad Q = \omega \theta \cdot R \cdot C$$

Parallel Resonance II

Analysis
Equations
Electrical Resonance
<i>Parallel Resonance II</i>
Reference

These seven equations represent an alternative method of expressing the properties of a resonant circuit in terms of the quality factor **Q**. The first equation links **Q** with the resonant frequency **ω₀** and the bandwidth **β**. The equations for **ω₁** and **ω₂** show the connection between the upper and lower cutoff frequencies

and ω_0 and Q . The fourth equation computes α , the damping coefficient, while the damped resonant frequency ω_d is expressed in terms of α and ω_0 or ω_0 and Q . The last equation is an alternative form of equating α with Q and ω_0 .



$$Q = \frac{\omega_0}{\beta} \quad \omega_1 = \omega_0 \cdot \left(\frac{-1}{2 \cdot Q} + \sqrt{\frac{1}{(2 \cdot Q)^2} + 1} \right) \quad \omega_2 = \omega_0 \cdot \left(\frac{1}{2 \cdot Q} + \sqrt{\frac{1}{(2 \cdot Q)^2} + 1} \right)$$

$$\alpha = \frac{1}{2 \cdot R \cdot C} \quad \omega_d = \sqrt{\omega_0^2 - \alpha^2} \quad \omega_d = \omega_0 \cdot \sqrt{1 - \frac{1}{4 \cdot Q^2}}$$

$$\alpha = \frac{\omega_0}{2 \cdot Q}$$

Resonance in Lossy Inductor

Analysis
Equations
Electrical Resonance
Resonance in Lossy Inductor
Reference

These four equations characterize the properties of a lossy inductor in parallel with an ideal capacitor sourced from a current source with an impedance of R_g . ω_0 represents the radian frequency when the admittance of the parallel circuit is purely conductive. Y_{res} and Z_{res} represent the impedance and admittance of the circuit at resonance. ω_m represents the frequency wherein the amplitude of the voltage across the resonant circuit is at maximum.



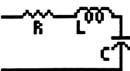
$$\omega_0 = \sqrt{\frac{1}{L \cdot C} - \left(\frac{R}{L} \right)^2} \quad Y_{res} = \frac{(L + R_g \cdot R \cdot C)}{L \cdot R_g} \quad Z_{res} = \frac{1}{Y_{res}}$$

$$\omega_m = \sqrt{\left(\frac{1}{L \cdot C} \right)^2 \cdot \left(1 + \frac{2 \cdot R}{R_g} \right) + \left(\frac{R}{L} \right)^2 \cdot \left(\frac{2}{L \cdot C} \right) - \left(\frac{R}{L} \right)^2}$$

Series Resonance

Analysis
Equations
Electrical Resonance
<i>Series Resonance</i>
Reference

These nine equations characterize the properties of a series resonant circuit. The first equation connects the resonant frequency ω_0 and the reactive parameters L and C . The second and third equations compute the magnitude Z and phase θ of the impedance. The equations for ω_1 and ω_2 represent the upper and lower cutoff frequencies beyond resonance, where the impedance is half the impedance at resonance. The expression for β represents the bandwidth for the resonant circuit. The last two equations determine the quality factor Q in terms of R , C , L , and ω_0 .



$$\omega_0=\frac{1}{\sqrt{L\cdot C}}$$

$$Z=\sqrt{R^2+\left(\omega\cdot L-\frac{1}{\omega\cdot C}\right)^2}$$

$$\theta=ATAN\left(\frac{\left(\omega\cdot L-\frac{1}{\omega\cdot C}\right)}{R}\right)$$

$$\omega_1=\frac{-R}{2\cdot L}+\sqrt{\left(\frac{R}{2\cdot L}\right)^2+\frac{1}{L\cdot C}}$$

$$\omega_2=\frac{R}{2\cdot L}+\sqrt{\left(\frac{R}{2\cdot L}\right)^2+\frac{1}{L\cdot C}}$$

$$\beta=\omega_2-\omega_1$$

$$\beta=\frac{R}{L}$$

$$Q=\frac{\omega_0\cdot L}{R}$$

$$Q=\frac{1}{R}\cdot\sqrt{\frac{L}{C}}$$

Chapter 27

OpAmp Circuits

Analysis
Equations
<i>OpAmp Circuits</i>
Reference

Seven commonly-used OpAmp circuits are presented in this chapter. An OpAmp is a direct-coupled high-gain amplifier that can be designed with the use of feedback to control its overall performance characteristics. The two inputs are labelled + and -. The manner in which input signals are connected to these terminals defines the inverting or non-inverting properties of the circuit.

- ☐ Basic Inverter
- ☐ Non-Inverting Amplifier
- ☐ Current Amplifier
- ☐ Transconductance Amplifier
- ☐ Level Detector (Inverting)
- ☐ Level Detector (Non-Inverting)
- ☐ Differentiator
- ☐ Differential Amplifier

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
Acc	CM current gain	unitless
Aco	CM gain from real OpAmp	unitless
Ad	Differential mode gain	unitless
Agc	Transconductance	S
Aic	Current gain	unitless
Av	Voltage gain	unitless
C1	Input capacitor	F
Cf	Feedback capacitor	F
CMRR	CM rejection ratio	unitless
Cp	Bypass capacitor	F
fcp	3dB bandwidth, circuit	Hz

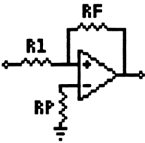
fd	Characteristic frequency	Hz
f0	Passband, geometric center	Hz
fop	3dB bandwidth, OpAmp	Hz
If	Maximum current through Rf	A
R1	Input resistor	Ω
R2	Current stabilizer	Ω
R3	Feedback resistor	Ω
R4	Resistor	Ω
Rf	Feedback resistor	Ω
Rin	Input resistance	Ω
RI	Load resistance	Ω
Ro	Output resistance, OpAmp	Ω
Rout	Output resistance	Ω
Rp	Bias current resistor	Ω
Rs	Voltage divide resistor	Ω
tr	10-90% rise time	s
ΔV_H	Hysteresis	V
VL	Detection threshold, low	V
Vomax	Maximum circuit output	V
VR	Reference voltage	V
Vrate	Maximum voltage rate	V/s
VU	Detection threshold, high	V
Vz1	Zener breakdown 1	V
Vz2	Zener breakdown 2	V

Basic Inverter

Analysis
Equations
OpAmp Circuits
<i>Basic Inverter</i>
Reference

These four equations define the characteristics of a basic inverter. The first equation links the voltage gain **Av** to the feedback resistance **Rf** and input resistance **R1**. The

optimum value of **Rp** is defined by the second equation to minimize output-voltage offset due to input bias current. The first pole frequency **fcp** (i.e., 3dB bandwidth) is defined by the third equation. Small signal rise time **tr** (10 to 90%) is defined by the fourth equation.



$$A_v = \frac{-R_f}{R_1}$$

$$R_p = \frac{R_1 \cdot R_f}{R_1 + R_f}$$

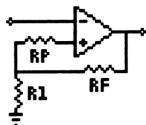
$$f_{CP} = f_{OP} \cdot A_v \cdot \left(\frac{R_1}{R_f} \right)$$

$$t_r = \frac{.35 \cdot R_f}{f_{OP} \cdot A_v \cdot R_1}$$

Non-Inverting Amplifier

Analysis
Equations
OpAmp Circuits
Non-Inverting Amplifier
Reference

These four equations define the properties of a non-inverting amplifier. The first equation expresses the voltage gain A_v in terms of the feedback resistor R_f and resistor



R_1 . The second equation gives the value of R_p needed in the input circuit to minimize offset current effects. The third equation defines the 3dB bandwidth of the circuit in terms of the first pole f_{op} of the OpAmp and A_v , R_1 , and R_f . The final equation expresses the small-signal rise time t_r .

$$A_v = 1 + \frac{R_f}{R_1}$$

$$R_p = \frac{R_1 \cdot R_f}{R_1 + R_f}$$

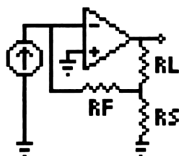
$$f_{CP} = \frac{f_{op} \cdot A_v \cdot R_1}{R_1 + R_f}$$

$$t_r = \frac{.35 \cdot (R_1 + R_f)}{f_{op} \cdot A_v \cdot R_1}$$

Current Amplifier

Analysis
Equations
OpAmp Circuits
Current Amplifier
Reference

Properties of a current amplifier are covered in this section. The first equation shows the



relationship between the current gain A_{ic} with feedback resistance R_f , load resistance R_L , output resistance of OpAmp R_o , voltage divide resistor R_s , and voltage gain A_v . The remaining equations define the input resistance R_{in} and output resistance R_{out} of the system.

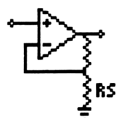
$$A_{ic} = \frac{(R_s + R_f) \cdot A_v}{R_L + R_o + R_s \cdot (1 + A_v)}$$

$$R_{in} = \frac{R_f}{1 + A_v}$$

$$R_{out} = R_s \cdot (1 + A_v)$$

Transconductance Amplifier

Analysis
Equations
OpAmp Circuits
Transconductance Amplifier
Reference



The two equations in this section specify a closed loop transconductance **A_{gc}** and output resistance **R_{out}** in terms of the resistance **R_s** and voltage gain **A_v**.

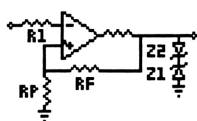
$$A_{gc} = \frac{1}{R_s}$$

$$R_{out} = R_s \cdot (1 + A_v)$$

Level Detector (Inverting)

Analysis
Equations
OpAmp Circuits
Level Detector (Inverting)
Reference

The first equation in this section computes the value of the resistor **R₁** attached to an OpAmp inverting input. The second equation calculates the hysteresis (or memory)



ΔV_H of the level detector circuit. The third and fourth equations define the upper and lower trip voltages **V_U** and **V_L** for an ideal inverting level detector, assuming a reference voltage **V_R** and breakdown voltages **V_{z1}** and **V_{z2}**, in terms of **R_p** and **R_f**.

$$R_1 = \frac{R_p \cdot R_f}{R_p + R_f}$$

$$\Delta V_H = \frac{(V_{z1} + V_{z2}) \cdot R_p}{R_p + R_f}$$

$$V_U = \frac{(V_R \cdot R_f + R_p \cdot V_{z1})}{R_f + R_p}$$

$$V_L = \frac{(V_R \cdot R_f - R_p \cdot V_{z2})}{R_f + R_p}$$

Level Detector (Non-Inverting)

Analysis
Equations
OpAmp Circuits
Level Detector (Non-Invert.)
Reference

The first equation in this section computes the value of the resistor **R1** attached to an OpAmp non-inverting input. The second equation calculates the hysteresis (or memory) ΔV_H of the level detector circuit. The third and fourth equations define the upper and lower trip voltages **VU** and **VL** for an ideal inverting level detector, assuming a reference voltage **VR** and breakdown voltages **Vz1** and **Vz2**, in terms of **Rp** and **Rf**.

$$R1 = \frac{R_P \cdot R_f}{R_P + R_f}$$

$$\Delta V_H = \frac{(V_{z1} + V_{z2}) \cdot R_P}{R_P + R_f}$$

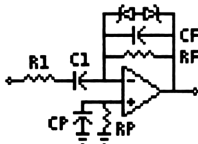
$$V_U = \frac{(V_R \cdot (R_f + R_P) + R_P \cdot V_{z1})}{R_f}$$

$$V_L = \frac{(V_R \cdot (R_P + R_f) - R_P \cdot V_{z2})}{R_f}$$

Differentiator

Analysis
Equations
OpAmp Circuits
Differentiator
Reference

These design equations represent all the components needed for a differentiator. The first equation defines the feedback resistor **Rf** in terms of the maximum output voltage **Vomax** and current **If**. Typically, **If** is of the order of 0.1 - 0.5 mA. The second equation computes the value for the resistor **Rp** used to cancel the effects of OpAmp input bias current. **C1** is the input capacitor required for the differentiator, and **R1** is the resistor utilized for stability. The characteristic frequency of the differentiator **fd** is expressed by the fifth equation. The last two equations compute the bypass capacitor **Cp** and the feedback capacitor **Cf**.



$$R_f = \frac{V_{omax}}{I_f}$$

$$R_P = R_f$$

$$C1 = \frac{V_{omax}}{R_f \cdot V_{rate}}$$

$$R1 = \frac{1}{2 \cdot \pi \cdot f_d \cdot C1}$$

$$f_d = \frac{1}{2 \cdot \pi \cdot R_f \cdot C1}$$

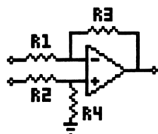
$$C_P = \frac{10}{2 \cdot \pi \cdot f_0 \cdot R_P}$$

$$C_f = \frac{1}{4 \cdot \pi \cdot f_0 \cdot R_f}$$

Differential Amplifier

Analysis
Equations
OpAmp Circuits
Differential Amplifier
Reference

These four equations show the primary relationships involved in the design of a differential amplifier. The first equation computes the differential gain **Ad** in terms of the input and feedback resistors **R1** and **R3**. The second equation shows the common-mode gain **Aco** in terms of **R3**, **R1**, and the common-mode rejection ratio **CMMR**. The third equation expands the definition of **Ad** from the first equation to accommodate a practical OpAmp with a finite voltage gain **Av**. The final equation shows the common-mode gain due to resistor mismatching.



$$A_d = \frac{R_3}{R_1}$$

$$A_{co} = \frac{R_3^2}{R_3 \cdot (R_1 + R_3) \cdot \text{CMMR}}$$

$$A_d = \frac{A_v \cdot R_3}{\sqrt{R_1^2 \cdot A_v^2 + R_3^2}}$$

$$A_{cc} = \frac{(R_4 \cdot R_1 - R_2 \cdot R_3)}{R_1 \cdot (R_2 + R_4)}$$

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Chapter 28

Solid State Devices

Analysis
Equations
<i>Solid State Devices</i>
Reference

This chapter covers equations describing a variety of solid state devices.

- ☐ Semiconductor Basics
- ☐ PN Junctions
- ☐ PN Junction Currents
- ☐ Transistor Currents
- ☐ Eber-Moll Equations
- ☐ Ideal Currents - pnp
- ☐ Switching Transients
- ☐ MOS Transistor I
- ☐ MOS Transistor II
- ☐ MOS Inverter (Resistive)
- ☐ MOS Inverter (Saturated)
- ☐ MOS Inverter (Depletion)
- ☐ CMOS Transistor Pair
- ☐ Junction FET

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
α	CB current gain	unitless
a	Linearly graded junction parameter	$1/m^4$
A	Area	m^2
A_1	EB junction area	m^2
A_2	CB junction area	m^2
α_f	Forward α	unitless
A_j	Junction area	m^2
α_r	Reverse α	unitless

β	CE current gain	unitless
b	Channel width	m
β_f	Forward β	unitless
β_r	Reverse β	unitless
Cj	Junction capacitance	F
CL	Load capacitance	F
Cox	Oxide capacitance per unit area	F/m ²
D	Diffusion coefficient	m ² /s
DB	Base diffusion coefficient	m ² /s
DC	Collector diffusion coefficient	m ² /s
DE	Emitter diffusion coefficient	m ² /s
Dn	n diffusion coefficient	m ² /s
Dp	p diffusion coefficient	m ² /s
ϵ_{ox}	Oxide permittivity	unitless
ϵ_s	Permittivity	unitless
Ec	Conduction band	J
EF	Fermi level	J
Ei	Intrinsic Fermi level	J
Ev	Valence band	J
fmax	Maximum frequency	Hz
γ	Body coefficient	V ^{.5}
gd	Drain conductance	S
gm	Transconductance	S
gmL	Transconductance, load device	S
Go	Conductance	S
I	Junction current	A
IO	Saturation current	A
IB	Base current	A
IC	Collector current	A
ICB0	CB leakage, E open	A
ICE0	CE leakage, B open	A
ICsat	Collector I at saturation edge	A
ID	Drain current	A
ID λ	Channel modulation drain current	A
ID0	Drain current	A
IDSat	Drain saturation current	A
IE	Emitter current	A
If	Forward current	A
Ir	Reverse current	A
Ir0	E-M reverse current component	A
IRG	G-R current	A
IRG0	Zero bias G-R current	A
λ	Modulation parameter	1/V
Is	Saturation current	A
kD	MOS constant, driver	A/V ²

kL	MOS constant, load	A/V^2
kn	MOS constant	A/V^2
kn1	MOS process constant	A/V^2
kN	MOS constant, n channel	A/V^2
kP	MOS constant, p channel	A/V^2
KR	Ratio	unitless
L	MOS transistor length	m
LC	Diffusion length, collector	m
LD	Drive transistor length	m
LE	Diffusion length, emitter	m
LL	Load transistor length	m
Ln	Diffusion length, n	m
IN	n-channel length	m
Lp	Diffusion length, p	m
lP	p-channel length	m
μ_n	n mobility	$m^2/(V*s)$
μ_p	p mobility	$m^2/(V*s)$
mn	n effective mass	unitless
mp	p effective mass	unitless
N	Doping concentration	$1/m^3$
Na	Acceptor density	$1/m^3$
nC	n density, collector	$1/m^3$
Nd	Donor density	$1/m^3$
nE	n density, emitter	$1/m^3$
ni	Intrinsic density	$1/m^3$
N0	Surface concentration	$1/m^3$
npo	n density, p type	$1/m^3$
p	p density	$1/m^3$
pB	p density, base	$1/m^3$
ϕ_F	Fermi potential	V
ϕ_{GC}	Work function potential	V
pno	p density, n type	$1/m^3$
Q	Total surface impurities	unitless
Qb	Bulk charge at bias	C/m^2
Qb0	Bulk charge at 0 bias	C/m^2
Qox	Oxide charge density	C/m^2
Qsat	Base Q, transition edge	C
ρ_n	n resistivity	$\Omega*m$
ρ_p	p resistivity	$\Omega*m$
RI	Load resistance	Ω
τ_B	lifetime in base	s
τ_D	Time constant	s
τ_L	Time constant	s
τ_o	Lifetime	s
τ_p	Minority carrier lifetime	s

τ_t	Base transit time	s
t	Time	s
T	Temperature	K
t_{ch}	Charging time	s
t_{dis}	Discharge time	s
t_{ox}	Gate oxide thickness	m
t_r	Collector current rise time	s
t_s	Charge storage time	s
t_{sd1}	Storage delay, turn off	s
t_{sd2}	Storage delay, turn off	s
T_{tr}	Transit time	s
V_1	Input voltage	V
V_a	Applied voltage	V
V_{bi}	Built-in voltage	V
V_{BE}	BE bias voltage	V
V_{CB}	CB bias voltage	V
V_{CC}	Collector supply voltage	V
V_{CEsat}	CE saturation voltage	V
V_{DD}	Drain supply voltage	V
V_{DS}	Drain voltage	V
$V_{Ds_{at}}$	Drain saturation voltage	V
V_{EB}	EB bias voltage	V
V_G	Gate voltage	V
V_{GS}	Gate to source voltage	V
V_{IH}	Input high	V
V_{in}	Input voltage	V
V_{IL}	Input low voltage	V
V_L	Load voltage	V
V_M	Midpoint voltage	V
V_{OH}	Output high	V
V_{OL}	Output low	V
V_o	Output voltage	V
V_p	Pinchoff voltage	V
V_{SB}	Substrate bias	V
V_T	Threshold voltage	V
V_{T0}	Threshold voltage at 0 bias	V
V_{TD}	Depletion transistor threshold	V
V_{TL}	Load transistor threshold	V
V_{TL0}	Load transistor threshold	V
V_{TN}	n channel threshold	V
V_{TP}	p channel threshold	V
W	MOS transistor width	m
W_B	Base width	m
W_D	Drive transistor width	m
W_L	Load transistor width	m

WN	n-channel width	m
WP	p-channel width	m
x	Depth from surface	m
xd	Depletion layer width	m
xn	Depletion width, n side	m
xp	Depletion width, p side	m
Z	JFET width	m

Semiconductor Basics

Analysis

Equations

Solid State Devices

Semiconductor Basics

Reference

Nine equations form the foundation of this module. The first two equations define the resistivities ρ_n and ρ_p of n- and p-type semiconductor material in terms of the electron and hole mobilities μ_n and μ_p and doping densities N_d and N_a . The third and fourth equations connect the electron and hole diffusion coefficients D_n and D_p , using the so-called Einstein's relationship in terms of μ_n and μ_p and temperature T . The next two equations compute the Fermi level E_F relative to the intrinsic Fermi Level E_i in terms of temperature T , N_a or N_d , and the intrinsic carrier density n_i . The intrinsic Fermi level E_i is calculated by the seventh equation in terms of the conduction and valence band levels E_c and E_v , temperature T and the effective masses m_p and m_n of holes and electrons. The eighth equation illustrates the diffusion of impurities in a semiconductor subject to an infinite source with a surface concentration N_0 at a depth x below the surface after a time t , given the diffusion coefficient D . The diffusion equation in this case follows the complementary error function distribution. The final equation details the diffusion from a finite impurity source Q over a surface area A with the classic Gaussian distribution.

$$\rho_n = \frac{1}{q \mu_n N_d}$$

$$\rho_p = \frac{1}{q \mu_p N_a}$$

$$\frac{D_n}{\mu_n} = \frac{k \cdot T}{q}$$

$$\frac{D_p}{\mu_p} = \frac{k \cdot T}{q}$$

$$E_i - E_F = k \cdot T \cdot \ln \left(\frac{N_a}{n_i} \right)$$

$$E_F - E_i = k \cdot T \cdot \ln \left(\frac{N_d}{n_i} \right)$$

$$E_i = \frac{(E_c + E_v)}{2} + \frac{3}{4} \cdot (k \cdot T) \cdot \ln \left(\frac{m_p}{m_n} \right)$$

$$N = N_0 \cdot \text{ERFC} \left(\frac{x}{2 \cdot \sqrt{D \cdot t}} \right)$$

$$N = \frac{Q}{A \cdot \sqrt{\pi \cdot D \cdot t}} \cdot e^{-\frac{x^2}{4 \cdot D \cdot t}}$$

PN Junctions

Analysis
Equations
Solid State Devices
<i>PN Junctions</i>
Reference

These seven equations cover the properties of PN junctions. The first equation shows the calculation for the built-in voltage **V_{bi}** for a step junction in terms of temperature **T**, the doping densities **N_d** and **N_a**, and the intrinsic density **n_i**. The next three equations focus on the depletion layers **x_n** and **x_p** in the p and the n regions of the PN junction in terms of the dielectric constant **ε_s**, doping densities **N_d** and **N_a**, built-in voltage **V_{bi}** and the applied voltage **V_a**. The variable **x_d** represents the total depletion region width for a given applied voltage. The fifth equation shows the capacitance **C_j** of a PN junction in terms of **ε_s**, junction area **A_j** and **x_d**. The last two equations calculate **V_{bi}** and **x_d** for a linearly-graded junction with a gradient parameter **a**.

$$V_{bi} = \frac{k \cdot T}{q} \cdot \ln \left(\frac{N_d \cdot N_a}{n_i^2} \right)$$

$$x_n = \sqrt{\frac{2 \cdot \epsilon_s \cdot \epsilon_0 \cdot \text{ABS}(V_{bi} - V_a)}{q} \cdot \frac{N_a}{N_d \cdot (N_a + N_d)}}$$

$$x_p = \frac{N_d}{N_a} \cdot x_n$$

$$x_d = x_n + x_p$$

$$C_j = \frac{\epsilon_s \cdot \epsilon_0 \cdot A_j}{x_d}$$

$$V_{bi} = \frac{2 \cdot k \cdot T}{q} \cdot \ln \left(\frac{a \cdot x_d}{2 \cdot n_i} \right)$$

$$x_d = \left(\frac{12 \cdot \epsilon_s \cdot \epsilon_0}{q \cdot a} \cdot \text{ABS}(V_{bi} - V_a) \right)^{\frac{1}{3}}$$

PN Junction Currents

Analysis
Equations
Solid State Devices
<i>PN Junction Currents</i>
Reference

Eight equations characterize many of the relationships that play a key role in computing currents in PN junctions. The first two equations show the current in two alternate forms. First, the junction current **I** in terms of the junction area **A_j**, diffusion coefficients **D_n** and **D_p**, diffusion lengths **L_n** and **L_p**, equilibrium densities of minority carriers **n_{po}** and **p_{no}**, applied bias **V_a**, and temperature **T**. The second equation is a simplified form of the first equation in which **I₀** is defined as the multiplier of the exponential term. The third equation calculates this saturation current **I₀**. The so-called Generation-Recombination current **IRG₀** at 0 bias is calculated by the fourth equation in terms of junction area **A_j**, average recombination time **τ₀**, intrinsic density **n_i**, depletion width

xd. On applying a voltage V_a , this generation recombination current I_{RG} increases exponentially, as shown by the fifth equation. The next equation computes G_0 , the small signal conductance, in terms of temperature T and currents I and I_0 . The last two equations synthesize the charge storage time t_s when the diode current is switched externally from I_f to I_r . It is seen from these two equations that t_s depends strongly upon the minority carrier lifetime τ_p .

$$\begin{aligned}
 I &= q \cdot A \cdot j \cdot \left(\frac{D_n}{L_n} \cdot n_{p0} + \frac{D_p}{L_p} \cdot p_{n0} \right) \cdot \left(e^{\frac{q \cdot V_a}{k \cdot T}} - 1 \right) & I &= I_0 \cdot \left(e^{\frac{q \cdot V_a}{k \cdot T}} - 1 \right) \\
 I_0 &= q \cdot A \cdot j \cdot \left(\frac{D_n}{L_n} \cdot n_{p0} + \frac{D_p}{L_p} \cdot p_{n0} \right) & I_{RG0} &= \frac{-q \cdot A \cdot j \cdot n_i \cdot x_d}{2 \cdot \tau_0} \\
 I_{RG} &= \frac{q \cdot A \cdot j \cdot n_i \cdot x_d}{2 \cdot \tau_0} \cdot \left(e^{\frac{q \cdot V_a}{2 \cdot k \cdot T}} - 1 \right) & G_0 &= \frac{q}{k \cdot T} \cdot (I + I_0) \\
 t_s &= \tau_p \cdot \ln \left(1 + \frac{I_f}{I_r} \right) & ERF \left(\sqrt{\frac{t_s}{\tau_p}} \right) &= \frac{1}{1 + \frac{I_r}{I_f}}
 \end{aligned}$$

Transistor Currents

Analysis
Equations
Solid State Devices
Transistor Currents
Reference

The seven equations in this section show top-level relationships between the emitter, base and collector currents I_E , I_B and I_C , respectively. The first equation defines the common base current gain α as the ratio of I_C to I_E . The second equation defines the common emitter current gain β in terms of α . The third equation represents Kirchoff's current law for the transistor. The next three equations represent alternate forms of the collector current in terms of α , I_E , I_B , β and the leakage currents I_{CE} , and I_{CB0} . The final equation links I_{CE0} and I_{CB0} in terms of β .

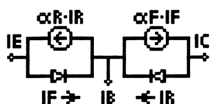
$$\begin{aligned}
 \alpha &= \frac{I_C}{I_E} & \beta &= \frac{\alpha}{1 - \alpha} & I_E &= I_B + I_C \\
 I_C &= \alpha \cdot I_E + I_{CB0} & I_C &= \frac{\alpha}{1 - \alpha} \cdot I_B + \frac{I_{CB0}}{1 - \alpha} & I_C &= \beta \cdot I_B + I_{CE0}
 \end{aligned}$$

$$I_{CE0} = I_{CB0} \cdot (\beta + 1)$$

Ebers-Moll Equations

Analysis
Equations
Solid State Devices
Ebers-Moll Equations
Reference

These ten equations show a collection of relevant relationships developed by J. J. Ebers and J. L. Moll in the mid-1950s recognizing the basic reciprocal behavior of a bipolar transistor. The first three equations connect the emitter, collector and base currents I_E , I_C and I_B in terms of forward and reverse current gain α_f and α_r and forward and reverse currents I_f and I_r . The corresponding common emitter current gains in the forward and reverse directions are given by β_f and β_r , in terms of α_f and α_r . The reciprocity relationships between



α_f and α_r , I_f and I_r , and the saturation current I_s are defined by the next two equations. The last three equations help define I_{CE0} and I_{CB0} in terms of α_f , α_r , and I_{r0} .

$$I_E = I_f - \alpha_r \cdot I_r \quad I_C = \alpha_f \cdot I_f - I_r \quad I_B = (1 - \alpha_f) \cdot I_f + (1 - \alpha_r) \cdot I_r$$

$$\beta_f = \frac{\alpha_f}{1 - \alpha_f}$$

$$\beta_r = \frac{\alpha_r}{1 - \alpha_r}$$

$$\alpha_f \cdot I_f = I_s$$

$$\alpha_r \cdot I_r = I_s$$

$$I_{CB0} = (1 - \alpha_r \cdot \alpha_f) \cdot I_{r0}$$

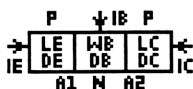
$$I_{CE0} = I_{CB0} \cdot (\beta_f + 1)$$

$$I_{CE0} = \frac{I_{r0} \cdot (1 - \alpha_f \cdot \alpha_r)}{1 - \alpha_f}$$

Ideal Currents - pnp

Analysis
Equations
Solid State Devices
Ideal Currents - pnp
Reference

The four equations in this set form the basis of transistor action resulting in emitter, base and collector currents in a pnp transistor. The first three equations show the emitter, collector and base currents I_E , I_C , and I_B in terms of emitter base area A_1 , diffusion coefficients D_E , D_B , and D_C , the minority carrier densities



n_E , p_B , and n_C , emitter and collector diffusion lengths L_E and L_C , base width W_B , emitter-base and collector base voltages V_{BE} and V_{BC} , base collection junction A_2 and temperature T . The last equation shows the

relationship between α , DB , pB , WB , DE , nE and LE . The corresponding equations for an npn transistor can be derived from this equation set by proper use of sign conventions.

$$\begin{aligned}
 I_E &= q \cdot A_1 \cdot \left(\frac{\text{DE} \cdot \text{nE}}{\text{LE}} + \frac{\text{DB} \cdot \text{pB}}{\text{WB}} \right) \cdot \left(e^{\frac{q \cdot V_{EB}}{k \cdot T}} - 1 \right) - q \cdot A_2 \cdot \frac{\text{DB}}{\text{WB}} \cdot \text{pB} \cdot \left(e^{\frac{q \cdot V_{CB}}{k \cdot T}} - 1 \right) \\
 I_C &= \frac{q \cdot A_1 \cdot \text{DB} \cdot \text{pB}}{\text{WB}} \cdot \left(e^{\frac{q \cdot V_{EB}}{k \cdot T}} - 1 \right) - q \cdot A_2 \cdot \left(\frac{\text{DC} \cdot \text{nC}}{\text{LC}} + \frac{\text{DB} \cdot \text{pB}}{\text{WB}} \right) \cdot \left(e^{\frac{q \cdot V_{CB}}{k \cdot T}} - 1 \right) \\
 I_B &= \frac{q \cdot A_1 \cdot \text{DE}}{\text{LE}} \cdot \text{nE} \cdot \left(e^{\frac{q \cdot V_{EB}}{k \cdot T}} - 1 \right) + \frac{q \cdot A_2 \cdot \text{DC}}{\text{LC}} \cdot \text{nC} \cdot \left(e^{\frac{q \cdot V_{CB}}{k \cdot T}} - 1 \right) \\
 \alpha &= \frac{\frac{\text{DB} \cdot \text{pB}}{\text{WB}}}{\frac{\text{DB} \cdot \text{pB}}{\text{WB}} + \frac{\text{DE} \cdot \text{nE}}{\text{LE}}}
 \end{aligned}$$

Switching Transients

Analysis
Equations
Solid State Devices
Switching Transients
Reference

These six equations show the key relationships in determining switching response times of bipolar transistors. The first equation shows the base charge at the edge of saturation Q_{sat} in terms of collector saturation current $I_{C\text{sat}}$ and base transit time τ_t . The collector saturation is determined (approximately) by the second equation in terms of supply voltage V_{CC} and load resistance R_{LD} . The third equation calculates the turn-on transient time τ_r in terms of base recombination time τ_B , $I_{C\text{sat}}$, base current I_B and base transit time τ_t . The next equation computes the storage delay τ_{sd1} when the bipolar transistor is switched from the saturation region to cutoff by switching base current from I_B to 0. The penultimate equation shows the storage delay τ_{sd2} when the base current is switched from I_B to $-I_B$. The final equation computes the saturation voltage $V_{CE\text{sat}}$, the voltage drop between the collector and the emitter under full saturation, in terms of the collector and base currents I_C and I_B and the forward and reverse α 's α_f and α_r .

$$Q_{sat} = I_{Csat} \cdot \tau_t$$

$$I_{Csat} = \frac{V_{CC}}{R_1}$$

$$t_r = \tau_B \cdot \text{LN} \left(\frac{1}{1 - \frac{I_{Csat} \cdot \tau_t}{I_B \cdot \tau_B}} \right)$$

$$t_{sd1} = \tau_B \cdot \text{LN} \left(\frac{I_B \cdot \tau_B}{I_{Csat} \cdot \tau_t} \right)$$

$$t_{sd2} = \tau_B \cdot \text{LN} \left(\frac{2 \cdot I_B \cdot \tau_B}{I_{Csat} \cdot \tau_t \cdot \left(1 + \frac{I_B \cdot \tau_B}{I_{Csat} \cdot \tau_t} \right)} \right)$$

$$V_{CEsat} = \frac{k \cdot T}{q} \cdot \text{LN} \left(1 + \frac{\frac{I_C}{I_B} \cdot (1 - \alpha_r)}{\alpha_r \cdot \left(1 - \frac{\frac{I_C}{I_B} \cdot (1 - \alpha_f)}{\alpha_f} \right)} \right)$$

MOS Transistor I

Analysis

Equations

Solid State Devices

MOS Transistor I

Reference

The seven equations in this section form the basic equations of charge, capacitance and threshold voltage for a MOS transistor. The first equation shows the Fermi potential ϕ_F defined in terms of temperature T , the intrinsic carrier density n_i , and the hole density p . The second equation shows the depletion layer x_d at the surface of a p-type semiconductor in terms of the relative dielectric constant ϵ_s , Fermi potential ϕ_F , and doping density N_a . The third equation computes the charge density Q_{b0} accumulated at the surface of the semiconductor due to band bending. The fourth equation shows how surface charge density Q_b is influenced by the substrate bias V_{SB} . A thin oxide layer with a thickness t_{ox} on the surface of the semiconductor results in a capacitance C_{ox} per unit area. The sixth equation defines the body coefficient γ in terms of C_{ox} , N_a , and ϵ_s . The final equation computes the threshold voltage for a MOS system with a work function potential of ϕ_{GC} and residual oxide charge density Q_{ox} .

$$\phi_F = \frac{k \cdot T}{q} \cdot \text{LN} \left(\frac{n_i}{p} \right)$$

$$x_d = \sqrt{\frac{2 \cdot \epsilon_s \cdot \epsilon_0 \cdot (2 \cdot \phi_F)}{q \cdot N_a}}$$

$$Q_{b0} = -\sqrt{2 \cdot q \cdot N_a \cdot \epsilon_s \cdot \epsilon_0 \cdot \text{ABS}(2 \cdot \phi_F)}$$

$$Q_b = -\sqrt{2 \cdot q \cdot N_a \cdot \epsilon_s \cdot \epsilon_0 \cdot \text{ABS}(-2 \cdot \phi_F + V_{SB})}$$

$$C_{ox} = \frac{\epsilon_{ox} \cdot \epsilon_0}{t_{ox}}$$

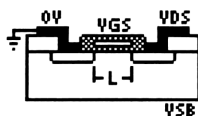
$$\gamma = \frac{1}{C_{ox}} \cdot \sqrt{2 \cdot q \cdot N_A \cdot \epsilon_s \cdot \epsilon_0}$$

$$V_{T0} = \phi_{GC} - 2 \cdot \phi_F - \frac{Q_{b0}}{C_{ox}} - \frac{Q_{ox}}{C_{ox}}$$

MOS Transistor II

Analysis
Equations
Solid State Devices
MOS Transistor II
Reference

These eleven equations describe the performance characteristics of a MOS transistor. The first two equations give two alternate forms for the process constant **kn1** in terms of electron mobility μ_n , oxide capacitance per unit area **Cox**, relative oxide permittivity ϵ_{ox} , and oxide thickness **tox**. The third equation links the process constant **kn1** to the device constant **kn**, device length **L**, and width **W**. The fourth equation defines the drain current **ID** when saturated in terms of **kn**, gate voltage **VGS**, threshold voltage **VT**, conductance parameter λ , and drain voltage **VDS**. The fifth equation computes **ID** under linear or saturated conditions in terms of **kn**, **VGS**, **VT**, and **VDS**. The expression for the threshold voltage **VT** is defined in terms of zero substrate bias threshold voltage **VTO**, body coefficient γ , substrate bias



VSB, and Fermi potential ϕ_F . The last four equations calculate performance parameters such as transconductance **gm**, transit time through the channel **Ttr**, maximum frequency of operation **fmax**, and drain conductance **gd**.

$$kn1 = \mu_n \cdot C_{ox}$$

$$kn1 = \frac{\mu_n \cdot \epsilon_{ox} \cdot \epsilon_0}{t_{ox}}$$

$$kn = \frac{kn1 \cdot W}{L}$$

$$ID = \frac{kn}{2} \cdot (V_{GS} - V_T)^2 \cdot (1 + \lambda \cdot V_{DS})$$

$$ID = IFTE \left(V_{GS} - V_T \leq V_{DS}, \frac{kn}{2} \cdot \left(2 \cdot (V_{GS} - V_T) \cdot V_{DS} - V_{DS}^2 \right), \frac{kn}{2} \cdot (V_{GS} - V_T)^2 \right)$$

$$V_T = V_{T0} + \gamma \cdot \left(\sqrt{ABS(-2 \cdot \phi_F + V_{SB})} - \sqrt{2 \cdot \phi_F} \right)$$

$$g_m = kn \cdot (V_{GS} - V_T)$$

$$T_{tr} = \frac{\frac{4}{3} \cdot L^2}{\mu_n \cdot (V_{GS} - V_T)}$$

$$f_{max} = \frac{g_m}{2 \cdot \pi \cdot C_{ox} \cdot W \cdot L}$$

$$g_d = kn \cdot (V_{GS} - V_T)$$

MOS Inverter (Resistive)

Analysis
Equations
Solid State Devices
<i>MOS Inverter (Resistive)</i>
Reference

These five equations represent the design equations for a MOS inverter with a resistive load. The first equation specifies the device constant **kD** for the driver transistor in terms of its gate capacitance **Cox**, mobility **μn**, width **WD**, and channel length **LD**. The second equation specifies the output voltage when input to the driver is below the threshold voltage. The third equation determines **VOL**, the output low voltage when the input is driven high. This equation is a quadratic in **VOL**, and the solution is meaningful for positive values of **VOL**. The next equation computes **VIH** in the linear region of the drain current equation. The final equation computes the midpoint voltage **VM** for which the driver transistor is in saturation.

$$k_D = \frac{\mu_n \cdot C_{ox} \cdot W_D}{L_D} \qquad V_{OH} = V_{DD}$$

$$V_{OL}^2 - 2 \cdot \left(\frac{1}{k_D \cdot R_1} + V_{DD} - V_T \right) \cdot V_{OL} + \frac{2 \cdot V_{DD}}{k_D \cdot R_1} = 0$$

$$\frac{k_D}{2} \cdot \left(2 \cdot (V_{IH} - V_T) \cdot V_O - V_O^2 \right) = \frac{(V_{DD} - V_O)}{R_1}$$

$$\frac{k_D}{2} \cdot (V_M - V_T)^2 = \frac{(V_{DD} - V_M)}{R_1}$$

MOS Inverter (Saturated)

Analysis
Equations
Solid State Devices
<i>MOS Inverter (Saturated)</i>
Reference

A MOS inverter with a saturated enhancement transistor load is the focus of this section. The first two equations define the device constants for the load transistor (**kL**, **WL**, **LL**) and the driver transistor (**kD**, **WD**, **LD**) in terms of the process parameters, namely mobility **μn** and gate capacitance per unit area **Cox**. The third equation defines the geometry ratio **KR** of the load and drive transistors. Output high **VOH** is calculated in terms of **VDD**, **VTO** and **γ**. The next equation defines the input voltage **Vin** in terms of **KR**, **VDD**, threshold of the load and drive transistors **VTL** and **VTD**. The sixth equation defines the threshold voltage of the load transistor. The equation that follows computes

the input high **VIH** in terms of **VDD**, **VTL**, **KR** and **VTO**. The output voltage **Vo** is computed in terms of **VDD**, **VTL**, **VTO** and **KR**. The last five equations show the performance parameters of the inverter circuit. The equation for **gmL** defines the transconductance of the load circuit while the equation for **τL** defines the characteristic time to charge the load capacitance **CL**. The charging time **tch** is the time required for the output rise to move from **Vo** to **V1**. The final two equations focus on the characteristic time **τD** and discharge time **tdis** for the circuit.

$$\begin{aligned}
 k_L &= \frac{\mu_n \cdot C_{ox} \cdot W_L}{L_L} & k_D &= \frac{\mu_n \cdot C_{ox} \cdot W_D}{L_D} & K_R &= \frac{k_D}{k_L} \\
 V_{OH} &= V_{DD} - \left(V_{T0} + \gamma \cdot \left(\sqrt{V_{OH} + 2 \cdot \phi_F} - \sqrt{2 \cdot \phi_F} \right) \right) \\
 K_R \cdot \left(2 \cdot (V_{in} - V_{TD}) \cdot V_o - V_o^2 \right) &= (V_{DD} - V_o - V_{TL})^2 \\
 V_{TL} &= V_{T0} + \gamma \cdot \left(\sqrt{V_o + 2 \cdot \phi_F} - \sqrt{2 \cdot \phi_F} \right) & V_{IH} &= \frac{2 \cdot (V_{DD} - V_{TL})}{\sqrt{3 \cdot K_R + 1}} + V_{T0} \\
 V_o &= \frac{(V_{DD} - V_{TL} + V_{T0} + V_{T0} \cdot \sqrt{K_R})}{1 + \sqrt{K_R}} & g_{mL} &= k_L \cdot (V_{DD} - V_{TL}) \\
 \tau_L &= \frac{C_L}{g_{mL}} & t_{ch} &= \tau_L \cdot \left(\frac{V_1}{V_o} - 1 \right) & \tau_D &= \frac{C_L}{k_D \cdot (V_1 - V_{T0})} \\
 t_{dis} &= \tau_D \cdot \left(\frac{2 \cdot V_{TD}}{V_1 - V_{TD}} + \ln \left(\frac{2 \cdot (V_1 - V_{TD})}{V_o} - 1 \right) \right)
 \end{aligned}$$

MOS Inverter (Depletion)

These six equations are the design equations for a MOS inverter with a depletion load. The first two equations compute device constants **kL** and **kD** for the load and the driver transistors in terms of their geometries **WD**, **WL**, **LD**, and **LL**. At the output low and output high, **VOL** and **VOH**, the driver is in the linear region while the load device is saturated. The fourth equation computes the threshold voltage **VTL** for the load transistor in terms of its zero bias threshold **VTL0**, Fermi potential **φF**, and body coefficient **γ**. The fifth equation shows the

Analysis
Equations
Solid State Devices
MOS Inverter (Depletion)
Reference

charging time for the capacitive load. The last equation computes current in the depletion load device I_0 .

$$k_L = \frac{\mu_n \cdot C_{ox} \cdot W_L}{L_L} \qquad k_D = \frac{\mu_n \cdot C_{ox} \cdot W_D}{L_D}$$

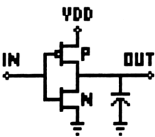
$$\frac{k_D}{2} \cdot (2 \cdot (V_{OH} - V_{T0}) \cdot V_{OL} - V_{OL}^2) = \frac{k_L}{2} \cdot V_{TL}^2$$

$$V_{TL} = V_{TL0} + \gamma \cdot (\sqrt{V_0 + 2 \cdot \phi_F} - \sqrt{2 \cdot \phi_F}) \qquad t_{ch} = \frac{C_L \cdot V_L}{I_0} \qquad I_0 = k_L \cdot V_{TL}^2$$

CMOS Transistor Pair

Analysis
 Equations
 Solid State Devices
CMOS Transistor Pair
 Reference

These five equations describe the properties of a CMOS inverter. The first two equations



compute device parameters for n and p channel devices. The next two equations compute input voltages **VIH** and **VIL**. The last equation compute **Vin** when the n-channel driver is in saturation and the p-channel device is in the linear region.

$$k_P = \frac{\mu_n \cdot C_{ox} \cdot W_P}{L_P} \qquad k_N = \frac{\mu_P \cdot C_{ox} \cdot W_N}{L_N}$$

$$V_{IH} = 2 \cdot V_0 + V_{TN} + \frac{\frac{k_P}{k_N} \cdot (V_{DD} - ABS(V_{TP}))}{1 + \frac{k_P}{k_N}}$$

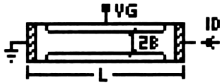
$$V_{IL} = \frac{\left(2 \cdot V_0 - V_{DD} - V_{TP} + \frac{k_N}{k_P} \cdot V_{TN} \right)}{1 + \frac{k_N}{k_P}}$$

$$\frac{k_N}{2} \cdot (V_{in} - V_{TN})^2 = \frac{k_P}{2} \cdot (V_{DD} - V_{in} - ABS(V_{TP}))^2$$

Junction FET

Analysis
Equations
Solid State Devices
Junction FET
Reference

These five equations describe the characteristics of a symmetrical junction field effect transistor. The first equation stipulates the drain current I_D in terms of the electron mobility μ_n , doping density N_d , channel width b , channel length L , channel depth Z , supply voltage V_{DD} , pinch-off voltage V_p , gate voltage V_G , and built-in voltage V_{bi} . The channel height b is related to the



dielectric constant ϵ_s , N_d , V_{bi} , and drain saturation voltage V_{Dsat} . The last two equations show the relationship for drain voltage and drain current upon saturation.

$$I_D = \frac{2 \cdot q \cdot Z \cdot \mu_n \cdot N_d \cdot b}{L} \cdot \left[V_{DD} - \frac{2}{3} \cdot (V_{bi} - V_p) \cdot \left[\left(\frac{V_{DD} + V_{bi} - V_G}{V_{bi} - V_p} \right)^{1.5} - \left(\frac{V_{bi} - V_G}{V_{bi} - V_p} \right)^{1.5} \right] \right]$$

$$I_{Dsat} = \frac{2 \cdot q \cdot Z \cdot \mu_n \cdot N_d \cdot b}{L} \cdot \left[V_{Dsat} - \frac{2}{3} \cdot (V_{bi} - V_p) \cdot \left[\left(\frac{V_{DD} + V_{bi} - V_G}{V_{bi} - V_p} \right)^{1.5} - \left(\frac{V_{bi} - V_G}{V_{bi} - V_p} \right)^{1.5} \right] \right]$$

$$b = \sqrt{\frac{2 \cdot \epsilon_0 \cdot \epsilon_s}{q \cdot N_d} \cdot (V_{bi} + V_{Dsat} - V_G)}$$

$$V_{Dsat} = V_G - V_p$$

$$I_{Dsat} = I_{D0} \cdot \left(1 - \frac{V_G}{V_p} \right)^2$$

Chapter 29

Linear Amplifiers

Analysis
Equations
<i>Linear Amplifiers</i>
Reference

In this chapter, linear circuit models (sometimes called small signal models) are used to make first level computations for amplifiers using bipolar or junction transistors. Device configurations include Darlington connections, emitter-coupled pair, differential amplifier and a source-coupled pair.

- ☐ BJT (Common Base)
- ☐ BJT (Common Emitter)
- ☐ BJT (Common Collector)
- ☐ FET (Common Gate)
- ☐ FET (Common Source)
- ☐ FET (Common Drain)
- ☐ Darlington (CC-CC)
- ☐ Darlington (CC-CE)
- ☐ Emitter-Coupled Amplifier
- ☐ Differential Amplifier
- ☐ Source-Coupled JFET Pair

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
α_0	Current gain, CE	unitless
A_c	Common mode gain	unitless
A_d	Differential mode gain	unitless
A_i	Current gain, CB	unitless
A_{ov}	Overall voltage gain	unitless
A_v	Voltage gain, CC/CD	unitless
β_0	Current gain, CB	unitless
CMMR	Common mode reject ratio	unitless
gm	Transconductance	S

μ	Amplification factor	unitless
r_b	Base resistance	Ω
r_c	Collector resistance	Ω
r_d	Drain resistance	Ω
r_e	Emitter resistance	Ω
RBA	External base resistance	Ω
RCA	External collector resistance	Ω
RDA	External drain resistance	Ω
REA	External emitter resistance	Ω
RG	External gate resistance	Ω
Ric	Common mode input resistance	Ω
Rid	Differential input resistance	Ω
Rin	Input resistance	Ω
RI	Load resistance	Ω
Ro	Output resistance	Ω
Rs	Source resistance	Ω

BJT (Common Base)

Analysis
Equations
Linear Amplifiers
BJT (Common Base)
Reference

These six equations represent properties of a transistor amplifier connected in the common base configuration at mid frequencies. The first equation connects common base current gain α_0 with common emitter current gain β_0 . The second equation computes the input impedance **Rin** at the input terminals of the amplifier. **Ro** represents the output resistance and **Ai** the current gain. The final two equations cover the voltage gain **Av** and overall voltage gain **Aov** for the amplifier system. **Aov** includes the effect of source impedance **Rs**.

$$\beta_0 = \frac{\alpha_0}{1 - \alpha_0}$$

$$R_{in} = r_e + \frac{r_b}{\beta_0}$$

$$R_o = r_c$$

$$A_i = \alpha_0$$

$$A_v = \frac{\alpha_0 \cdot R_I}{r_e + \frac{r_b}{\beta_0}}$$

$$A_{ov} = \frac{\alpha_0 \cdot r_c \cdot \left(\frac{R_{in}}{R_{in} + R_s} \right)}{r_e + \frac{r_b}{\beta_0}}$$

BJT (Common Emitter)

Analysis
Equations
Linear Amplifiers
BJT (Common Emitter)
Reference

These six equations represent properties of a transistor amplifier connected in the common emitter configuration at mid frequencies. The first equation connects common base current gain α_0 with common emitter current gain β_0 . The second equation computes the input R_{in} , in terms of base resistance r_b , emitter resistance r_e , and β_0 . The output resistance R_o is defined by the third equation in terms of collector resistance, r_c . The next equation defines current gain A_i . The final two equations cover the voltage gain A_v and overall voltage gain A_{ov} for the amplifier system. A_{ov} includes the effect of source impedance R_s .

$$\beta_0 = \frac{\alpha_0}{1 - \alpha_0}$$

$$R_{in} = r_b + \beta_0 \cdot r_e$$

$$R_o = r_c$$

$$A_i = -\beta_0$$

$$A_v = \frac{-\beta_0 \cdot R_L}{\beta_0 \cdot r_e + r_b}$$

$$A_{ov} = \frac{-\beta_0 \cdot R_L}{R_s + R_{in}}$$

BJT (Common Collector)

Analysis
Equations
Linear Amplifiers
BJT (Common Collector)
Reference

These six equations are the properties of a transistor amplifier connected in the common collector configuration at the mid frequencies. The first equation connects common base current gain α_0 with common emitter current gain β_0 . The second equation computes the input impedance R_{in} in terms of base resistance r_b , emitter resistance r_e , β_0 , and load resistance R_L . R_o represents the output resistance. The current gain A_i is shown in the next equation in terms of r_c , α_0 , r_e , and R_L . The final two equations cover the voltage gain A_v and overall voltage gain A_{ov} for the amplifier system. A_{ov} includes the effect of source impedance R_s .

$$\beta_0 = \frac{\alpha_0}{1 - \alpha_0}$$

$$R_{in} = r_b + \beta_0 \cdot r_e + (\beta_0 + 1) \cdot R_L$$

$$R_o = r_e + \frac{(R_s + r_b)}{\beta_0}$$

$$A_i = \frac{r_c}{r_c \cdot (1 - \alpha \theta) + R_L + r_e} \quad A_v = \frac{\alpha \theta \cdot R_L}{r_e + R_L} \quad A_{ov} = \frac{(\beta \theta + 1) \cdot R_L}{R_s + R_{in} + (\beta \theta + 1) \cdot R_L}$$

FET (Common Gate)

Analysis
Equations
Linear Amplifiers
FET (Common Gate)
Reference

The four equations in this section focus on an FET amplifier in the common gate configuration. The first equation defines the amplification factor μ in terms of transconductance g_m and drain resistance r_d . The second equation computes input resistance R_{in} as a function of load resistance R_L , r_d and μ . Voltage gain A_v is defined in the third equation. The final equation computes the output resistance R_o in terms of r_d , μ , and external gate resistance R_G .

$$\mu = g_m \cdot r_d \quad R_{in} = \frac{(R_L + r_d)}{\mu + 1} \quad A_v = \frac{(\mu + 1) \cdot R_L}{r_d + R_L}$$

$$R_o = r_d + (\mu + 1) \cdot R_G$$

FET (Common Source)

Analysis
Equations
Linear Amplifiers
FET (Common Source)
Reference

These four equations represent the key properties of an FET amplifier in the mid frequency range. The first equation defines the amplification factor μ in terms of transconductance g_m and drain resistance r_d . The second equation computes input resistance R_{in} as a function of load resistance R_L , r_d and μ . Voltage gain A_v is defined in the third equation. The final equation computes the output resistance.

$$\mu = g_m \cdot r_d \quad R_{in} = \frac{(R_L + r_d)}{\mu + 1} \quad A_v = -g_m \cdot \left(\frac{r_d \cdot R_L}{r_d + R_L} \right)$$

$$R_o = r_d$$

FET (Common Drain)

Analysis
Equations
Linear Amplifiers
FET (Common Drain)
Reference

The four equations in this section focus on an FET amplifier connected in the common drain configuration. The first equation defines the amplification factor μ in terms of transconductance g_m and drain resistance r_d . The second equation computes input resistance R_{in} as a function of load resistance R_L , r_d and μ . Voltage gain A_v is defined in the third equation. The final equation computes the output resistance, R_o .

$$\mu = g_m \cdot r_d$$

$$R_{in} = \frac{(R_L + r_d)}{\mu + 1}$$

$$A_v = \frac{\mu \cdot R_L}{(\mu + 1) \cdot R_L + r_d}$$

$$R_o = \frac{r_d}{\mu + 1}$$

Darlington (CC-CC)

Analysis
Equations
Linear Amplifiers
Darlington (CC-CC)
Reference

The Darlington configuration connected as a common collector-common collector is a frequently-used configuration for achieving large current gains. The first two equations yield the input and output resistances R_{in} and R_o , computed in terms of emitter resistance r_e , load resistance R_L , current gain β_0 , base resistance r_b , and source resistance R_s . The final equation computes overall current gain A_i for the transistor pair.



$$R_{in} = \beta_0 \cdot (r_e + \beta_0 \cdot (r_e + R_L))$$

$$R_o = r_e + \frac{(\beta_0 \cdot (r_e + r_b) + R_s)}{\beta_0^2}$$

$$A_i = \frac{\beta_0^2 \cdot R_{BA}}{R_{BA} + \beta_0 \cdot (R_L + r_e)}$$

Darlington (CC-CE)

Analysis
Equations
Linear Amplifiers
<i>Darlington (CC-CE)</i>
Reference

The Darlington configuration connected as a common collector-common emitter configuration is covered in this section. The first two equations define the



input resistance **Rin** and output resistance **Ro**, in terms of base resistance **rb**, emitter resistance **re**, collector resistance **rc**, and current gain **β0**. The final equation calculates voltage gain **Av**.

$$R_{in}=r_b+\beta_0\cdot r_e$$

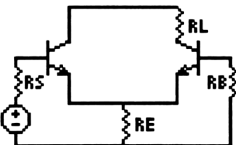
$$R_o=\frac{r_c}{\beta_0}$$

$$A_v=\frac{\frac{-R_L}{r_e}\cdot r_e}{r_e+\frac{R_S}{\beta_0^2}}$$

Emitter-Coupled Amplifier

Analysis
Equations
Linear Amplifiers
<i>Emitter-Coupled Amplifier</i>
Reference

Two classes of emitter-coupled amplifiers are covered in this section. The first equation shows the general relationship between **β0** and **α0**, the current gains under common base and common emitter configurations. The next three equations show the input resistance **Rin**, output resistance **Ro**, and voltage gain **Av** for a common collector-common base method of connection. The last three



equations correspond to cascade configuration of the transistors, which is a combination of common emitter-common base configuration resulting in a current gain **Ai** with corresponding input resistance **Rin** and output resistance **Ro**.

$$\beta_0=\frac{\alpha_0}{1-\alpha_0}$$

$$R_{in}=\beta_0\cdot(r_e+\beta_0\cdot(R_L+r_e))$$

$$R_o=r_e+\frac{(\beta_0\cdot(r_e+r_b)+R_S)}{\beta_0^2}$$

$$A_v=\frac{R_L}{r_e}\cdot\left(\frac{\beta_0\cdot r_e}{2\cdot\beta_0\cdot r_e+R_L}\right)$$

$$A_i=-\alpha_0\cdot\beta_0$$

$$R_{in}=\beta_0\cdot r_e+r_b$$

$$R_o=r_c$$

Differential Amplifier

Analysis
Equations
Linear Amplifiers
Differential Amplifier
Reference

These four equations cover a differential amplifier. The gain A_d in the differential mode of operation is given by the first equation. The second equation shows the gain A_c for a common mode input. The last two equations show input resistance for differential and common mode inputs R_{id} and R_{ic} .

$$A_d = \frac{-1}{2} \cdot g_m \cdot R_{CA}$$

$$A_c = \frac{-\alpha \theta \cdot R_{CA}}{2 \cdot R_{EA} + r_e}$$

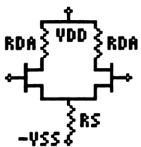
$$R_{id} = 2 \cdot (r_b + \beta \theta \cdot r_e)$$

$$R_{ic} = \beta \theta \cdot R_{EA}$$

Source-Coupled JFET Pair

Analysis
Equations
Linear Amplifiers
Source-Coupled JFET Pair
Reference

The first two equations cover differential and common mode gain for a source-coupled JFET pair. The third equation shows the amplification factor, while the last equation shows the common mode rejection ratio.



$$A_d = \frac{-\frac{1}{2} \cdot g_m \cdot (r_d \cdot R_{DA})}{r_d + R_{DA}}$$

$$A_c = \frac{-\mu \cdot R_{DA}}{(\mu + 1) \cdot 2 \cdot R_S + r_d + R_{DA}}$$

$$\mu = g_m \cdot r_d$$

$$CMMR = g_m \cdot R_S$$

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Mohammed S. Ghausi, *Electronic Devices and Circuits: Discrete and Integrated*, Holt, Rinehart and Winston, New York NY 1985.

Chapter 30

Class A, B, and C Amplifiers

Analysis
Equations
<i>Class A, B, and C Amplifiers</i>
Reference

This chapter covers equations describing the performance of Class A, B, and C power amplifiers.

- ☐ Class A Amplifier
- ☐ Power Transistor
- ☐ Push-Pull Principle
- ☐ Class B Amplifier
- ☐ Class C Amplifier

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

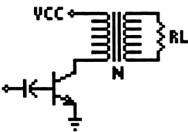
Variable	Description	Unit
gm	Transconductance	S
hFE	CE current gain	unitless
hOE	CE output conductance	S
I	Current	A
IB	Base current	A
IC	Collector current	A
ΔIC	Current swing from operating pt.	A
ICBO	Collector current EB open	A
ICQ	Current at operating point	A
Idc	DC current	A
Imax	Maximum current	A
K	Constant	unitless
m	Constant	1/K
η	Efficiency	unitless
n	Turns ratio	unitless
N1	# turns in primary	unitless

N2	# turns in secondary	unitless
Pd	Power dissipated	W
Pdc	DC power input to amp	W
Po	Power output	W
PP	Compliance	V
Q	Quality factor	unitless
θ_{JA}	Thermal resistance	W/K
R	Equivalent resistance	Ω
R0	Internal circuit loss	Ω
R2	Load resistance	Ω
RB	External base resistance	Ω
Rc	Coupled load resistance	Ω
Re	External emitter resistance	Ω
RI	Load resistance	Ω
S	Instability factor	unitless
TA	Ambient temperature	K
TJ	Junction temperature	K
ΔT_j	Change in temperature	K
V0	Voltage across tank circuit	V
V1	Voltage across tuned circuit	V
VBE	Base emitter voltage	V
VCC	Collector supply voltage	V
ΔV_{CE}	Voltage swing from operating pt.	V
VCEmax	Maximum transistor rating	V
VCEmin	Minimum transistor rating	V
Vm	Maximum amplitude	V
VPP	Peak-peak volts, secondary	V
XC	Tuned circuit parameter	Ω
XC1	π equivalent circuit parameter	Ω
XC2	π equivalent circuit parameter	Ω
XL	π series reactance	Ω

Class A Amplifier

Analysis
Equations
Class A, B, and C Amplifiers
Class A Amplifier
Reference

The eight equations in this section form the basis for analyzing a Class A amplifier with an ideal transformer coupled resistive load. The first equation specifies the



equivalent load resistance **R** from the load resistance **RI** in the secondary of the transformer with a turns ratio **n**. The second equation defines the AC current swing ΔI_C in terms of the voltage swing ΔV_{CE} and **R**. The next equation computes the maximum collector current **I_{max}**

in terms of ICQ and ΔIC . The DC power available P_{dc} is shown in the fourth equation. The compliance PP is defined as the full voltage swing across the emitter and collector. VPP represents the peak to peak voltage in the secondary. The final two equations compute the output power P_o and the conversion efficiency η .

$R = n^2 \cdot R_L$	$\Delta IC = \frac{\Delta V_{CE}}{R}$	$I_{max} = ICQ + \Delta IC$
$P_{dc} = V_{CC} \cdot ICQ$	$PP = V_{CEmax} - V_{CEmin}$	$VPP = n \cdot PP$
$P_o = \frac{\Delta IC^2 \cdot R}{8}$	$\eta = \frac{P_o}{P_{dc}}$	

Power Transistor

Analysis
Equations
Class A, B, and C Amplifiers
Power Transistor
Reference

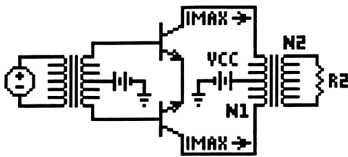
Power amplifiers generate heat needing rapid transfer to the ambient. The six equations in this section focus on these thermal problems, the instability factor and the currents. The first equation defines the junction temperature T_J as linearly related to the power dissipation P_d and thermal resistance θ_{JA} . The next two equations focus on the collector current IC and base current IB in terms of the current gain hFE , leakage current $ICBO$, external emitter resistance Re and external base resistance RB . The fourth equation expresses IC in terms of hFE , Re , RB , $ICBO$, and V_{BE} . The instability factor S is given by the fifth equation, while the final equation computes IC in terms of hFE , $ICBO$, a parameter m , S , and the change in junction temperature ΔT_j .

$T_J = T_A + \theta_{JA} \cdot P_d$	$IC = hFE \cdot IB + (1 + hFE) \cdot ICBO$
$IB = \frac{-(IC \cdot Re - V_{BE})}{Re + RB}$	$IC = \frac{-hFE \cdot V_{BE}}{hFE \cdot Re + RB} + \frac{hFE \cdot (Re + RB)}{hFE \cdot Re + RB} \cdot ICBO$
$S = \frac{\left(1 + \frac{RB}{Re}\right) \cdot hFE}{hFE + \frac{RB}{Re}}$	$IC = -hFE \cdot IB + S \cdot ICBO \cdot (1 + m \cdot \Delta T_j)$

Push-Pull Principle

Analysis
Equations
Class A, B, and C Amplifiers
Push-Pull Principle
Reference

These three equations introduce the push-pull principle, commonly used in power amplifier design. Two transistors have their collector outputs connected to the center-tapped primary winding of a transformer. The secondary winding is connected to a load **R2**. The first equation computes an equivalent resistance **R** based on the maximum current supplied to the load **Imax**. The power



output is computed by the second equation in terms of **VCC** and **R**. The final equation computes the power in terms of load resistance **R2** and transformer windings **N1** and **N2**.

$$R = \frac{V_{CC}}{I_{max}}$$

$$P_o = \frac{V_{CC}^2}{2 \cdot R}$$

$$P_o = \frac{\left(\frac{N_2}{2 \cdot N_1} \right)^2 \cdot V_{CC}^2}{2 \cdot R_2}$$

Class B Amplifier

Analysis
Equations
Class A, B, and C Amplifiers
Class B Amplifier
Reference

Power transistors that are connected in a push-pull mode and biased to cutoff, operate under the Class B condition where alternate half-cycles of input are of forward polarity for each transistor. The nine equations in this section define the characteristic properties of this class of amplifiers. The first equation represents the power output at any signal level in terms of the constant **K**, supply voltage **VCC**, and an equivalent resistance **R**. The second equation defines the DC current **Idc** as the average value of a sinusoidal half-wave adjusted by **K**. The next two equations focus on the DC power **Pdc** in terms of **VCC**, **K**, **R**, and **Imax**. The efficiency of power conversion **η** is given by the next equations. The eighth equation covers the voltage across a tuned RLC circuit in terms of the transconductance **gm**, load resistance **RL**, and output conductance **hOE**. The final equation calculates the average collector current for a half-sine wave.

$$P_o = \frac{K^2 \cdot V_{CC}^2}{2 \cdot R}$$

$$I_{dc} = \frac{2 \cdot K \cdot I_{max}}{\pi}$$

$$P_{dc} = \frac{2 \cdot K \cdot I_{max} \cdot V_{CC}}{\pi}$$

$$P_{dc} = \frac{2 \cdot K \cdot V_{CC}^2}{\pi \cdot R}$$

$$\eta = \frac{P_o}{P_{dc}}$$

$$\eta = \frac{\pi \cdot K}{4}$$

$$P_d = \frac{2 \cdot V_{CC}^2}{\pi \cdot R} \cdot \left(K - \frac{K^2 \cdot \pi}{4} \right)$$

$$V_1 = \frac{g_m \cdot R_L \cdot V_m}{2 \cdot \sqrt{2}} \cdot \left(\frac{1}{1 + \frac{h_{OE} \cdot R_L}{2}} \right)$$

$$I_C = \frac{g_m \cdot V_m}{\pi} \cdot \left(\frac{1}{1 + \frac{h_{OE} \cdot R_L}{2}} \right)$$

Class C Amplifier

Analysis

Equations

Class A, B, and C Amplifiers

Class C Amplifier

Reference

These six equations outline the properties of a Class C amplifier. The first equation defines the efficiency of conversion η in terms of the current I , the coupled-in load R_c , and equivalent internal circuit loss resistance R_0 . The tuned circuit parameters have a capacitive reactance of X_C , which is given in terms of the load voltage V_0 , quality factor Q , and power P_o . X_L is expressed in terms of X_C and Q , load resistance R_L , and resistance R_2 . The equations for X_{C1} and X_{C2} represent load harmonic suppression values in the output circuit.

$$\eta = \frac{I^2 \cdot R_c}{I^2 \cdot (R_c + R_0)}$$

$$X_C = \frac{V_0^2}{Q \cdot P_o}$$

$$X_L = \frac{X_C \cdot Q^2}{Q^2 + 1}$$

$$X_{C1} = \frac{-R_1}{Q}$$

$$X_L = \frac{1}{Q} \cdot (R_1 + \sqrt{R_1 \cdot R_2})$$

$$X_{C2} = \frac{-R_2}{Q}$$

Chapter 31

Transformers

Analysis
Equations
<i>Transformers</i>
Reference

This chapter covers equations for simplified design parameters of transformers.

- ☐ Ideal Transformer
- ☐ Linear Equivalent Circuit

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
I1	Primary current	A
I2	Secondary current	A
N1	# primary turns	unitless
N2	# secondary turns	unitless
R1	Primary resistance	Ω
R2	Secondary resistance	Ω
Rin	Equiv. primary resistance	Ω
Rl	Resistive part of load	Ω
V1	Primary voltage	V
V2	Secondary voltage	V
X1	Primary reactance	Ω
X2	Secondary reactance	Ω
Xin	Equivalent primary reactance	Ω
Xl	Reactive part of load	Ω
Zin	Primary impedance	Ω
ZL	Secondary load	Ω

Ideal Transformer

Analysis
Equations
Transformers
Ideal Transformer
Reference

Four equations describe the properties of an ideal transformer. The first equation links the primary and secondary voltages **V1** and **V2** in terms of the primary and secondary turns **N1** and **N2**. The second equation shows the corresponding relationship between the primary and secondary currents **I1** and **I2**. The third equation shows the condition equating primary and secondary power. The final equation shows the impact of a load impedance **ZL** experienced at the primary winding terminal on the primary impedance **Zin**.



$$\frac{V1}{V2} = \frac{N1}{N2}$$

$$I1 \cdot N1 = I2 \cdot N2$$

$$V1 \cdot I1 = V2 \cdot I2$$

$$Zin = \left(\frac{N1}{N2} \right)^2 \cdot ZL$$

Linear Equivalent Circuit

Analysis
Equations
Transformers
Linear Equivalent Circuit
Reference

The first two equations define the primary voltage and current **V1** and **I1** in terms of **V2** and **I2**. The last two equations expand the equivalent resistance and reactance at the primary terminals in terms of the primary winding resistance **R1**, secondary winding resistance **R2**, load resistance **RL**, and load reactance **XL**.

$$V1 = \frac{N1}{N2} \cdot V2$$

$$I1 = \frac{I2 \cdot N2}{N1}$$

$$Rin = R1 + \left(\frac{N1}{N2} \right)^2 \cdot (R2 + RL)$$

$$Xin = X1 + \left(\frac{N1}{N2} \right)^2 \cdot (X2 + XL)$$

Chapter 32

Motors and Generators

Analysis
Equations
<i>Motors and Generators</i>
Reference

Thirteen sections covering various aspects of AC and DC motors and generators are included in this module:

- ☐ Energy Conversion
- ☐ DC Generator
- ☐ Separately-Excited DC Generator
- ☐ DC Shunt Generator
- ☐ DC Series Generator
- ☐ Separately-Excited DC Motor
- ☐ DC Shunt Motor
- ☐ DC Series Motor
- ☐ Permanent Magnet Motor
- ☐ Induction Motor I
- ☐ Induction Motor II
- ☐ Single-Phase Induction Motor
- ☐ Synchronous Machines

Variables

The table below lists all the variables used in this chapter, along with a brief description and appropriate units.

Variable	Description	Unit
A	Area	m ²
ap	# parallel paths	unitless
B	Magnetic induction	T
Ea	Average emf induced in armature	V
Ef	Field voltage	V
Ema	Phase voltage	V
Es	Induced voltage	V
Eta	Average emf induced per turn	V

F	Magnetic pressure	Pa
H	Magnetic field intensity	A/m
Ia	Armature current	A
If	Field current	A
IL	Load current	A
Ir	Rotor current per phase	A
Isb	Backward stator current	A
Isf	Forward stator current	A
K	Machine constant	unitless
Kf	Field coefficient	A/Wb
KM	Induction motor constant	unitless
L	Length of each turn	m
η	Phase delay	r
N	Total # armature coils	unitless
Ns	# stator coils	unitless
ρ	Resistivity	Ω/m
ϕ	Flux	Wb
p	# poles	unitless
P	Power	W
Pa	Mechanical power	W
Pma	Power in rotor per phase	W
Pme	Mechanical power	W
Pr	Rotor power per phase	W
Rl	Rotor resistance per phase	Ω
Ra	Armature resistance	Ω
Rd	Adjustable resistance	Ω
Re	Ext. shunt resistance	Ω
Rel	Magnetic reluctance	A/Wb
Rf	Field coil resistance	Ω
Rl	Load resistance	Ω
Rr	Equivalent rotor resistance	Ω
Rs	Series field resistance	Ω
Rst	Stator resistance	Ω
s	Slip	unitless
sf	Slip for forward flux	unitless
sm	Maximum slip	unitless
T	Internal torque	N*m
Tb	Backward torque	N*m
Tf	Forward torque	N*m
Tgmax	Breakdown torque	N*m
TL	Load torque	N*m
Tloss	Torque loss	N*m
Tmax	Pullout torque	N*m
Tmmax	Maximum positive torque	N*m
Ts	Shaft torque	N*m

Va	Applied voltage	V
Vf	Field voltage	V
Vfs	Field voltage	V
Vt	Terminal voltage	V
ωm	Mechical radian frequency	r/s
ωme	Electrical radian frequency	r/s
ωr	Electrical rotor speed	r/s
ωs	Electrical stator speed	r/s
Wf	Magnetic energy	J
XL	Inductive reactance	Ω

Energy Conversion

Analysis
Equations
Motors and Generators
<i>Energy Conversion</i>
Reference

The four equations in this section display the fundamental relationship amongst electrical, magnetic and mechanical aspects of a system. For example, the first two equations show two ways of computing energy density **Wf** stored in a magnetic field. The first equation uses the field intensity **H** and flux density **B** in a magnetic region with length **L** and area **A**. The second equation uses the magnetic reluctance **Rel** and flux ϕ to compute **Wf**. The third equation defines the mechanical force **F** due to the flux density **B**, while the last equation shows the rms value of the emf **Es** induced by **Ns** turns moving with an angular velocity ωs sweeping a magnetic flux of ϕ .

$$Wf = \frac{1}{2} \cdot H \cdot B \cdot L \cdot A$$

$$Wf = \frac{1}{2} \cdot Rel \cdot \phi^2$$

$$F = \frac{B^2}{2 \cdot \mu_0}$$

$$Es = \frac{Ns \cdot \omega s \cdot \phi}{\sqrt{2}}$$

DC Generator

Analysis
Equations
Motors and Generators
<i>DC Generator</i>
Reference

The eleven equations in this section describe the properties of a DC generator. The first equation describes the relation between electrical radian frequency ωme , the mechanical angular frequency ωm , and the number of poles in the generator **p**. The next equation expresses the emf generated per turn **Eta** with the relative motion of the coil with respect to the magnetic field. The next pair of

equations illustrate two ways to express induced armature emf E_a as a function of number of armature coils N , the number of parallel paths a_p , number of poles p , the mechanical radian frequency ω_m , a machine constant K , and flux ϕ . The machine constant K , expressed by the fifth equation, is seen to be dependent purely on the characteristics of the machine. The next equation shows the conversion of mechanical energy available as torque T and mechanical angular velocity ω_m to its electrical counterpart – namely, the emf and current in the armature E_a , and I_a and the voltage and current in the field windings E_f and I_f . The next equation for torque connects T with K , ϕ , and the current I_a . The armature resistance is given by the equation for R_a in terms of N , a_p , coil length L , area A and its resistivity ρ . V_f represents the voltage across the field winding carrying a current I_f and a resistance R_f . The terminal voltage V_t represents the induced voltage minus the IR drop in the armature. The final equation represents the shaft torque T_s needed to generate the induced emf, assuming a given value for equivalent loss of torque T_{loss} .

$\omega_m = \frac{P}{2} \cdot \omega$	$E_t = \frac{P}{\pi} \cdot \omega_m \cdot \phi$	$E_a = \frac{N}{a_p} \cdot \left(\frac{P}{\pi} \right) \cdot \omega_m \cdot \phi$
$E_a = K \cdot \omega_m \cdot \phi$	$K = \frac{N \cdot P}{a_p \cdot \pi}$	$T \cdot \omega_m = E_a \cdot I_a + E_f \cdot I_f$
$T = K \cdot \phi \cdot I_a$	$R_a = \frac{\rho \cdot N}{a_p} \cdot \left(\frac{L}{A} \right)$	$V_f = R_f \cdot I_f$
$V_t = K \cdot \omega_m \cdot \phi - R_a \cdot I_a$	$T_s = K \cdot \phi \cdot I_a + T_{loss}$	

Separately-Excited DC Generator

Analysis
Equations
Motors and Generators
<i>Sep.-Excited DC Generator</i>
Reference

The five equations in this section describe the properties of a separately excited DC generator. The first equation computes the field current I_f in terms of field voltage V_f s, external shunt resistance R_e , and field coil resistance R_f . The second equation evaluates armature induced voltage E_a as a function of machine constant K , mechanical radian frequency ω_m , and flux ϕ . The third and fourth equations are alternate forms of expressing terminal voltage V_t in terms of load current I_L , load resistance R_L , armature resistance R_a . The final equation shows the armature current I_L in terms of K , ϕ , ω_m , R_a and R_L .

$$I_f = \frac{V_{fs}}{R_e + R_f}$$

$$E_a = K \cdot \omega_m \cdot \phi$$

$$V_t = I_L \cdot R_L$$

$$V_t = E_a - R_a \cdot I_L$$

$$I_L = \frac{K \cdot \phi \cdot \omega_m}{R_a + R_L}$$

DC Shunt Generator

The first equation in this section expresses induced armature voltage E_a in terms of machine constant K , mechanical angular frequency ω_m , and flux ϕ . The second equation defines terminal voltage V_t in terms of field current I_f , external resistance R_e , and field coil resistance R_f . The third equation computes V_t in terms of load current I_L and load resistance R_L . The fourth equation expresses V_t as induced emf E_a minus armature IR drop. The armature current I_a is the sum of the load current I_L and field current I_f . The final equation is an alternate form of expression for E_a .

Analysis

Equations

Motors and Generators

DC Shunt Generator

Reference

$$E_a = K \cdot \omega_m \cdot \phi$$

$$V_t = (R_e + R_f) \cdot I_f$$

$$V_t = I_L \cdot R_L$$

$$V_t = E_a - R_a \cdot I_a$$

$$I_a = I_L + I_f$$

$$E_a = R_a \cdot I_a + (R_e + R_f) \cdot I_f$$

DC Series Generator

The two equations in this section describe the properties of a series DC generator. The first equation specifies the field current and the armature current to be the same. The second equation computes the terminal voltage V_t in terms of induced emf E_a , load current I_L , armature resistance R_a , and series field windings R_s .

Analysis

Equations

Motors and Generators

DC Series Generator

Reference

$$I_a = I_f$$

$$V_t = E_a - (R_a + R_s) \cdot I_L$$

Separately-Excited DC Motor

Analysis
Equations
Motors and Generators
Sep.-Excited DC Motor
Reference

These eight equations form the foundation of the workings of a separately excited motor. The first equation calculates the field voltage V_f in terms of the field current I_f and field coil resistance R_f . The second equation shows the computation of terminal voltage V_t in terms of machine constant K , magnetic flux ϕ , mechanical radian frequency ω_m , armature current I_a , and armature resistance R_a . The third equation calculates the load torque T_L in terms of K , ϕ , I_a and T_{loss} . The fourth equation calculates E_a , the back emf induced in the rotor. The next equation links torque T with K , ϕ , and I_a . The reciprocal power relationship between ω_m and ϕ is shown in the next equation. The seventh equation shows the relationship between T , T_{loss} and T_L . The last equation shows power providing a torque T , with an angular velocity ω_m .

$V_f = R_f \cdot I_f$	$V_t = K \cdot \phi \cdot \omega_m + R_a \cdot I_a$	$T_L = K \cdot \phi \cdot I_a - T_{loss}$
$E_a = K \cdot \omega_m \cdot \phi$	$T = K \cdot I_a \cdot \phi$	$\omega_m = \frac{V_t}{K \cdot \phi} - \frac{R_a \cdot T}{(K \cdot \phi)^2}$
$T = T_{loss} + T_L$	$P = T \cdot \omega_m$	

DC Shunt Motor

Analysis
Equations
Motors and Generators
DC Shunt Motor
Reference

These seven equations describe the principal characteristics of a DC shunt motor. The first equation expresses the terminal voltage V_t in terms of the field current I_f and field resistance R_f along with the external field resistance R_e . The second equation defines the terminal voltage V_t in terms of the back emf (expressed in terms of the machine constant K , flux swept ϕ , and angular velocity ω_m) and the IR drop in the armature circuit. The third equation refers to the torque available at the load T_L due to the current I_a in the armature minus the loss of torque due to friction and other reasons. The fourth equation gives the definitive relationship between the back emf E_a , K , ϕ and ω_m . The next equation shows the reciprocal quadratic relationship between ω_m , V_t , K , ϕ ,

Ra, Rd and **T**. The last two equations compute torque **T** in terms of **Tloss**, load torque **TL**, flux ϕ , **Ia**, and **K**.

$V_t = (R_e + R_f) \cdot I_f$	$V_t = K \cdot \phi \cdot \omega_m + R_a \cdot I_a$	$T_L = K \cdot \phi \cdot I_a - T_{loss}$
$E_a = K \cdot \omega_m \cdot \phi$	$\omega_m = \frac{V_t}{K \cdot \phi} - \frac{(R_a + R_d) \cdot T}{(K \cdot \phi)^2}$	$T = T_{loss} + T_L$
$T = K \cdot \phi \cdot I_a$		

DC Series Motor

Analysis
 Equations
 Motors and Generators
DC Series Motor
 Reference

These eight equations describe the performance characteristics of a series DC motor. The first equation links the terminal voltage to back emf (**Ea** defined by the third equation) and the the IR drop through the armature due to armature resistance **Ra**, adjustable resistance **Rd**, and series resistance **Rs**. The second equation connects load torque **TL** with machine constant **K**, flux ϕ , load current **IL**, and the torque loss **Tloss**. The third equation defines the equation for the back emf in the armature **Ea** in terms of **K**, ϕ , and mechanical frequency ω_m . The fourth equation shows torque generated at the rotor due the magnetic flux ϕ and current **IL**. The next relationship shows the reciprocal quadratic nature of the link between ω_m , **Vt**, **K**, ϕ , **Ra**, **Rs**, **Rd**, and torque **T**. The next equation shows that the generated torque **T** is the sum of load torque **TL** and lost **Tloss**. The last two equations show the connection between **K**, ϕ , a field constant **Kf**, load current **IL**, and torque **T**.

$V_t = K \cdot \phi \cdot \omega_m + (R_a + R_s + R_d) \cdot I_L$	$T_L = K \cdot \phi \cdot I_L - T_{loss}$	$E_a = K \cdot \omega_m \cdot \phi$
$T = K \cdot \phi \cdot I_L$	$\omega_m = \frac{V_t}{K \cdot \phi} - \frac{(R_a + R_s + R_d) \cdot T}{(K \cdot \phi)^2}$	$T = T_{loss} + T_L$
$K \cdot \phi = K_f \cdot I_L$	$T = K_f \cdot I_L^2$	

Permanent Magnet Motor

Analysis
Equations
Motors and Generators
Permanent Magnet Motor
Reference

These five equations characterize the permanent magnet motor. The first equation shows the back emf E_a in terms of machine constant K , flux ϕ , and radian velocity ω_m . The second equation shows the connection between generated torque T , K , ϕ and armature current I_a . The terminal voltage V_t is the sum of back emf E_a and the IR drop in the armature. The fourth equation shows conservation of various torques T , T_L and T_{loss} . The final equation shows the quadratic relationship of ω_m in terms of K , V_t , ϕ , T and R_a .

$$E_a = K \cdot \phi \cdot \omega_m$$

$$T = K \cdot \phi \cdot I_a$$

$$V_t = E_a + R_a \cdot I_a$$

$$T = T_{loss} + T_L$$

$$\omega_m = \frac{V_t}{K \cdot \phi} - \frac{R_a \cdot T}{(K \cdot \phi)^2}$$

Induction Motor I

Analysis
Equations
Motors and Generators
Induction Motor I
Reference

These eleven equations define the relationships amongst key variables in evaluating the performance of an induction motor. The first equation indicates the relationship between the radian frequency induced in the rotor ω_r , the angular speed of the rotating magnetic field of the stator ω_s , the number of poles p , and the mechanical angular speed ω_m . The next three equations describe the slip s in three ways in terms of ω_r and ω_s , ω_m , p , the induced rotor power per phase P_r , and the power transferred to the rotor per phase P_{ma} . P_{ma} is defined in terms of the rotor current I_r and the rotor phase voltage E_{ma} . The next two equations account for the mechanical power P_{me} in terms of p , ω_m , ω_s , P_{ma} , and torque T . The torque equation can be expressed in terms of p , P_{ma} , and ω_s , as shown by the next equation. The last three equations show an equivalent circuit representation of induction motor action and link power with rotor resistance R_r , rotor current I_r , slip s , and a machine constant K_M .

$$\omega_r = \omega_s - \frac{p}{2} \cdot \omega_m$$

$$s = 1 - \frac{p}{2} \cdot \left(\frac{\omega_m}{\omega_s} \right)$$

$$\frac{P_r}{P_{ma}} = s$$

$$\omega_r = s \cdot \omega_s$$

$$P_{ma} = 3 \cdot I_r \cdot E_{ma}$$

$$P_{me} = 3 \cdot \left(\frac{p}{2} \right) \cdot \left(\frac{\omega_m}{\omega_s} \right) \cdot P_{ma}$$

$$P_{me} = T \cdot \omega_m$$

$$T = 3 \cdot \left(\frac{p}{2} \right) \cdot \left(\frac{P_{ma}}{\omega_s} \right)$$

$$P_{ma} = R_r \cdot I_r^2 + \frac{(1-s)}{s} \cdot R_r \cdot I_r^2$$

$$P_a = \frac{(1-s)}{s} \cdot R_r \cdot I_r^2$$

$$R_r = \frac{R_1}{KM^2}$$

Induction Motor II

Analysis

Equations

Motors and Generators

Induction Motor II

Reference

These seven equations describe equivalent circuit analysis of an induction motor. The first equation shows power **P_{ma}** in the rotor per phase, as defined in terms of the rotor current **I_r**, rotor resistance **R_r**, and slip **s**. The second equation shows the expression for torque **T** in terms of poles **p**, **P_{ma}** and radian frequency of the induced voltage in the stator. The third equation is an alternate representation of torque in terms of terminal voltage **V_a**, stator resistance **R_{st}**, **R_r**, inductive reactance **X_L**, and **ω_s**. The equation for **T_{max}** represents the maximum positive torque available at the rotor, given the parameters of the induction motor **R_{st}**, **R_r**, **X_L**, **V_a**, **p**, and **ω_s**. The torque equation shows a relationship between torque **T** and slip **s**; **s_m** represents the condition when **dT/ds=0**. The sixth equation defines the so-called breakdown torque **T_{gmax}** of the motor. The final equation connects **R_r** with machine constant **KM**.

$$P_{ma} = \frac{R_r}{s} \cdot I_r^2 \quad T = \frac{3}{2} \cdot \left(\frac{p \cdot P_{ma}}{\omega_s} \right) \quad T = \frac{3}{2} \cdot \left(\frac{p}{\omega_s} \right) \cdot \left(\frac{R_r}{s} \right) \cdot \left(\frac{V_a^2}{\left(R_{st} + \frac{R_r}{s} \right)^2 + X_L^2} \right)$$

$$T_{max} = \frac{3}{4} \cdot \left(\frac{p}{\omega_s} \right) \cdot \left(\frac{V_a^2}{\sqrt{R_{st}^2 + X_L^2} + R_{st}} \right)$$

$$s_m = \frac{R_r}{\sqrt{R_{st}^2 + X_L^2}}$$

$$T_{gmax} = - \left(\frac{3}{4} \right) \cdot \left(\frac{p}{\omega_s} \right) \cdot \left(\frac{V_a^2}{\sqrt{R_{st}^2 + X_L^2} - R_{st}} \right)$$

$$R_r = \frac{R_1}{KM^2}$$

Single-Phase Induction Motor

Analysis
Equations
Motors and Generators
<i>Single-Phase Induct. Motor</i>
Reference

These three equations describe the properties of a single-phase induction motor. The first equation defines the slip frequency **sf** with respect to the forward rotating flux, the radian frequency of induced current in the rotor, and the angular mechanical speed of the rotor **ωm**. The final two equations represent the forward and backward torques **Tf** and **Tb** for the system.

$$sf = 1 - \frac{p}{2} \cdot \left(\frac{\omega_m}{\omega_s} \right) \quad T_f = \frac{p}{2} \cdot \left(\frac{1}{\omega_s} \right) \cdot \left(\frac{I_{sf}^2 \cdot R_r}{2 \cdot sf} \right) \quad T_b = - \left(\frac{p}{2} \right) \cdot \left(\frac{1}{\omega_s} \right) \cdot \left(\frac{I_{sb}^2 \cdot R_r}{2 \cdot (2 - sf)} \right)$$

Synchronous Machines

Analysis
Equations
Motors and Generators
<i>Synchronous Machines</i>
Reference

These five equations focus on the basic properties of a synchronous machine. The first equation links the radian mechanical and electrical speeds **ωm** and **ωs** with the number of poles **p**. The second equation shows maximum torque **Tmax** in terms of current **If**, terminal voltage **Va**, **p**, and **ωs**. **Pma** represents the power produced in the load with a phase delay of **θ**. The last two equations show torque relationships with mechanical power **Pme**, **ωm**, **Pma**, and **ωs**.

$$\omega_m = \frac{2}{p} \cdot \omega_s \quad T_{max} = 3 \cdot \left(\frac{p}{2} \right) \cdot \left(\frac{I_f \cdot V_a}{\omega_s} \right) \quad P_{ma} = V_a \cdot I_a \cdot \cos(\theta)$$

$$T = \frac{P_{me}}{\omega_m} \quad T = 3 \cdot \left(\frac{p}{2} \right) \cdot \left(\frac{P_{ma}}{\omega_s} \right)$$

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Reference

Chapter 33

Reference: Navigation Guide

Analysis
Equations
<i>Reference</i>

This chapter is designed as a navigation guide to introduce you to the Reference tables, and show you the keys available at each screen. At the end of the chapter is a detailed Reference example.

Introduction.....	203
Finding Reference.....	204
Reference Screens.....	204
Using Reference Tables	205
Reference Menu Keys	205
Example: Electron Charge	206

Introduction

EE•Pro is divided into three major sections: Analysis, Equations, and Reference. This chapter addresses the Reference section, which includes Reference tables covering resistor colors, standard (or preferred) component values, semiconductor properties, Boolean expressions, Boolean algebra properties, transforms, constants, SI prefixes, and the Greek alphabet.

The Reference tables contain indispensable information for solving problems. You can find physical constants, look up properties of semiconductors, and access Fourier, Laplace, and z-transforms – all with context-sensitive help. Some Reference tables, such as Resistor Color Chart and Standard Component Values, are more sophisticated and can perform calculations. Many Reference tables include a picture for more information.

Unlike Analysis screens (which tend to be similar) and Equations screens (which tend to be identical), each Reference screen may differ significantly, depending on the type of Reference information being presented.

Finding Reference

The Reference section is found at the home screen of EE•Pro.

1. Start EE•Pro:

- HP 48GX: Press .
- HP 48SX: Press .
- Press to show the home screen.

EE•Pro is structured with a hierarchy of screens for choosing a specific topic. This is the home screen. To return here at any time, press or .



2. Select Reference by moving the highlight bar to Reference and pressing or . The screen now displays Reference as its title and a list of Reference tables from which to choose.

3. Select a Reference table by moving the highlight bar to the desired item and pressing or . This will display the selected Reference table. For the purposes of this navigation guide, select Reference, then Constants.



Pressing (if available) or returns you to the previous screen.

Pressing (if available) or returns you to the home screen.

Reference Screens

A basic Reference screen displays a Reference table. Most of the Reference tables contain information organized in the same manner as a printed reference book. The information may consist of data, equations, text, or a combination of these types. The screen pictured here is the Constants reference table.



All the screens in this chapter assume units are on. (Press , then to toggle units on or off.)

Using Reference Tables

The instructions below are general instructions for using the basic Reference tables. For a detailed example using the Constants, see page 206. In addition, each section in each Reference chapter contains at least one example.

1. Choose parameters (if available). Some Reference tables have **Choose** fields which control the specific data to be displayed, while other Reference tables consist of only one table of data.
2. Locate the specific item of interest. If necessary, use the search feature to scan through the data to find the item. Because the search feature will only scan the labels and data displayed on the main part of the screen, it may be necessary to press **DESC** or **VAR** to toggle the positions of the help text and the data. That way, the search feature can be used to search the information normally displayed in the help text area at the bottom of the screen.
3. *Optional:* Press **→STK** to copy the desired item(s) to the stack for use in further calculations.
4. When finished, press **←** to return to the Reference screen or press **↩ HOME** to return to the home screen.

Some Reference tables, such as Resistor Color Chart or Standard Component Values, are more sophisticated and can perform calculations, much like Analysis routines. For these types of Reference tables, the basic steps are identical to those used in Analysis routines, as described on page 17.

Reference Menu Keys

These are descriptions of the menu keys available in Reference screens:

→STK Copies one or all of the items to the HP 48 stack.

VIEW Displays the highlighted item in text view.

PICT Displays a picture (if available). This menu key will not appear for Reference tables which do not have a picture.

OPTS Displays the option menu. For more information, see “Options Menu” page 9.

DESC Toggles positions of data and help text (if appropriate). This menu key will not appear for Reference tables which do not have switchable help text.



SOLVE Performs a calculation using the entered values. This menu key will not appear for Reference tables which do not have a custom solving routine.

Example: Electron Charge

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On Help: On Font: Small
-------------------------------------	---	--

Find the constant for electron charge.

1. Press **DESC** or **VAR** to toggle the position of the constant values and the help text (the constant names), so that the names of the constants are listed in the main display area with the constants themselves. This places the names of the constants where they can be accessed by the search feature, which does not search through items displayed in the help text at the bottom of the screen.
2. Press **OPTS** **NXT** **FIND** to activate the search feature.
3. Type the name or part of the name of the item and press **ENTER**. For example, type CHARGE to find the electronic charge on an electron. The search feature is not case-sensitive, so typing in all caps is acceptable. The e- charge is the constant q and its value is 1.60217733E-19_C.
4. Press **EXIT** to leave the options menu.



NOTE



When you exit a Reference table, the position of the data and the help text will revert to the default setting. Pressing **DESC** only toggles the positions while you are at a particular screen.

5. When finished press **◀** to return to the Reference screen or press **▶** **HOME** to return to the home screen.

Chapter 34

Resistor Color Chart

Analysis
Equations
Reference
Resistor Color Chart

This chapter covers the resistor color chart reference table, which is a sophisticated routine to allow you to specify the color bands of a resistor and compute the value and tolerance. Using the Resistor Color Chart screen is similar to using most Analysis screens.

Field Descriptions

- Num. of Bands:** (*Number of Bands*) Press **CHOOS** to select 3, 4, or 5.
- Band 1:** (*see table below*) Press **CHOOS** to select color.
- Band 2:** (*see table below*) Press **CHOOS** to select color.
- Band 3:** (*see table below*) Press **CHOOS** to select color.
- Band 4:** (*see table below*) Press **CHOOS** to select color.
- Band 5:** (*see table below*) Press **CHOOS** to select color.
- Value:** (*Resistor Value*) Returns a unit object.
- Tolerance:** (*Resistor Tolerance*) Returns a percent.

SILV	±E2	±10%	YEL 4 ×E4
GOL	±E1	± 5%	GRN 5 ×E5 ±.50%
BLK 0	×E0		BLU 6 ×E6 ±.25%
BRN 1	×E1	± 1%	VIDL 7 ×E7 ±.10%
RED 2	×E2	± 2%	GRY 8 ×E8 ±.05%
ORA 3	×E3		WHI 9 ×E9
RESISTOR COLOR CHART			

Band positions represent:

	3-Band	4-Band	5-Band
Band 1	digit	digit	digit
Band 2	digit	digit	digit
Band 3	multiplier	multiplier	digit
Band 4	N/A	tolerance	multiplier
Band 5	N/A	N/A	tolerance

Colors represent:

	DIGIT	MULTIPLIER	TOLERANCE
SILVER	-	÷E2	10%
GOLD	-	÷E1	5%
BLACK	0	xE0	-
BROWN	1	xE1	1%
RED	2	xE2	2%
ORANGE	3	xE3	-
YELLOW	4	xE4	-
GREEN	5	xE5	0.5%
BLUE	6	xE6	0.25%
VIOLET	7	xE7	0.1%
GREY	8	xE8	0.05%
WHITE	9	xE9	-

Using the Resistor Color Chart

- 1. With the highlight bar on **Num. of Bands**, press **CHOOS** to select 3, 4 or 5. This will determine the number of **Band** fields that appear.
- 2. In each **Band** field, press **CHOOS** to select the desired color of the band.
- 3. Press **SOLVE** to find the value of the resistor and its tolerance.

Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On Help: On Font: Small
-------------------------------------	---	--

Find the value and tolerance of a resistor with band colors yellow, black, and green.

- 1. Choose 3 for **Num. of Bands**.
- 2. Choose Yellow for **Band 1**, Black for **Band 2**, and Green for **Band 3**.
- 4. Press **SOLVE** to calculate **Value** and **Tolerance**.

RESISTOR COLOR CHART
NUM. OF BANDS: 3
BAND 1: YELLOW
BAND 2: BLACK
BAND 3: GREEN
VALUE: 4 MΩ
TOLERANCE: ±20%
RESULT: RESISTOR TOLERANCE
→STK VIEW PICT OPTS SOLVE

NOTE



In the small font, it is not possible to distinguish between the prefix for milli (m) and Mega (M), so be sure to switch to the large font if there is any chance of ambiguity in the value. Press **OPTS** **FONT** to toggle the font size.

Chapter 35

Standard Component Values

Analysis Standard Component Values Equations Reference

This chapter covers the standard component values reference table, which is a sophisticated routine to allow you to compute the closest standard value (also known as the “preferred” value) of a resistor, capacitor, or inductor. Using the Standard Component Values screen will be similar to using most Analysis screens.

Field Descriptions

Value: (*Desired Value or Design Spec.*) Enter a real number.

Tolerance: (*Tolerance of Component*) Press **CHOOS** to select a tolerance $\pm 20\%$ down to $\pm 0.05\%$.

Component: (*Type of Component*) Press **CHOOS** to select Resistor, Inductor, or Capacitor.


Value: (*Closest Standard Value to the Desired Value*) Returns a unit object.

Bands: (*Resistor Color Bands - if the Component is a Resistor*) Returns the color bands in a resistor.

Using Standard Component Values

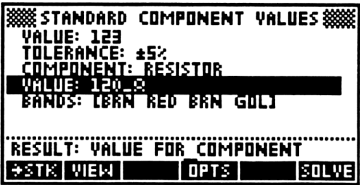
1. In the **Value** field, enter the desired value of the component.
2. In the **Tolerance** field, press **CHOOS** or **ENTER** to choose the tolerance of the component.
3. In the **Component** field, press **CHOOS** or **ENTER** to choose the type of component.
4. Press **SOLVE** to find the closest standard value for the component and (if a resistor) the color bands.

Example

MODES (Press )	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On Help: On Font: Small
--	---	--

Find the closest standard value for a 123 Ω resistor at 5% tolerance.

- 1. Enter 123 for **Value**.
- 2. Choose 5% for **Tolerance**.
- 3. Choose Resistor for **Component**.
- 3. Press **SOLVE** to calculate **Value** and **Bands**.



Chapter 36

Semiconductor Properties

Analysis
Equations
Reference
<i>Semiconductor Properties</i>

This chapter covers the semiconductor properties reference table. A number of different sections include a wide variety of commonly-used semiconductor data. All data can be viewed, printed, or copied to the stack for use in further calculations.

Field Descriptions

Below is a list of fields found in each section. Due to limited space in this manual, the list has been abbreviated. The complete list of properties can be found in EE•Pro itself. All properties listed are at 300 K unless otherwise specifically stated.

Module	Fields
Semiconductors	Semiconductor: Press CHOOS or ↕ to select Si or GaAs. Atoms: (<i>Atoms</i>) Displays real number. At Wt: (<i>Atomic Weight</i>) Displays real number. Br Fld: (<i>Breakdown Field</i>) Displays real number. ...
III-V, II-VI Compounds	Compound: Press CHOOS or ↕ to select compound. EG: (<i>Band Gap</i>) Displays real number. μn: (<i>n - Mobility</i>) Displays real number. μp: (<i>p - Mobility</i>) Displays real number. ...

Module	Fields
Si Donor Levels	Li: Displays real number. Sb: Displays real number. P: Displays real number. ...
Si Acceptor Levels	Mg(CD): Displays real number. Mg(CB): Displays real number. Cs: Displays real number. ...
SiO2/Si3N4 Colors	Color: Press CHOOS or to select color. SiO2: (<i>Film Thickness</i>) Displays real number. Si3N4: (<i>Film Thickness</i>) Displays real number. Order: (<i>Order</i>) Displays real number.

Using Semiconductor Properties

1. If the first field is a choose field (Semiconductors, III-V & II-VI Compounds, and SiO2/Si3N4 Colors), press **CHOOS** or to select the desired item. The properties of that item will then be displayed in the remaining fields.
2. Scroll down to select the desired property.
3. Once you have selected a property, you can
 - Press **VIEW** to display it in a text view.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **PRINT** to send one or all to a printer.
4. *Optional:* When finished, press to go to the previous screen or **HOME** to go to the home screen.

Example

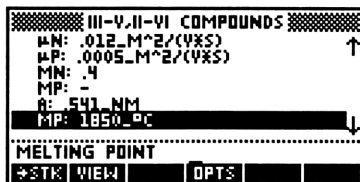
MODES	∠: Degrees	Result: Symbolic
(Press)	Coord: Rectangular	Units: On
	Format: Standard	Help: On
	Digits: N/A	Font: Small

Find the density of zinc sulfide.

1. From the Semiconductor Properties menu, scroll down to III-V, II-VI Compounds and press .
2. If there are no units, press **UNITS** to display them.
3. In the **Compound** field press **CHOOS** to select ZnS.

4. Find the melting point by

- Scrolling down to the **p** field or
- Press **OPTS** **NXT** **FIND**. Type ρ (**R**) and press **ENTER**. (If necessary, first press **ON** to clear the previous search.)



5. Once you have found the density, you can

- Press **VIEW** to display the property in a text view.
- Press **→STK** to copy one or all to the HP 48 stack.
- Press **OPTS** **NXT** **PRINT** to send one or all to a printer.

5. When you are finished, press **◀** to return to the Semiconductor Properties screen.

Chapter 37

Boolean Expressions

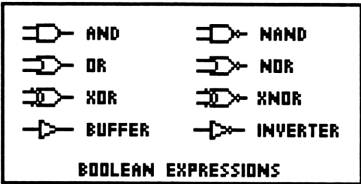
Analysis
Equations
Reference
<i>Boolean Expressions</i>

This chapter covers the Boolean expressions reference table, which includes 16 commonly-used Boolean expressions and also a diagram of the most commonly-used logic components.

Using Boolean Expressions

This section lists the rules for two-valued Boolean algebra, where “AND” is represented by “.”, “OR” is represented by “+”, and “NOT” is represented by “/”.

1. Scroll through the Boolean Expressions screen with and or search with **FIND** to select an expression.
2. When you have found the desired item:
 - Press **VIEW** to display it in a text view.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **PRINT** to print one or all to a printer.
3. You can view a picture of the logic components by pressing **PICT** at any time.
4. *Optional:* When finished, press to go to the previous screen or **HOME** to go to the home screen.



Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Find the Exclusive expression.

1. Press **DESC** to toggle the help text and the expressions.
2. Press **OPTS** **NXT** **FIND** to search for the property.



3. Type EXCL and press **ENTER** to start the search. The highlight bar will move to the first match, which is the answer. Press **EXIT** to exit the options menu.
4. Press **VIEW** to display the property in a text view, as shown.
5. When you have finished viewing the property, press any key to return to the previous screen.
6. *Optional:* Press **DESC** to toggle the help text and the expressions back to their original positions.



Bibliography

Mano, M. Morris, *Digital Logic and Computer Design*, Prentice-Hall, Inc., Englewood Cliffs, NJ, 1979, pp 34-54.

Chapter 38





Boolean Algebra Properties

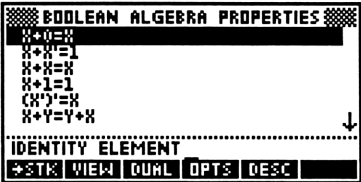
Analysis
Equations
Reference
<i>Boolean Algebra Properties</i>

This chapter covers the Boolean algebra properties reference table, which includes 10 commonly-used Boolean algebra properties and their duals.

Using Boolean Algebra Properties

This section lists the rules for two-valued Boolean algebra, where “AND” is represented by “.”, “OR” is represented by “+”, and “NOT” is represented by “’”.

1. Scroll through the Boolean Algebra Properties screen with  and  or search with **FIND** to select an expression.
2. When you have found the desired item:
 - Press **VIEW** to display it in a text view.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **NXT** **PRINT** to print one or all to a printer.
3. You can view the duals of the Boolean Algebra Properties by pressing **DUAL** at any time.
4. *Optional:* When finished, press  to go to the previous screen or  **HOME** to go to the home screen.

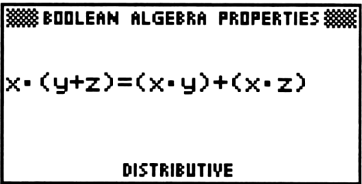


Example

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Find the expression of the Distributive Property.

1. Press **DESC** to toggle the help text and the expressions.
2. Press **OPTS** **NXT** **FIND** to search for the property.
3. Type DIST and press **ENTER** to start the search. (If necessary, first press **ON** to delete the previous search string.) The highlight bar will move to the first match, which is the answer. Press **EXIT** to exit the options menu.
4. Press **VIEW** to display the property in a text view, as shown.
5. When you have finished viewing the property, press any key to return to the previous screen.
6. *Optional:* press **DESC** to toggle the help text and the expressions back to their original positions.



Bibliography

Mano, M. Morris, *Digital Logic and Computer Design*, Prentice-Hall, Inc., Englewood Cliffs, NJ, 1979, pp 34-54.

Chapter 39

Transforms

Analysis Equations Reference <i>Transforms</i>

This chapter covers the Transforms reference table, which includes definitions, properties, and transform pairs for continuous-time Fourier transforms, bilateral Laplace transforms, and bilateral z-transforms. All formulas can be viewed in the EquationWriter, printed, or copied to the stack for future use. However, these sections do not include any Analysis-type routines.

Using Transforms

1. Select Fourier Transforms, Laplace Transforms, or z-Transforms and press **ENTER** or **▶**.
2. Select Definitions, Properties or Transform Pairs and press **ENTER** or **▶**.
By default, the forward transforms are displayed.
3. Select the desired equation and:
 - Press **INV** to display the inverse transforms, which will switch the positions of the time and frequency functions.
 - Press **DESC** to toggle the help text and the transform (not available in Transform Pairs).
 - Press **VIEW** to display the transform in a text view.
 - Press **◀** or **▶** **VIEW** to display the transform in a graphics view. If the graphics form is wider than the screen, press **◀** and **▶** to scroll. When you have finished viewing the transform, press any key to return to the previous screen.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **NXT** **PRINT** to send one or all to a printer.
4. When you have finished with Transforms, press **◀** to go to the previous screen, **▶** **HOME** to go to the home screen, or **ON** to quit EE•Pro.

Example 1

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

What is the definition of the Inverse Fourier transform?

1. In the initial Transforms screen, move the highlight bar to Fourier Transforms and press **ENTER** or **▶**.
2. Move the highlight bar to Definitions and press **ENTER** or **▶**.
3. Move the highlight bar to the second definition and press **◀ VIEW** to view it in a graphics view.
4. Press **◀** and **▶** to scroll. When you have finished viewing the transform, press any key to return to the previous screen.

DEFINITIONS
F(s): $f(-\infty) \cdot F(t) \cdot \exp(-180 \cdot t)$
F(t): $1/2 \cdot \exp(t) \cdot \exp(-180 \cdot t)$
INVERSE FOURIER TRANSFORM
STK VIEW INV OPTS DESC

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) \cdot \exp(j \cdot \omega \cdot t) d\omega$$

F(T) ↔

Example 2

MODES (Press CST)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
-------------------------------------	---	---

Look up the Laplace transform of the time function $f(t)=t$.

1. In the initial Transforms screen, move the highlight bar to Laplace Transforms and press **ENTER** or **▶**.
2. Move the highlight bar to Transform Pairs and press **ENTER** or **▶**.
3. Scroll down to $t: 1/s^2$ and press **◀ VIEW** to view it in a graphics view.
4. When you have finished viewing the transform, press any key to return to the previous screen.

TRANSFORM PAIRS
F(s): F(s)
f(t): 1
f(t)->: $\exp(-\lambda \cdot s)$
U(s): $1/s$
U(s)->: $\exp(-\lambda \cdot s)/s$
T: $1/s^2$
STK VIEW INV OPTS DESC

$$\frac{1}{s^2}$$

T

Chapter 40

Constants

Analysis
Equations
Reference
<i>Constants</i>

This chapter covers the Constants reference table, which includes 43 commonly-used universal constants, descriptions, and units. Many of these constants are embedded in equations in the Equations sections of EE*Pro, and their values are automatically inserted during Solver computations. All constants can be viewed, printed, or copied to the stack for future use.

Using Constants

1. Scroll through the Constants screen with and or search with **FIND** to select a constant.
2. When you have found the desired item:
 - Press **VIEW** to display it in a text view.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **PRINT** to send one or all to a printer.
3. *Optional:* When finished, press to go to the previous screen or to go to the home screen.

Example

MODES (Press)	∠: Degrees Coord: Rectangular Format: Standard Digits: N/A	Result: Symbolic Units: On or Off Help: On Font: Small
--------------------------	---	---

Look up the value of the Boltzmann constant.

1. Press **DESC** or to toggle the position of the constant values and the help text, so that the names of the constants are listed in the main display area. (If necessary, first press to clear the previous search string.)
2. Press **OPTS** **FIND** to activate the search feature.

CONSTANTS
1.380658E-23_J/K
K

3. Type BOLTZ and press **ENTER** to start the search. The highlight bar will move to the first match, which is the answer. To turn units on or off, press **NXT** **UNITS**.
4. Press **NXT** **VIEW** to display the constant in text view as shown here.
5. When you have finished, press any key to return to the previous screen.
6. *Optional:* Press **EXIT** to exit the options menu.
7. *Optional:* Press **DESC** or **VAR** to toggle the help text back to its original position at the bottom of the screen.

Constants Reference Table

Const.	Description	Const.	Description
π	circle ratio	μq	mass μ / mass e-
e	Napier constant	c1	1st radiation constant
γ	Euler constant	c2	2nd radiation constant
ϕ	golden ratio	b	Wien displacement
α	fine structure	λc	e- Compton wavelength
c	speed of light	λn	n Compton wavelength
$\epsilon 0$	permittivity	λp	p+ Compton wavelength
F	Faraday constant	NA	Avogadro constant
G	Newton constant	$\phi 0$	magnetic flux quantum
g	acceleration of gravity	R	molar gas constant
h	Planck constant	a0	Bohr radius
hb	Dirac constant	$R\infty$	Rydberg constant
k	Boltzmann constant	σ	Stefan-Boltzmann constant
$\mu 0$	permeability	μB	Bohr magneton
q	e- charge	μe	e- magnetic moment
em	e- charge / mass	μN	nuclear magneton
me	e- rest mass	μp	p+ magnetic moment
mn	n rest mass	$\mu \mu$	μ magnetic moment
mp	p+ rest mass	SP	standard pressure
$m\mu$	μ rest mass	ST	standard temperature
pe	mass p+ / mass e-	Vm	molar volume at STP
re	classical e- radius		

Bibliography

Based on Cohen and Taylor, "The 1986 Adjustment of the Fundamental Physical Constants," *Rev. Mod. Phys.*, Vol. 59, No. 4, October 1987, 1139-1145.





Chapter 41

SI Prefixes

Analysis
Equations
Reference
<i>SI Prefixes</i>

This chapter covers the SI Prefixes reference table, which includes all currently-accepted prefixes for Le Systeme International d'Unites. All of these prefixes are recognized by the HP 48GX, and all but the most recent four of them (Y, Z, y, and z) are recognized by the HP 48SX.

Using SI Prefixes

1. Scroll through the SI Prefixes screen with  and  or search with **FIND**.
2. When you have found the desired item:
 - Press **VIEW** to display it in a text view.
 - Press **→STK** to copy one or all to the HP 48 stack.
 - Press **OPTS** **NXT** **PRINT** to print one or all to a printer.
3. *Optional:* When finished, press  to go to the previous screen or  **HOME** to go to the home screen.



Chapter 42

Greek Alphabet

Analysis
Equations
Reference
Greek Alphabet

This chapter covers the Greek Alphabet reference table, which includes a picture displaying all uppercase and lowercase letters in the Greek alphabet. Many of these characters are built-in to the HP 48 fonts, but not all.

ALPHA	Α α	IOTA	Ι ι	RHO	Ρ ρ
BETA	Β β	KAPPA	Κ κ	SIGMA	Σ σ
GAMMA	Γ γ	LAMBDA	Λ λ	TAU	Τ τ
DELTA	Δ δ	MU	Μ μ	UPSILON	Υ υ
EPSILON	Ε ε	NU	Ν ν	PHI	Φ φ
ZETA	Ζ ζ	XI	Ξ ξ	CHI	Χ χ
ETA	Η η	OMICRON	Ο ο	PSI	Ψ ψ
THETA	Θ θ	PI	Π π	OMEGA	Ω ω
GREEK ALPHABET					

Press any key to return to the previous screen. (This is simply a display. These characters can not be copied to the stack.)

(Note that the uppercase and lowercase Greek letters alternate positions from one line to the next.)

Programming & Advanced Use

Chapter 43

Programmable Commands

This chapter covers programming with *EE•Pro* and includes a summary of the programmable commands. Each of these commands can be executed directly from the HP 48 stack or included in user programs. For more information about programming, see the HP 48 manual.

This chapter covers:

- ☐ Using Programmable Commands
- ☐ Object Syntax
- ☐ EE Library Commands
- ☐ AC Circuits
- ☐ Polyphase Circuits
- ☐ Filter Design
- ☐ Gain and Frequency
- ☐ Fourier Transforms
- ☐ Two-Port Networks
- ☐ Transformer Performance
- ☐ Transmission Lines
- ☐ Binary Arithmetic
- ☐ Register Operations
- ☐ Bit Operations
- ☐ Binary Conversions
- ☐ Binary Comparisons
- ☐ Binary Modes
- ☐ Miscellaneous Binary Operations
- ☐ Karnaugh Map
- ☐ Algebraic Functions
- ☐ Error Functions
- ☐ Capital Budgeting
- ☐ Reference

Using Programmable Commands

Programmable commands can be used from the stack or incorporated into a user program. The tables in this chapter are organized to provide you with the inputs and outputs of each command, as well as the types of arguments accepted. The object syntax table lists the abbreviations used for the different argument types. For more information about writing programs see your HP 48 User's Guide.

Using Programmable Commands From the Stack

1. Type the input argument(s). For example, type the input array for the \rightarrow FFT command [1 2 3 2 1].
2. Enter the command by either typing it or using the EE•Pro library menu:
 - \rightarrow FFT or
 - Press (HP 48GX) or (HP 48SX) then \rightarrow FFT.

Object Syntax

These are the various objects listed as inputs or outputs in this chapter.

Object Syntax	Description	Examples
x y a b c d	Real number	1.523 5.55 10
m n	Positive integer (real number)	1 2 3
(x,y)	Complex number or rectangular point	(0,1) (1,2) (1.5,-3.3)
z	Real or complex number	1.523 (0,1)
x_unit	Real number with units	10_m/s 20.587_ft
{list}	List of objects	{ 2 2 3 } { (0,1) (1,2) }
[array]	Real or complex array	[1 2 3] [(0,1) (1,2)]
'name'	Global or local name	'X' 'Y' 'Z'
'symb'	Algebraic expression or name	'SIN(X)' 'LN(Z)' 'X'
#bin	Binary integer	10110
'expr_x'	Real number, algebraic or global name	2.7 'SIN(X)' 'X'
'expr_z'	Real or complex number, algebraic or global name	2.7 (10, 52) 'SIN(X)' 'X'
T/F	1 (True) or 0 (False)	1 0

EE Library Commands

These are the commands in the EE•Pro library menu.

Command/Description	Input(s)	Output
EE Runs EE•Pro	-	-
ABOUTEE Displays the EE•Pro 'About' screen	-	-
CMDSEE Displays the EE•Pro commands in the menu keys	-	-
GOEE Goes to the specified screen in EE•Pro, see chapter 32	{list}	specified screen

AC Circuits

These commands are found in the **CMDS** **AC** menu. For more information, see Chapter 3, “AC Circuits.”

Command/Description	Input(s)	Output(s)
VZDIV Voltage Divider (Z)	Vs: 'expr_z' Z: {Z ₁ .. Z _n }	IL: 'expr_z' V: {V ₁ .. V _n }
VYDIV Voltage Divider (Y)	Vs: 'expr_z' Y: {Y ₁ .. Y _n }	IL: 'expr_z' V: {V ₁ .. V _n }
CZDIV Current Divider (Z)	Is: 'expr_z' Z: {Z ₁ .. Z _n }	VL: 'expr_z' I: {I ₁ .. I _n }
CYDIV Current Divider (Y)	Is: 'expr_z' Y: {Y ₁ .. Y _n }	VL: 'expr_z' I: {I ₁ .. I _n }
ZCPERF Circuit Performance (Z)	Vs: 'expr_z' Zs: 'expr_z' ZL: 'expr_z'	VL: 'expr_z' IL: 'expr_z' P: 'expr_x' Q: 'expr_x' VI: 'expr_z' θ: 'expr_x' PF: 'expr_x' Pmax: 'expr_x' ZLopt: 'expr_z'

YPERF Circuit Performance (Y)	Vs: 'expr_z' Ys: 'expr_z' YL: 'expr_z'	VL: 'expr_z' IL: 'expr_z' P: 'expr_x' Q: 'expr_x' VI: 'expr_z' θ: 'expr_x' PF: 'expr_x' Pmax: 'expr_x' YLopt: 'expr_z'
Y↔Δ Wye to Delta Conversion	Z1: 'expr_z' Z2: 'expr_z' Z3: 'expr_z'	ZA: 'expr_z' ZB: 'expr_z' ZC: 'expr_z'
Δ↔Y Delta to Wye Conversion	ZA: 'expr_z' ZB: 'expr_z' ZC: 'expr_z'	Z1: 'expr_z' Z2: 'expr_z' Z3: 'expr_z'

Polyphase Circuits

These commands are found in the **CMDS PHASE** menu. For more information, see Chapter 4, “Polyphase Circuits.”

Command/Description	Input(s)	Output(s)
Y↔Δ Wye to Delta Conversion	Z1: 'expr_z' Z2: 'expr_z' Z3: 'expr_z'	ZA: 'expr_z' ZB: 'expr_z' ZC: 'expr_z'
Δ↔Y Delta to Wye Conversion	ZA: 'expr_z' ZB: 'expr_z' ZC: 'expr_z'	Z1: 'expr_z' Z2: 'expr_z' Z3: 'expr_z'
ΔLOAD Balanced Delta Load	VAB: 'expr_z' Z: 'expr_z'	VBC: 'expr_z' VCA: 'expr_z' VAN: 'expr_z' VCN: 'expr_z' IA: 'expr_z' IB: 'expr_z' IC: 'expr_z' P: 'expr_x' WAB: 'expr_x' WAC: 'expr_x'

YLOAD Balanced Wye Load	V12: 'expr_z' Z: 'expr_z'	V23: 'expr_z' V31: 'expr_z' V1N: 'expr_z' V2N: 'expr_z' V3N: 'expr_z' I1: 'expr_z' I2: 'expr_z' I3: 'expr_z' P: 'expr_x' W12: 'expr_x' W13: 'expr_x'
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Filter Design

These commands are found in the **CMDS FILTER** menu. For more information, see Chapter 6, “Filter Design.”

Command/Description	Input(s)	Output(s)
CHLP Low Pass Chebyshev Filter	R: x f0: x f1: x ΔdB: x Ripple: x	C1: x L2: x ... # of arguments: x
CHHP High Pass Chebyshev Filter	R: x f0: x f1: x ΔdB: x Ripple: x	L1: x C2: x ... # of arguments: x
CHBP Band Pass Chebyshev Filter	R: x f0: x f1: x ΔdB: x Bandwidth: x Ripple: x	C1: x L1: x L2: x C2: x ... # of arguments: x
CHBE Band Elimination Chebyshev Filter	R: x f0: x f1: x ΔdB: x Bandwidth: x Ripple: x	L1: x C1: x C2: x L2: x ... # of arguments: x
BWLP Low Pass Butterworth Filter	R: x f0: x f1: x ΔdB: x	C1: x L2: x ... # of arguments: x

BWHP High Pass Butterworth Filter	R: x f0: x f1: x ΔdB: x	L1: x C2: x ... # of arguments: x
BWBP Band Pass Butterworth Filter	R: x f0: x f1: x ΔdB: x Bandwidth: x	C1: x L1: x L2: x C2: x ... # of arguments: x
BWBE Band Elimination Butterworth Filter	R: x f0: x f1: x ΔdB: x Bandwidth: x	L1: x C1: x C2: x L2: x ... # of arguments: x
ACLP Low Pass Active Filter	f0: 'expr_x' A: 'expr_x' Q: 'expr_x' C: 'expr_x'	R1: 'expr_x' C2: 'expr_x' R3: 'expr_x' R4: 'expr_x' C5: 'expr_x'
ACHP High Pass Active Filter	f0: 'expr_x' A: 'expr_x' Q: 'expr_x' C: 'expr_x'	C1: 'expr_x' R2: 'expr_x' C3: 'expr_x' C4: 'expr_x' R5: 'expr_x'
ACBP Band Pass Active Filter	f0: 'expr_x' A: 'expr_x' Q: 'expr_x' C: 'expr_x'	R1: 'expr_x' R2: 'expr_x' C3: 'expr_x' C4: 'expr_x' R5: 'expr_x'

Gain and Frequency

These commands are found in the **CMDS** **GAIN** menu. For more information, see Chapter 7, “Gain and Frequency.”

Command/Description	Input(s)	Output(s)
XFERPZ Transfer Function, Roots	Constant: c Zeros: [A _M .. A ₀] Poles: [A _N .. A ₀]	H(s): 'symb'
XFERND Transfer Function, Coefficients	Constant: c Num: [R ₁ .. R _M] Denom: [R ₁ .. R _N]	H(s): 'symb'

PFER Partial Fraction Expansion, Roots	Constant: c Zeros: [R ₁ .. R _M] Poles: [R ₁ .. R _N]	PFE: 'symb'
PFEC Partial Fraction Expansion, Coefficients	Constant: c Num: [A _M .. A ₀] Denom: [A _N .. A ₀]	PFE: 'symb'

Fourier Transforms

These commands are found in the **CMDS** **FFT** menu. For more information, see Chapter 8, “Fourier Transforms.”

Command/Description	Input(s)	Output(s)
→FFT Fast Fourier Transform	Time: [array]	Freq: [array]
FFT→ Inverse Fast Fourier Transform	Freq: [array]	Time: [array]

Two-Port Networks

These commands are found in the **CMDS** **2PORT** menu. For more information, see Chapter 9, “Two-Port Networks.”

Note: 'name' can be the global name 'z', 'y', 'h', 'g', 'a', or 'b'.

Command/Description	Input(s)	Output(s)
PCON Parameter Conversion	Input Type: 'name' ..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z' Output Type: 'name'	..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z'
PCPERF Circuit Performance	Parameter Type: 'name' ..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z' Vs: 'expr_z' Zs: 'expr_z' ZL: 'expr_z'	Zin: 'expr_z' Iout: 'expr_z' Vout: 'expr_z' Zout: 'expr_z' I2/I1: 'expr_z' V2/V1: 'expr_z' V2/Vs: 'expr_z' GP: 'expr_z' Pav: 'expr_z' Pmax: 'expr_z' Zlopt: 'expr_z'

I2PCAS Inter-connected Two-Ports in Cascade configuration	1st Input Type: 'name' ..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z' 2nd Input Type: 'name' ..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z' Output Type: 'name'	..11: 'expr_z' ..12: 'expr_z' ..21: 'expr_z' ..22: 'expr_z'
I2PSS Inter-connected Two-Ports in Series-Series configuration	same as I2PCAS	same as I2PCAS
I2PPP Inter-connected Two-Ports in Parallel-Parallel configuration	same as I2PCAS	same as I2PCAS
I2PSP Inter-connected Two-Ports in Series-Parallel configuration	same as I2PCAS	same as I2PCAS
I2PPS Inter-connected Two-Ports in Parallel-Series configuration	same as I2PCAS	same as I2PCAS

Transformer Performance

These commands are found in the **CMDS** **[NEXT]** **XFMR** menu. For more information, see Chapter 10, “Transformer Performance.”

Command/Description	Input(s)	Output(s)
OCTST Open Circuit Test	V1: 'expr_x' V2: 'expr_x' I1: 'expr_x' P1: 'expr_x'	n: 'expr_x' Q1: 'expr_x' Gc: 'expr_x' Bc: 'expr_x'
SCTST Closed Circuit Test	V1: 'expr_x' I1: 'expr_x' P1: 'expr_x' kVA: 'expr_x' V1R: 'expr_x'	n: 'expr_x' Q1: 'expr_x' R1: 'expr_x' R2: 'expr_x' X1: 'expr_x' X2: 'expr_x'
CHAIN Chain Parameters	Z1: 'expr_z' Z2: 'expr_z' n: 'expr_x' Gc: 'expr_x' Bc: 'expr_x'	A: 'expr_z' B: 'expr_z' C: 'expr_z' D: 'expr_z'

Transmission Lines

These commands are found in the **CMDS** **NXT** **XMS** menu. For more information, see Chapter 11, “Transmission Lines.”

Command/Description	Input(s)	Output(s)
XLCHR Line Characteristics	L: 'expr_x' R: 'expr_x' G: 'expr_x' C: 'expr_x' ZL: 'expr_z' d: 'expr_x' f: 'expr_x'	Z0: 'expr_z' Y0: 'expr_z' α: 'expr_x' β: 'expr_x' λ: 'expr_x' vp: 'expr_x' Zoc: 'expr_z' Zsc: 'expr_z' p: 'expr_z' SWR: 'expr_x'
XLPAR Line Parameters	Zoc: 'expr_z' Zsc: 'expr_z' d: 'expr_x' f: 'expr_x'	R: 'expr_x' L: 'expr_x' G: 'expr_x' C: 'expr_x' Z0: 'expr_z' Y0: 'expr_z' α: 'expr_x' β: 'expr_x' vp: 'expr_x'
XLFAULT Fault Location Estimate	Xin: 'expr_x' R0: 'expr_x' β: 'expr_x'	docmin: 'expr_x' dscmin: 'expr_x'
XLZ Lossless Line Impedance	ZL: 'expr_z' R0: 'expr_x'	β*d1: 'expr_x' β*d1-sc: 'expr_x' β*d1-oc: 'expr_x' β*d2: 'expr_x' β*d2-sc: 'expr_x' β*d2-oc: 'expr_x'

Binary Arithmetic

These commands are found in the **CMDS** **NXT** **COMP** **ARTH** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
ADD16C Binary Addition	Binary: #bin x Binary: #bin x	Sum: #bin x

SUB16C Binary Subtraction	Binary: #bin x Binary: #bin x	Difference: #bin x
MULT16C Binary Multiplication	Binary: #bin x Binary: #bin x	Product: #bin x
DIV16C Binary Division	Dividend: #bin x Divisor: #bin x	Quotient: #bin
RMD16C Remainder	Dividend: #bin x Divisor: #bin x	Remainder: #bin
NEG16C Binary Negation	Binary: #bin	Result: #bin
ABS16C Absolute Value	Binary: #bin	Result: #bin

Register Operations

These commands are found in the **CMDS** **NXT** **COMP** **REG** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
SL16C Shift Left	Binary: #bin	Result: #bin
SR16C Shift Right	Binary: #bin	Result: #bin
RL16C Rotate Left	Binary: #bin	Result: #bin
RR16C Rotate Right	Binary: #bin	Result: #bin
RLC16C Rotate Left Through Carry	Binary: #bin	Result: #bin
RRC16C Rotate Right Through Carry	Binary: #bin	Result: #bin
SLN16C Shift Left n Bits	Binary: #bin n: #bin x	Result: #bin
SRN16C Shift Right n Bits	Binary: #bin n: #bin x	Result: #bin
RLN16C Rotate Left n Bits	Binary: #bin n: #bin x	Result: #bin
RRN16C Rotate Right n Bits	Binary: #bin n: #bin x	Result: #bin
RLCN16C Rotate Left Through Carry n Bits	Binary: #bin n: #bin x	Result: #bin
RRCN16C Rotate Right Through Carry n Bits	Binary: #bin n: #bin x	Result: #bin
ASR16C Arithmetic Shift Right	Binary: #bin	Result: #bin

Bit Operations

These commands are found in the **CMDS** **NXT** **COMP** **BIT** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
SB Set Bit	Binary: #bin Bit #: #bin x	Result: #bin
CB Clear Bit	Binary: #bin Bit #: #bin x	Result: #bin
B? Check Bit	Binary: #bin Bit #: #bin x	Result: #bin
ΣB Sum of Bits	Binary: #bin	Result: #bin

Binary Conversions

These commands are found in the **CMDS** **NXT** **COMP** **CNVT** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
R→B16C Real to Binary Conversion	Real: x	Result: #bin
B→R16C Binary to Real Conversion	Binary: #bin	Result: x
→IEEE Real to IEEE 32-bit Format Conversion	Real: x	Result: #bin
IEEE→ IEEE 32-bit Format to Real Conversion	Binary: #bin	Result: x

Binary Comparisons

These commands are found in the **CMDS** **NXT** **COMP** **CMPR** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
==16C Binary Equals	Binary: #bin x Binary: #bin x	Result: T/F
≠16C Binary Not Equals	Binary: #bin x Binary: #bin x	Result: T/F
<16C Binary Less Than	Binary: #bin x Binary: #bin x	Result: T/F

>16C Binary Greater Than	Binary: #bin x Binary: #bin x	Result: T/F
≤16C Binary Less Than or Equal	Binary: #bin x Binary: #bin x	Result: T/F
≥16C Binary Greater Than or Equal	Binary: #bin x Binary: #bin x	Result: T/F

Binary Modes

These commands are found in the **CMDS** **[NXT]** **COMP** **MODES** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
SETC Set Carry Flag	-	Set User Flag 4
CLRC Clear Carry Flag	-	Clear User Flag 4
CRRY? Check Carry Flag	-	Test Flag 4: T/F
SETR Set Range Flag	-	Set User Flag 5
CLRR Clear Range Flag	-	Clear User Flag 5
RNG? Check Range Flag	-	Test User Flag 5: T/F
UNSGN Set Unsigned Mode	-	Put 48 in unsigned mode
ONES Set One’s Complement Mode	-	Put 48 in one’s complements mode
TWOS Set Two’s Complement Mode	-	Put 48 in two’s complements mode
CMP? Complement Mode	-	Complement mode: 0,1,2

Miscellaneous Binary Operations

These commands are found in the **CMDS** **[NXT]** **COMP** **[NXT]** **MISC** menu. These operations cannot be found in any *EE•Pro* screen. They are provided as programmable commands in order to complete the set of commands that are provided by the HP 16C “Computer Scientist Calculator”

Command/Description	Input(s)	Output(s)
DBLx Double-word Multiply	Binary: #bin Binary: #bin	Product, 1st ½: #bin Product, 2nd ½: #bin

DBL+ Double-word Divide	Dividend, 1st ½: #bin Dividend, 2nd ½: #bin Divisor: #bin	Quotient: #bin
DBLR Double-word Divide Remainder	Dividend, 1st ½: #bin Dividend, 2nd ½: #bin Divisor: #bin	Remainder: #bin
LJ16C Left Justify	Binary: #bin	Binary: #bin n: #bin (number of bits shifted)
MSKL Left-justified Mask with n Bits	n: #bin x	Binary: #bin
MSKR Right-justified Mask with n Bits	n: #bin x	Binary: #bin
FLOAT	Binary: #bin ₁ Binary: #bin ₂	REAL: #bin ₁ *2 ^(#bin₁)
FIXED	Real: x	32-bit Mantissa: #bin Exponent of 2: #bin

Karnaugh Map

These commands are found in the **CMDS** **[NXT]** **COMP** **[NXT]** menu. For more information, see Chapter 12, “Computer Engineering.”

Command/Description	Input(s)	Output(s)
KMAP Karnaugh Map	Minterms: {# ₁ .. # _N } Don't Care: {# ₁ .. # _M } Vars: 'A..Z'	Prime Implicants: 'string'

Algebraic Functions

These commands are found in the **CMDS** **[NXT]** **ALGB** menu. For more information, see Chapter 13, “Algebraic Functions.”

Command/Description	Input(s)	Output(s)
PFEC Partial Fraction Expansion, Coefficients	Constant: c Num: [A _M .. A ₀] Denom: [A _N .. A ₀]	PFE: 'symb'
PFER Partial Fraction Expansion, Roots	Coefficient: c Num: [R ₁ .. R _M] Denom: [R ₁ .. R _N]	PFE: 'symb'
POLYC Polynomial Coefficients	Roots: [R ₁ .. R _N]	Coefs: [A _N .. A ₀]

POLYE Polynomial Equation	Coefs: [$A_N .. A_0$] Var: 'name'	Poly: 'symb'
POLYR Polynomial Roots	Coefs: [$A_N .. A_0$]	Roots: [$R_1 .. R_N$]
SIMPL Symbolic Simplification	Expr: 'expr_z'	Simpl: 'symb'
TYLRA Taylor Polynomial	Expr: 'symb' Var: 'name' Order: x Point: 'expr_z'	Taylor: 'symb'

Error Functions

These commands are found in the **CMDS** **NXT** **ERROR** menu. For more information, see Chapter 14, “Error Function.”

Command/Description	Input(s)	Output(s)
ERF Error Function	X: x	Result: x
ERFC Inverse Error Function	X: x	Result: x

Capital Budgeting

These commands are found in the **CMDS** **NXT** **BUDG** menu. For more information, see Chapter 15, “Capital Budgeting.”


Command/Description	Input(s)	Output(s)
PAYB Payback Period	Cash: [$T_0 .. T_n$]	Payback: x
NPV Net Present Value	Cash: [$T_0 .. T_n$] Discount rate: x	NPV: x
IRR Internal rate of return	Cash: [$T_0 .. T_n$]	IRR: x
PIDX Profitability Index	Cash: [$T_0 .. T_n$] Discount rate: x	PI: x

Reference

These commands are found in the **CMDS** **NXT** **NXT** **REF** menu. For more information, see Chapter 35 “Standard Component Values” and Chapter 40, “Constants”.

Command/Description	Input(s)	Output(s)
RVAL Standard Resistor Value	Value: x Tolerance: y	Std Value: x_unit Color Bands: “string”
LVAL Standard Inductor Value	Value: x Tolerance: y	Std Value: x_unit
CVAL Standard Capacitor Value	Value: x Tolerance: y	Std Value: x_unit
CONS Constant Function	Constant: ‘name’	Value: x or x_unit

CONS: Constants

This command provides programmable access to the values of the constants in the Constants reference table. The value of the constant will be returned with units if user flag 61 is clear or without units if user flag 61 is set. (For more information, see Appendix C, “User Flags.”) CONS can be used in an algebraic expression, such as 'CONS(h)', or in a user program, such as « 'h' CONS ». CONS is also affected by system flags -2 and -3, which control symbolic constants and numeric results—if either flag -2 or -3 is set, 'h' CONS will return a numeric value, but if both are clear, 'h' CONS will return 'CONS(h)', which will only evaluate to a numeric value after . To replace a built-in constant with a different value, you can place an override constant in a variable named “\$” followed by the constant name, such as '\$h'.

Example: *Create an equation with a constant.* The mass-energy relation is $E = mc^2$. To write this as an HP 48 equation which accesses the speed of light constant included in EE•Pro, use the equation:

$$'E = m * CONS(c) ^ 2'$$

This equation will call the command CONS to access the value of the speed of light constant **c**. The value of **c** will be returned as 299792458_m/s if flag 61 is clear (units on), or as 299792458 if flag 61 is set (units off).

Example: *Override a built-in constant.* To solve gravitational problems on the moon (instead of the Earth), the acceleration of gravity **g**, must be overridden. To override the built-in value of 9.80665 m/s (the gravitational acceleration at the surface of the Earth), store the value 1.55 m/s into the variable '\$g'. The value of **g** will now be returned by CONS as 1.55 m/s. To return to the original value, purge the variable '\$g' from user memory.

Chapter 44

Programmable Screens

EE•Pro is designed to allow you to jump directly to any Analysis, Equation, or Reference screen from the HP 48 stack with the GOEE command. This chapter describes how to use these “programmable screens.”

This chapter covers:










- ☐ Using Programmable Screens
- ☐ Analysis Screens
- ☐ Equations Screens
- ☐ Reference Screens

Using Programmable Screens

The GOEE command, located in the library menu of EE•Pro, allows you to jump directly to a particular screen in EE•Pro.


















Example: HP 48 Stack

Browse Constants from the HP 48 stack.

1. From the HP 48 stack, type   3  7  to put the list { 3 7 } on the stack.
2. Press  (on the HP 48GX) or   (on the HP 48SX), then press   and the Constants screen will appear.

Example: User Program

Create a user program that goes directly to the Constants reference table from the HP 48 stack.

1. Type     3  7        to put the program « { 3 7 } GOEE » on the stack.
2. Type    GOCONS  to put the name 'GOCONS' on the stack. Press  to store the program into GOCONS.

3. To execute GOCONS from the HP 48 stack, press **VAR** **GOCO** and the Constants screen will appear.
The program could also be stored in your custom menu for quick access.
For more information, see your HP 48 User's Guide.

Analysis Screens

This is a summary of the EE•Pro Analysis screens and their corresponding path lists for use with the GOEE command.

Menu Item	Path
Home	{ }
Analysis	{ 1 }
AC Circuits	{ 1 1 }
Impedance Calculations	{ 1 1 1 }
Voltage Divider	{ 1 1 2 }
Current Divider	{ 1 1 3 }
Circuit Performance	{ 1 1 4 }
Wye \leftrightarrow Δ Conversion	{ 1 1 5 }
Polyphase Circuits	{ 1 2 }
Wye \leftrightarrow Δ Conversion	{ 1 2 1 }
Balanced Wye Load	{ 1 2 2 }
Balanced Δ Load	{ 1 2 3 }
Ladder Network	{ 1 3 }
Filter Design	{ 1 4 }
Chebyshev Filter	{ 1 4 1 }
Butterworth Filter	{ 1 4 2 }
Active Filter	{ 1 4 3 }
Gain and Frequency	{ 1 5 }
Transfer Function	{ 1 5 1 }
Bode Plots	{ 1 5 2 }
Fourier Transforms	{ 1 6 }
FFT	{ 1 6 1 }
Inverse FFT	{ 1 6 2 }
Two-Port Networks	{ 1 7 }
Parameter Conversion	{ 1 7 1 }
Circuit Performance	{ 1 7 2 }
Interconnected Two-Ports	{ 1 7 3 }
Transformer Performance	{ 1 8 }
Open Circuit Test	{ 1 8 1 }
Short Circuit Test	{ 1 8 2 }

Chain Parameters	{ 1 8 3 }
Transmission Lines	{ 1 9 }
Line Characteristics	{ 1 9 1 }
Line Parameter Calculations	{ 1 9 2 }
Fault Location Estimate	{ 1 9 3 }
Lossless Line Impedance	{ 1 9 4 }
Computer Engineering	{ 1 10 }
Binary Arithmetic	{ 1 10 1 }
Register Operations	{ 1 10 2 }
Bit Operations	{ 1 10 3 }
Binary Conversions	{ 1 10 4 }
Binary Comparisons	{ 1 10 5 }
Karnaugh Map	{ 1 10 6 }
Algebraic Functions	{ 1 11 }
Partial Fraction Expansion	{ 1 11 1 }
Piecewise Functions	{ 1 11 2 }
Polynomial Coefficients	{ 1 11 3 }
Polynomial Equation	{ 1 11 4 }
Polynomial Roots	{ 1 11 5 }
Symbolic Simplification	{ 1 11 6 }
Taylor Polynomial	{ 1 11 7 }
Error Functions	{ 1 12 }
Capital Budgeting	{ 1 13 }

Equations Screens

This is a summary of the EE•Pro Equations screens and their corresponding path lists for use with the GOEE command.

Menu Item	Path
Home	{ }
Equations	{ 2 }
Resistive Circuits	{ 2 1 }
Resistance and Conductance	{ 2 1 1 }
Ohm's Law and Power	{ 2 1 2 }
Temperature Effect	{ 2 1 3 }
Maximum Power Transfer	{ 2 1 4 }
V and I Source Equivalence	{ 2 1 5 }
Capacitance and Electric Fields	{ 2 2 }
Point Charge	{ 2 2 1 }

Long Charged Line	{ 2 2 2 }
Charged Disk	{ 2 2 3 }
Parallel Plates	{ 2 2 4 }
Parallel Wires	{ 2 2 5 }
Coaxial Cable	{ 2 2 6 }
Sphere	{ 2 2 7 }
Inductance and Magnetism	{ 2 3 }
Long Line	{ 2 3 1 }
Long Strip	{ 2 3 2 }
Parallel Wires	{ 2 3 3 }
Loop	{ 2 3 4 }
Coaxial Cable	{ 2 3 5 }
Skin Effect	{ 2 3 6 }
Electron Motion	{ 2 4 }
Electron Beam Deflection	{ 2 4 1 }
Thermionic Emission	{ 2 4 2 }
Photoemission	{ 2 4 3 }
Meters and Bridge Circuits	{ 2 5 }
Amp, Volt, and Ohmmeter	{ 2 5 1 }
Wheatstone Bridge	{ 2 5 2 }
Wien Bridge	{ 2 5 3 }
Maxwell Bridge	{ 2 5 4 }
Owen Bridge	{ 2 5 5 }
Sym. Resistive Attenuator	{ 2 5 6 }
Unsym. Resistive Attenuator	{ 2 5 7 }
RL and RC Circuits	{ 2 6 }
RL Natural Response	{ 2 6 1 }
RC Natural Response	{ 2 6 2 }
RL Step Response	{ 2 6 3 }
RC Step Response	{ 2 6 4 }
RL Series to Parallel	{ 2 6 5 }
RC Series to Parallel	{ 2 6 6 }
RLC Circuits	{ 2 7 }
Series Impedance	{ 2 7 1 }
Parallel Admittance	{ 2 7 2 }
RLC Natural Response	{ 2 7 3 }
Underdamped Transient	{ 2 7 4 }
Critically-Damped Transient	{ 2 7 5 }
Overdamped Transient	{ 2 7 6 }
AC Circuits	{ 2 8 }
RL Series Impedance	{ 2 8 1 }
RC Series Impedance	{ 2 8 2 }
Impedance \leftrightarrow Admittance	{ 2 8 3 }
Two Impedances in Series	{ 2 8 4 }
Two Impedances in Parallel	{ 2 8 5 }

Polyphase Circuits	{ 2 9 }
Balanced Δ Network	{ 2 9 1 }
Balanced Wye Network	{ 2 9 2 }
Power Measurements	{ 2 9 3 }
Electrical Resonance	{ 2 10 }
Parallel Resonance I	{ 2 10 1 }
Parallel Resonance II	{ 2 10 2 }
Resonance in Lossy Inductor	{ 2 10 3 }
Series Resonance	{ 2 10 4 }
OpAmp Circuits	{ 2 11 }
Basic Inverter	{ 2 11 1 }
Non-Inverting Amplifier	{ 2 11 2 }
Current Amplifier	{ 2 11 3 }
Transconductance Amplifier	{ 2 11 4 }
Level Detector (Inverting)	{ 2 11 5 }
Level Detector (Non-Inverting)	{ 2 11 6 }
Differentiator	{ 2 11 7 }
Differential Amplifier	{ 2 11 8 }
Solid State Devices	{ 2 12 }
Semiconductor Basics	{ 2 12 1 }
PN Junctions	{ 2 12 2 }
PN Junction Currents	{ 2 12 3 }
Transistor Currents	{ 2 12 4 }
Ebers-Moll Equations	{ 2 12 5 }
Ideal Currents - pnp	{ 2 12 6 }
Switching Transients	{ 2 12 7 }
MOS Transistor I	{ 2 12 8 }
MOS Transistor II	{ 2 12 9 }
MOS Inverter (Resistive)	{ 2 12 10 }
MOS Inverter (Saturated)	{ 2 12 11 }
MOS Inverter (Depletion)	{ 2 12 12 }
CMOS Transistor Pair	{ 2 12 13 }
Junction FET	{ 2 12 14 }
Linear Amplifiers	{ 2 13 }
BJT (Common Base)	{ 2 13 1 }
BJT (Common Emitter)	{ 2 13 2 }
BJT (Common Collector)	{ 2 13 3 }
FET (Common Gate)	{ 2 13 4 }
FET (Common Source)	{ 2 13 5 }
FET (Common Drain)	{ 2 13 6 }
Darlington (CC-CC)	{ 2 13 7 }
Darlington (CC-CE)	{ 2 13 8 }
Emitter-Coupled Amplifier	{ 2 13 9 }
Differential Amplifier	{ 2 13 10 }
Source-Coupled JFET Pair	{ 2 13 11 }

Class A, B, and C Amplifiers	{ 2 14 }
Class A Amplifier	{ 2 14 1 }
Power Transistor	{ 2 14 2 }
Push-Pull Principle	{ 2 14 3 }
Class B Amplifier	{ 2 14 4 }
Class C Amplifier	{ 2 14 5 }
Transformers	{ 2 15 }
Ideal Transformer	{ 2 15 1 }
Linear Equivalent Circuit	{ 2 15 2 }
Motors and Generators	{ 2 16 }
Energy Conversion	{ 2 16 1 }
DC Generator	{ 2 16 2 }
Separately-Excited DC Genr.	{ 2 16 3 }
DC Shunt Generator	{ 2 16 4 }
DC Series Generator	{ 2 16 5 }
Separately-Excited DC Motor	{ 2 16 6 }
DC Shunt Motor	{ 2 16 7 }
DC Series Motor	{ 2 16 8 }
Permanent Magnet Motor	{ 2 16 9 }
Induction Motor I	{ 2 16 10 }
Induction Motor II	{ 2 16 11 }
Single-Phase Induction Motor	{ 2 16 12 }
Synchronous Machines	{ 2 16 13 }

Reference Screens

This is a summary of the EE•Pro Reference screens and their corresponding path lists for use with the GOEE command.

Menu Item	Path
Home	{ }
Reference	{ 3 }
Resistor Color Chart	{ 3 1 }
Standard Component Values	{ 3 2 }
Semiconductor Properties	{ 3 3 }
Semiconductors	{ 3 3 1 }
III-V, II-VI Compounds	{ 3 3 2 }
Si Donor Levels	{ 3 3 3 }
Si Acceptor Levels	{ 3 3 4 }
SiO2/Si3N4 Colors	{ 3 3 5 }
Boolean Expressions	{ 3 4 }
Boolean Algebra Properties	{ 3 5 }
Transforms	{ 3 6 }
Fourier Transforms	{ 3 6 1 }
Definitions	{ 3 6 1 1 }
Properties	{ 3 6 1 2 }
Transform Pairs	{ 3 6 1 3 }
Laplace Transforms	{ 3 6 2 }
Definitions	{ 3 6 2 1 }
Properties	{ 3 6 2 2 }
Transform Pairs	{ 3 6 2 3 }
z-Transforms	{ 3 6 3 }
Definitions	{ 3 6 3 1 }
Properties	{ 3 6 3 2 }
Transform Pairs	{ 3 6 3 3 }
Contants	{ 3 7 }
SI Prefixes	{ 3 8 }
Greek Alphabet	{ 3 9 }

Chapter 45

Tips for Using the Solver

This chapter covers tips for using the solver in the Equations section.

- ☐ Creating a Working Directory
- ☐ How are Multiple Equations Solved?
- ☐ Using Guesses to Improve Solving
- ☐ Solver Icons

Creating a Working Directory

Every time the solver solves an equation, it stores the variable values into your HP 48 user memory, in the directory you were at when you ran *EE•Pro*. If you would prefer to organize the equation variables into a specific subdirectory in your HP 48 user memory, follow these steps:

1. Quit *EE•Pro* to the HP 48 stack.
2. Press to go to the HOME directory of your HP 48.
3. Press to display the variables in the HOME directory.
4. Decide on a name for the work subdirectory (e.g., WORK).
5. Type WORK to put the name on the stack.
6. Type CRDIR to create the subdirectory 'WORK' in your HOME directory. It should appear in the variable menu as .

You have now created the subdirectory { HOME WORK }. In order to store all equation variables created by *EE•Pro* in { HOME WORK }, each time you run the software, first follow these steps:

1. Press to go to the HOME directory of your HP 48.
2. Press to display the variables in the HOME directory.
3. Press to switch to the { HOME WORK } subdirectory.
4. Start *EE•Pro*, as described in Chapter 1, "Getting Started."

For more information on directories, see the HP 48 manual.

How are Multiple Equations Solved?

The solver in the Equations section of EE•Pro is a *systematic* solver, not a *simultaneous* one. For example, the solver can solve this set of equations, provided it is given a known value of either x or y :

$$\begin{aligned}x + y + z &= 5 \\x + y &= 3\end{aligned}$$

However, the solver cannot solve this set of equations, when neither x or y is known in advance:

$$\begin{aligned}x + y &= 2 \\x - y &= 0\end{aligned}$$


The solver iterates through a set of equations, searching for an equation with only one unknown variable. When an equation satisfying this requirement is found, the solver uses the built-in HP 48 root-finder to solve for the unknown variable. After the value is found, that variable is marked as found, and the solver continues to search. The solver does not terminate its search until one of three conditions occurs:

- All equations are solved, and all unknown variables are found.
- All variables marked as wanted are found.
- No more equations can be solved, because all remaining unsolved equations have more than one unknown variable.

All variables for which values are found in a solving operation are marked with a shaded circle at the solver screen.

Using Guesses to Improve Solving

Pressing **SOLVE** calls the built-in HP 48 root-finder to solve each equation. The root-finder requires an initial value on which to base its search for the solution. If no value exists, the solver uses a default guess of 1, but you can provide a guess to override that value. The root-finder then generates pairs of intermediate values and interpolates between them to find the solution. The time required to find the solution (the root) depends on how close the initial guess is to the actual solution.

You can shorten the solution time by providing a guess close to the expected solution. Go to the Solver screen and move the highlight bar to the variable in question, and enter a guess. The variable will automatically be marked as known, so move the highlight bar back to the variable and press **KNOW** or  to unmark the variable as known, so it will be calculated by the solver. Then press **SOLVE** and the solver will use the current value as the initial guess for the variable.

There is another advantage to using a guess, which is that you can help the solver find a specific solution to an equation which may have multiple valid solutions or roots.

Example: Imagine solving the equation $x^2 = 9$. Possible solutions include 3 and -3. Both of these solutions are right, but which one do you want? If you enter a guess of -1 for x , the solver will find the -3 solution, but if you enter a guess of 1 for x (which is the default guess), the solver will find the 3 solution. Depending on which solution you want, you may have to enter a guess for x .

Solver Icons

At the Solver screen, the status of variables is indicated by icons which appear to the left of the variable name. You control the presence of some of the icons, and the solver controls the presence of the other icons.

To display the icon screen from the Solver screen, press **ICONS**.



Press any key to return to the previous screen.

User-Controlled Icons

You control the presence of unknown (blank icon), known, and wanted icons by pressing **KNOW** or **WANT**.

UNKNOWN: *Solve if possible.* The solver will calculate the values of all unknown variables, unless it first stops because all wanted variables have been found. As a result of a calculation, the solver may change the status of unknown variables to solution found or no solution. However, if there

are not enough known variables to solve for the unknown variable, the status will remain unchanged as unknown.

- **KNOWN: *User-defined.*** The values of the known variables are used to calculate the values of the unknown and wanted variables. The solver will not change the status of known variables.
- ✓ **WANTED: *Solve, then stop.*** The solver will calculate the values of all wanted variables and then stop. While solving for the wanted variables, the solver may also have to calculate the values of some unknown variables in order to find solutions to the wanted variables. As a result of a calculation, the solver may change the status of wanted variables to solution found or no solution. However, if there are not enough known variables to solve for the wanted variable, the status will remain unchanged as wanted.

Solver-Controlled Icons

The solver places icons for solution found and no solution. Each time you change a value or press **SOLVE** to start a new calculation, the solution found and no solution icons are all removed and the variables reset to unknown.

- **SOLUTION FOUND: *Solution found.*** A solution found icon indicates a solution has been found for the variable. Solutions may be indicated either as *zeros* or *sign reversals*, both of which are accurate solutions.
- ~ **NO SOLUTION: *Extremum.*** An extremum icon indicates a solution has not been found for the variable. This occurs when the solver finds a point where the value of the variable being solved approximates a local minimum or maximum, or when the largest (MAXR) or smallest (–MAXR) number is encountered.
- ✱ **NO SOLUTION: *Bad guess.*** A bad guess icon indicates a solution has not been found for the variable. This occurs when the initial guess for the variable is outside the domain of the equation. An example of this is a negative value inside a square root, which will cause a bad guess error, because the solver does not support complex numbers.
- ▢ **NO SOLUTION: *Constant?*** A constant icon indicates a solution has not been found for the variable. This occurs when the value of the variable is the same at every point sampled across the domain of the equation.

For more information, see Chapter 16, “Equations Navigation Guide.”

Chapter 46

Tips for Using the Plotter

This chapter covers advanced use of the plotter in the Equations section.

❑ How are Equations Plotted?

How are Equations Plotted?

To plot an equation, it must be in the form $y = f(x)$, where x represents the independent variable and y the dependent variable. The plotter must be able to isolate the dependent variable on the left side of the equation before plotting. For this reason, there are equations in which certain variables should not be selected as the dependent variable, because they cannot be isolated.

Example: *How can the first equation in the RLC Circuits-Overdamped Transient module be plotted?* The equation is:

$$s1 = -\alpha + \sqrt{\alpha^2 - \omega_0^2}$$

In this equation, any variable can be selected as the independent variable, but only $s1$ or ω_0 should be selected as the dependent variable, because α appears more than once in the equation and cannot be isolated easily.

This table shows the possible combinations of the independent and dependent variables for the equation above and shows exactly what form the equation takes for plotting in each case.

Dependent	Independent	Isolated Equation
$s1$	α	$s1 = f(\alpha) = -\alpha + \sqrt{\alpha^2 + \omega_0^2}$
$s1$	ω_0	$s1 = f(\omega_0) = -\alpha + \sqrt{\alpha^2 + \omega_0^2}$
ω_0	$s1$	$\omega_0 = f(s1) = s1 \cdot \sqrt{\alpha^2 - SQ(s1 + \alpha)}$

ωo	α	$\omega o = f(\alpha) = s1 \cdot \sqrt{\alpha^2 - SQ(s1 + \alpha)}$
α	ωo	Cannot isolate α easily
α	$s1$	Cannot isolate α easily

When isolating $s1$ or ωo , the plotter also automatically selects the principal value (or branch) of the solution, if there are multiple solutions. Observe that the first three equations also have a negative solution to the square root, but the principal solution is the positive one, so that is what is used for plotting.

After plotting an equation, to examine the form of the actual equation which was plotted, quit EE•Pro and look at the variable 'EQ' in the user memory of your HP 48. (Note: 'EQ' is not created until the plot is drawn.)



Appendixes and Index

Appendix A

Service and Warranty

Technical Support

You can get answers to your questions about EE•*Pro* from Sparcom Corporation. If you cannot find the information in this manual or in the HP 48S/SX or HP 48G/GX User's Guide, contact us in one of the following ways:

- **E-Mail**
From Internet: support@sparcom.com
From Compuserve: >Internet:support@sparcom.com
From FidoNet: To:support@sparcom.com
- **Standard Mail**
Sparcom Corporation
Attn: Technical Support Department
P.O. Box 927
Corvallis, OR 97339, USA
- **Telephone**
(503) 757-8416
Monday to Friday, 9 a.m. to 12 p.m., Pacific Time
- **Facsimile**
(503) 753-7821

Shipping Instructions

If your card requires service:

1. Call Sparcom Corporation for a Return Merchandise Authorization (RMA) number.
2. Ship the card back to Sparcom Corporation in the following manner:
 - Include your return address, phone number and a description of the problem.
 - **INCLUDE YOUR RMA NUMBER WITH THE MERCHANDISE.** The RMA number must be written on the outside of the package, or the package will be returned to you unopened.
 - If the card is still under warranty, include the proof of purchase date.
 - Include a check, purchase order, or credit card number and expiration date (VISA or MasterCard) to cover the estimated charge.
 - Should the card require further service, Sparcom Corporation will notify you of the additional repairs and charges.
 - Ship your card, postage prepaid, in protective packaging adequate to prevent damage. Ship the package to:

Sparcom Corporation
RMA # _____
897 NW Grant Avenue
Corvallis, OR 97330, USA
 - It is highly recommended that you insure the shipment.

Cards are usually serviced and reshipped within five working days.

Service Charge for Out-of-Warranty Cards

Charges for out-of-warranty repairs are individually determined based on time and material. These charges are subject to your local sales or value-added tax, wherever applicable.

Limited 90-Day Warranty

What Is Covered

The card is warranted by Sparcom Corporation against defects in materials and workmanship for ninety days from the date of original purchase. If you sell your card or give it as a gift, the warranty is automatically transferred to the new owner and remains in effect for the original ninety-day period. During the warranty period, we will repair or, at our option, replace at no charge a card that proves to be defective, provided you return the card, shipping prepaid, to Sparcom Corporation. (Replacement may be made with a newer card of equal or better functionality.)

This warranty gives you specific legal rights, and you may also have other rights that vary from state to state, province to province, or country to country.

What Is Not Covered

This warranty does not apply if the card has been damaged by accident or misuse or as the result of service or modification by other than an authorized Sparcom Corporation service center.

No other express warranty is given. The repair or replacement of the card is your exclusive remedy. ANY OTHER IMPLIED WARRANTY OF MERCHANTABILITY OR FITNESS IS LIMITED TO THE NINETY-DAY DURATION OF THIS WRITTEN WARRANTY. Some states, provinces, or countries do not allow limitations on how long an implied warranty lasts, so the above limitation may not apply to you. IN NO EVENT SHALL SPARCOM CORPORATION BE LIABLE FOR CONSEQUENTIAL DAMAGES. Some state, provinces, or countries do not allow the exclusion or limitation of incidental or consequential damages, so the above limitation or exclusion may not apply to you.

Cards are sold on the basis of specifications applicable at the time of manufacture. Sparcom Corporation shall have no obligation to modify or update cards, once sold.

Appendix B

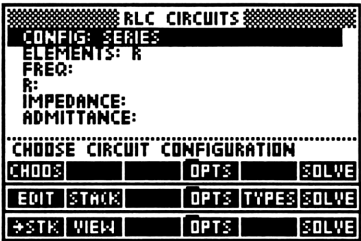
Key and Screen Summary

This appendix covers:

- ☐ Screen Summary
- ☐ Key Summary

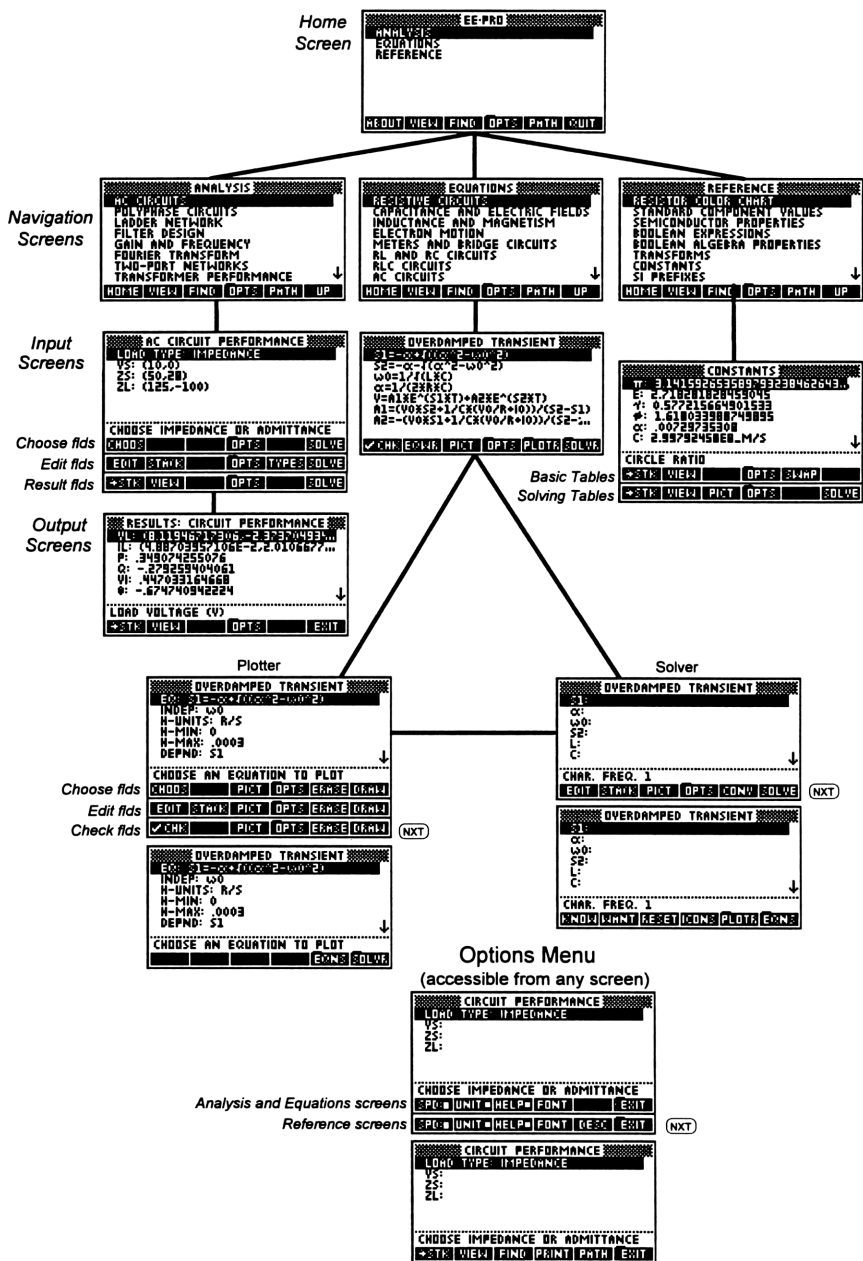
This appendix provides a summary of the structure of *EE•Pro*, the different types of screens, and the keys available at each screen.

The screen summary on the following page provides a “map” of *EE•Pro* and how it is organized. Screens with multiple menu rows, such as the Analysis screen shown here, indicate that the menu keys change depending on which field is highlighted. In the case of the options menu, the menu keys change depending on which section you were in when you entered the options menu.



Following the screen summary is a listing of the keyboard commands that are available throughout the program and at each type of screen.

































Screen Summary



Key Summary



EE•Pro

The following key commands are available throughout EE•Pro.

-  or  Moves the highlight bar up or down one item.
-   or   Moves the highlight bar to top or bottom of screen.
-   or   Moves the highlight bar to top or bottom of list.
-  or   Goes to the previous screen.
-   or   Goes to the home screen.
-  or  Enters the highlighted section (in a navigation screen).
-  or   Goes to the next or previous menu row (if appropriate).
-  Goes to the custom settings screen.
-   or   Goes to the first or second page of the options menu.
-   HP 48GX: Displays the highlighted item in a text view.
-   HP 48SX: Displays the highlighted item in a text view.
-  Quits EE•Pro to the HP 48 stack.

Home Screen



- ABOUT** Displays product information and current version.
- VIEW** Displays the highlighted item in text view (larger font, one item per screen).  or  **VIEW** displays the highlighted item in graphics view (if highlighted item is an equation, etc.).
- FIND** Searches for the specified character or string.
- OPTS** Displays the options menu, see page 266.
- PATH** Displays screens chosen to reach the current screen.
- QUIT** Quits EE•Pro to the HP 48 stack.

Navigation Screens

ANALYSIS	EQUATIONS	REFERENCE
AC CIRCUITS POLYPHASE CIRCUITS LADDER NETWORK FILTER DESIGN GAIN AND FREQUENCY FOURIER TRANSFORM TWO-PORT NETWORKS TRANSFORMER PERFORMANCE	RESISTIVE CIRCUITS CAPACITANCE AND ELECTRIC FIELDS INDUCTANCE AND MAGNETISM ELECTRON MOTION METERS AND BRIDGE CIRCUITS RL AND RC CIRCUITS RLC CIRCUITS AC CIRCUITS	RESISTOR COLOR CHART STANDARD COMPONENT VALUES SEMICONDUCTOR PROPERTIES BOOLEAN EXPRESSIONS BOOLEAN ALGEBRA PROPERTIES TRANSFORMS CONSTANTS SI PREFIXES
HOME VIEW FIND OPTS PATH UP	HOME VIEW FIND OPTS PATH UP	HOME VIEW FIND OPTS PATH UP

- HOME** Goes to the home screen.
- VIEW** Displays the highlighted item in text view (larger font, one item per screen). Press or **VIEW** to display the highlighted item in graphics view (if highlighted item is an equation, etc.).
- FIND** Searches for the specified character or string.
- OPTS** Displays the options menu, see page 266.
- PATH** Displays screens chosen to reach the current screen.
- UP** Goes to the previous screen.

Analysis Input Screens

IMPEDANCE CALCULATIONS	IMPEDANCE CALCULATIONS	IMPEDANCE CALCULATIONS
CONFIG: SERIES ELEMENTS: R FREQ: R: X: Y:	CONFIG: SERIES ELEMENTS: R FREQ: R: X: Y:	CONFIG: SERIES ELEMENTS: R FREQ: R: X: Y:
CHOOSE CIRCUIT CONFIGURATION CHOO: OPTS SOLVE	ENTER FREQUENCY (HZ) EDIT STACK OPTS TYPE SOLVE	RESULT: IMPEDANCE (Z) →STK VIEW OPTS SOLVE

Choose fields

Edit fields

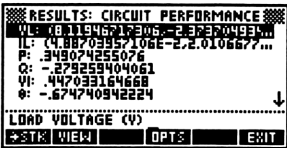
Result fields

- CHOO** Displays possible choices for a choose field (*Choose fields only*).
- EDIT** Edits the highlighted item (*Edit fields only*).
- STACK** Copies the highlighted item to the HP 48 stack and temporarily goes to the HP 48 stack environment (*Edit fields only*).
- TYPE** Displays the allowed object types for an edit field (*Edit fields only*).
- STK** Copies one or all of the items shown to the HP 48 stack (*Result fields only*).
- VIEW** Displays the highlighted item in text view (larger font, one item per screen). Press or **VIEW** to display the highlighted item in graphics view (if highlighted item is an equation, etc.).
- OPTS** Displays the options menu, see page 266.
- SOLVE** Performs a calculation using the displayed values.



- Enters the highlighted section (in a navigation screen).
- Edits the highlighted item (for an edit field).
- Displays the possible choices (for a choose field).
- Copies item(s) shown to the stack (for a result field).

Analysis Output Screens



- STK** Copies one or all of the items shown to the HP 48 stack.
- VIEW** Displays the highlighted item in text view.
- OPTS** Displays the options menu, see page 266.
- EXIT** Returns to the input screen.

Equations Screens



- ✓CHK** Checks or unchecks the highlighted item for solving or plotting.
- EQWR** Displays the highlighted item in graphics view.
- PICT** Displays a picture for the equation set (if available).
- OPTS** Displays the options menu, see page 266.
- PLOTR** Goes to the Plotter screen.
- SOLVR** Goes to the Solver screen.



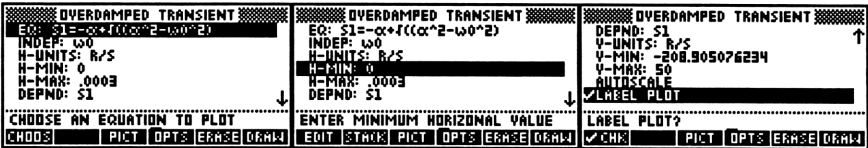
Enters the highlighted section (in a navigation screen).

Checks or unchecks the highlighted equation.



Checks or unchecks the highlighted equation.

Plotter Screens



Choose fields

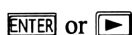
Edit fields

Check fields



all fields

- CHOOSE** Displays possible choices for a choose field (*Choose fields only*).
- EDIT** Edits the highlighted item (*Edit fields only*).
- STACK** Copies the highlighted item to the HP 48 stack and temporarily goes to the HP 48 stack environment.
- ✓CHK** Checks or unchecks the highlighted item. This selects or unselects an item for solving or plotting (*Check fields only*).
- PICT** Displays a picture for the equation set (if available).
- OPTS** Displays the options menu, see page 266.
- ERASE** Erases any previous plots.
- DRAW** Plots the current equation.
- EQNS** Goes to the Equations screen.
- SOLVR** Goes to the Solver screen.



Edits the highlighted item (for an edit field).

Displays the possible choices (for a choose field).

Checks or unchecks highlighted item (for check field).



Toggles through possible choices (for a choose field).



Toggles units on or off.

Solver Screens



- EDIT** Edits the highlighted item.
- STACK** Copies the highlighted item to the HP 48 stack and temporarily goes to the HP 48 stack environment.
- PICT** Displays a picture for the equation set (if available).
- OPTS** Displays the options menu, see page 266.
- CONV** Displays the possible units for converting the highlighted variable.
The appropriate units appear in the menu keys. Press **NXT** and/or **EXIT** to return to the Solver.
- SOLVE** Erases any previous plots.
- KNOW** Marks or unmarks the highlighted variable as known.
- WANT** Marks or unmarks the highlighted variable as wanted.
- RESET** Resets one or all of the variables.
- ICONS** Displays the icons used to indicate variable status.
- PLOTS** Goes to the Plotter screen.
- EQNS** Goes to the Equations screen.



Edits the highlighted variable.



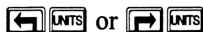
Marks or unmarks highlighted variable as known.



Toggles positions of variable values and descriptions.



Resets one or all of the variables.



Toggles units on or off.

Reference Screens



→STK Copies one or all of the items shown to the HP 48 stack.

VIEW Displays the highlighted item in text view. Press or **VIEW** for graphics view (if highlighted item is an equation, etc.).

PICT Displays a picture for the reference table (if appropriate).

DUAL Displays the duals of the property or expression (if appropriate).

OPTS Displays the options menu, see page 266.

DESC Toggles position of data and help text (if appropriate).

SOLVE Activates the custom solving routine (if appropriate).



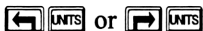
Enters highlighted section (in a navigation screen).

Edits the highlighted item (for an edit field).

Copies item(s) shown to the stack (for a result field).

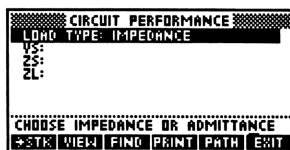


Toggles position of data and help text (if appropriate).



Toggles units on or off.

Options Menu





SPD Changes the scrolling speed of the highlight bar.

UNIT Toggles units on or off.

HELP Toggles display of help text at the bottom of the screen.

FONT Toggles font size between large and small.

- DESC** • Toggles position of data and help text (*if appropriate*).
- STK** Copies one or all of the items shown to the HP 48 stack.
- VIEW** Displays the highlighted item in text view. Press  or  **VIEW** for graphics view (if highlighted item is equation).
- FIND** Searches for the specified character or string.
- PRINT** Prints one or all of the items shown to an HP 48 printer.
- PATH** Displays screens chosen to reach the current screen.
- EXIT** Leaves the options menu.

Appendix C

User Flags

This appendix covers:





- ☐ Flag 4: Carry Flag
- ☐ Flag 5: Range Flag
- ☐ Flags 13 & 14: Binary Sign Mode
- ☐ Flag 57: Font Size
- ☐ Flag 58: Help Text
- ☐ Flag 61: Units
- ☐ User Flag Summary

Flag 4: Carry Flag

The carry flag, used by the binary commands in the Computer Engineering section of *EE•Pro*, is controlled by the setting of user flag 4:

- **Flag 4 Clear:** *Places a 0 in the Carry bit.*
- **Flag 4 Set:** *Places a 1 in the Carry bit.*

To change the carry flag while using *EE•Pro*, go to Analysis, Computer Engineering, then to one of the listed sections (e.g., Register Operations). Press **MODE**, then choose Clear or Set for the **Carry** field.





To set or clear the carry flag from the HP 48 stack, type 4   SF or 4   CF.

Flag 5: Range Flag

The range flag, used by the binary commands in the Computer Engineering section of *EE•Pro*, is controlled by the setting of user flag 5:

- **Flag 5 Clear:** Places a 0 in the Range bit.
- **Flag 5 Set:** Places a 1 in the Range bit.

To change the range flag while using *EE•Pro*, go to Analysis, Computer Engineering, then to one of the listed sections (e.g. Register Operations). Press **MODE**, then choose Clear or Set for the **Range** field.





To change the range flag from the HP 48 stack, type 5   SF or 5   CF.

Flags 13 and 14: Binary Sign Mode

The binary sign mode is controlled by the setting of user flags 13 and 14 in combination:

Mode	Flag 13	Flag 14
Unsigned	Clear	Clear
One's Complement	Set	Clear
Two's Complement	Set	Set

To change the binary mode while using *EE•Pro*, go to Analysis, Computer Engineering, then to one of the listed sections (e.g. Register Operations). Press **MODE**, then choose Unsigned, One's Complement, or Two's Complement for the **Sign** field.





To set or clear flag 13 (or 14) from the HP 48 stack, type 13   SF or 13   CF.

Flag 57: Font Size

The display font size is controlled by the setting of user flag 57:

- **Flag 57 Clear:** *Small display font.* The small font contains 3x5 uppercase letters and fits eight vertical lines of text on the screen (without help text).
- **Flag 57 Set:** *Large display font.* The large font contains 5x7 uppercase and lowercase letters and fits six vertical lines of text on the screen (without help text).

To change the font size while using *EE•Pro*, press **OPTS**, then **FONT**.





To change the font size from the HP 48 stack, type 57   SF or 57   CF.

Flag 58: Help Text

The presence of context-sensitive help text along the bottom of the screen is controlled by the setting of user flag 58.

- **Flag 58 Clear:** *Help text on.* Help text is displayed at the bottom of the HP 48 screen, directly above the menu keys. Help text is always displayed in the small font, regardless of the setting of flag 57.
- **Flag 58 Set:** *Help text off.* When help text is off, one or two more lines available on the screen for displaying information.

To toggle help text while using EE•Pro, press **OPTS**, then **HELP**. When the block inside the key appears (**HELP**), the help text is turned on.





To toggle help text from the HP 48 stack, type 58   SF or 58   CF.

Flag 61: Units

The presence of units is controlled by the setting of user flag 61.

- **Flag 61 Clear:** *Units on.* Equations can be solved and plotted with or without units, and Reference tables can be displayed with or without units.
- **Flag 61 Set:** *Units off.*

To toggle units while using EE•Pro, press **OPTS**, then **UNITS**. When the block inside the key appears (**UNIT**), units are turned on.

To toggle units from the HP 48 stack, type 61   SF or 61   CF.

User Flag Summary

Flag	Affects	Clear	Set
4	Carry Flag	Value of Carry bit is 0	Value of Carry bit is 1
5	Range Flag	Result within the range	Result outside the range
13 & 14	Binary Mode	Unsigned: 13 - Clear, 14 - Clear One's Complement: 13 - Set, 14 - Clear Two's Complement: 13 - Set, 14 - Set	
57	Font Size	Small font (default)	Large font
58	Help Text	Help text on (default)	Help text off
61	Units	Units on	Units off (default)

Appendix D

Questions and Answers

This appendix lists the most common questions about *EE•Pro*. Scan this list before you call customer support—you might save yourself a phone call!

This appendix covers:

- ☐ General Questions
- ☐ Analysis Questions
- ☐ Equations Questions
- ☐ Reference Questions

General Questions

These are the most commonly asked questions about general features of *EE•Pro*. For more information, see Chapter 1, “Getting Started.”

- Q** I can't get out of a screen. When I quit by pressing **ON** and go back into *EE•Pro* I'm right back where I was when I exited. How do I get back to the home screen?
- A** Pressing **ENTER** usually goes into a section, but you may have a difficult time finding your way back out. The easiest way to remember how to navigate the screens is to learn that **▲**, **▼**, **◀**, and **▶** are the only four keys you need to use to navigate through *EE•Pro*. **▲** and **▼** move the highlight bar up and down. **▶** usually enters a section, and **◀** usually returns back out of a section to the previous screen. Repeatedly pressing **◀** will eventually get you to the home screen. Or press **▶****HOME** or **▶****◀** to go directly to the home screen.
- Q** I tried pressing **◀** and **▶****◀** to go up a section but the HP 48 just beeps. How do I get out of this screen?
- A** Some screens allow you to make selections, such as a choose screen, or change settings, such as the Custom Settings screen. The only way to

exit these screens is by pressing **OK**, which accepts the current selection or settings, or by pressing **CANCEL** or **ON**, which exits the screen without making any changes. After you have exited the screen, you should be able to go up a section by pressing **◀** or **▶◀**.

Q Why is there a 'SPARCOM' directory in my HP 48 user memory? (It appears as **SPARC** when you press **VAR** to display the variable menu.)

A Special parameter variables are stored in the 'SPARCOM' directory by *EE•Pro*. One of those variables is 'EEPAR', which contains information about which screen you were at when you quit *EE•Pro*, so that screen will re-appear the next time you run the software.

Variables created during equation solving and plotting are not necessarily stored in the 'SPARCOM' directory, but in whatever directory you were at when you ran the software. This is so that you can create working subdirectories to organize your sets of variables if you commonly solve different sets of equations.

Q What do three dots (...) mean at the end of an item on the screen?

A The three dots (an ellipsis) indicate the item is too wide to fit on the screen. To display the item in a text view, move the highlight bar to it and press **VIEW** or **▶CMD** (HP 48GX) or **▶VST** (HP 48SX). To display the item in a graphics view, move the highlight bar to it and press **▶VIEW**.

Q I solved a problem a long time ago, and I want to find those values again for a problem I'm working on now, but I can't find them. Where are they?

A Values entered in Analysis screens are usually forgotten by *EE•Pro* when you leave the Analysis screen, because they are not stored in user memory. (An exception to this is the Capital Budgeting section, which *does* store project files in user memory.) However, values entered in Equations screens *are* stored in variables in user memory. Those variables will remain in whatever directory you were at when you solved the problem, unless you have cleared your HP 48 memory or reset the variables since you originally solved the problem.

Q I'm trying to find something which I know is in *EE•Pro* somewhere, but the find operation keeps telling me, "String Not Found."

A The find feature only searches information in the current screen. It cannot find an item if it is not displayed on the current screen. If you












need to find out where a feature is located in *EE•Pro*, use the table of contents or index of this manual.

- Q** I can't find an item in a menu. I think I'm in the right spot but I can't find the correct menu key label. Where can it be?
- A** Some menus have more than one page. Try pressing **[NXT]**. If the menu *does* have more than six items, the next menu page will be displayed.

Analysis Questions

These are the most commonly asked questions about the Analysis section of *EE•Pro*. For more information, see Chapter 2, "Analysis: Navigation Guide" and your HP 48 User's Guide.

- Q** My screen doesn't look exactly the same as the example in the manual. What could be wrong?
- A** The mode settings on your HP 48 may be set incorrectly. Each example displays a box with all relevant mode settings. Press **[CST]** to display the Custom Settings screen and verify that they match those used in the example.
- Q** The result isn't the value I expected. What could be wrong?
- A** Your HP 48 may be in an incorrect mode. For example, you may be expecting an answer in degrees but your HP 48 may be set to radians. Press **[CST]** to display the Custom Settings screen, correct any mode settings, and re-solve the problem.
- Q** When I press **[SOLVE]**, the result is an expression, not a number. Why?
- A** If you enter a variable name or an algebraic expression as your input, some of your results may be symbolic. If you want to further evaluate or manipulate a symbolic result, move the highlight bar to the field containing the result and press **[→STK]** to copy it to the stack. Press **[ON]** to go to the stack where you can further evaluate the result.
- Q** When I press **[SOLVE]**, I get the message, "Undefined Name." Why?
- A** Your HP 48 may be in numeric results mode instead of symbolic results mode. Press **[CST]** to display the Custom Settings screen, change the result mode to Symbolic, and re-solve.

- Q** How can I avoid getting an “Infinite Result” error in my calculations in EE•Pro?
- A** You can set flag -22 (Infinite Result Exception) to return the value 9.999999999999E499 (MAXR) instead:
1. Go to the stack. If you are in EE•Pro, press  to get to the stack.
 2. Type in -22   SF and press . The flag is now set.
 3. To return to EE•Pro, press   (on the HP 48GX) or   (on the HP 48SX), then  .
- Q** Units mode is turned on in the Custom Settings screen (). Why can't I enter units?
- A** Analysis screens *do not* allow unit objects. Only Equations and Reference screens have unit management.

Equations Questions

These are the most commonly asked questions about the Equations section of EE•Pro. For more information, see Chapter 16, “Equations: Navigation Guide” and your HP 48 User’s Guide.

- Q** I turned units off and all my values changed. What happened?
- A** When units are on, values can be entered and saved in any unit. When units are off, values can be entered in any unit, but the values will automatically be displayed on the screen in the default SI units. This is necessary so that when you press **SOLVE** to solve an equation, all the values will be consistent with each other and your answer will be correct. If you don't want to be restricted to SI units, turn units back on.
- Q** I entered values for some variables and pressed **SOLVE**, but I get the message, “Too many unknowns to finish solving.” Why?
- A** Sometimes the solver doesn't have enough information (i.e., enough known variables) to solve for all the remaining, unknown variables. If you don't yet have an answer to your problem, then you will have to enter more known values and re-solve.
- Q** There are already values stored in some of my variables. How do I clear those values?

A The values remain from previous solving operations. It is okay to ignore the values, because as long as they aren't marked as known, they will be overwritten by new solutions. If you want to reset the variables, press **RESET** or **DEL** to clear one or all of the variables.

Q I entered values for some variables and pressed **SOLVE**, but I get the message, "Bad Guess(es)". Why?

A There are several possibilities, but in all cases, the solver has encountered trouble while trying to solve for a particular variable. The problem variable is marked with an icon indicating a bad guess error occurred while solving for that variable.

Q The solution to my problem is clearly wrong! (An angle might be negative or unreasonably large.) Why?

A This is most likely to happen when angles are involved in the equation(s) you are solving. What has happened is that the HP 48 has found a non-principal solution to your equation.

Example: Imagine solving the equation $\sin(x) = 0.5$. Solutions include: 30° , 390° , -330° , 750° , etc., but the *principal* solution is 30° .

If a non-principal solution is found, it may then be used to solve other equations, leading to strange results.

Example (cont.): Now imagine solving the equation $x + y = 90^\circ$. If x is 30° , then y should be 60° . But if a non-principal solution for x was found, such as 750° , then the value of y will be -660° , which although technically correct, is also not a principal solution.

The way to fix this problem is to put in an initial guess for angle variables.

Example (cont.): Before solving for x , enter the value 45° for x and then press **KNOW** or **$\frac{\pi}{2}$** to unmark x as known. Now, when you press **SOLVE** to solve for x , the guess of 45° will be used, and it is close enough to the principal solution of 30° that the solver is very likely to find the principal solution.

Q I tried plotting an equation and got the message, "Variable Not Defined in Solver Screen." Why?

A When plotting, all variables other than the independent and dependent variables *must* have values. The other variables will be held constant

during plotting, but if they are undefined, this error will occur. Go to the Solver screen and enter values for the other variables in the equation you are plotting, return to the Plotter screen, and re-plot.

Q I tried plotting an equation and got the message, “Unable to Isolate.” Why?

A The variable you have selected as the dependent variable occurs more than once in the equation, which means it can’t be isolated. This means that you can’t plot the equation with that variable as the dependent variable. (Note: In a few cases, it will actually be possible to isolate the variable, but not by a simple isolation, so the HP 48 will be unable to do so.)

Reference Questions

These are the most commonly asked questions about the Reference section of *EE•Pro*. For more information, see Chapter 33, “Reference: Navigation Guide” and your HP 48 User’s Guide.

Q Why is the menu key **DESC** available in some screen and not in others?

A Some screens have information in the help text that may be useful to view in the main display area of the screen, instead of only line by line. **DESC** will be available in these screens. When turned on, the help text information will be swapped with the data normally shown in the main display area. However, if the help text is sparse or non-existent, then **DESC** will not be available.

Index

A

- ABOUTEE, 229
- AC Circuits, 21, 144
 - circuit performance, 24
 - commands, 229
 - current divider, 23
 - impedance calculations, 21
 - impedance to admittance, 146
 - RC series impedance, 146
 - RL series impedance, 145
 - two impedances in parallel, 148
 - two impedances in series, 147
 - voltage divider, 22
 - wye to delta conversion, 26
- active filter, 45
- advanced use, 225
 - multiple equations, 250
 - plotter tips, 253
 - solver icons, 251
 - solver tips, 249
 - using guesses, 250
 - working directory, 249
- Algebraic Functions, 81
 - commands, 239
 - partial fraction expansion, 81
 - piecewise functions, 82
 - polynomial coefficients, 85
 - polynomial equation, 85
 - polynomial roots, 86
 - symbolic simplification, 87

- Taylor polynomial, 88

Alpha

- entry mode, 10
- lock, 4
- amp, volt and ohmmeter, 129
- Analysis, 13
 - fields, see fields
 - finding, 16
 - menu keys, 18
 - navigation guide, 15
 - screen paths, 243
 - screens, key summary, 263, 264
 - using analysis functions, 17
- Analysis Screens, 16
- angle measure setting, 11

B

- bad guess icon, 105
- balanced delta load, 31
- balanced delta network, 149
- balanced wye load, 30
- balanced wye network, 150
- basic inverter, 156
- binary arithmetic, 73
- binary comparisons, 78
- binary conversions, 77
- bit operations, 76
- BJT (common base), 177
- BJT (common collector), 178
- BJT (common emitter), 178
- Bode Gain Plot, 50

Bode Phase Plot, 50
Boolean Algebra Properties
 reference table, 216
Boolean Expressions reference
 table, 214
Butterworth filter, 43

C

Capacitance and Electric Fields,
 117
 charged disk, 118
 coaxial cable, 120
 long charged line, 118
 parallel plates, 119
 parallel wires, 119
 point charge, 118
 sphere, 120
Capital Budgeting, 90
 commands, 240
capturing a screen, 5
card
 installing, 6
 removing, 7
chain parameters, 64
charged disk, 118
Chebyshev filter, 41
check fields, 110
choose fields, 18, 109
circuit performance, 24, 56
Class A, B, and C Amplifiers,
 183
 class A amplifier, 184
 class B amplifier, 186
 class C amplifier, 187
 power transistor, 185
 push-pull principle, 186
CMDSEE, 229
CMOS transistor pair, 174
coaxial cable, 120, 124
commands
 AC circuits, 229
 algebraic, 239
 binary arithmetic, 235
 binary comparisons, 237
 binary conversions, 237

 binary modes, 238
 binary operations, misc., 238
 bit operations, 237
 capital budgeting, 240
 EE library, 229
 error functions, 240
 filter design, 231
 finding, 228
 fourier transforms, 233
 gain and frequency, 232
 Karnaugh map, 239
 object syntax, 228
 polyphase circuits, 230
 reference, 240
 register operations, 236
 transformer performance, 234
 transmission lines, 235
 two-port networks, 233
Computer Engineering, 72
 binary arithmetic, 73
 binary comparisons, 78
 binary conversions, 77
 bit operations, 76
 commands, 235, 236, 237,
 238, 239
 register operations, 74
CONS, 229
constant icon, 105
Constants reference table, 220
copying an item to the stack, 10
critically-damped transient, 142
current amplifier, 157
current divider, 23
custom settings screen, 11, 72
customer support, iii

D

Darlington (CC-CE), 180, 181
DC generator, 192
DC series generator, 194
DC series motor, 196
DC shunt generator, 194
DC shunt motor, 195
dependent variable, 107, 108
differential amplifier, 160, 182

differentiator, 159

E

Ebers-Moll equations, 168

edit fields, 18, 109

EE, 229

Electrical Resonance, 151

- parallel resonance, 152

- parallel resonance II, 152

- resonance in lossy inductor, 153

- series resonance, 154

Electron Motion, 125

- electron beam deflection, 126

- photoemission, 126

- thermionic emission, 126

emitter-coupled amplifier, 181

energy conversion, 192

environmental limits, 5

Equations, 95

- displaying a picture, 99

- finding, 98

- menu keys, 100

- navigation guide, 97

- screen paths, 244

- screens, 99

- screens, key summary, 264

- selecting equations, 100

- Solver, 100

- viewing an equation, 99

Error Functions, 89

- commands, 240

examples

- AC circuit performance

 - parameters, 26

- active filter, 47

- balanced delta load, 33

- balanced wye load, 31

- binary arithmetic, 74

- binary comparison, 78

- binary conversions, 77

- Boolean algebra properties, 217

- Boolean expressions, 215

- Butterworth filter, 45

- capital budgeting, 92

- chain parameters, 65

- Chebyshev filter, 43

- compute the impedance of a parallel RLC circuit, 20

- Constants reference table, 206, 220

- create an equation with a constant, 241

- current divider, 24

- delta to wye conversion, 27, 29

- fault location estimate, 70

- FFT, 53

- find the transfer function for a circuit, 49

- inverse FFT, 53

- inverse Fourier transform definition, 219

- Karnaugh map, 80

- ladder network, 37, 39

- line characteristics, 67

- line parameters, 69

- open circuit test, 62

- overdamped parallel RLC circuit, 110

- override a built-in constant, 241

- partial fraction expansion, 82

- piecewise function, 84

- plot Overdamped Transient, 253

- polynomial coefficients, 85

- polynomial equation, 86

- polynomial roots, 86

- register operations, 75

- resistor colors, 208

- RLC impedance calculations, 22

- Semiconductor Properties, 212

- short circuit test, 63

- standard component values, 210

- stub impedance matching, 71

- Taylor polynomial, 88
- two-port circuit performance, 57
- two-port parameter conversion, 56
- two-ports, interconnected, 60
- voltage divider, 23
- wye to delta conversion, 29
- extremum icon, 104

F

- fault location estimate, 69
- FET (common drain), 180
- FET (common gate), 179
- FET (common source), 179
- FFT, 52
- fields
 - check, 110
 - choose, 18, 109
 - edit, 18, 109
 - result, 19
 - types, 18
- Filter Design, 41
 - active filter, 45
 - Butterworth filter, 43
 - Chebyshev filter, 41
 - commands, 231
- finding
 - an item, 10
 - Analysis, 16
 - commands, 228
 - Equations, 98
 - Reference, 204
- flags, see user flags
 - range and carry, 73
- font size, 9, 12, 103
- Fourier Transform
 - commands, 233
- Fourier Transforms, 52
 - FFT, 52
 - inverse FFT, 53

G

- Gain and Frequency, 48

- Bode plots, 50
- commands, 232
- transfer function, 48
- getting started, 1
- GOEE, 229
- GOMATH, 242
- graphics view, 10
- Greek Alphabet reference table, 223
- guesses, 250

H

- help, 272
- help text, 9, 12
- home screen, 8
 - key summary, 262
- HP 48GX
 - differences from HP 48SX, 4

I

- icons, see Solver
- ideal currents - pnp, 168
- ideal transformer, 189
- IFTE in piecewise functions, 83
- impedance calculations, 21
- impedance to admittance, 146
- independent variable, 106, 108
- Inductance and Magnetism, 121
 - coaxial cable, 124
 - long line, 122
 - long strip, 122
 - loop, 123
 - parallel wires, 123
 - skin effect, 124
- induction motor I, 197
- induction motor II, 198
- installing EE•Pro (installing a card), 6
- interconnected two-ports, 58
- internal rate of return, 90
- inverse FFT, 53

J

- junction FET, 175

K

- Karnaugh map, 79
- key features, 2
- key summary
 - Analysis screens, 263, 264
 - EE•Pro, 262
 - Equations screens, 264
 - home screen, 262
 - navigation screens, 263
 - options menu, 266
 - Plotter screens, 264
 - Reference screens, 266
 - Solver screens, 265
- keys, see menu keys
- keystrokes, 3

L

- Ladder Network, 34
- level detector, 158, 159
- library menu, 7
- line characteristics, 66
- line parameters, 68
- Linear Amplifiers, 176
 - BJT (common base), 177
 - BJT (common collector), 178
 - BJT (common emitter), 178
 - Darlington (CC-CE), 180, 181
 - differential amplifier, 182
 - emitter-coupled amplifier, 181
 - FET (common drain), 180
 - FET (common gate), 179
 - FET (common source), 179
 - source-coupled JFET pair, 182
- linear equivalent circuit, 189
- long charged line, 118
- long line, 122
- long strip, 122
- loop, 123

M

- manual

- conventions, 3
- headings, explanation, 3
- how to use, 2
- organization, 2
- what to read next, 3
- maximum power transfer, 115
- Maxwell bridge, 131
- memory requirements, 5
- menu keys
 - ABOUT, 7, 8
 - Analysis screens, 18
 - CHK, 100, 110
 - CHOOS, 109
 - CONV, 105
 - DESC, 205
 - DRAW, 109, 110
 - EDIT, 105, 109
 - EEPRO, 7
 - EQNS, 106, 110
 - Equations screens, 100
 - EQWR, 100
 - ERASE, 109, 110
 - EXIT, 9, 10
 - FIND, 8, 10
 - FONT, 9
 - HELP, 9
 - HOME, 8
 - ICONS, 106
 - KNOW, 105
 - OPTS, 8, 100, 105, 109, 110, 205
 - PATH, 8, 10
 - PICT, 100, 105, 109, 110, 205
 - PLOTR, 100, 106
 - Plotter screens, 109
 - PRINT, 10
 - QUIT, 8
 - Reference screens, 205
 - RESET, 105
 - SOLVE, 105
 - Solver screens, 105
 - SOLVR, 100, 110
 - SPD, 9
 - STACK, 105, 109

- STK, 10, 205
 - UNITS, 9
 - UP, 8
 - VIEW, 8, 10, 205
 - WANT, 104, 105
 - menus
 - convert, 102
 - options, 9
 - Meters and Bridge Circuits, 128
 - amp, volt and ohmmeter, 129
 - Maxwell bridge, 131
 - Owen bridge, 131
 - symmetrical resistive attenuator, 132
 - unsymmetrical resistive attenuator, 132
 - Wheatstone Bridge, 130
 - Wien Bridge, 130
 - modes
 - angle measure, 11
 - font size, 12
 - help text, 12
 - numeric, 12
 - symbolic, 12
 - units, 12
 - MOS inverter (depletion), 173
 - MOS inverter (resistive), 172
 - MOS inverter (saturated), 172
 - MOS transistor I, 170
 - MOS transistor II, 171
 - Motors and Generators, 190
 - DC generator, 192
 - DC series generator, 194
 - DC series motor, 196
 - DC shunt generator, 194
 - DC shunt motor, 195
 - energy conversion, 192
 - induction motor I, 197
 - induction motor II, 198
 - permanent magnet motor, 197
 - separately-excited DC generator, 193
 - separately-excited DC motor, 195
 - single-phase induction motor, 199
 - synchronous machines, 199
 - moving around the screen, 8
- N**
- navigation guides
 - Analysis, 15
 - Equations, 97
 - Reference, 203
 - navigation screens
 - key summary, 263
 - net present value, 90
 - non-inverting amplifier, 157
 - numeric results mode, 12
- O**
- Ohm's law and power, 114
 - OpAmp Circuits, 155
 - basic inverter, 156
 - current amplifier, 157
 - differential amplifier, 160
 - differentiator, 159
 - level detector, 158, 159
 - non-inverting amplifier, 157
 - transconductance amplifier, 158
 - open circuit test, 61
 - options menu, 9
 - key summary, 266
 - overdamped transient, 143
 - Owen bridge, 131
- P**
- parallel admittance, 141
 - parallel plates, 119
 - parallel resonance, 152
 - parallel resonance II, 152
 - parallel wires, 119, 123
 - parameter conversion, 54
 - partial fraction expansion, 81
 - parts
 - Analysis, 13
 - Equations, 95

- Programming & Advanced Use, 225
- Reference, 201
- paths
 - Analysis screens, 243
 - Equation screens, 244
 - Reference screens, 248
- payback period, 90
- permanent magnet motor, 197
- photoemission, 126
- piecewise functions, 82
 - entry rules, 83
- Plotter
 - autoscale, 107
 - drawing the plot, 107
 - field descriptions, 108
 - field types, see fields
 - menu keys, 109
 - plotting an equation, 106
 - screens, 106
 - screens, key summary, 264
 - selecting an equation to plot, 106
 - selecting the dependent variable, 107, 108
 - selecting the independent variable, 106, 108
 - setting the horizontal range, 107
 - setting the vertical range, 107
 - tips for using, 253
- plug-in card, see card
- PN junction currents, 166
- PN junctions, 166
- point charge, 118
- polynomial
 - coefficients, 85
 - equation, 85
 - roots, 86
 - simplifying, 87
 - Taylor, 88
- Polyphase Circuits, 28, 149
 - balanced delta load, 31
 - balanced delta network, 149
 - balanced wye load, 30

- balanced wye network, 150
- commands, 230
- power measurements, 150
- wye to delta conversion, 28
- power measurements, 150
- power transistor, 185
- printing an item, 10
- profitability index, 90
- programmable screens, 242
- push-pull principle, 186

Q

- questions and answers, 272

R

- RAM, see memory requirements
- RC natural response, 135
- RC series impedance, 146
- RC series to parallel, 138
- RC step response, 136
- Reference, 201
 - commands, 240
 - finding, 204
 - navigation guide, 203
 - screen paths, 248
 - screens, 204
 - screens, key summary, 266
 - using reference tables, 205
- Reference tables
 - Boolean Algebra Properties, 216
 - Boolean Expressions, 214
 - Constants, 220
 - Greek Alphabet, 223
 - Resistor Color Chart, 207
 - Semiconductor Properties, 211
 - SI prefixes, 222
 - Standard Component Values, 209
 - Transforms, 218
- register operations, 74
- removing a card, 7
- Resistive Circuits, 113

- maximum power transfer, 115
- Ohm's law and power, 114
- resistance and conductance, 114
- temperature effect, 115
- V and I source equivalence, 116
- Resistor Color Chart reference table, 207
- resonance in lossy inductor, 153
- result fields, 19
- result mode setting, 12
- RL and RC Circuits, 134
 - RC natural response, 135
 - RC series to parallel, 138
 - RC step response, 136
 - RL natural response, 135
 - RL series to parallel, 137
 - RL step response, 136
- RL series impedance, 145
- RLC Circuits, 139
 - critically-damped transient, 142
 - overdamped transient, 143
 - parallel admittance, 141
 - RLC natural response, 141
 - series impedance, 140
 - underdamped transient, 142
- roots
 - of a polynomial, 86

S

- screen captures, 5
- Screen Summary, 261
- screens
 - Analysis, 16
 - custom settings, 11, 72
 - Equations, 99
 - home, 8
 - moving around, 8
 - Plotter, 106
 - programmable, 242
 - Reference, 204
 - Solver, 100
- search for (find) an item, 10

- sections
 - Analysis, 13
 - Equations, 95
 - Programming & Advanced Use, 225
 - Reference, 201
- semiconductor basics, 165
- Semiconductor Properties reference table, 211
- separately-excited DC generator, 193
- separately-excited DC motor, 195
- series impedance, 140
- series resonance, 154
- service, 257
 - charges, 258
- shipping instructions, 258
- short circuit test, 62
- SI prefixes reference table, 222
- single-phase induction motor, 199
- skin effect, 124
- software
 - custom settings, 9
 - starting, 7
- Solid State Devices, 161
 - CMOS transistor pair, 174
 - Ebers-Moll equations, 168
 - ideal currents - pnp, 168
 - junction FET, 175
 - MOS inverter (depletion), 173
 - MOS inverter (resistive), 172
 - MOS inverter (saturated), 172
 - MOS transistor I, 170
 - MOS transistor II, 171
 - PN junction currents, 166
 - PN junctions, 166
 - semiconductor basics, 165
 - switching transients, 169
 - transistor currents, 167
- Solver
 - converting a value, 102
 - entering values, 101
 - font size, 103
 - icons, 251

- known variables, 104
- menu keys, 105
- no solution found, 104
- resetting variables, 102
- screens, 100
- screens, key summary, 265
- solution found, 104
- solving an equation, 101, 106
- tips for using, 249
- units off, 102
- units on, 102
- using the stack, 102
- wanted variables, 103
- source-coupled JFET pair, 182
- Sparcom Corporation
 - contacting, 257
 - phone number, 257
- speed setting, 9
- sphere, 120
- stack usage, 102
- Standard Component Values
 - reference table, 209
- starting EE•Pro, 7
- stub impedance matching, 70
- switching transients, 169
- symbolic results mode, 12
- symbolic simplification, 87
- symmetrical resistive attenuator, 132
- synchronous machines, 199

T

- Taylor polynomial, 88
- technical support, iii, 257
- temperature effect, 115
- thermionic emission, 126
- transconductance amplifier, 158
- transfer function, 48
- Transformer Performance, 61
 - chain parameters, 64
 - commands, 234
 - open circuit test, 61
 - short circuit test, 62
- Transformers, 188
 - ideal transformer, 189

- linear equivalent circuit, 189
- Transforms reference table, 218
- transistor currents, 167
- Transmission Lines, 66
 - commands, 235
 - fault location estimate, 69
 - line characteristics, 66
 - line parameters, 68
 - stub impedance matching, 70
- troubleshooting, 272
- two impedances in parallel, 148
- two impedances in series, 147
- Two-Port Networks, 54
 - circuit performance, 56
 - commands, 233
 - interconnected two-ports, 58
 - parameter conversion, 54

U

- underdamped transient, 142
- units setting, 9, 12
- unsymmetrical resistive
 - attenuator, 132
- user flags
 - flag 57, 268, 269
 - flag 58, 270
 - flag 61, 270
 - summary, 271
- using the stack, 102

V

- V and I source equivalence, 116
- variables
 - bad guess, 252
 - constant?, 252
 - converting, 102
 - dependent variable (for plotting), 107, 108
 - entering (for Plotter), 106
 - entering (for Solver), 101
 - entering, units on/off, 102
 - extremum, 252
 - independent variable (for plotting), 106, 108

- known, 104, 252
- no solution, 252
- no solution found, 104, 252
- resetting, 102
- solution found, 104, 252
- unknown, 251
- wanted, 103, 252
- viewing an item
 - graphics view, 10
 - text view, 10
- voltage divider, 22

W

- Wheatstone Bridge, 130
- Wien Bridge, 130
- working directory
 - creating, 249
- wye to delta conversion, 26, 28

